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A

NEW TREATISE

ON

SURVEYING AND NAVIGATION

THEORETICAL AND PRACTICAL:

WITH

USE OF INSTRUMENTS, ESSENTIAL ELEMENTS OF TRIGONOMETRY,
AND THE NECESSARY TABLES,

FOR

SCHOOLS, COLLEGES, AND PRACTICAL SURVEYORS.

EDITED BY

OREN ROOT, A.M.,
PROFESSOR OF MATHEMATICS IN HAMILTON COLLEGE.

IVISON, BLAKEMAN, TAYLOR & CO.,
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EDITOR'S PREFACE.

In the preparation of the present edition of Surveying and Navigation, no effort has been made to preserve the identity of the former work; but the aim has been to prepare an entirely *new treatise*, far more complete than the former, not only in the range and variety of topics, but also in improved methods and practical applications, and to combine the *best practical* with the *highest theoretical* character, making the work worthy a place in the Series for which it was intended.

The object kept in view by the editor has been two-fold.

1*st.* To prepare a work suitable for class instruction in schools and colleges, furnishing clear rules with plain explanations, and an abundance of examples and illustrations.

2*d.* To prepare a work valuable as a book of reference for the practical surveyor, containing all necessary tables, and all processes required for any practical operations.

The chapter on Trigonometry is taken mainly from Robinson's New Geometry and Trigonometry, as the subject was there treated with such clearness that few changes seemed desirable.

The more practical rules of Mensuration, even though common, have been given, with examples, in order to make the sections as complete as possible, and to make the book useful to young students as well as to those more advanced.

The Examples in the Chapters on Land Surveying have been formed mainly from the field notes of actual operations, and are sufficiently numerous to familiarize any student with the working of all practical cases.

The section upon Division of Land is also made up to a great extent from notes of actual surveys, and gives ample illustration of methods, to enable any one with a good knowledge of mathematical principles to master any case that may come before him. In the Division of Land, cases are so diverse, that mathematical principles, and not specific rules must be relied upon, mainly, by the surveyor.

The subjects of Leveling, Road and Canal Surveying, and Topography, belong more properly to civil engineering, and a full discussion of these topics would require separate volumes. The sections upon these subjects are intended, therefore, to furnish only the more elemental and simple points.

The chapter on Navigation is intended for class instruction merely, as extensive works, with more complete tables, are necessary for the practical navigator, such as are supplied by Bowditch and others. A method of obtaining difference of longitude, not given in any of the text-books, and also a method of obtaining meridional parts have been given.

It has been the intention of the editor so to arrange the work that a student, who did not desire a full course of trigonometry, could, after the study of geometry by the use of this text-book, obtain the necessary propositions for the practical surveyor in clear and concise form, and thus fit himself more speedily for practical work.

The arrangement of the work, including as it does Trigonometry and Mensuration, requires that two terms should be employed in its completion; those students, however, who have before studied Trigonometry, by *omitting* CHAPTER II. and also SECTION III. of CHAPTER III. can readily master the Surveying proper in *one* term.

It is just to acknowledge here the services, as co-editor in the preparation of this work, of Oren Root jr., A.M., of Rome, N.Y., whose attainments as a mathematical scholar, and experience as a teacher are well-known.

This treatise is now submitted to the public, with the hope that it will fully commend itself, for fulness of matter, and scientific arrangement; for clear statement, and accurate definition; for rules concise and of easy application; for examples numerous, apt, and strictly practical; for whatever, in short, the student, and the practical surveyor could reasonably expect in a first class text-book on this subject.

HAMILTON COLLEGE, Sept. 1st, 1863.

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SURVEYING AND NAVIGATION.

CHAPTER I.

INSTRUMENTS.

SECTION I.

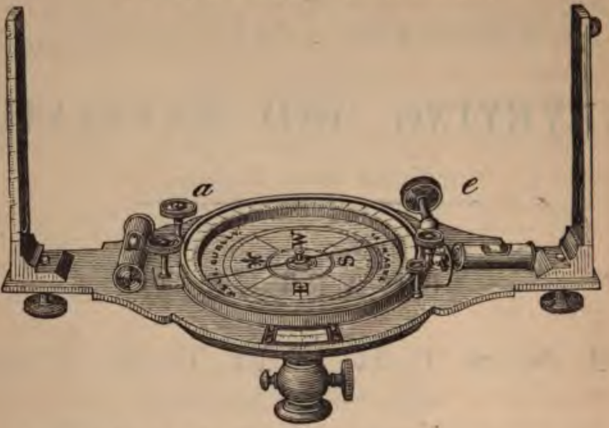
SURVEYING INSTRUMENTS.

IN **Mensuration, Surveying,** and **Navigation,** the known quantities or conditions are determined by measurements.

The more common and important instruments used for these measurements are the Surveyor's Compass, the Solar Compass, the Transit, the Level, the Plane Table, the Sextant, and various Plotting Instruments. These are described in the present chapter, and rules or directions given for their use.

It is hoped that the descriptions given will prove to be clear, and readily understood. Yet both teacher and student should remember that it is impossible to gain a perfect idea of a complex instrument by a description merely. In all possible cases, the instrument itself should be studied in connection with the description; the various adjustments should be made in presence of the student, and some practice given in the use of the instruments. Surveying and Navigation are important *applications* of geometrical science, and care should be taken always to secure to the student, as far as possible, the *practical* objects of a study of these branches.

SURVEYOR'S COMPASS.



The **Surveyor's Compass** consists essentially of a graduated circle, in the centre of which a magnetic needle is suspended, so as to turn freely in a horizontal direction.

The compass plate has two spirit levels placed at right angles to each other to level the compass in both directions, and at its ends standards or sights through the slits of which the compass is directed to the object sighted upon.

The graduated circle is divided into degrees and half degrees, and figured from 0 to 90 on each side of the north and south ends of the compass box; the line of the sights passes through the zero divisions of the circle.

In the best compasses also the circle is made to turn about its centre, in order that the line of zeros may be moved a short distance to either side of the line of sight, that allowance may be made for the *variation of the needle*, and to read the needle to single minutes of a degree, as will be hereafter explained.

In the compass shown in the cut, the movement of the circle is effected by a pinion at *a*, working into a circular rack on the outside of the compass box. The space over which the circle is moved is shown in degrees and minutes by a divided arc and *vernier*, near the letter *S.*

The arc is divided to degrees and half-degrees, and figured each way from its centre. The vernier is divided into thirty equal spaces, which together exactly correspond in length with twenty-nine half-degrees of the arc.

Each division of the vernier is therefore one-thirtieth, or in other words, one minute longer than a single division of the arc, and the vernier thus reads to single minutes.

The compass shown in the cut has also a horizontal circle beneath the main plate, read by two opposite verniers, by which horizontal angles can be taken to single minutes without the use of the needle.

Adjustments :—

1. Bring the bubbles into the centre by the pressure of the hand on different parts of the plate, and turn the compass half way around; should the bubbles run to the ends of the tubes, it would indicate that those ends were the highest; lower them by tightening the screws immediately underneath, and loosening those under the lower ends, until by estimation, half the error is removed; level the plate again, and repeat the operation until the bubbles will remain in the centre during an entire revolution of the compass.

2. The sights are tested by a plumb line, with which their slits must coincide when the compass is horizontal. If they do not, file off the under side of the base, until the connection is made.

3. The needle should cut opposite degrees in any part of the circle. If it does not, bend the centre pin until it will cut at a given degree, say 0 or 90. Then holding the needle in the same position, turn the compass half way around, and note whether it now cuts on precisely the same degrees at both ends; if not, correct half the error by bending the needle, and the remainder by bending the centre pin. Repeat this operation until the needle is perfectly straight, when it may be brought into line with all other divisions of the circle by bending the centre pin.

1. *To use the Surveyor's Compass.*

Place the instrument on its staff or tripod, level the compass plate, lower the needle upon its pivot, and direct the sights to any object the bearing of which is desired, always keeping the south end nearest the person.

Wait until the needle is perfectly at rest, and read the bearing from the north end of the needle.

2. *To turn off the Variation of the Needle.*

Place the compass on some well-defined line of the old survey, and turn the pinion, *a*, until the needle indicates the same bearing as that given in the field notes of the original survey; the reading of the vernier will give the change of variation during the period which has elapsed since the original survey.

3. *To read to Minutes by the Vernier.*

First make the zero of the vernier coincide with that of the divided arc; then noting the number of whole degrees given by the needle, move back the compass circle until the nearest whole degree mark is made to coincide with the point of the needle; count the minutes from the zero point of the vernier, until a division on the vernier is found exactly in line with another on the divided arc, and this reading, added to the whole degrees, will give the bearing to single minutes.

NOTE.—The Surveyor's Compass, the Solar Compass, the Surveyor's Transit, and the Y Level, as represented and described in this chapter, are manufactured by the well-known firm of W. & L. E. GURLEY, TROY, N. Y., whose instruments for accuracy, adaptation, and finish, are unsurpassed by any others made in this country. For further information, price, etc., see advertisement at the end of this work.

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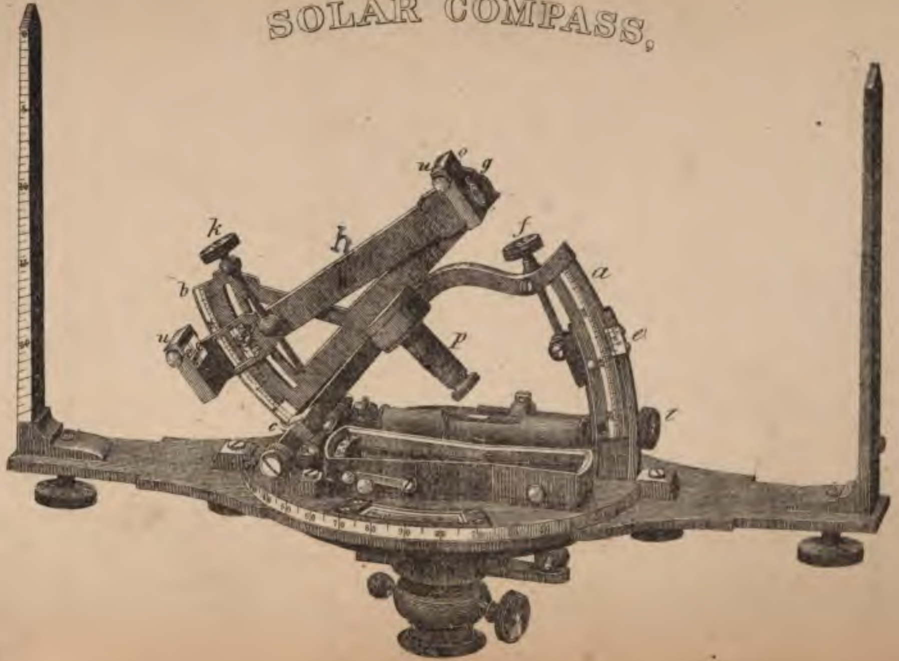
SOLAR COMPASS,



THE SOLAR COMPASS.

This instrument, used with the sun in determining meridians, or true north and south lines, is always employed in tracing the important lines of government lands.

The **Solar Apparatus** consists mainly of three arcs of circles, by which can be set off the latitude of a place, the declination of the sun, and the hour of the day.

These arcs, designated in the cut by the letters, *a*, *b*, and *c*, are therefore termed the latitude, the declination, and the hour arcs respectively.

The **Latitude Arc,** *a*, has its center of motion in two pivots, one of which is seen at *d*, the other is concealed in the cut.

It is moved either up or down within a hollow arc, seen in the cut, by a tangent screw at *f*, and is securely fastened in any position by a clamp screw.

The latitude arc is graduated to quarter degrees, and reads by its vernier, *e*, to single minutes; it has a range of about thirty-five degrees, so as to be adjustable to the latitude of any place in the United States.

The **Declination Arc**, *b*, is also graduated to quarter degrees, and has a range of about twenty-four degrees.

Its vernier, *v*, reading to single minutes, is fixed to a movable arm, *h*, having its center of motion in the center of the declination arc at *g*; the arm is moved over the surface of the declination arc, and its vernier set to any reading by turning the head of the tangent screw, *k*. It is also securely clamped in any position by a screw, concealed in the engraving.

Solar Lenses and Lines.—At each end of the arm, *h*, is a rectangular block of brass, in which is set a small convex lens, having its focus on the surface of a little silver plate, fastened by screws to the inside of the opposite block.

The silver plate, with its peculiar lines, will be referred to more particularly hereafter.

The **Hour Arc,** *c*, is supported by the two pivots of the latitude arc, already spoken of, and is also connected with that arc by a curved arm, as shown in the figure.

The hour arc has a range of about 120°, is divided to half degrees, and figured in two series; designating both the hours and the degrees, the middle division being marked 12 and 90 on either side of the graduated lines.

The Polar Axis.—Through the center of the hour arc passes a hollow socket, *p*, containing the spindle of the declination arc, by means of which this arc can be moved from side to side over the surface of the hour arc, or turned completely round as may be required.

The hour arc is read by the lower edge of the graduated side of the declination arc.

The axis of the declination arc, or indeed the whole socket, *p*, is appropriately termed the polar axis.

The parts just described constitute properly the *solar apparatus.*

Besides these, however, are seen the needle box, *n*, with its arc and tangent screw, *t*, and the spirit levels, for bringing the whole instrument to a horizontal position.

The **Needle Box,** *n*, has an arc of about 36° in extent, divided to half degrees, and figured from the center or zero mark on either side.

The needle, which is made as in other instruments, except that the arms are of unequal lengths, is raised or lowered by a lever shown in the cut.

The needle box is attached by a projecting arm to a tangent screw, *t*, by which it is moved about its center, and its needle set to any variation.

This variation is also read off by the vernier on the end of the projecting arm, reading to single minutes a graduated arc attached to the plate of the compass.

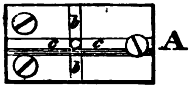
Lines of Refraction.—The inside faces of the sights are also graduated and figured, to indicate the amount of refraction to be allowed when the sun is near the horizon. These are not shown in the cut.

The Horizontal Limb in all Solar Compasses is divided upon silver, and reads by two opposite verniers to single minutes of a degree, the number of minutes being counted off in the same direction in which the vernier moves.

PRINCIPLES OF THE SOLAR COMPASS.

We are now prepared to proceed to the explanation of the peculiar construction of the instrument we are considering.

The little silver plate before referred to, is shown in detail in the following figure. On the surface are marked two sets of lines intersecting each other at right angles; of these, *b b* are termed the hour lines, and *c c*, the equatorial lines, as having reference respectively to the hour of the day and the position of the sun, in relation to the equator.



Below the equatorial lines are also marked three other lines, which are five minutes apart, and are of service in making allowance for refraction, as will be hereafter explained.

The interval between the two lines, *c*, *c*, as well as between *b*, *b*, is just sufficient to include the circular image of the sun, as formed by the solar lens, on the opposite end of the revolving arm.

When, therefore, the instrument is made perfectly horizontal, the equatorial lines and the opposite lenses being accurately adjusted to each other by a previous operation, and the sun's image brought within the equatorial lines, his position in the heavens, with reference to the horizon, will be defined with precision.

Suppose the observation to be made at the time of one of the equinoxes; the arm, *h*, set at zero on the declination arc, *b*, and the polar axis, *p*, placed exactly parallel to the axis of the earth.

Then the motion of the arm, *h*, if revolved on the spindle of the declination arc around the hour circle, *c*, will exactly correspond with the motion of the sun in the heavens, on the given day and at the place of observation; so that if the sun's image was brought between the lines, *c c*, in the morning, it would continue in the same position, passing neither above nor below the lines, as the arm was made to revolve in imitation of the motion of the sun about the earth.

In the morning as the sun rises from the horizon, the arm, *h*, will be in a position nearly at right angles to that shown in the cut, the lens being turned towards the sun, and the silver plate on which his image is thrown directly opposite.

As the sun ascends, the arm must be moved around, until when he has reached the meridian, the graduated side of the declination arc will indicate 12 on the hour circle, and the arm, *h*, the declination arc, *b*, and the latitude arc, *a*, will be in the same plane.

As the sun declines from the meridian, the arm, *h*, must be moved in the same direction, until at sunset its position will be the exact reverse of that it occupied in the morning.

Allowance for Declination.—Let us now suppose the observation made when the sun has passed the equinoctial point, and when his position is affected by declination.

By referring to the Almanac, and setting off on the arc his declination for the given day and hour, we are still able to determine his position with the same certainty, as if he remained on the equator.

When the sun's declination is south, that is, from the 22d of September to the 20th of March in each year, the arc, *b*, is turned towards the plates of the compass, as shown in the engraving, and the solar lens, *o*, with the silver plate opposite, are made use of in the surveys.

The remainder of the year, the arc is turned from the plates, and the other lens and plate employed.

When the Solar Compass is accurately adjusted, and its plates made perfectly horizontal, the latitude of the place, and the declination of the sun for the given day and hour, being also set off on the respective arcs, *if the image of the sun is brought between the equatorial lines the polar axis will be in the plane of the meridian of the place, or in a position* *parallel to the axis of the earth, and the sights will indicate a true north and south line.* The slightest deviation from this position will cause the image to pass above or below the lines, and thus discover the error.

We thus, from the position of the sun in the solar system, obtain a certain direction absolutely unchangeable, from which to run our lines, and measure the horizontal angles required.

This simple principle is not only the basis of the construction of the Solar Compass, but the sole cause of its superiority to the ordinary or magnetic instrument.

The sights and the graduated limb being adjusted to the solar apparatus, and the latitude of the place, and the declination of the sun also set off upon the respective arcs, we are able not only to run the true meridian, or a due east and west course, but also to set off the horizontal angles with minuteness and accuracy from a direction which never changes, and is unaffected by attraction of any kind.

Adjustments :—

The adjustments of this instrument, with which the surveyor will have to do, are simple and few in number, and will now be given in order.

1. *To adjust the Equatorial Lines and Solar Lenses.*

First detach the arm, *h*, from the declination arc by withdrawing the screws shown in the cut from the ends of the posts of the tangent screw, *k*, and also the clamp screw, and the conical pivot with its small screws, by which the arm and declination arc are connected.

The arm, *h*, being thus removed, attach the adjuster in its place by replacing the conical pivot and screws, and insert the clamp screw so as to clamp the adjuster at any point on the declination arc.

Now level the instrument, place the arm, *h*, on the adjuster, with the same side resting against the surface of the declination arc as before it was detached. Turn the instrument on its spindle so as to bring the solar lens to be adjusted in the direction of the sun, and raise or lower the adjuster on the declination arc, until it can be clamped in such a position as to bring the sun's image, as near as may be, between the equatorial lines on the opposite silver plate; and bring the image precisely into position by the tangent screw of the latitude arc, or the leveling screws of the tripod. Then carefully turn the arm half way over, until it rests upon the adjuster by the opposite faces of the rectangular blocks, and again observe the position of the sun's image.

If it remains between the lines as before, the lens and plate are in adjustment; if not, loosen the three screws which confine the plate to the block, and move the plate under their heads, until one half the error in the position of the sun's image is removed.

Again bring the image between the lines, and repeat the operation until it will remain in the same situation in both positions of the arm, when the adjustment will be completed.

To adjust the other lens and plate, reverse the arm end for end on the adjuster, and proceed precisely as in the former case until the same result is attained.

In tightening the screws over the silver plate, care must be taken not to move the plate.

This adjustment now being complete, the adjuster should be removed, and the arm, *h*, with its attachments, replaced as before.

2. *To adjust the Vernier of the Declination Arc.*

Having leveled the instrument, and turned its lens in the direction of the sun, clamp to the spindle, and set the vernier, *v*, of the declination arc, at zero, by means of the tangent screw at *k*, and clamp to the arc.

See that the spindle moves easily and yet truly in the socket, or polar axis, and raise or lower the latitude arc by turning the tangent screw, *f*, until the sun's image is brought between the equatorial lines on one of the plates. Clamp the latitude arc by the screw, and bring the image precisely into position by the leveling screws of the tripod or socket, and without disturbing the instrument, carefully revolve the arm, *h*, until the opposite lens and plate are brought in the direction of the sun, and note if the sun's image comes between the lines as before.

If it does, there is no index error of the declination arc; if not, with the tangent screw, *k*, move the arm until the sun's image passes over half the error; again bring the image between the lines, and repeat the operation as before, until the image will occupy the same position on both the plates.

We shall now find, however, that the zero marks on the arc and the vernier do not correspond; and to remedy this error, the little flat head screws above the vernier must be loosened until it can be moved so as to make the zeros coincide, when the operation will be completed.

3. *To adjust the Solar Apparatus to the Compass Sights.*

First level the instrument, and with the clamp and tangent screws set the main plate at 90° by the verniers of the horizontal limb. Then remove the clamp screw, and raise the latitude arc until the polar axis is, by estimation, very nearly horizontal, and if necessary, tighten the screws on the pivots of the arc, so as to retain it in this position.

Fix the vernier of the declination arc at zero, and direct the equatorial sights to some distant and well marked object, and observe the same through the compass sights. If the same object is seen through both, and the verniers read to 90° on the limb, the adjustment is complete; if not, the correction must be made by moving the sights, or changing the position of the verniers.

HOW TO USE THE SOLAR COMPASS.

Before this instrument can be used at any given place, it is necessary to set off upon its arcs both the declination of the sun as affected by its meridional refraction for the given day, and the latitude of the place where the observation is made.

1. *To set off the Declination.*

The declination of the sun, given in the Ephemeris of the Nautical Almanac from year to year, is calculated for apparent noon at Greenwich, England.

To determine it for any other hour at a place in the United States, reference must be had, not only to the difference of time arising from the longitude, but also to the change of declination from day to day.

The longitude of the place, and therefore its difference in time, if not given directly in the tables of the Almanac, can be ascertained very nearly by reference to that of other places given, which are situated on, or very nearly on, the same meridian.

It is the practice of surveyors in the States east of the Mississippi, to allow a difference of *six* hours for the difference in longitude, calling the declination given in the Almanac for 12 M., that of 6 A. M. at the place of observation.

Beyond the parallel of Santa Fe the allowance would be about *seven* hours; and in California, Oregon, and Washington Territory, about *eight* hours.

Having thus the difference of time, we very readily obtain the declination for a certain hour in the morning, which would be earlier or later as the longitude was greater or less, and the same as that of apparent noon at Greenwich on the given day.

To obtain the declination for the other hours of the day, take from the Almanac the declination for apparent noon of the given day, and also that of the day following, subtract one from the other, as it may have increased or decreased, and we have the change of declination for 24 hours; divide this by 24, and we obtain the change of declination for a single hour, which is to be added to, or subtracted from, that of the starting hour, according as the declination is increasing or decreasing between the two days taken.

To make this more plain, we will give an example. Suppose it was required to obtain the declination for the different hours of April 16th, 1863, at Troy, N. Y.

The longitude in time is 4 hours 54 minutes 40 seconds, or practically 5 hours, so that the declination given in the Almanac, for the given day at Greenwich, would be that of 7 A.M. at Troy. To obtain the hourly change,

Say declination at Greenwich, April 17,	10° 23′ 58″
" " " 16,	10 2 44
Change for 24 hours	21 14

Reduce to seconds, and divide by 24, and we have an hourly change of 53 seconds, which, as the declination is increasing, is to be added every hour after 7 A. M.

Hence, sun's declination at Greenwich noon, as by the table,

being	10 2 44	
Add meridional refraction	38	
	10 3 22	Dec. for 7 A. M.
Add hourly change....	53	
	10 4 15	" 8 "
" "	53	
	10 5 8	" 9 "
" "	53	
	10 6 1	" 10 "
" "	53	
	10 6 54	" 11 "
" "	53	
	10 7 47	" 12 M.
" "	53	
	10 8 40	" 1 P. M.
" "	53	
	10 9 33	" 2 "
" "	53	
	10 10 26	" 3 "

	10 10 26	Dec. for 3 P. M.
Add hourly change....	53	
	10 11 19	" 4 "
" "	53	
	10 12 12	" 5 "
" "	53	
	10 13 5	" 6 "
" "	53	
	10 13 58	" 7 "

In the case taken, the declination is increasing from day to day, and therefore the hourly change is added; if, on the contrary, the declination was decreasing, the hourly change should be subtracted.

The calculation of the declination for the different hours of the day should, of course, be made and noted, before the surveyor commences his work, that he may lay off the change from hour to hour, from a table prepared as above described.

It is considered sufficiently accurate by most government surveyors, to set off the declination only three or four times in the day, at intervals of two or three hours as required.

2. *To set off the Latitude.*

Find the declination of the sun for the given day at noon at the place of observation, as just described, and with the tangent screw set it off upon the declination arc, and clamp the arm firmly to the arc.

Observe in the Almanac the equation of time for the given day, in order to know about the time the sun will reach the meridian.

Then, about fifteen or twenty minutes before this time, set up the instrument, level it carefully, fix the divided surface of the declination arc at 12 on the hour circle, and turn the instrument upon its spindle until the solar lens is brought into the direction of the sun.

Loosen the clamp screw of the latitude arc, and with the tangent screw raise or lower this arc until the image of the sun is brought precisely between the equatorial lines, and turn the instrument from time to time, so as to keep the image also between the hour lines on the plate.

As the sun ascends, its image will move below the lines, and the arc must be moved to follow it. Continue thus, keeping it between the two sets of lines until its image begins to pass above the equatorial lines, which is also the moment of its passing the meridian.

Now read off the vernier of the arc, and we have the latitude of the place, which is always to be set off on the arc when the compass is used at the given place.

3. *To Run Lines with the Solar Compass.*

Having set off, in the manner just given, the latitude and declination upon their respective arcs, the instrument being also in adjustment, the surveyor is ready to run lines by the sun.

To do this, the instrument is set over the station and carefully leveled, the plates clamped at zero on the horizontal limb, and the sights directed north and south, the direction being given, when unknown, approximately by the needle.

The solar lens is then turned to the sun, and with one hand on the instrument, and the other on the revolving arm, both are moved from side to side, until the sun's image is made to appear on the silver plate; when, by carefully continuing the operation, it may be brought precisely between the equatorial lines.

Allowance being now made for refraction, the line of sights will indicate the true meridian; the observation may now be made, and the flag-man put in position.

When a due east and west line is to be run, the verniers of the horizontal limb are set at 90°, and the sun's image kept between the lines as before.

USE OF THE NEEDLE.

In running lines, the magnetic needle is always kept with the sun; that is, the point of the needle is made to indicate 0 on the arc of the compass box, by turning the tangent screw connected with its arm on the opposite side of the plate. By this means, the lines can be run by the needle alone, in case of the temporary disappearance of the sun; but in such cases, of course, the surveyor must be sure that no local attraction is exerted.

The variation of the needle, which is noted at every station, is read off in degrees and minutes on the arc, by the edge of which the vernier of the needle box moves.

TIME OF DAY BY THE SUN.

The time of day is best ascertained by the Solar Compass when the sun is on the meridian, as at the time of making the observation for latitude.

The time thus given is that of apparent noon, and can be reduced to mean time by merely applying the equation of time as directed in the Almanac, and adding or subtracting as the sun is slow or fast.

ADVANTAGES OF THE SOLAR COMPASS IN SURVEYING.

It will readily occur to all who have read the preceding description of the Solar Compass, that while it is indispensable in the surveys of public lands, it also possesses important advantages over the magnetic compass when used in the ordinary surveys of farms, &c.

For not only can lines be run and angles be measured without regard to the diurnal variation, or the effect of local attraction, but the bearings, being taken from the true meridian, will remain unchanged for all time.

The constant uncertainty caused by the variation of the needle, and the litigation to which it so often gives rise, may thus be entirely prevented by the use of the Solar Compass in this kind of work.

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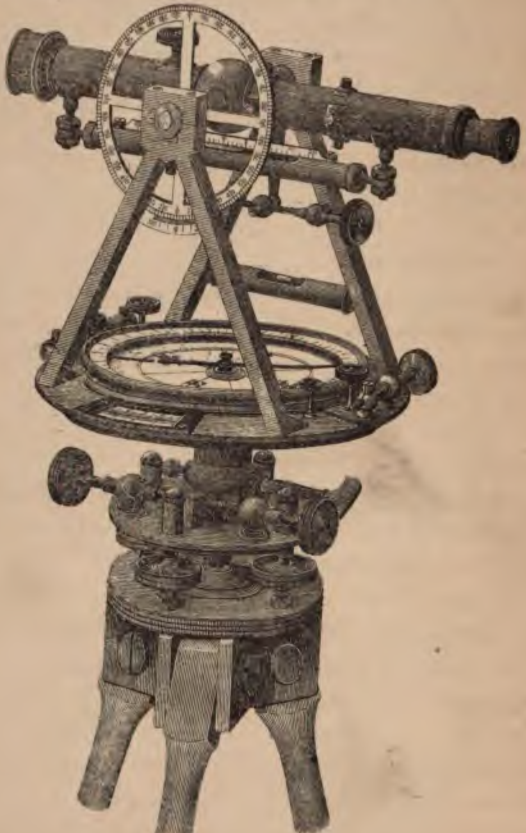
SURVEYOR'S TRANSIT.



THE TRANSIT.

The **Transit** is an instrument designed for measuring either horizontal or vertical angles. It consists of a telescope revolving by its cross bar, in the top of standards attached to a horizontal vernier plate, that moves around a graduated circle or limb beneath.

The telescope "*transits*," or turns, completely around in a vertical plane, so as to be directed to opposite points without revolving the instrument. Within the tube of the telescope, and in the exact focus of the object and eye-glasses, is a small ring, upon which are stretched two fine spider lines at right angles to each other, and forming by their intersection a minute point, by which the telescope can be directed to any object desired.

The vertical circle is connected with the axis of the telescope, and turns with it.

Both the horizontal and vertical circles are divided to half-degrees, and read by their verniers to single minutes.

Clamp and tangent screws are also connected with both the horizontal and vertical circles, by which they are slowly moved a short distance in either direction, and set with the utmost nicety to any position desired.

A compass circle with a magnetic needle is always connected with the Transit, and is used precisely like that of the Surveyor's Compass already described.

When this circle is fixed to the vernier plate, the instrument is termed an *Engineer's Transit;* when it can be turned, like that of the compass, to set off the variation of the needle, as represented in the engraving, it is called a *Surveyor's Transit.*

A level, as shown in the engraving, is often placed on the under side of the telescope, and is used to determine a horizontal line.

Adjustments :—

1. The intersection of the spider lines must be in the optical axis of the telescope, so that the instrument, when placed in the middle of a straight line, will, by the revolution of the telescope, cut its extremities.

To do this, set up the instrument firmly, level the plates, and having clamped all firmly together, direct the telescope by the cross wires to some distant object; revolve the telescope, and find an object in the opposite direction, which the cross-wires will bisect; the two objects would be exactly in line, if the telescope was in adjustment.

To test this, turn the instrument half way around, set the cross-wires precisely upon the second object found, and again revolve the telescope in the direction of the first object.

If the cross-wires strike it, the telescope is in adjustment: if not, by the capstan head screws, shown near the cross-bar, move the ring until, by estimation, one-fourth the error is corrected.

Repeat the operation until the adjustment is complete, and the cross-wires will cut the ends of a straight line.

2. The vertical circle, with its vernier, must be adjusted to the horizontal cross-wire of the telescope.

To do this, level the instrument carefully, and set the zeros of the circle and vernier in exact coincidence; and have the clamp to the telescope axis firmly fastened.

Find or set some distant object, which the horizontal cross-wire will precisely indicate; unclamp the telescope axis, turn the instrument half way around, revolve the telescope, and set the horizontal wire upon the same point; and note whether the zeros of the vertical circle and its vernier correspond as before. If not, slacken the two screws which confine the vernier, and move it until half the error is removed.

Repeat the same operation until the adjustment is complete.

The other adjustments of the transit are mainly the same as those of the compass already given.

1. *To measure horizontal angles with the transit.*

Set the instrument, by a suspended plummet, directly over the point of observation, level the plates by means of the large screws underneath, bring the telescope upon one of the points to be observed, and note the exact reading of the horizontal circle or limb.

Then unclamp the horizontal plates, and turn the telescope so as to strike the second object selected; note the reading of the verniers of the limb, and the difference between the two readings will be the angle required.

2. *To measure vertical angles with the transit.*

If the instrument is in adjustment, direct the telescope to any object whose altitude is required, and read the angle by the vertical circle and vernier; this will be the altitude required.

3. *To run levels with the transit.*

Level the instrument carefully, bring the telescope into a horizontal position, clamp the axis, and with the tangent screw bring the level bubble under the telescope precisely into the centre, and the horizontal cross-wire will indicate a level line in any direction.

THE SURVEYOR'S CHAIN.

In farm surveying, lines are measured with a chain 66 feet, or 4 rods long. This chain is divided into 100 links, each being 7.92 inches long; 10 square chains make an acre, and as the links are hundredths of a chain, we can say, 2 chains and 46 links, or 2.46 chains, or 246 links. And the area computed in chains can be expressed in acres by moving the decimal point one place to the left. To facilitate the counting, every tenth link is indicated by a small piece of brass.

NOTE.—Engineers measure lines with a chain 100 feet long. This is divided into 100 links, each link being one foot long.

PLANE TABLE.

The **Plane Table** is exactly what the name indicates; it is a plane board table, about two feet long and 20 inches wide, resting on a tripod, to which it is firmly screwed, yet capable of an easy motion on its centre, having a ball and socket like a compass staff.

Directly under the table is a brass plate, in which *four milled screws* are worked, for the purpose of adjusting the table, the screws pressing against the table.

To level the table, a small detached spirit-level may be used. The level being placed on the table over two of the screws, the screws are turned contrary ways until the level is horizontal; after which it is placed over the other two screws, and made horizontal in the same manner.

The table has a clamp screw to hold it firmly during observations, and also a tangent screw to turn it minutely and gently, after the manner of the theodolite.

The upper side of the table is bordered by four narrow brass plates, and the centre of the table is marked by a pin.

About this center, and tangent to the corners of the table, *conceive* a circle to be described. Suppose the circumference of this circle to be divided into degrees and parts of a degree, and radii to be drawn through the center, and each point of division.

The points in which these radii intersect the outer edge of the brass border, are marked by lines on the brass plates; these lines, of course, show degrees and parts of degrees; they are marked from right to left, from 0 to 180° on both sides, but on some tables the numbers run all the way round, from 0 to 360°.

Near the two ends of the table are two grooves, into which are fitted brass plates, which are drawn down into their places by screws coming up from the under side. The object of these grooves and corresponding plates, is to hold down paper firmly and closely to the table.

The paper, before being put on, should be moistened to expand it; then, carefully drawn over the table, and fastened down by the plates that fit into the grooves; on drying, it will closely fit the table.

A delicate fine-edged ruler is used with the plane table; it has vertical sights, the lines of which are in the same vertical plane as the edge of the ruler.

The plane table may be used for three distinct objects.

1st. For the measurement of horizontal angles.

2d. For the determination of the shorter lines of a survey, both as to extent and position.

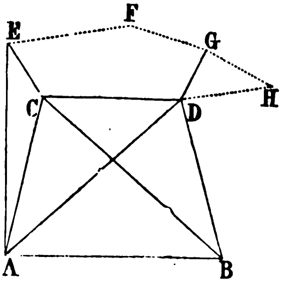
3d. For the purpose of mapping down localities, harbors, water courses, &c.

1. *To measure a horizontal angle.*

Place the center of the table over the angular point. Level the table, then place the edge of the ruler against the pin at the center; direct the sights to one object, and note the degree on the brass plate; then turn the ruler to the other object, and note the degree as before. The difference of the degrees thus noted is the angle sought.

If the ruler passed over 0 in turning from one object to the other, subtract the larger angle from 180°, and to the remainder add the smaller angle.

2. *To determine lines in extent and position.*



Let CD, in the diagram, be a base line; place the table over C so that the point on the table, where we wish C to be represented, shall fall directly over C; and place the table in such position that CD shall take the desired direction on the table.

Now level the instrument, and clamp it fast; it is then ready for use.

Sight to the other end of the base line, and mark it along the fine edge of the ruler.

In the same manner, sight along the direction of *CE*, and mark that direction in a fine lead line, that can be easily rubbed out; the point *E* is *somewhere* in that line.

Sight in the direction of *F*, and mark the line on the paper; *F* is somewhere in that line. In this manner, sight to as many objects as desired, as *G*, *H*, *B*, *A*, &c.

Now the base *on the paper*, may be as long, or as short as we please; suppose the *real base* on the ground to be 1,200 feet; this may be represented on the table by 3, 4, 5, 10, or 12 inches, more or less. Suppose we represent it by 6 inches; then one inch on the paper will correspond with 200 feet on the ground (*horizontally*).

Take *CD*, six inches, and place a pin at *D*, remove the instrument to the other end of the base, and place *D* of the table right over the end of the base, by the aid of a plumb, and give the table such a position as will cause *CD* on the table, to correspond with the direction of the base.

Level the table and clamp it. Now, if *CD* on the table does not exactly correspond with the direction of the base on the ground, make it correspond by means of the tangent screw.

Now from *D*, by means of the ruler and its sight vanes, draw lines on the paper, in the direction of the points *E*, *F*, *G*, *H*, *B*, *A*, &c.; and where these lines intersect those from the other end of the base to the same points, are the real localities of those points, *in proportion* to the base line. Lines drawn from point to point, where these lines intersect, as *EF*, *FG*, *GH*, &c., will determine the relative distances from point to point, at the rate of 200 feet to the inch.

Lines drawn from the center of the table, parallel to *FE* and *FG*, will determine the angle *EFG*, in case the angle is required. After the points, *E*, *F*, *G*, &c., have been determined, the light pencil lines to them, from the ends of the base, may be rubbed out, except those that we may wish to retain.

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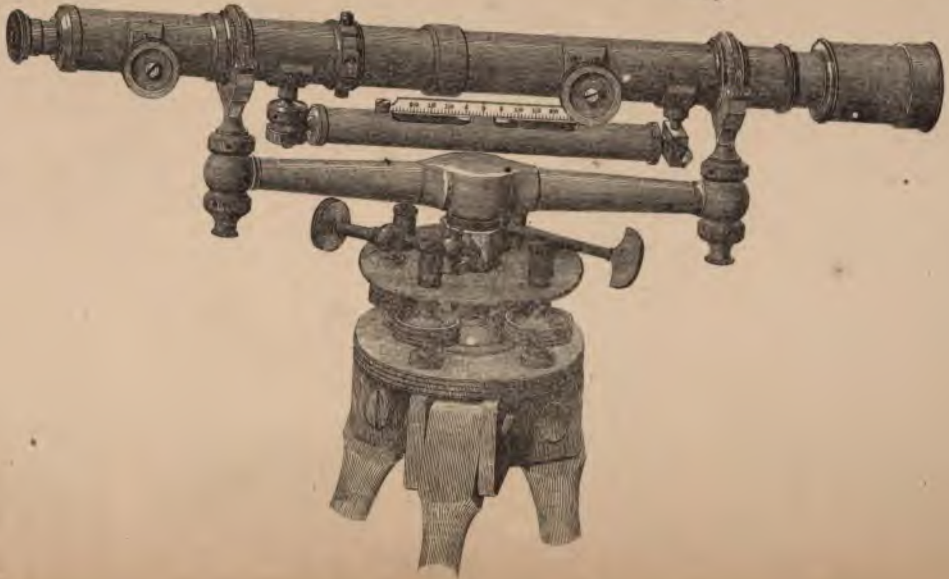
20 INCH Y LEVEL,



THE ENGINEER'S LEVEL.

The engineer's level is an instrument by which we can mark a horizontal line, or a line parallel to the surface of tranquil water, and by which we can ascertain how much certain points are above or below the line marked out. This instrument consists essentially of a telescope and an attached level.

Adjustments :—

1. The intersection of the spider lines should be in the optical axis of the telescope.

Direct the telescope to some distant object, and bring the intersection of the spider lines upon some distinct point; then revolve the telescope on its bearings. If the intersection moves from the point, change the position of the spider lines by the screws attached, until the intersection will remain upon the same point while the telescope is revolved upon its bearings.

2. The level attached should be parallel to the optical axis of the telescope.

Bring the bubble to the middle of the level tube; then take the telescope from its bearings, and reverse it. If the bubble does not remain at the middle, the tube must be changed in position by the screws at its end, until the bubble will settle at the middle after the telescope is reversed.

3. The optical axis of the telescope should be perpendicular to the axis of the instrument, so that the bubble will remain in the middle of its tube during an entire revolution of the instrument on its axis. Bring the telescope directly over two opposite leveling screws; then bring the bubble to the middle of its tube, and revolve the instrument on its vertical axis; if the bubble moves from the middle, one of the standards or wyes must be moved by the nuts on either side of the bar until the instrument can be revolved without displacing the bubble.

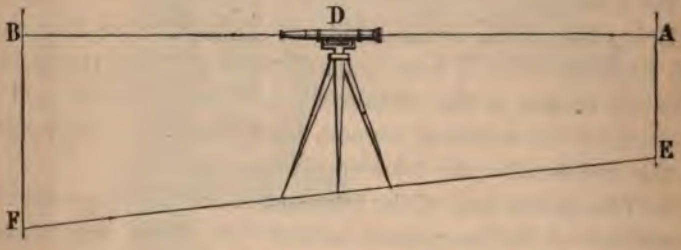
The Tripod Head of the engineer's level has two parallel plates connected by a ball and socket-joint, upon which the upper plate moves. There are four large-headed screws called leveling screws, which move in bearings in the upper plate, and which, by pressing upon the lower plate, keep the two plates firmly apart.

To level the instrument, turn the telescope directly over two opposite leveling screws. Then turn these two screws in contrary directions moving both thumbs in or out as may be required until the bubble is in place. Then place the telescope directly over the other opposite leveling screws, and turn these two in contrary directions, until the bubble is in place.

There are also clamp and tangent screws, giving a slow motion to the telescope, to enable the observer to bring the spider lines precisely upon any point. The use of these will be readily understood from an examination of the instrument.

To Test the Adjustment of the Level.

It is important that the level should be in as perfect adjustment as possible. The accuracy of the adjustments may be tested as follows.



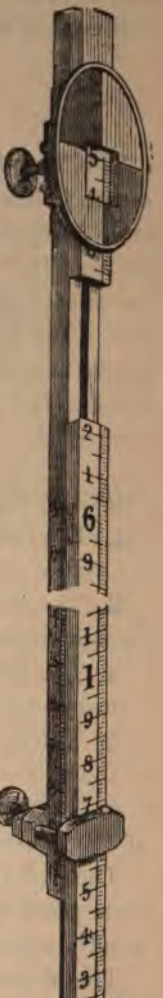
. Measure very carefully the distance between two stations, as *E* and *F*, and set the instrument exactly midway between them as represented in the last figure.

Then level the instrument, and find the difference of the levels between *E* and *F* (two pegs driven into the ground).

Now, suppose *A E* measures on the rod, .	4.752 feet.
And *B F* " " " .	6.327 feet.
Then *E* is above *F*	1.575 feet.

Now bring the level near to one of the stations as *E*, and level it very accurately, and sight to the rod *A E*.

Now, suppose the target stands at	5.137 feet.
To this add	1.575 feet.
	6.712



The rod man now goes to the station *F*, puts his target on the rod exactly at 6.712, and the telescope is turned upon it, and the horizontal spider line ought to just coincide with the target, and will, if the instrument is in perfect adjustment; if it is not, the error is taken out by the screws shown on the outside of the tube. If the error was but slight, as in such cases it always is, with good instruments, the adjustment is as complete as it can be made.

THE LEVELING ROD.

The **Engineer's Leveling Rod** is formed of two pieces of wood sliding from each other, and graduated into feet, tenths, and hundreds, with verniers reading to thousandths of a foot. The target is circular, and painted white and red in alternate quadrants. It is kept in place by a clamp-screw, and it carries upon the front side of the rod a vernier reading to the thousandth of a foot. The front surface on which the target moves, reads to six and a half feet; when a greater height is required, the horizontal line of the target is fixed at that point, and the upper half of the rod carrying the target is moved out of the lower, the reading being now obtained by a vernier on the graduated side, up to an elevation of nearly twelve feet.

The verniers on the engineer's leveling rod are so constructed that ten spaces of the vernier scale are just equal to nine of the smallest spaces on the graduated rod; and as these last spaces are hundredths of a foot, the verniers will read to the thousandth of a foot.

THE THEODOLITE.

The **Theodolite** is an instrument designed for the measurement of either horizontal or vertical angles. It answers the same purposes, therefore, in the main, as the transit. Like the transit, it has two graduated circles, one horizontal, and the other vertical; also a telescope, and generally a compass box. The telescope, however, rests in Y shaped supports, as in the engineer's level, and may be reversed without disturbing the position of the vertical circle with which it is connected.

Adjustments :—

1. The intersection of the spider lines should be in the optical axis of the telescope.
2. The level attached to the telescope should be parallel to the optical axis of the telescope.
3. The axis of the telescope should be parallel to the horizontal plate.
4. The optical axis of the telescope should be perpendicular to the axis of motion.
5. The vertical circle should be perpendicular to the axis of the telescope and the horizontal plate.

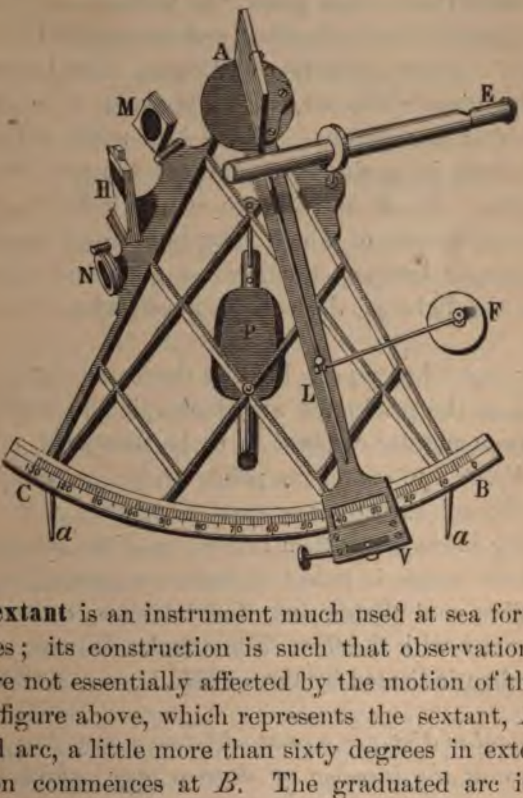
The first two of these adjustments are made precisely as the corresponding adjustments of the level. The other three are usually attended to by the maker.

The theodolite is less convenient in practical field work than the transit, and has never been popular in our own country.

SECTION II.

INSTRUMENTS IN NAVIGATION.

THE SEXTANT.



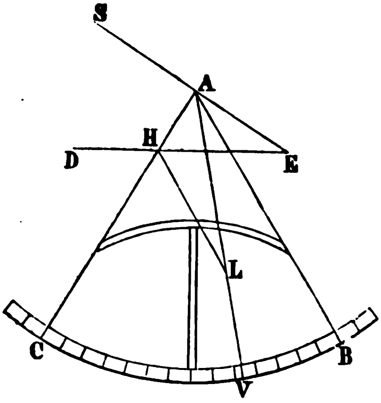
The **Sextant** is an instrument much used at sea for measuring angles; its construction is such that observations made with it are not essentially affected by the motion of the ship.

In the figure above, which represents the sextant, *BC* is a graduated arc, a little more than sixty degrees in extent; the graduation commences at *B*. The graduated arc is firmly connected with a frame of brass or ebony. *A V* is a revolving *index bar*, turning on a pivot at the center of the circular part at *A*, this point being also the center of the graduated arc. Attached to the index bar, near *V*, is a *vernier scale*, which slides over the graduated arc, and which may be fastened at any point by a clamp screw, or moved gently by a tangent screw. There is also a microscope attached to the bar, which may be turned over the vernier, and used to distinguish the lines of graduation. At *A* is a small plane mirror, perpendicular to the plane of the sector; it is attached to the index bar, and revolves with it. This is called the ***index glass.*** Attached to the frame of the instrument, at *H*, is another mirror, called the *horizon glass.* It is fixed at right angles with the plane of the instrument, and is parallel to the index glass when the index is at zero of the arc. The lower half of the horizon glass is silvered, so as to make it a reflector; the upper half is transparent. There is a small telescope, *E*, which is fixed in a ring, and directed towards the horizon glass at *H*. At *M* and *N* are sets of colored glasses or screens, one or more of which may be thrown between the two mirrors, or between the horizon glass and telescope, to moderate the light of the sun or moon, when under observation.

The sextant when used is held by the handle at *P*, so that the plane of the graduated arc shall coincide with the two points whose angular distance is to be measured. The telescope is directed to one of the points or bodies, which is seen directly through the upper or transparent part of the horizon glass. The index bar is then turned, until the other point or body, whose image is reflected from the index glass to the horizon glass and thence into the telescope, comes into apparent contact with the first. The angular distance of the two points is then indicated by the vernier.

The angular distance measured between any two objects is always twice the number of degrees over which the index bar moves.

To show this, we will make use of a diagram, showing only the lines of direction assumed by the principal parts of the instrument. *A V* is the direction of the plane of the index



glass, and HL the direction of the plane of the horizon glass. The eye piece of the telescope is supposed to be at E.

Now conceive a ray of light coming from an object S, and striking the mirror A, the index mirror being turned so as to throw the reflecting ray into the mirror H; this mirror again reflects it towards E, and an eye anywhere in the line DH will see the image of the object behind the mirror H. Conceive the ray of light from S to pass right through the mirror at A, to meet the line HE; then, it is obvious that the angle SED measures the angle between the object S and its image D.

It is a principle in optics that the angle of incidence is equal to the angle of reflection; from this it follows that VA bisects the angle EAH in the diagram; and LH, the direction of the horizon glass, bisects the angle EHC. In the triangle EAH, the angle at E is equal to the difference of the exterior angle EHC, and the interior angle EAH.

Also, in the triangle LAH, the angle at L is equal to the difference of the exterior angle LHC, and the interior angle LAH. Therefore we have

$$E = EHC - EAH,$$
$$L = LHC - LAH.$$

But EHC is twice LHC, and EAH is twice LAH; whence it follows that the angle E is twice the angle L; but the angle L is equal to the angle BAV, because HL is parallel to AB. Therefore the angle at E is twice the angle BAV, which is measured by the arc BV, over which the zero of the index arm has moved. It is obvious that double the number of degrees in the arc BV will be the number of degrees in the angle E.

For convenience, however, every half degree of the graduated arc is reckoned as a degree; for it represents a degree of the angle measured. In the figure representing the sextant, the arc BC is sixty-five degrees in extent, but the 130 half degrees into which it is divided are reckoned as 130 degrees.

Adjustments:

1. The index glass should be perpendicular to the plane of the instrument.

Place the index near the middle of the arc, and look into the index glass in the direction of the plane of the instrument. If the reflected arc appear in a line with the arc seen direct, the index glass is perpendicular to the plane of the instrument; if not, the index glass must be moved until the arc and its image appear in a line.

2. The horizon glass should be parallel to the index glass when the index is placed at zero.

Clamp the index at zero, hold the instrument vertically, and see if the distant horizon coincides with its image, as seen in the horizon glass, so as to form one continued line; if not, the horizon glass must be moved by its screws until the object and its image coincide.

3. The horizon glass should be perpendicular to the plane of the instrument.

Clamp the index at zero, and look at some smooth portion of the distant horizon while holding the instrument perpendicular; a continued unbroken line will be seen in both parts of the horizon glass; and if, on turning the instrument from the perpendicular, the horizontal line *continues unbroken*, the horizon glass is in full adjustment; but if a break in the line is observed, the glass is not perpendicular to the plane of the instrument, and must be made so by the screw adapted to that purpose.

After an instrument has been examined according to these directions, it may be considered as in an approximate adjustment; a re-examination will render it more perfect.

Finally, we may find its *index error* as follows: Measure the sun's diameter both on and off the arch—that is, both ways from 0; and if it measures the same, there is *no index error*. But if there is a difference, half that difference will be the index error, *additive*, if the greater measure is off the arch, *subtractive*, if on the arch.

1. *To measure the altitude of the sun at sea.*

Turn down the proper screen or screens to defend the eye. Put the index at 0, having it loose, look directly at the sun through the tube, and you will see its image in the silvered part of the horizon glass. Now move the index, and the image will drop; drop it to the horizon, and clamp the index.

Let the instrument slightly vibrate each side of the perpendicular, on the line of sight as a center, and the image of the sun will apparently sweep along the horizon in a circle. While thus sweeping, move the tangent screw, so that the lower limb of the sun will just touch the horizon, without going below it. The reading of the index will be the altitude corresponding to that instant, provided there be no index error.

2. *To measure the angular distance between two bodies as the sun or moon, or the moon and a star.*

The most brilliant of the two objects is always reflected to the other. Loosen the index, place it at 0, and direct the line of sight to the brighter object, and catch a view of its image in the silvered part of the horizon glass.

Turn the plane of the instrument into the plane between the two objects; now move the index, keeping the eye on the image, and bring it along to the other object; bring them as near as possible, then gently clamp the index.

Hold up the instrument again, in the plane between the two objects, and view one object through the transparent part of the horizon glass; and when the instrument is in the right position, the image of the other object will appear also in the same field of view, and then, with the tangent screw, make the limb of the reflected object just touch the other, as it moves past it, to and fro, by the gentle motion of the instrument, until the observer is satisfied that he has got the measure as near as he can.

The limb of the sextant is divided into degrees, and each degree subdivided into six equal parts by short lines, each of these parts being read as ten minutes.

The vernier is so constructed that 60 spaces on the vernier scale are just equal to 59 of the smallest spaces on the limb; and as these spaces are 10′ each, the vernier will read to 10″.

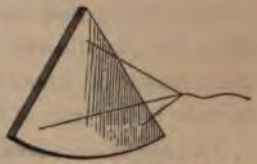
Now, if the zero mark of the vernier coincides with any line on the limb, then that line will indicate the angle. Thus, if it coincides with the line marked 30, then the angle is 30°. If the zero coincides with the next long mark beyond that marked 30, then the angle is 31°. If the zero does not coincide with the next long line, but is beyond it, and coincides with one of the shortest lines, then the angle will be 31° and so many minutes, counting each small space as 10′. When the zero division of the vernier does not coincide with any line upon the limb, but stands between two of them, then look along the vernier scale for a line that does coincide with a line on the limb; then count from the zero to the coinciding line upon the vernier, calling each small space of the vernier 10″; the result added to the reading of the limb will give the angle. If, for example, the zero of the vernier is between the second and third short lines, which are between the first and second long lines beyond 30 on the limb, and the fourth short line beyond 3 on the vernier coincides with a line on the limb; then from the limb we read 31° 20′, and from the vernier we read 3′ 40″, and the two readings give for the angle

31° 23′ 40″.

In reading from any vernier, first ascertain the value of the lowest division of the limb of the instrument, and then find the relation of one division of the vernier to one division of the limb. This can be done by finding how many of the divisions of the limb are equal to the graduated part of the vernier.

THE LOG.

The rate at which a ship sails is measured by a line running off of a reel, called the *log line.*



The log is nothing more than a piece of thin board in the form of a sector, of about six inches radius: the circular part is loaded with lead to make it stand perpendicular in the water.

The line is so attached to it that the flat side of the log is kept toward the ship, that the resistance of the water against the face of the log may prevent it, as much as possible, from being dragged after the ship by the weight of the line or the friction of the reel.

The time which is usually occupied in determining a ship's rate is half a minute, and the experiment for the purpose is generally made at the end of every hour, but in common merchantmen at the end of every second hour. As the time of operating is half a minute, or the hundred and twentieth part of an hour, if the line were divided into 120ths of a nautical mile, whatever number of those parts a ship might run in a half minute, she would, at the same rate of sailing, run exactly a like number of miles in an hour. The 120th part of a mile is by seamen called a *knot*, and the knot is generally subdivided into smaller parts, called *fathoms.* Sometimes (and it is the most convenient method of division) the knot is divided into ten parts, more frequently perhaps into eight; but in either case the subdivision is called a *fathom*.

The *sixtieth* part of a degree is called a *nautical mile.*

We shall consider a fathom the tenth of a knot, and as the nautical mile is 6,079 feet, the 120th part of it is 50.66, the length of a knot on the line, and a little over five feet is the length of a fathom.

The operation of ascertaining the rate of sailing is called by seamen *heaving the log.*

At the end of an hour the *loaded chip,* or log, is thrown over the stern into the sea; a quantity of the line, called the *stray line,* is allowed to run off, then the glass is turned, and the number of knots that runs off the reel during the *half* minute is the rate of the ship's motion.

The log is then hauled in, and the same operation is repeated at the end of the next hour.

The officer of the watch, who has been on deck during the hour, will mark on the slate or board, called the log board, the number of miles and parts of a mile which the ship has sailed during the last hour, according to the best of his *judgment;* the log was thrown only to help make up that judgment, for the rate at the time the log was thrown may have been considerably more or less than the average motion during the hour.

SECTION III.

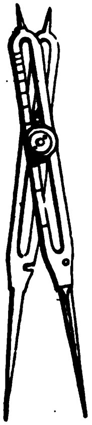
PLOTTING INSTRUMENTS.

Plotting Instruments are those instruments used in delineating upon paper the lines of any survey, in their relative position and true proportion.

The following are instruments which require no extended description.

1. The **Proportional Compass** is an instrument employed for laying off lines proportional to given lines. It can be so adjusted, by moving the pivot, as to secure any required ratio between the lines to be drawn and the given lines. (*See Fig.* 1.)

1.



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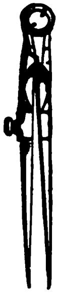

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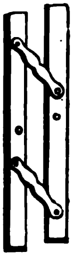

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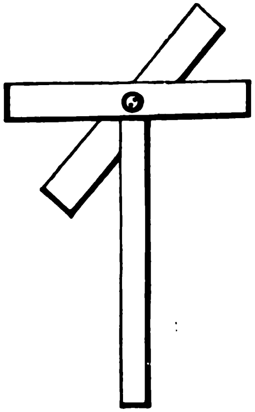

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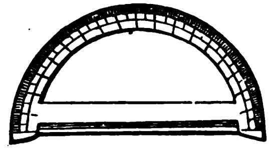

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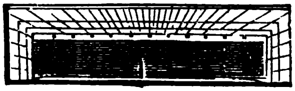

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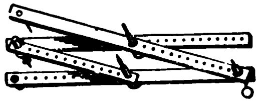


2. The **Dividers** are used in describing arcs of circles with given radii, and in transferring proportional lines to paper. (*See Fig* 2.)

3. The **Parallel Rule** is used in drawing lines parallel to a given line. (*See Fig.* 3.)

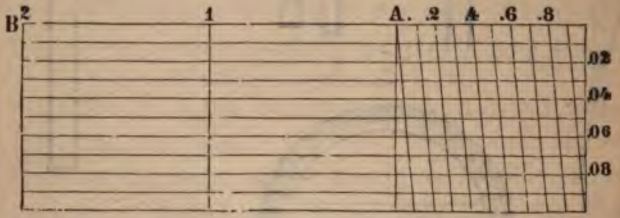
4. The **T Square** is used in drawing perpendiculars and parallels. (*See Fig.* 4.)

5. The **Protractor** is a graduated semi-circle used in measuring angles and in transferring them to paper. (*See Fig.* 5.)

6. The **Engineer's Protractor** is only another form of the instrument last described. It consists of a rectangular piece of ivory or metal, graduated upon three sides by lines converging to a center in the fourth side. The graduations represent degrees, or parts of a degree, as in the other form. (*See Fig.* 6.)

7. The **Pantograph** is an instrument used for taking an enlarged or diminished copy of any figure, the exact form being preserved. It can be so adjusted that the lines of the copy shall bear any required ratio to the corresponding lines of the original. (*See Fig.* 7.)

THE DIAGONAL SCALE OF EQUAL PARTS.



This scale is used in transferring lines measured in units, tens and hundreds, or units, tenths and hundredths.

To represent 2 chains and 46 links, place one foot of the dividers on the sixth parallel below 2, and extend the other foot to where the diagonal .4 intersects the parallel .06; and the space included will represent 2 chains 46 links on a scale of one chain to the inch, or 24 chains 60 links on a scale of ten chains to the inch, or 246 chains on a scale of one hundred chains to the inch.

GUNTER'S SCALE.

Gunter's Scale is commonly two feet in length, containing the plane scale, and the scale of sines, chords, and tangents on one side of it, and the scale for the *logarithms* of numbers, sines, and tangents on the other. The logarithmic scale is not much used.

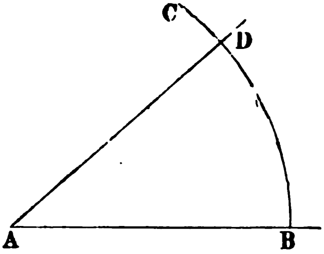
The plane scale includes, in addition to the scale of equal parts, a line of chords formed by transferring the chords of the several arcs, into which a quadrant is divided, to a straight line, the distance from 0 to 60 being the radius of the quadrant; also.

a line of rhumbs, which is a line of chords where the quadrant is divided into 8 equal parts, called points.

There are also lines of natural sines, tangents and secants, and a line of semi-tangents used in projections, as a line of longitudes used in navigation, and a line of latitudes used in the construction of sun-dials.

The lines of equal parts are by far the most useful of the plane scale; these lines are sometimes so graduated as to give 10, 15, 20, 25, &c., parts to the inch.

1. *To lay down a given angle with the line of chords.*



Let it be required to construct an angle of 40° at the point *A*. With the dividers take 60 from the line of chords, and with one foot at *A* describe the arc *BC* with 60 as radius; then from the same line of chords take 40, and with one foot of the dividers at *B*, mark the point *D* with the other foot, and draw the line *AD*.

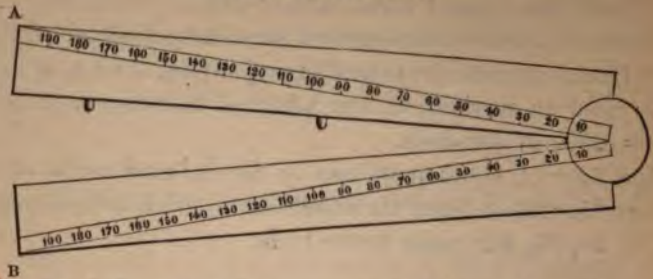
The angle *BAD* will be the required angle of 40°.

2. *To measure an angle with the line of chords.*

Let it be required to measure the angle at *A* in the diagram. With the chord of 60, and *A* as center, describe the arc *BD*, intersecting the sides that include the angle; then extend the dividers from *B* to *D*, and with that distance apply them to the line of chords, one foot being at the zero of the line; the other will point out the degrees in the angle.

Angles are constructed and measured much more readily with a protractor than with the lines on the plane scale.

THE SECTOR.



The **Sector** consists of two graduated arms, movable about a common point as center. On each arm are several lines diverging from the central point. One of these lines is divided into equal parts, and is called the line of lines; another is so graduated as to form a line of chords; another the line of sines; another the line of tangents, &c. The lines of chords, sines, and tangents, are constructed upon the same radius, so that when the sector is open to any angle, the distance from 60 to 60 on the line of chords is the same as the distance from 90 to 90 on the line of sines, or the distance from 45 to 45 on the line of tangents.

The principle of the sector depends upon the proportionality of the sides of similar triangles; and as the lines on one arm are graduated precisely the same as the corresponding lines on the other arm, it is obvious that when the sector is open at any angle, as in the diagram, we shall have—

$$CA : AB :: CA' : A'B'.$$

Therefore $A'B'$ is the same part of AB that CA is of CA. Hence if CA' is a chord of any angle to CA as radius, $A'B'$ will be a chord of the same angle to AB as radius; and if CA' is a sine of any angle to CA as radius, then $A'B'$ will be a sine of the same angle to AB as radius.

Examples.—1. To find the chord of 40° to a radius of 5 inches, open the sector so that the distance from 60 to 60 on the line of chords shall be 5 inches; then the distance from 40 to 40 on the same line will be the chord required.

2. To find the sine of 44° to a radius of 6 inches, open the sector so that the distance from 90 to 90 on the line of sines shall be 6 inches; then the distance from 44 to 44 on the line of sines will be the sine required.

The sector is also used in drawing lines to any proposed scale.

Example.—To draw a line of 37 feet on a scale of 20 feet to the inch; open the sector so that the distance from 20 to 20 on the line of equal parts shall be one inch; then the distance from 37 to 37 on the same line will represent 37 feet on a scale of 20 feet to the inch.

To divide a given line into any number, say 5 equal parts, open the sector so that the distance from 5 to 5 on the line of equal parts shall equal the given line; then the distance from 1 to 1 on the line of equal parts will be one of the required parts.

The advantage of the sector will appear from the following problem.

A map is before me, its scale is 20 miles to an inch; I wish to find the distance in a right line between two points laid down on it.

1st. I take one inch in the dividers, and open the sector so that the distance between 20 and 20 on the two arms, shall just correspond to the measure in the dividers, that is, shall be one inch. Let the sector lie on the table thus opened.

2d. Now take the distance you wish to measure, in the dividers; place one foot on one arm of the sector, and the other foot on the other arm; so that the feet of the dividers shall fall on the same number on both arms of the sector.

The number thus marked by the dividers will be the distance required. The distance between any two other points may be measured on the same map, without any computation whatever.

It is obvious from the construction of the sector that such problems as finding *third* proportionals, *fourth* proportionals, or *mean* proportionals, can readily be solved from the line of equal parts; and also that the various proportions in trigonometry can be worked by taking the sides of the triangles from the line of equal parts, and the degrees and minutes from the lines of sines, tangents

On some sectors there are other lines, such as a line of polygons, a line of solids, etc. But these are more curious than useful.

SECTION IV.

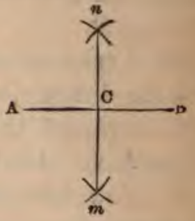
PROBLEMS SOLVED INSTRUMENTALLY.

With the instruments previously described, solve the following problems. The references are to Robinson's New Geometry. Thus, (th. 15, b. 1, cor. 1), indicates theorem 15, book 1, corollary 1, where the demonstrations of the problem referred to will be found.

PROBLEM I.

To bisect a given finite straight line.

Let AB be the given line, and from its extremities, A and B, with any radius greater than the half of AB, describe arcs, cutting each other in n and m. Join n and m; and C, where it cuts AB, will be the middle of the line required.

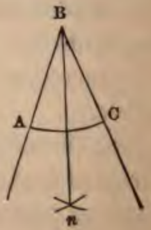


Proof, (th. 18, b. 1, sch. 2).

PROBLEM II.

To bisect a given angle.

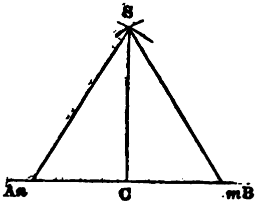
Let ABC be the given angle. With any radius, from the center B, describe the arc AC. From A and C, as centers, with a radius greater than the half of AC, describe arcs intersecting in n, and join Bn; it will bisect the given angle.



Proof, (th. 21, b. 1).

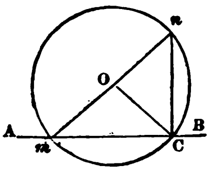
PROBLEM III.

From a given point, in a given line, to draw a perpendicular to that line.



Let AB be the given line, and C the given point. Take n and m at equal distances on opposite sides of C; and from the points m and n, as centers, with any radius greater than nC or mC, describe arcs cutting each other in S. Join SC, and it will be the perpendicular required.

Proof, (th. 23, b. 1, cor.).



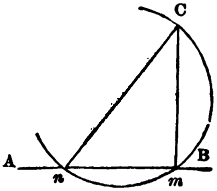
The following is another method, which is preferable when the given point, C, is at or near the end of the line.

Take any point, O, which is manifestly one side of the perpendicular, and join OC; and with OC, as a radius, describe an arc, cutting AB in m and C. Join mO, and produce it to meet the arc, again, in n; mn is then a diameter to the circle. Join Cn, and it will be the perpendicular required.

Proof, (th. 9, b. 3).

PROBLEM IV.

From a given point without a line, to draw a perpendicular to that line.

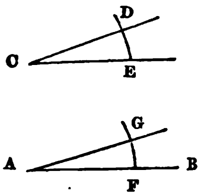


Let AB be the given line, and C the given point. From C draw any oblique line, as Cn. Find the middle point of Cn by (Prob. I.), and from that point as a center describe a semicircle, having Cn as a diameter. From m, where the semi-circumference cuts AB, draw Cm, and it will be the perpendicular required.

Proof, (th. 9, b. 3).

PROBLEM V.

At a given point in a line, to make an angle equal to another given angle.



Let A be the given point in the line AB, and DCE the given angle.

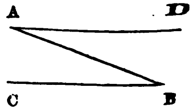
From C as a center, with any radius CE, draw the arc ED.

From A as a center, with the radius $AF=CE$, describe an indefinite arc; and from F as a center, with FG as a radius, equal to ED, describe an arc, cutting the other arc in G, and join AG — GAF will be the angle required.

Proof, (th. 5, b. 3).

PROBLEM VI.

From a given point, to draw a line parallel to a given line.

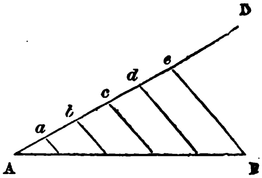


Let A be the given point, and CB the given line. Draw AB, making an angle, ABC; and from the given point A, in the line AB, draw the angle $BAD=ABC$, by the last problem.

AD and CB make the same angle with AB; they are, therefore, parallel. (Th. 7, b. 1, cor. 1).

PROBLEM VII.

To divide a given line into any number of equal parts.



Let AB represent the given line, and let it be required to divide it into any number of equal parts, say five. From one end of the line A, draw AD, indefinite in both length and position. Take any convenient distance in the dividers, as Aa, and set it off on the line AD, thus making the parts Aa, ab, bc, &c., equal. Through the last point, *e*, draw *EB*, and through the points *a*, *b*, *c*, and *d*, draw parallels to *eB* (problem 6); these parallels will divide the line as required.

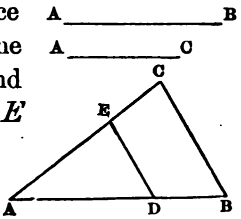
Proof (th. 17, b. 2).

PROBLEM VIII.

To find a third proportional to two given lines.

Let *AB* and *AC* be any two lines. Place them at any angle, and join *CB*. On the greater line, *AB*, take $AD = AC$, and through *D* draw *DE* parallel to *BC*; *AE* is the third proportional required.

Proof, (th. 17, b. 2.)

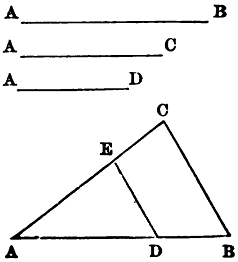


PROBLEM IX.

To find a fourth proportional to three given lines.

Let *AB*, *AC*, *AD*, represent the three given lines. Place the first two together, at a point forming any angle, as *BAC*, and join *BC*. On *AB* place *AD*, and from the point *D*, draw (problem 6) *DE* parallel to *BC*; *AE* will be the fourth proportional required.

Proof, (th. 17, b. 2).

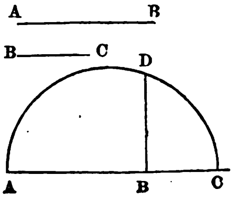


PROBLEM X.

To find the middle, or mean proportional, between two given lines.

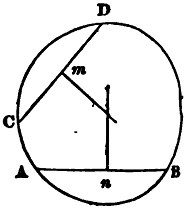
Place *AB* and *BC* in one right line, and on *AC* as a diameter describe a semi-circle (postulate 3), and from the point *B* draw *BD* at right angles to *AC* (problem 3); *BD* is the mean proportional required.

Proof, (cor. to th. 17, b. 3).



PROBLEM XI.

To find the center of a given circle.

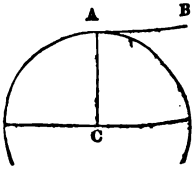


Draw any two chords in the given circle, as *AB* and *CD*; and from the middle point, *n*, of *AB*, draw a perpendicular to *AB*; and from the middle point, *m*, draw a perpendicular to *CD*; and where these two perpendiculars intersect will be the center of the circle.

Proof, (th. 1, b. 3, cor).

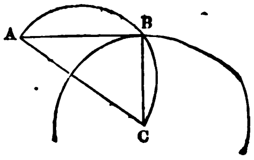
PROBLEM XII.

To draw a tangent to a given circle, from a given point, either in or without the circumference of the circle.



When the given point is in the circumference, as *A*, draw *AC* the radius, and from the point *A*, draw *AB* perpendicular to *AC*; *AB* is the tangent required.

Proof, (th. 4, b. 3).



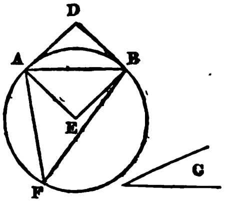
When *A* is without the circle, draw *AC* to the center of the circle; and on *AC*, as a diameter, describe a semi-circle; and from *B*, where the semi-circumference cuts the given circumference, draw *AB*, and it will be tangent to the circle.

Proof, (th. 9, b. 3), and (th. 4, b. 3).

PROBLEM XIII.

On a given line, to describe a segment of a circle, that shall contain an angle equal to a given angle.

Let AB be the given line, and C the given angle. At the ends of the given line, make angles DAB, DBA, each equal to the given angle, C. Then draw AE, BE, perpendiculars to AD, BD; and from the center E, with radius EA or EB, describe a circle; then AFB will be the segment required, as any angle F, made in it, will be equal to the given angle C.

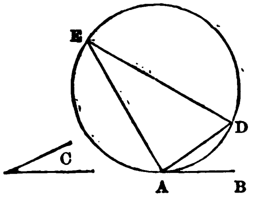


Proof, (th. 11, b. 3), and (th. 8, b. 3).

PROBLEM XIV.

To cut a segment from any given circle, that shall contain a given angle.

Let C be the given angle. Take any point, as A, in the circumference, and from that point draw the tangent AB; and from the point A, in the line AB, make the angle $BAD = C$ (problem 5), and AED is the segment required.

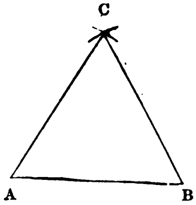


Proof. (th. 11, b. 3), and (th. 8, b. 3).

PROBLEM XV.

To construct an equilateral triangle on a given finite straight line.

Let AB be the given line, and from one extremity, A, as a center, with a radius equal to AB, describe an arc. From the other extremity, B, with the same radius, describe another arc. From C, where these two arcs intersect, draw CA and CB; ABC will be the triangle required.

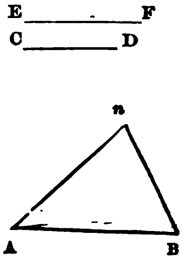


The construction is a sufficient demonstration. Or (ax. 1).

PROBLEM XVI.

To construct a triangle having its three sides equal to three given lines, any two of which shall be greater than the third.

Let AB, CD, and EF represent the three lines. Take any one of them, as AB, to be one side of the triangle. From A as the center, with a radius equal to EF, describe an arc; and from B as a center, with a radius equal to CD, describe another arc, cutting the former in n. Join An and Bn, and AnB will be the △ required.

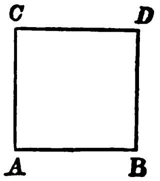


Proof, (ax. 1).

PROBLEM XVII.

To describe a square on a given line.

Let AB be the given line, and from the extremities, A and B, draw AC and BD perpendicular to AB. (Problem 3.)



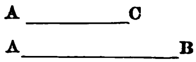
From A, as a center, with AB as radius, strike an arc across the perpendicular at C; and from C, draw CD parallel to AB; $ACDB$ is the square required.

Proof, (th. 26, b. 1).

PROBLEM XVIII.

To construct a rectangle, or a parallelogram, whose adjacent sides are equal to two given lines.

Let AB and AC be the two given lines. From the extremities of one line, draw perpendiculars to that line, as in the last problem; and from these perpendiculars, cut off portions equal to the other line; and by a parallel, complete the figure.

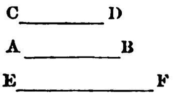


When the figure is to be a parallelogram, with oblique angles, describe the angles by problem 5.

Proof, (th. 26, b. 1).

PROBLEM XIX.

To describe a rectangle that shall be equivalent to a given square and have a side equal to a given line.



Let AB be a side of the given square, and CD one side of the required rectangle.

Find the third proportional, EF, to CD and AB (problem 8). Then we shall have,

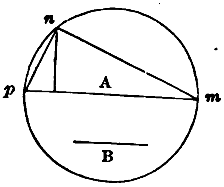
$$CD : AB :: AB : EF$$

Construct a rectangle with the two given lines, CD and EF (problem 18), and it will be equivalent to the given square, (th. 3, b. 2).

PROBLEM XX.

To construct a square that shall be equivalent to the difference of two given squares.

Let A represent a side of the greater of two given squares, and B a side of the lesser square.

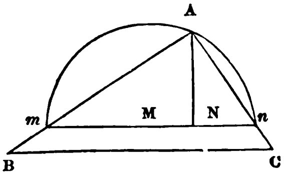


On A, as a diameter, describe a semicircle, and from one extremity, p, as a center, with a radius equal to B, describe an arc, n, and, from the point where it cuts the circumference, draw mn and np; mn is the side of a square, which, when constructed, (problem 17), will be equivalent to the difference of the two given squares.

Proof, (th. 9, b. 3, and 36, b. 1).

PROBLEM XXI.

To construct a square, that shall be to a given square, as a line M *to a line* N.

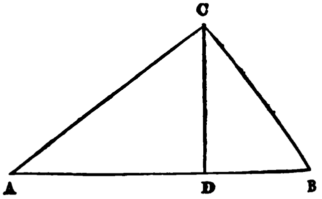


Place M and N in a line, and on the sum describe a semicircle. From the point where they meet, draw a perpendicular to meet the circumference in A. Join Am and An, and produce them indefinitely.

On An or An produced, take AC=to the side of the given square; and from C draw BC parallel to mn; AB is a side of the required square.

PROBLEM XXII.

The angles and one side of a triangle being given, to find by construction the other sides.



Draw the given side. From the ends of it lay off the angles that are adjacent to the given side; extend the other sides until they intersect. The distances from the point of intersection to the extremities of the given line applied to the same scale of equal parts, from which the given line was taken, will give the other sides.

Example.

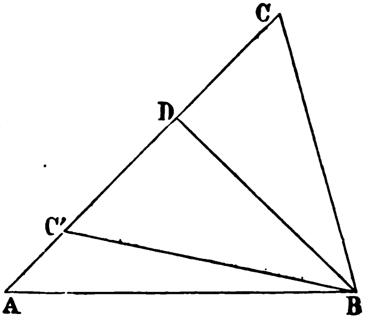
One side of a triangle is 24 chains, and the adjacent angles are 37° and 64°. Required the other sides.

Take from the scale of equal parts 24 chains, calling 10 chains an inch, and draw the line AB. At A construct an angle of 37°, and at B an angle of 64°. Draw the lines meeting at C. Then AC applied to the scale will give 22, and BC applied will give 14.7 chains. If the altitude of the triangle is wanted, draw from C a perpendicular to AB, by problem 4. Then apply CD to the scale, and it will give 13.2 chains for the altitude.

PROBLEM XXIII.

Two sides and an opposite angle of a triangle being given, to find the remaining side and the other angles by construction.

Draw one of the given sides; from one end of it, lay off the given angle; and extend a line indefinitely, from which



the required side is to be taken. From the other end of the first side, with the remaining given side for radius, describe an arc cutting the indefinite line. The points of intersection will determine the required triangle. If the radius is such that the arc touches the indefinite line, as at *D*, the triangle will be right angled. If the arc does not intersect, the problem is impossible.

Example.

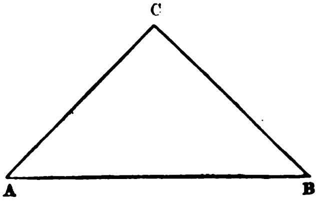
Two sides of a triangle are 21 and 25 chains and the angle opposite 21 is 46°. Required the third side.

From the scale of equal parts, calling 10 chains an inch, take 25 chains for AB, the base of the triangle. At A construct an angle of 46°, and draw the indefinite line AC.

Then take from the same scale of equal parts 21 chains, and with one foot of the dividers at B, and with 21 as radius, describe an arc cutting the indefinite line in C and C'; and AC or AC' will be the required side. These applied to the scale will give $AC=28.2$ chains, or $AC'=6.4$ chains. This example admits of two answers.

PROBLEM XXIV.

Given two sides and the included angle to construct the triangle, and to measure the third side.



Let the given sides be 23 and 28 chains, and the included angle 51°.

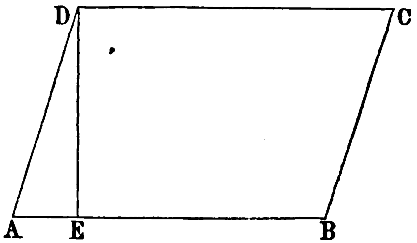
Take 28 from the scale of equal parts, and draw the line AB equal that length. At A construct an angle of 51°, with the line of chords, or with the protractor; draw the line AC, and make it 23 from the scale, and join BC; then apply BC to the same scale, and it will be found equal to 22.2 chains.

The angles can also be measured by applying the protractor with the center at the angle to be measured.

Or, from the line of chords take 60 as radius, and describe a circle to intersect the sides that include the angle to be measured, the centre being at the angle. The distance between the points of intersection, applied to the line of chords, will give the angle in degrees.

PROBLEM XXV.

To measure a parallelogram with a scale of equal parts.



Let $ABCD$ be a parallelogram. Take the base AB, and with the dividers apply it to a scale of equal parts, and this will give the relative length of AB.

Then from one of the angles as at D, draw a perpendicular to AB by problem 4, as DE; then apply DE to the same scale of equal parts, and this will give the length of DE relatively. If $ABCD$ is constructed on a scale of 10 chains to the inch, then will $AB = 25$ chains, and $DE = 13.2$ chains.

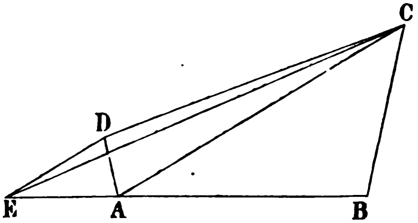
These are sufficient to determine the area of the parallelogram.

PROBLEM XXVI.

To measure a trapezium.

Let $ABCD$ be any trapezium; draw the diagonal AC. From D draw DE parallel to AC, and join EC; then the triangle EBC will be equivalent to the trapezium $ABCD$. Since DE is parallel to AC, the triangle ADC is equivalent to *AEC;* to each add the triangle *ABC*, then will result *ABCD*=*EBC*.

Now apply *EB* to a scale of equal parts, and draw a perpendicular from *C* to *AB*, and apply that to the same scale.

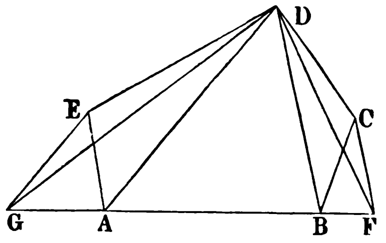


If *ABCD* is drawn to a scale of 10 chains to the inch, then will $AB = 20$ chains, $EB = 34.5$ chains, and the altitude of the triangle *EBC* will be 13.2 chains. These lines will determine the measure of the triangle, and consequently of the trapezium.

PROBLEM XXVII.

To measure instrumentally a figure of five sides.

Let *ABCDE* be any figure of five sides; draw the diagonals *AD* and *BD;* then draw *EG* parallel to *AD*, and *CF* parallel to *BD;* then join *GD* and *FD;* then will the triangle *GFD* be equivalent to the figure *ABCDE*. Since *EG* is parallel to *AD*, the triangle *AED*=*AGD;* and since *CF* is parallel to *DB*, we have *BCD*=*BFD;* whence it follows that



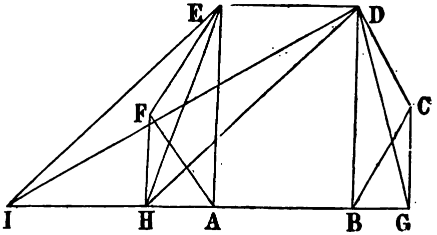
$$GFD = ABCDE.$$

Then apply *GF* to the scale of equal parts, and if $AB =$ 20 chains, then will $GF = 32$ chains, and the perpendicular from *D* on *AB* will be 17.4 chains, which is the altitude of the triangle.

These lines determine the measure of the figure *ABCDE*.

PROBLEM XXVIII.

To measure any figure of six sides.



Draw the diagonals *EA* and *DB*; draw *FH* parallel to *EA*, and *CG* parallel to *DB*; then join *EH* and *DG*. Draw the diagonal *DH*, and draw *EI* parallel to *DH* and join *DI*, and *IGD* will be equivalent to *ABCDEF*. Since *FH* is parallel to *AE*, we have *AFE*=*AHE*; and since *CG* is parallel to *DB*, we have *BCD*=*BGD*; and also since *EI* is parallel to *DH*, we have *HED* = *HID*; whence it follows that *IGD* = *ABCDEF*.

Now, if we apply *IG* to a scale of equal parts, we shall get its length, and we find that if *AB* is 12 chains, then *IG* = 33.5 chains; we also find that a perpendicular from *D* to the base *AB* will equal 17.3 chains.

Wherefore the measure of *ABCDEF* is determined.

CHAPTER II.

LOGARITHMS AND TRIGONOMETRY.

MENSURATION, Surveying and Navigation are practical applications of geometry and trigonometry.

The geometrical principles involved can be best acquired by the study of that science in its full extent, as laid down in the common elementary text-books.

The principles of trigonometry required do not, however, include all those given in the text books upon that subject, or all that are important to the general student.

It is therefore considered best to give a brief *resumé* of those theorems practically involved in the subsequent matter of the work, for the purpose of refreshing the recollection of those who have already pursued the study, and as a condensed course for those desiring to fit themselves immediately for practice.

It is intended to include in this chapter only those matters intimately connected with practice. For a fuller discussion of both Logarithms and Trigonometry, the student is referred to Robinson's New Geometry and Trigonometry.

For greater ease in the solution of almost all the practical problems of Mensuration, Surveying and Navigation, a clear knowledge of Logarithms is essential; and the student should make himself perfectly familiar with their use.

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* The student who is acquainted with Logarithms and Trigonometry, and desires to take up Surveying, may omit this entire chapter if he chooses, and also so much of Mensuration in the following chapter as may be deemed advisable.

SECTION I.

OF LOGARITHMS.

The **Logarithm** of any quantity is an exponent expressing the power to which a constant or fixed quantity must be raised to equal the given quantity. Thus, in the equations

$$a^n = x,$$
$$a^m = y,$$

where a is a constant, n is the logarithm of x, and m is the logarithm of y.

Likewise in the numeral equations,

$$10^2 = 100,$$
$$10^3 = 1,000,$$

where 10 is the constant, 2 is the logarithm of 100, and 3 is the logarithm of 1,000.

Thus logarithms are *signs*, showing the relation which different quantities bear to one assumed or constant quantity.

In many operations it is found far more convenient to compare quantities by their relations than absolutely, and logarithms have thus become of vast utility to the practical mathematician.

A **System of Logarithms** comprises the logarithms of numbers derived from any assumed constant quantity.

This assumed constant is called the base of the system, and any number being taken as the base, a system of logarithms may be formed from it.

The main qualification is that of convenience. Two systems have been prepared, called from the projectors, Napier's and Briggs' logarithms. The one in common use is the Briggs' system, which has for its base the number 10.

In writing the logarithm of a number or letter, the contraction "log." is used. Thus, in the equation $a^n=x$, we have

$$n = \log.\ x.$$

In the Briggs system, where 10 is the base, it follows from the definition of a logarithm, that as $10^5=100,000$, $5=\log. 100,000$. In like manner we have

$$
\begin{array}{rrlr}
10^4 = & 10,000, & \text{whence} & 4 = \log. 10,000; \\
10^3 = & 1,000, & \text{"} & 3 = \log. 1,000; \\
10^2 = & 100, & \text{"} & 2 = \log. 100; \\
10^1 = & 10, & \text{"} & 1 = \log. 10; \\
10^0 = & 1, & \text{"} & 0 = \log. 1; \\
10^{-1} = & .1, & \text{"} & -1 = \log. .1; \\
10^{-2} = & .01, & \text{"} & -2 = \log. .01; \\
10^{-3} = & .001, & \text{"} & -3 = \log. .001;
\end{array}
$$

From an examination of the above numbers and their logarithms, it is seen that as the logarithm of 1 is 0, and the logarithm of 10 is 1,—the log. of any number between 1 and 10 will be greater than 0, and less than 1; that is, it will be a decimal. So also the logarithm of any number between 10 and 100 will be greater than 1 and less than 2: that is, it will be 1 and a decimal. Returning to $0=\log. 1$, we find that -1 is the log. of .1. Now any number between 1 and .1—that is, any *decimal* greater than .1—will have a logarithm greater than -1, but still negative or less than 0; that is, the logarithm will be -1 plus a decimal. So taking $-1=\log. .1$, and $-2=\log. .01$, any number between .1 and .01 will have for its logarithm a number less than -1, and greater than -2; or, -2 plus a decimal.

It will also be noticed that while the quantities increase and decrease by multiplying or dividing by 10, the logarithms increase and decrease by the addition or subtraction of 1, which accords with the algebraic rule, that adding exponents multiplies, and subtracting exponents divides the quantities themselves. For example,

$$
\begin{aligned}
10^1 &= 10, \\
10^2 &= 100.
\end{aligned}
$$

Multiplying, $10^{1+2} = 10^3 = 1,000.$

Thus increasing or decreasing any number in a tenfold ratio, will increase or decrease the logarithm by unity.

From the foregoing are deduced the following:

1. All powers of 10 and their reciprocals will have for logarithms *integral* numbers.

2. All other numbers will have for logarithms an integer together with a decimal, or simply a decimal.

3. Increasing or decreasing numbers in a tenfold ratio, increases or decreases only the integer, without affecting the decimal of the logarithm.

4. The integer of the logarithm depends entirely upon the local value of the number, or the position which the figures occupy with reference to the decimal point.

5. The integer of the logarithm of any number greater than unity will always be one less than the number of integral places which that number contains.

6. The integer of any number less than unity will always be equal to the number of places the first significant figure is removed from the decimal point.

7. The integer belonging to the logarithm of a decimal, will always have the minus sign.

8. The decimal, however connected with this *negative* integer, will be *positive*.

From the integer of a logarithm, the position of the first significant figure with reference to unity may always be determined.

REMARK.—To make clear the distinction between a logarithm *to be subtracted*, and one simply having a negative integer, the minus sign in the latter case is placed *above* the integer, not before it, as in the other case.

The integral portion of a logarithm is called its *characteristic* or *index*.

LOGARITHMIC TABLE.

It is now necessary to explain the table of logarithms and its use.

In the table connected with this work (as is the usual form), the logarithms of numbers from 1 to 100 are given entire, with both index and decimal. Thus the logarithm of any number within those limits may be taken at once complete from the table.

For numbers above 100 to 10,000, only the decimals are given; for, as the index depends entirely upon the position of the highest significant figure, it may be readily supplied. Thus, the decimal of the logarithm of 7956, as found in the table, is .900695; and since the number has four integral places, we have only to prefix the integer 3, and we have

$$3.900695 = \log. 7956.$$

Should we divide the number successively by 10, we must subtract 1 each time from the logarithm; hence

$$\begin{aligned} 2.900695 &= \log. 795.6, \\ 1.900695 &= \text{``} \quad 79.56, \\ 0.900695 &= \text{``} \quad 7.956. \end{aligned}$$

In the table, the decimal part of the logarithms of all these numbers is the same, the significant figures alone being considered. The index gives the position of the figures with reference to unity.

1. *To find the logarithm of any number from the table.*

The logarithm of a number containing three figures will be found with great ease.

The figures are arranged in a column, headed N., at the left of the page; in the second column, headed 0, opposite the proper figures in the first column, will be found the decimal of the logarithm.

If the number contain four figures, the first three will be found as before, the fourth figure will be found at the head of one of the columns, commencing with 0 at the left, and passing to 9 at the right.

In the column headed by the fourth figure, and opposite the first three in the left hand column, will be found the decimal of the logarithm.

It is to be noted that, as the first two terms of the decimal are the same for several successive numbers, they are only given in the column at the left, headed 0, and must be prefixed to the four figures given in the other columns.

Also, when dots are found in place of figures, the two leading decimals must be taken from the line *below*, and ciphers used in place of the dots. For illustration take the following examples.

1. To find the logarithm of the number 154.

Turning to page 4 of the table of logarithms, in the column at the left headed N., we find the number 154; opposite, in the column headed 0, we find 7521, the last four figures of the decimal. Two lines above, we find 18 the first two figures to be prefixed. We thus have for the decimal of the logarithm, .187521. Since the number has three integral places, the index will be 2. Hence,

Log. 154 = 2.187521, *Ans.*

2. To find the logarithm of the number 3725.

We find 372 at the side of the table, and in the column marked 5 at the top, and opposite 372, we find .571126, for the decimal part of the logarithm. Hence,

Log. 3725 = 3.571126, *Ans.*

3. To find the logarithm of the number 834785.

This number is so large that we cannot find it in the table, but we can find the numbers 8347 and 8348. The logarithms of these numbers are the same as the logarithms of the numbers 834700 and 834800, except the indices.

	834700,	log. 5.921530
	834800,	log. 5.921582
Differences,	100	52

The given number is between two assumed numbers, and its logarithm must lie between the logarithms of those assumed numbers. Now the differences between the logarithms are *very nearly* proportional to the differences between the numbers; so nearly that, where the numbers are not too widely separated, for all practical purposes the proportion may be considered exact. We may, therefore, form the proportion,

Difference between assumed numbers:
Difference between lesser assumed and the given number::
Difference between log.'s of assumed numbers:
Difference between log.'s of lesser and the given number.
Using the differences found above,

$$100 : 85 :: 52 : 44.2,$$

$$\text{Or,} \quad 1 : .85 :: 52 : 44.2.$$

In the last proportion, the difference between the lesser assumed and the given number, considered as a decimal, and multiplied by the difference between the logarithms of the two assumed numbers gives the difference between the logarithm of that lesser number and the logarithm of the given number. This difference added to the logarithm of the lesser number, as a correction, gives the required logarithm.

Thus, Log. 834700 = 5.921530
Difference or correction, = 44.2
Log. 834785 = 5.921574.2.

The difference between the logarithms of the two assumed numbers, is called the *Tabular Difference;* and for convenience, this is given in the column headed 4, and in a line by itself. For example, on page 4, under column 4, in the sixth line, we find 281, which is the Tabular Difference for the logarithms immediately preceding and following.

From these illustrations we derive, for finding from the table the logarithm of a number consisting of more than four places of figures, the following

RULE.

Take from the table the logarithm of the number expressed by the four superior figures; this, with the proper index, is the approximate logarithm. Multiply the number expressed by the remaining figures of the number, regarded as a decimal, by the tabular difference, and the product will be the correction to be added to the approximate logarithm to obtain the true logarithm.

EXAMPLES.

1. What is the log. of 357.32514?

The log. of 357.3 is............ 2.553033
No. not included, .2514
Tabular difference, 122
Prod., 30.6708; correction, 31
log. sought, 2.553064
The log. of 35732.514 is 4.553064
" .035732514 "......—2.553064.

2. What is the log. of 7912532?

Approximate log.,........ 6.898286
.532 × 55 = correction,........ 29
True log. = 6.898315, *Ans.*

2. *A logarithm being given, to find its corresponding number.*

For example, what number corresponds to the log. 6.898315?

The index 6 shows that the entire part of the number must contain seven places of figures. With the decimal part, .898315, of the log., we turn to the table, and find the next less decimal part to be .898286, which corresponds to the superior places, 7912.

The difference between the given log. and the one next less is 29. This we divide by the tabular difference, 55, because we are working the converse of the preceding problem Thus,

$$29 \div 55 = .52727+.$$

Place the quotient to the right of the four figures before found, and we shall have 7912527.27 for the number sought.

This example was taken from the preceding case, and the number found should have been 7912532; and so it would have been, had we used the true difference, 29.26, in place of 29.

When the numbers are large, as in this example, the result is liable to a small error, to avoid which the logarithms should contain a great number of decimal places; but the logarithms in our table contain a sufficient number of decimal places for most practical purposes.

Hence, for finding the number corresponding to any given logarithm, we have the following

RULE.

Look in the table for the decimal part of the given logarithm, and if not found take the decimal next less, and take out the four corresponding figures.

Take the difference between the given logarithm and the next less in the table; divide that difference by the tabular difference, and write the quotient on the right of the four superior figures, and the result is the number sought.

Point off the whole number required by the given index.

EXAMPLES.

1. Given the logarithm 3.743210, to find its corresponding number true to three places of decimals. *Ans.* 5536.177.

2. Given the logarithm 2.633356, to find its corresponding number true to two places of decimals. *Ans.* 429.89.

3. Given the logarithm -3.291746, to find its corresponding number. *Ans.* .0019577.

4. What number corresponds to the log. 3.233568?
Ans. 1712.25.

5. What is the number of which 1.532708 is the log.?
Ans. 34.0963.

6. Find the number whose log. is 1.067889.
Ans. 11.692.

APPLICATIONS OF LOGARITHMS.

From the definitions and principles heretofore given, the rules for applying logarithms may be readily deduced.

To multiply by logarithms.

RULE.

Add the logarithms of multiplicand and multiplier; the sum will be the logarithm of the product. From the table find the number corresponding to this logarithm, and it will be the product required.

EXAMPLES.

1. What is the product of 7896 and 9872?

Log. 7896 = 3.897407
" 9872 = 3.994405
Log. of product = 7.891812
Approximate log. = .891760 = log. 7794
Difference = 52
Tabular difference = 56.
Correction $\frac{52}{56}$ = .928571.
Therefore, 7.891812 = log. 77949285.71.

Ans. 77949285.71 nearly.

Remark.—As the logarithms are not exact, the correction carried out beyond two places becomes inaccurate;—hence the result in the preceding example is incorrect, though the error is slight. When great accuracy is required, and large numbers are used, the logarithms must be more accurately calculated, and carried out to more decimal places, or their use dispensed with.

2. Required the product of 976.24 and 9.76.
Ans. 9528.11.

3. Required the continued product of 8.761, 3.426, 7.97, and 5.63. *Ans.* 1346.814+.

4. Required the continued product of 9.913, 5.864, 11.23, 4.51, and 7.62.

To divide by logarithms.

As before, logarithms are considered as exponents. By algebraic rule for division, the difference between exponents of dividend and divisor will be the exponent of the quotient. Hence the following.

RULE.

Subtract the logarithm of the divisor, from that of the dividend; the result will be the logarithm of the quotient. Find the number corresponding to this from the table, and it will be the quotient required.

EXAMPLES.

1. Divide 8967.42 by 32.1.

Log. 8967.42 = 3.952668
" 32.1 = 1.506505

Log. of quotient = 2.446163
Approximate log. = 2.446071 = log. 2793

Difference = 92
Tabular difference = 155
Correction = 92 $\div$ 155 = .59
Hence, 2.446163 = log. 279.359

Ans. 279.359.

2. What is the quotient of 739.86 divided by 23.12?
Ans.

3. What is the value of the fraction $\frac{976}{1277}$ expressed decimally? *Ans.*

4. What is the quotient of 36278 divided by 97?

To solve proportions by logarithms.

RULE.

Add the logarithms of the means, and subtract that of the given extreme; or add the logarithms of the extremes, and subtract that of the given mean. The result in either case will be the logarithm of the required term, which will be found by taking from the table the number corresponding to the logarithmic result.

The reason for this rule is evident from the rule for solving proportions by multiplication and division, and the rules before given for the use of logarithms.

EXAMPLES.

1. Required the fourth term in the proportion

$$97 : 126 = 321 : ?$$

$$\begin{array}{rl} \text{Log. } 126 & = 2.100371 \\ \text{Log. } 321 & = \underline{2.506505} \\ & 4.606876 \\ \text{Subtract log. } 97 & = \underline{1.986772} \\ \text{Log. extreme} & = 2.620104 \\ 2.620104 & = \text{log. } 416.97. \ \textit{Ans.} \end{array}$$

2. Required the fourth term in the proportion
$32.71 : 142.81 = 76.4 : ?$ *Ans.* 333.56.

3. Required the third term in the proportion
$43.24 : 217.16 = ? : 137.39.$ *Ans.* 27.35.

the solution of proportions by logarithms, and in other where division is performed, the Arithmetical Complet of the logarithm of the divisor is often used.

ıe **Arithmetical Complement** of any number is the reıder after subtracting that number from a unit of the next er order.

obtain the complement, ***subtract each figure, commencing e left, from* 9, *save that upon the right, which subtract n*** 10.

solve a proportion with the use of the arithmetical comıent, we have the following

RULE.

irst obtain the complement of the logarithm of the term to sed as a divisor; to this add the logarithms of the two s to be multiplied, subtract 10 *from the result, and there remain the logarithm of the term required.*

apply to simple division this method, add the complet of the logarithm of the divisor to the logarithm of the lend, and diminish the result by 10, or by 100 should the rithm of the divisor exceed 10.

hat the use of the complement does not change the result ident from the following equation.

$$((10-a)+b+c)-10=b+c-a,$$

re a=log. of divisor, b and c=log.'s of factors of the dend.

EXAMPLES.

. Find the unknown term in the proportion

$$376 : x = 497 : 1891$$

$$\begin{aligned} \text{Co. log. } 497 &= 7.303644 \\ \text{log. } 376 &= 2.575188 \\ \text{log. } 1891 &= \underline{3.276692} \\ \text{Sum less } 10 = \text{log. } x &= 3.155524 \end{aligned}$$

Sum less 10 = log. x = 3.155524
App. log. = log. 1430 = .155336

Difference, = 188
Tab. Diff. = 304. 188 ÷ 304 = 62 correction.
Hence, 3.155524 = log. 1430.62 Ans. = 1430.62.

2. Required the unknown term in the proportion

$$3796 : 9843 = 4265 : x.$$

3. Required the unknown term in the proportion

$$472 : 976 = x : 2345.$$

4. Required the unknown term in the proportion

$$7.693 : 11 = 9.679 : x.$$

To perform involution by logarithms.

RULE.

To involve a quantity to any power, multiply its logarithm by the index of the power; the product will be the logarithm of the power required.

For if $10^2 = 100$, when $2 = \log. 100$, raising both sides to second power, $10^4 = 100^2 = 10000$. In this equation $4 = 2 \times 2 = \log. 10000$; that is, the log. of 100, multiplied by the index 2, gives the log. of the square of 100.

EXAMPLES.

1. Required the cube of 32.

Log. 32 = 1.505150
Multiply by 3

Log. of power = 4.515450
App. log. = 515344 = log. 3276

106 ÷ 132 = 737

4.515450 = log. 32767.37

Ans. by logarithms, 32767.37
" " multiplication, 32768.

The error of .63 in the first result is caused by the inaccuracy of the logarithms, which generally affects results beyond the sixth or seventh place from the left.

2. Required the fourth power of 2.763.

3. Required the ninth power of .0176.

NOTE.—The *decimal* of every logarithm is *positive*.

To perform evolution by logarithms.

RULE.

Divide the logarithm of the quantity by the index denoting the root required; the result will be the logarithm of the root desired.

This rule would follow like the preceding from the algebraic rule for the same operation.

EXAMPLES.

1. Required the cube root of 7896.34.

$$\begin{array}{rcl} \text{Log. of } 7896.34 & = & 3.897426 \\ \text{Divided by } 3 & = & 1.299142 \\ 1.299142 & = & \text{log. } 19.913, \textit{ Ans.} \end{array}$$

2. Required the fifth root of 9764.

Ans. 6.279.

3. Required the cube root of 89763.

Ans. 44.774.

4. Required the sixth root of 97643.89.

SECTION II.

OF PLANE TRIGONOMETRY.

NOTE.—References to geometry refer to Robinson's New Geometry and Trigonometry; those to plane and spherical trigonometry refer to the sections on those subjects which follow. *R. A.* and *O. A.* Spher. Trig. are used to distinguish propositions, concerning right-angled and oblique-angled triangles. When the numbers alone of propositions or proportions are given, they refer to those in the same section.

Trigonometry, in its literal and restricted sense, has for its object the measurement of triangles. When it treats of plane triangles it is called *Plane Trigonometry.* In a more enlarged sense, trigonometry is the science which investigates the relations of all possible arcs of the circumference of a circle to certain straight lines, termed *trigonometrical lines* or *circular functions*, connected with and dependent on such arcs, and the relations of these trigonometrical lines to each other.

The measure of an angle is the arc of a circle intercepted between the two lines which form the angle—the center of the arc always being at the point where the two lines meet.

The arc is measured by *degrees*, *minutes*, and *seconds;* there being 360 degrees to the whole circle, 60 minutes in one degree, and 60 seconds in one minute. Degrees, minutes, and seconds, are designated by °, ′, ″; thus, 27° 14′ 21″, is read 27 degrees 14 minutes 21 seconds.

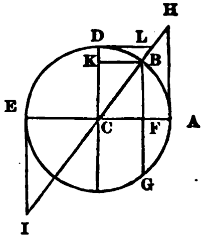
The circumferences of all circles contain the same number of degrees, but the greater the radius, the greater is the absolute length of a degree. The circumference of a carriage wheel, the circumference of the earth, or the still greater and indefinite circumference of the heavens, has the same number of degrees; yet the same number of degrees in each and every circumference is the measure of precisely the same angle.

DEFINITIONS.

1. The **Complement** of an arc is 90° minus the arc.

2. The **Supplement** of an arc is 180° minus the arc.

3. The **Sine** of an angle, or of an arc, is a line drawn from one end of an arc, perpendicular to a diameter drawn through the other end. Thus, BF is the sine of the arc AB, *and also* of the arc BDE. BK is the sine of the arc BD.



4. The **Cosine** of an arc is the perpendicular distance from the center of the circle to the sine of the arc; or, it is the same in magnitude as the sine of the complement of the arc. Thus, CF is the cosine of the arc AB; but $CF = KB$, is the sine of BD.

5. The **Tangent** of an arc is a line touching the circle in one extremity of the arc, and continued from thence, to meet a line drawn through the center and the other extremity. Thus, AH is the tangent to the arc AB, and DL is the tangent of the arc DB.

6. The **Cotangent** of an arc is the tangent of the complement of the arc. Thus, DL, which is the tangent of the arc DB, is the cotangent of the arc AB.

REMARK.—The *co* is but a contraction of the word complement.

7. The **Secant** of an arc is a line drawn from the center of the circle to the extremity of the tangent. Thus, CH is the secant of the arc AB, or of its supplement BDE.

8. The **Cosecant** of an arc is the secant of the complement. Thus, CL, the secant of BD, is the cosecant of AB.

9. The **Versed Sine** of an arc is the distance from the extremity of the arc to the foot of the sine. Thus, AF is the versed sine of the arc AB, and DK is the versed sine of the arc DB.

For the sake of brevity, these technical terms are contracted thus: for sine AB, we write *sin.* AB; for cosine

AB, we write *cos. AB;* for tangent *AB*, we write *tan. AB*, etc.

From the preceding definitions we deduce the following obvious consequences:

1st. That when the arc *AB* becomes insensibly small, or zero, its sine, tangent, and versed sine are also nothing, and its secant and cosine are each equal to radius.

2d. The sine and versed sine of a quadrant are each equal to the radius; its cosine is zero, and its secant and tangent are infinite.

3d. The chord of an arc is twice the sine of one half the arc. Thus, the chord *BG* is double the sine *BF*.

4th. The versed sine is equal to the difference between the radius and the cosine.

5th. The sine and cosine of any arc form the two sides of a right-angled triangle, which has a radius for its hypotenuse. Thus, *CF* and *FB* are the two sides of the right-angled triangle *CFB*.

Also, the radius and tangent always form the two sides of a right-angled triangle, which has the secant of the arc for its hypotenuse. This we observe from the right-angled triangle *CAH*.

To express these relations analytically, we write

$$\text{sin.}^2 + \text{cos.}^2 = R^2 \qquad (1)$$

$$R^2 + \text{tan.}^2 = \text{sec.}^2 \qquad (2)$$

From the two equiangular triangles *CFB*, *CAH*, we have

$$CF : FB = CA : AH.$$

That is,

$$\text{cos.} : \text{sin.} = R : \text{tan.}; \text{ whence, tan.} = \frac{R.\text{sin.}}{\text{cos.}} \qquad (3)$$

Also,

$$CF : CB = CA : CH.$$

That is,

$$\text{cos.} : R = R : \text{sec.}; \text{ whence, cos. sec.} = R^2. \qquad (4)$$

The two equiangular triangles, CAH and CDL, give

$$CA : AH = DL : DC.$$

That is,

$$R : \text{tan.} = \text{cot.} : R; \text{ whence, tan. cot.} = R^2. \qquad (5)$$

Also,

$$CF : FB = DL : DC.$$

That is,

$$\text{cos.} : \text{sin.} = \text{cot.} : R; \text{ whence, cos. } R = \text{sin. cot.} \qquad (6)$$

From equations (4) and (5), we have

$$\text{cos. sec.} = \text{tan. cot.} \qquad (7)$$

Or,

$$\text{cos.} : \text{tan.} = \text{cot.} : \text{sec.}$$

We also have

$$\text{ver. sin.} = R - \text{cos.} \qquad (8)$$

The *ratios* between the various trigonometrical lines are always the same for arcs of the same number of degrees, whatever be the length of the radius; and we may, therefore, assume radius of any length to suit our convenience. The preceding equations will be more concise, and more readily applied, by making the radius equal unity. This supposition being made, we have, for equations 1 to 6, inclusive,

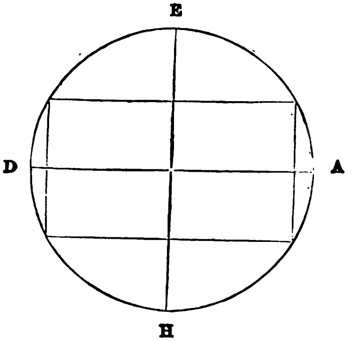
$$\text{sin.}^2 + \text{cos.}^2 = 1. \qquad (1)$$

$$1 + \text{tan.}^2 = \text{sec.}^2 \qquad (2)$$

$$\text{tan.} = \frac{\text{sin.}}{\text{cos.}} \quad (3) \qquad \text{cos.} = \frac{1}{\text{sec.}} \quad (4)$$

$$\text{tan.} = \frac{1}{\text{cot.}} \quad (5) \qquad \text{cos.} = \text{sin. cot.} \quad (6)$$

Let the circumference, $AEDH$, be divided into four equal parts by the diameters, AD and EH, the one horizontal and the other vertical. These equal parts are called *quadrants*, and they may be distinguished as the *first*, *second*, *third*, and *fourth* quadrants.



The center of the circle is taken as the origin of distances, or the zero point, and the different directions in which distances are estimated from this point are indicated by the signs + and —. If those from C to the right be marked +, those from C to the left must be marked —; and if distances from C upwards be considered plus, those from C downwards must be considered minus.

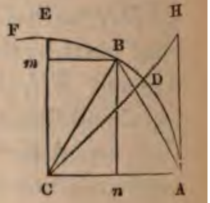
If one extremity of a varying arc be constantly at A, and the other extremity fall successively in each of the several quadrants, we may readily determine, by the above rule, the algebraic signs of the sines and cosines of all arcs from 0° to 360°. Now, since all other trigonometrical lines can be expressed in terms of the sine and cosine, it follows that the algebraic signs of all the circular functions result from those of the sine and cosine.

We shall thus find for arcs terminating in the

	sin.	cos.	tan.	cot.	sec.	cosec.	vers.
1st quadrant,	+	+	+	+	+	+	+
2d "	+	—	—	—	—	+	+
3d "	—	—	+	+	—	—	+
4th "	—	+	—	—	+	—	+

PROPOSITION I.

The chord of 60° *and the tangent of* 45° *are each equal to radius; the sine of* 30°, *the versed sine of* 60°, *and the cosine of* 60° *are each equal to one half the radius.*



With C as a center, and CA as a radius, describe the arc ABF, and from A lay off the arcs $AD=45°$, $AB=60°$, and $AE=90°$; then is $EB=30°$.

1st. The side of a regular inscribed hexagon is the radius of the circle (Geom. Prob. 28, B. IV), and as the arc subtended by each side of the hexagon contains 60°, we have the chord of of 60° equal to the radius.

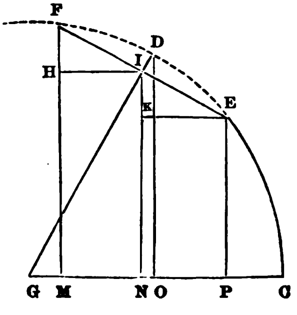
2d. The triangle CAH is right-angled at A, and the angle C is equal to 45°, being measured by the arc AD; hence the angle at H is also equal to 45°, and the triangle is isosceles. Therefore $AH = CA =$ radius of the circle.

3d. The triangle ABC is isosceles, and Bn is a perpendicular from the vertex upon the base; hence $An = nC = Bm$. But Bm is the sine of the arc BE, Cn is the cosine of the arc AB, and An is the versed sine of the same arc, and each is equal to one half the radius.

Hence the proposition; *the chord of* 60°, *etc.*

PROPOSITION II.

Given, the sine and the cosine of two arcs, to find the sine and the cosine of the sum and of the difference of the same arcs expressed by the sines and cosines of the separate arcs.



Let G be the center of the circle, CD the greater arc, and DF the less, and denote these arcs by a and b respectively.

Draw the radius GD; make the arc DE equal to the arc DF, and draw the chord EF. From F and E, the extremities, and I, the middle point of the chord, let fall the perpendiculars FM, EP, and IN, on the radius GC. Also draw DO, the sine of the arc CD, and let fall the perpendiculars IH on FM, and EK on IN.

Now, by the definition of sines and cosines, $DO = \sin.a$; $GO = \cos.a$; $FI = \sin.b$; $GI = \cos.b$. We are to find

$$FM = \sin.(a+b);\ GM = \cos.(a+b);$$
$$EP = \sin.(a-b);\ GP = \cos.(a-b).$$

Because IN is parallel to DO, the two △'s, GDO, GIN, are equiangular and similar. Also, the △ FHI is similar to the △ GIN; for the angles, FIG and HIN, are right angles;

from these two equals, taking away the common angle HIG, we have the angle $FIH =$ the angle GIN. The angles at H and N are right angles; therefore, the $\triangle$'s FHI, GIN, and GDO, are equiangular and similar; and the side HI is homologous to IN and DO.

Again, as $FI = IE$, and IK is parallel to FM,

$$FH = IK, \text{ and } HI = KE.$$

By similar triangles we have

$$GD : DO = GI : IN.$$

That is, $R : \sin.a = \cos.b : IN$; $IN = \dfrac{\sin.a \cos.b}{R}$. (1)

Also, $GD : GO = FI : FH.$

That is, $R : \cos.a = \sin.b : HF$; or, $FH = \dfrac{\cos.a \sin.b}{R}$. (2)

Also, $GD : GO = GI : GN.$

That is, $R : \cos.a = \cos.b : GN$; or $GN = \dfrac{\cos.a \cos.b}{R}$. (3)

Also, $GD : DO = FI : IH.$

That is, $R : \sin.a = \sin.b : IH$; or, $IH = \dfrac{\sin.a \sin.b}{R}$. (4)

By adding the first and second of these equations, we have

$$IN + FH = FM = \sin.(a+b).$$

That is, $\sin.(a+b) = \dfrac{\sin.a \cos.b + \cos.a \sin.b}{R}$.

By subtracting the second from the first, since

$IN - FH = IN - IK = EP$, we have

$$\sin.(a-b) = \frac{\sin.a \cos.b - \cos.a \sin.b}{R}.$$

By subtracting the fourth from the third, we have

$GN - IH = GM = \cos.(a+b)$ for the first member.

Hence, $\cos.(a+b) = \dfrac{\cos.a \cos.b - \sin.a \sin.b}{R}$. (5)

By adding the third and fourth, we have

$$GN + IH = GN + NP = GP = \cos.(a-b).$$

Hence, $\cos.(a-b)=\dfrac{\cos.a\ \cos.b+\sin.a\ \sin.b}{R}$. (6)

Collecting these four expressions, and considering the radius unity, we have

$$(A)\begin{cases}\sin.(a+b)=\sin.a\ \cos.b+\cos.a\ \sin.b & (7)\\ \sin.(a-b)=\sin.a\ \cos.b-\cos.a\ \sin.b & (8)\\ \cos.(a+b)=\cos.a\ \cos.b-\sin.a\ \sin.b & (9)\\ \cos.(a-b)=\cos.a\ \cos.b+\sin.a\ \sin.b & (10)\end{cases}$$

Formulæ (A) accomplish the objects of the proposition, and from these equations many useful and important deductions can be made. The following are the most essential:

By adding (7) to (8), we have (11); subtracting (8) from (7) gives (12). Also, (9) added to (10) gives (13); (9) taken from (10) gives (14).

$$(B)\begin{cases}\sin.(a+b)+\sin.(a-b)=2\ \sin.a\ \cos.b & (11)\\ \sin.(a+b)-\sin.(a-b)=2\ \cos.a\ \sin.b & (12)\\ \cos.(a+b)+\cos.(a-b)=2\ \cos.a\ \cos.b & (13)\\ \cos.(a-b)-\cos.(a+b)=2\ \sin.a\ \sin.b & (14)\end{cases}$$

If we put $a+b=A$, and $a-b=B$, then (11) becomes (15), (12) becomes (16), (13) becomes (17), and (14) becomes (18).

$$(C)\begin{cases}\sin.A+\sin.B=2\ \sin.\left(\dfrac{A+B}{2}\right)\cos.\left(\dfrac{A-B}{2}\right) & (15)\\ \sin.A-\sin.B=2\ \cos.\left(\dfrac{A+B}{2}\right)\sin.\left(\dfrac{A-B}{2}\right) & (16)\\ \cos.A+\cos.B=2\cos.\left(\dfrac{A+B}{2}\right)\cos.\left(\dfrac{A-B}{2}\right) & (17)\\ \cos.B-\cos.A=2\ \sin.\left(\dfrac{A+B}{2}\right)\sin.\left(\dfrac{A-B}{2}\right) & (18)\end{cases}$$

If we divide (15) by (16), observing that $\dfrac{\sin.}{\cos.}=\tan.$, and $\dfrac{\cos.}{\sin.}=\cot.=\dfrac{1}{\tan.}$, as we learn by equations (6) and (5), we shall have

$$\frac{\sin.A+\sin.B}{\sin.A-\sin.B}=\frac{\sin.\left(\frac{A+B}{2}\right)}{\cos.\left(\frac{A+B}{2}\right)}\times\frac{\cos.\left(\frac{A-B}{2}\right)}{\sin.\left(\frac{A-B}{2}\right)}=\frac{\tan.\left(\frac{A+B}{2}\right)}{\tan.\left(\frac{A-B}{2}\right)} \quad (19)$$

Whence,

$$\sin.A+\sin.B : \sin.A-\sin.B=\tan.\left(\frac{A+B}{2}\right) : \tan.\left(\frac{A-B}{2}\right)$$

That is: *The sum of the sines of any two arcs is to the difference of the same sines, as the tangent of one half the sum of the same arcs is to the tangent of one half their difference.*

By operating in the same way with the different equations in formulæ (C), we find,

$$(D)\left\{\begin{array}{ll}
\dfrac{\sin.A+\sin.B}{\cos.A+\cos.B}=\tan.\left(\dfrac{A+B}{2}\right) & (20)\\
\dfrac{\sin.A+\sin.B}{\cos.B-\cos.A}=\cot.\left(\dfrac{A-B}{2}\right) & (21)\\
\dfrac{\sin.A-\sin.B}{\cos.A+\cos.B}=\tan.\left(\dfrac{A-B}{2}\right) & (22)\\
\dfrac{\sin.A-\sin.B}{\cos.B-\cos.A}=\cot.\left(\dfrac{A+B}{2}\right) & (23)\\
\dfrac{\cos.A+\cos.B}{\cos.B-\cos.A}=\dfrac{\cot.\left(\frac{A+B}{2}\right)}{\tan.\left(\frac{A-B}{2}\right)} & (24)
\end{array}\right.$$

These equations are all true, whatever be the value of the arcs designated by A and B; we may, therefore, assign any possible value to either of them, and if in equations (20), (21), and (24), we make $B=0$, we shall have,

$$\frac{\sin.A}{1+\cos.A}=\tan.\frac{A}{2}=\frac{1}{\cot.\frac{1}{2}A} \quad (25)$$

$$\frac{\sin.A}{1-\cos.A}=\cot.\frac{A}{2}=\frac{1}{\tan.\frac{1}{2}A} \quad (26)$$

$$\frac{1+\cos.A}{1-\cos.A}=\frac{\cot.\frac{1}{2}A}{\tan.\frac{1}{2}A}=\frac{1}{\tan^2.\frac{1}{2}A} \quad (27)$$

If we now turn back to formulæ (A), and divide equation (7) by (9), and (8) by (10), observing at the same time that $\frac{\sin.}{\cos.}=\tan.$, we shall have,

$$\tan.(a+b)=\frac{\sin.a\ \cos.b+\cos.a\ \sin.b}{\cos.a\ \cos.b-\sin.a\ \sin.b}$$
$$\tan.(a-b)=\frac{\sin.a\ \cos.b-\cos.a\ \sin.b}{\cos.a\ \cos.b+\sin.a\ \sin.b}$$

By dividing the numerators and denominators of the second members of these equations by ($\cos.a\ \cos.b$), we find,

$$\tan.(a+b)=\frac{\dfrac{\sin.a\ \cos.b}{\cos.a\ \cos.b}+\dfrac{\cos.a\ \sin.b}{\cos.a\ \cos.b}}{\dfrac{\cos.a\ \cos.b}{\cos.a\ \cos.b}-\dfrac{\sin.a\ \sin.b}{\cos.a\ \cos.b}}=\frac{\tan.a+\tan.b}{1-\tan.a\ \tan.b}\qquad(28)$$

$$\tan.(a-b)=\frac{\dfrac{\sin.a\ \cos.b}{\cos.a\ \cos.b}-\dfrac{\cos.a\ \sin.b}{\cos.a\ \cos.b}}{\dfrac{\cos.a\ \cos.b}{\cos.a\ \cos.b}+\dfrac{\sin.a\ \sin.b}{\cos.a\ \cos.b}}=\frac{\tan.a-\tan.b.}{1+\tan.a\ \tan.b}\qquad(29)$$

If in equation (11), formulæ (B), we make $a=b$, we shall have,

$$\sin.2a=2\ \sin.a\ \cos.a\qquad(30)$$

Making the same hypothesis in equation (13), gives,

$$\cos.2a+1=2\ \cos.^2a\qquad(31)$$

The same hypothesis reduces equation (14) to

$$1-\cos.2a=2\ \sin.^2a\qquad(32)$$

The same hypothesis reduces equation (28) to

$$\tan.2a=\frac{2\ \tan.a}{1-\tan.^2a}\qquad(33)$$

If we substitute a for $2a$ in (31) and (32), we shall have

$$1+\cos.a=2\ \cos.^2\tfrac{1}{2}a.\qquad(34)$$
and $$1-\cos.a=2\ \sin.^2\tfrac{1}{2}a.\qquad(35)$$

PROPOSITION III.

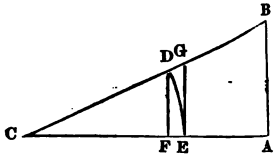
In any right-angled plane triangle, we may have the following proportions:

1st. *The hypotenuse is to either side, as the radius is to the sine of the angle opposite to that side.*

2d. *One side is to the other side, as the radius is to the tangent of the angle adjacent to the first side.*

3d. *One side is to the hypotenuse, as the radius is to the secant of the angle adjacent to that side.*

Let *CAB* represent any right-angled triangle, right-angled at *A*.



(Here, and in all cases hereafter, we shall represent the angles of a triangle by the large letters *A*, *B*, *C*, and the sides opposite to them, by the small letters *a*, *b*, *c*.)

From either acute angle, as *C*, take any distance, as *CD*, *greater* or *less* than *CB*, and describe the arc *DE*. This arc measures the angle *C*. From *D*, draw *DF* parallel to *BA*; and from *E*, draw *EG*, also parallel to *BA* or *DF*.

By the definitions of sines, tangents, secants, etc., *DF* is the sine of the angle *C*; *EG* is the tangent, *CG* the secant, and *CF* the cosine.

Now, by proportional triangles we have,

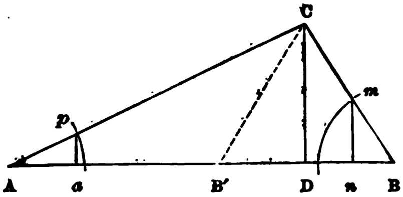
$$\begin{aligned} CB : BA &= CD : DF;\ \text{or, } a : c = R : \sin.C \\ CA : AB &= CE : EG;\ \text{or, } b : c = R : \tan.C \\ CA : CB &= CE : CG;\ \text{or, } b : a = R : \sec.C \end{aligned}$$

Hence the proposition.

Scholium.—If the hypotenuse of a triangle is made radius, one side is the sine of the angle opposite to it, and the other side is the cosine of the same angle. This is obvious from the triangle *CDF*.

PROPOSITION IV.

In any triangle, the sines of the angles are to one another as the sides opposite to them.



Let ABC be any triangle. From the points A and B, as centers, with any radius, describe the arcs measuring these angles, and draw pa, CD, and mn, perpendicular to AB.

Then,

$$pa = \sin.A, \text{ and } mn = \sin.B.$$

By the similar △'s, Apa and ACD, we have,

$$R : \sin.A = b : CD; \text{ or } R(CD) = b \sin.A. \qquad (1)$$

By the similar △'s, Bmn and BCD, we have,

$$R : \sin.B = a : CD; \text{ or } R(CD) = a \sin.B. \qquad (2)$$

By equating the second members of equations (1) and (2)

$$b \sin.A = a \sin.B.$$

Hence,

$$\sin.A : \sin.B = a : b$$

Or, $$a : b = \sin.A : \sin.B.$$

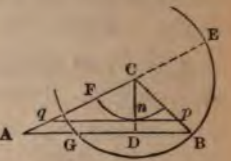
Scholium 1.—When either angle is 90°, its sine is radius.

Scholium 2.—When CB is less than AC, and the angle B, acute, the triangle is represented by ACB. When the angle B becomes B', it is obtuse, and the triangle is ACB'; but the proportion is equally true with either triangle; for the angle $CB'D = CBA$, and the sine of $CB'D$ is the same as the sine of $AB'C$. In practice we can determine which of these triangles is proposed, by the side AB being greater or less than AC; or, by the angle at the vertex C being large, as ACB, or small, as ACB'.

In the solitary case in which AC, CB, and the angle A, are given, and CB less than AC, we can determine both of the △'s ACB and ACB'; and then we surely have the right one.

PROPOSITION V.

If from any angle of a triangle, a perpendicular be let fall on the opposite side or base, the tangents of the segments of the angle are to each other as the segments of the base.



Let ABC be the triangle. Let fall the perpendicular CD, on the side AB.

Take any radius, as Cn, and describe the arc which measures the angle C. From n, draw qnp parallel to AB. Then it is obvious that np is the tangent of the angle DCB, and nq is the tangent of the angle ACD.

Now, by reason of the parallels AB and qp, we have,

$$qn : np = AD : DB$$

That is, $$\tan. ACD : \tan. DCB = AD : DB.$$

PROPOSITION VI.

If a perpendicular be let fall from any angle of a triangle to its opposite side or base, this base is to the sum of the other two sides, as the difference of the sides is to the difference of the segments of the base.

(See Figure to Proposition V.)

Let AB be the base, and from C, as a center, with the shorter side as radius, describe the circle, cutting AB in G, and AC in F; produce AC to E.

It is obvious that AE is the sum of the sides AC and CB, and AF is their difference.

Also, AD is one segment of the base made by the perpendicular, and $BD = DG$ is the other; therefore, the difference of the segments is AG.

As A is a point without a circle, by Cor. Th. 18, B. III, we have

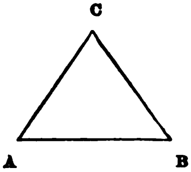
$$AE \times AF = AB \times AG$$

Hence, $$AB : AE = AF : AG.$$

PROPOSITION VII.

The sum of any two sides of a triangle is to their difference, as the tangent of one half the sum of the angles opposite to these sides, is to the tangent of one half their difference.

1st *Demonstration.*



Let ABC be any plane triangle. Then, by Proposition IV, we have,

$$BC : AC = \sin.A : \sin.B.$$

Hence,

$$BC+AC:BC-AC=\sin.A+\sin.B:\sin.A-\sin.B \text{(Th.9,B.II)}.$$

But,

$$\tan.\left(\frac{A+B}{2}\right) : \tan.\left(\frac{A-B}{2}\right) = \sin.A + \sin.B : \sin.A - \sin.B, \text{(eq. (19), Trig.)}$$

Comparing the two latter proportions, (Th. 6, B. II), we have,

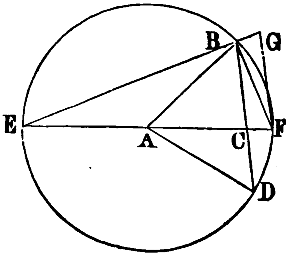
$$BC + AC : BC - AC = \tan.\left(\frac{A+B}{2}\right) : \tan.\left(\frac{A-B}{2}\right)$$

Hence the proposition.

For those, who prefer a demonstration wholly geometrical, we give the following:

2d *Demonstration.*

Let ABC be a plane triangle; about A as a center, with AB, the greater side, as radius describe a circle, meeting AC, produced in E and F, and BC in D. Join DA, EB, and FB; and draw FG parallel to BC, meeting EB in G.



The angle EAB is the sum of the angles at the base of the triangle ABC (B. I. Th. 12); and EFB at the circumference is equal to one half EAB at the center: EFB is therefore equal to one half the sum of the base angles of the triangle.

The angle ACB is equal to CAD and ADC together; or since ADC equals ABC, ACB is equal to the sum of CAD and ABC. CAD is therefore equal to the difference between the base angles ACB and ABC. Now DBF at the circumference is one half FAD at the center; and therefore DBF, or its equal (since BC and FG are parallel) BFG is equal to one half the difference of the base angles of the triangle.

Since the angle EBF is inscribed in a semi-circle, it is a right angle; and if BF be taken as radius, and a circle described from F as a center, BE and BG would be tangents (B. III, Th. 4); BE being the tangent of the angle EFB, and BG of BFG; or since these angles are the half sum and half difference of the base angles of the triangle, BE and BG would be tangents of the half sum and half difference of those angles.

From the construction of the figure it is plain that EC equals $AC+AB$ and CF equal $AB-AC$.

In the triangle EFG, since BC is parallel to FG, we have (B. II, Th. 17),

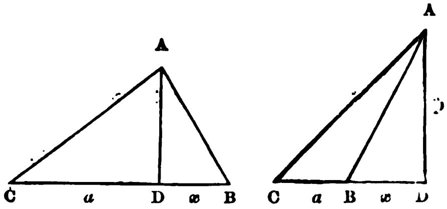
$$EC : CF = EB : BG, \text{ or}$$

$$AB+AC : AB-AC = \tan.\tfrac{1}{2}\,(ACB+ABC) : \tan.\tfrac{1}{2}\,(ACB-ABC).$$

That is: the sum of two sides is to their difference as the tangent of half the sum of the opposite angles is to the tangent of half their difference.

PROPOSITION VIII.

Given the three sides of any plane triangle, to find some relation which they must bear to the cosines of the respective angles.



Let ABC be the triangle, and let the perpendicular fall either upon, or without the base, as shown in the figures. By recurring to Geom. Th. 41, B. I., we shall find

$$CD = \frac{a^2+b^2-c^2}{2a}. \qquad (1)$$

Now, by Proposition 3, we have

$$R : \cos. C = b : CD.$$

Therefore, $$CD = \frac{b \cos. C}{R}. \qquad (2)$$

Equating these two values of CD, and reducing, we have

$$\cos. C = \frac{R(a^2+b^2-c^2)}{2ab}. \qquad (m)$$

In this expression we observe, that the part c, whose square is found in the numerator with the minus sign, is the side opposite to the angle; and that the denominator is twice the rectangle of the sides adjacent to the angle. From these observations we at once draw the following expressions for the cosine A, and cosine B:

$$\cos. A = \frac{R(b^2+c^2-a^2)}{2bc}. \qquad (n)$$

$$\cos. B = \frac{R(a^2+c^2-b^2)}{2ac}. \qquad (p)$$

As these expressions are not convenient for logarithmic computation, we modify them as follows:

If we put $2a = A$, in equation (31), we have

$$\cos. A + 1 = 2\cos.^2 \tfrac{1}{2}A.$$

In the preceding expression (n), if we consider radius unity, and add 1 to both members, we shall have

$$\cos. A+1 = 1+\frac{b^2+c^2-a^2}{2bc}.$$

Therefore, $$2\cos.^2\tfrac{1}{2}A = \frac{2bc+b^2+c^2-a^2}{2bc}$$

$$= \frac{(b+c)^2-a^2}{2bc}.$$

Considering $b+c$ as one quantity, and observing that $(b+c)^2-a^2$ is the difference of *two squares*, we have $(b+c)^2-a^2=(b+c+a)(b+c-a)$; but $(b+c-a)=b+c+a-2a$.

Hence, $$2\cos.^2\tfrac{1}{2}A = \frac{(b+c+a)(b+c+a-2a)}{2bc}.$$

Or, $$\cos.^2\tfrac{1}{2}A = \frac{\left(\frac{b+c+a}{2}\right)\left(\frac{b+c+a}{2}-a\right)}{bc}.$$

By putting $\frac{a+b+c}{2} = s$, and extracting square root, the final result for radius unity is

$$\cos.\tfrac{1}{2}A = \sqrt{\frac{s(s-a)}{bc}}.$$

For any other radius we must write

$$\left.\begin{aligned} &\cos.\tfrac{1}{2}A = \sqrt{\frac{R^2s(s-a)}{bc}}. \\ \text{By inference,}\quad &\cos.\tfrac{1}{2}B = \sqrt{\frac{R^2s(s-b)}{ac}}. \\ \text{Also,}\quad &\cos.\tfrac{1}{2}C = \sqrt{\frac{R^2s(s-c)}{ab}}. \end{aligned}\right\}$$

In every triangle, the sum of the three angles is equal to 180°; and if one of the angles is small, the other two must be comparatively large; if two of them are small, the third one must be large. The greater angle is always opposite the greater side; hence, by merely inspecting the given sides, any person can decide at once which is the greater angle; and of the three preceding equations, *that one* should be taken which applies to the greater angle, whether that be the particular angle required or not; because the equations bring out the *cosines* to the angles; and the cosines to very small arcs vary so slowly, that it may be impossible to decide, with sufficient numerical accuracy, to what particular arc the cosine belongs. For instance, the cosine 9.999999, carried to the table, applies to several arcs; and, of course, we should not know which one to take; but this difficulty does not exist when the angle is large; therefore, compute the largest angle first, and then compute the other angles by Proposition IV.

Equations showing the relations between the sides of a triangle and the *sines* of the angles, may be readily obtained; but as those above given for the cosines in terms of the sides are more easily applied and most generally used, we deem them sufficient for our purpose.

OF THE TABLES OF SINES, COSINES, ETC.

NATURAL SINES, ETC.

When the radius of the circle is taken as the unit of measure, the numerical values of the trigonometrical lines belonging to the different arcs of the quadrant, become *natural* sines, cosines, etc. They are then, in fact, but numbers expressing the number of times that these lines contain the radius of the circle in which they are taken. The tables usually contain only the sines and cosines, because these are generally sufficient for practical purposes, and the others, when required, are readily expressed in terms of them.

For the method of calculating these functions, the student is referred to Robinson's New Geometry and Trigonometry, page 265 and on.

Natural sines and cosines are rarely used, except in cases where addition or subtraction is to be performed; in all cases of multiplication or division, logarithmic numbers are preferable, and great pains is taken to adapt the formulæ of trigonometry to the use of logarithms.

Natural sines and cosines are given in the tables connected with this work, and may be found in connection with logarithmic sines and cosines, in two columns at the right, headed "N. sin." and "N. cos." The degrees under 45° are found at the top of the page, those above 45° at the bottom, and the minutes either on the left or right hand, as the degrees are found at the top or bottom of the page. Natural sines and cosines are all calculated with unity as the radius.

OF LOGARITHMIC SINES, ETC.

The logarithmic sines and cosines, tangents and cotangents, are the logarithms of the number representing these lines in a circle whose radius is 10,000,000,000. The radius has a logarithm of 10; and since the trigonometrical lines are proportional to the radii of the circles in which they are calculated, the logarithmic sines, &c., may be found by adding 10 to the logarithms of the natural sines, &c., as given in the tables. The reason why so great a value is assumed for the radius is, that when the radius is *unity*, the sines and cosines are *decimals*, and consequently their logarithms have *negative indices.* To avoid this a radius is assumed, whose logarithm 10, added to the logarithm of the decimal, will in all ordinary cases make the index positive.

In dealing with logarithmic numbers in trigonometry, wherever radius is introduced, its logarithm, 10, must be used; in natural numbers the radius, being unity, is neglected, where it is connected with other numbers as a *factor.*

The abbreviations sin., cos., tan., cotan., &c., refer to the natural numbers; for the logarithmic terms, log. sin., log. tan., &c., are used.

The secants and cosecants of arcs are not given in the table, because they are very little used in practice; and if any particular secant is required, it can be determined by subtracting the cosine from 20; and the cosecant can be found by subtracting the sine from 20. For,

$$\text{sec.} = \frac{R^2}{\text{cos.}}, \text{ and cosec.} = \frac{R^2}{\text{sin.}}$$

The sine of every degree and minute of the quadrant is given, directly, in the table, commencing at 0°, and extending to 45°, at the head of the table; and from 45° to 90°, at the bottom of the table, increasing backward.

The same column that is marked sine at the top, is marked cosine at the bottom; and the reason for this is apparent to any one who has examined the definitions of sines.

The difference of two consecutive logarithms is given, corresponding to *ten* seconds. Removing the decimal point one figure, will give the difference for *one* second; and if we multiply this difference by any proposed number of seconds, we shall have a difference of logarithm corresponding to that number of seconds above the preceding degree and minute.

For example, find the sine of 19° 17′ 22.

The sine of 19° 17′, taken directly from the table, is	9.518829
The difference for 10″ is 60.2; for 1″, is 6.02; and	
6.02 × 22 =	132
Hence, the sine of 19° 17′ 22″	9.518961

From this it will be perceived that there is no difficulty in obtaining the sine or tangent, cosine or cotangent, of any angle greater than 30′.

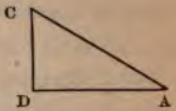
Conversely: Given, the logarithmic sine 9.982412, to find its corresponding arc. The sine next less in the table is 9.982404, which gives the arc 73° 48′. The difference between this and the given sine is 8, and the difference for 1″ is .61; therefore, the number of seconds corresponding to 8, must be discovered by dividing 8 by the decimal .61, which gives 13. Hence, the arc sought is 73° 48′ 13″.

These operations, so similar to those required in the logarithms of simple numbers, will need no rule.

PRACTICAL APPLICATIONS.

Having mastered the necessary principles, and the explanation of the tables containing the numerical values needed, the student may now give his attention to the application of these principles and the use of these numbers, in the solution of plane triangles.

I. OF RIGHT-ANGLED TRIANGLES.



For all the examples which follow, but one figure is necessary; and in each case the pupil will refer to the one here given, AC being the hypotenuse, D the right angle, and each angle being represented by the letter at the vertex.

NOTE.—In all numerical solutions, unless otherwise noted, the reference numbers connected with equations and proportions, refer to corresponding numbers in the preceding theoretical explanations.

In every right-angled plane triangle, the right angle being always known, there remain five parts: the hypotenuse, base, perpendicular, base angle, and perpendicular angle.

Any two of these being given, the others may be found, provided one of the known quantities be a side.

CASE I.

Given the hypotenuse and an angle.

(1.) To find the other angle.

Since $A + C = 90° \therefore 90° - A = C$ and $90° - C = A$.

(2.) To find other sides.

(Prop. III) in verting first proportion,

$$R : AC = \begin{cases} \left\{ \begin{matrix} \sin. A : CD \\ \cos. A : AD \end{matrix} \right\} & (1) \\ \left\{ \begin{matrix} \sin. C : AD \\ \cos. C : CD \end{matrix} \right\} & (2) \end{cases}$$

From either the first or second *couplet of proportion*, CD and AD become known.

EXAMPLES.

1. Given hypotenuse $= 68$, and base angle $= 37^\circ\ 30'$.

$90^\circ - A = 90^\circ - 37^\circ\ 30' = 52^\circ\ 30' = C$, perpendicular angle.

By first couplet of proportion above,

$$\begin{aligned} R : 68 &: : \sin.\ 37^\circ\ 30' : CD \\ R : 68 &: : \cos.\ 37^\circ\ 30' : AD \end{aligned} \qquad (1)$$

$$\begin{aligned} &\text{Log. } 68 &&= 1.832509 \\ &\text{Log. sin. } 37^\circ\ 30' &&= \underline{9.784447} \\ &\text{Sum less } 10^* &&= 1.616956 \\ &\qquad 1.616956 &&= \log.\ CD = \log.\ 41.396. \end{aligned}$$

$$\begin{aligned} &\text{Log. } 68 &&= 1.832509 \\ &\text{Log. cos. } 37^\circ\ 30' &&= \underline{9.899467} \\ &\text{Sum less } 10 &&= 1.731976 \\ &\qquad 1.731976 &&= \log.\ AD = \log.\ 53.948. \end{aligned}$$

$$\textit{Ans.} \begin{cases} C = 52^\circ\ 30' \\ CD = 41.396 \\ AD = 53.948 \end{cases}$$

2. Given $AC = 236$, $C = 49^\circ\ 50'$, to find A, AD and CD.

$$\textit{Ans.} \begin{cases} A = 40^\circ\ 10' \\ AD = 180.34 \\ CD = 152.22 \end{cases}$$

3. Given $AC = 92.76 : A = 24^\circ\ 16'$, to find other parts.

$$\textit{Ans.} \begin{cases} C = 65^\circ\ 44' \\ AD = 84.56 \\ CD = 38.12 \end{cases}$$

4. Given $AC = 102.8 : A = 42^\circ\ 48'$, to find other parts.

---

* The 10 here subtracted is the logarithm of the first term of the proportion.

CASE II.

Given the hypotenuse and one side.

(1.) To find angles.

By Prop. III., as before,

$$R : AC = \begin{cases} \left.\begin{matrix} \sin.A : CD \\ \cos.A : AD \end{matrix}\right\} & (1) \\ \left.\begin{matrix} \sin.C : AD \\ \cos.C : CD \end{matrix}\right\} & (2) \end{cases}$$

From (1), A may be found; and as before $90°-A=C$. Or from (2) C may be found; and $90°-C = A$.

(2.) To find other side.

By Geom., B. I., Th. 39,

$$\sqrt{AC^2-AD^2} = CD \text{ or } \sqrt{AC^2-CD^2} = AD. \qquad (3)$$

By Prop. III., 2d proportion,

$$R : \tan.A = AD : CD \qquad (4)$$

$$R : \tan.C = CD : AD \qquad (5)$$

From either of which the side required may be found.

EXAMPLES.

1. Given $AC = 100$, $AD = 48$.

Solution.

$$R : 100 = \cos.A : 48 \qquad (1)$$

Log. R + log. 48 $= 11.681241$
Subtract log. 100 $= 2.000000$

Log. cos. A $= 9.681241 =$ log. cos. 61° 18′ 53″
$A = 61° 18' 53''$; $90° - 61° 18' 53'' = 28° 41' 7'' = C$.

$$R : \tan. 28° 41' 7'' = CD : 48 \qquad (5)$$

Log. R + log. 48 $= 11.681241$
Log. tan. 28° 41′ 7″ $= 9.738106$

Log. CD $= 1.943134 =$ log. 87.73.

Ans. $A = 61° 18' 53''$; $C = 28° 41' 7''$; $CD = 87.73$.

2. Given $AC = 300$, and $CD = 130$

$$\text{Ans.}\left\{\begin{aligned} A &= 25^\circ\ 40'\ 45'' \\ C &= 64^\circ\ 19'\ 15'' \\ AD &= 270.37 \end{aligned}\right.$$

3. Given $AC = 1896$, and $CD = 479$.

4. Given $AC = 241$, and $AD = 78$.

CASE III.

Given one side and an angle.

(1.) To find other angle.

Subtract given angle from 90°.

(2.) To find hypotenuse.

By Prop. III., 1st proportion,

$$AC : AD = R : \sin.\ C \text{ or } \cos.\ A \qquad (1)$$
$$AC : CD = R : \sin.\ A \text{ or } \cos.\ C. \qquad (2)$$

By Prop. III., 3d proportion,

$$AD : AC = R : \text{secant } A \qquad (3)$$
$$CD : AC = R : \text{secant } C. \qquad (4)$$

Proportions (1) and (2) would be used most generally, as sines are more easily obtained from table than secants.

3. To find other side.

(*a*) Use AC and angle, and apply Case I.
(*b*) Use AC and given side according to Case II.
(*c*) By Prop. III., 2d proportion,

$$AD : CD = R : \tan.\ A, \qquad (5)$$
$$\text{Or,}\quad CD : AD = R : \tan.\ C. \qquad (6)$$

EXAMPLES.

1. Given $AD = 39$, and $A = 41^\circ\ 10'$.

(1.) $90^\circ - 41^\circ\ 10' = 48^\circ\ 50' = C$.

816303 A

(2.) $AC : 39 = R : \text{sin. } 48^\circ\ 50'$. (1)

$$\begin{aligned} \text{Log. } R + \text{log. } 39 &= 11.591065 \\ \text{(Less) log. sin. } 48^\circ\ 50' &= \underline{\ \ 9.876678} \\ \text{Log. } AC &= \ \ 1.714387 = \text{log. } 51.81. \\ AC &= 51.81 \end{aligned}$$

(3.) $CD : 39 = R : \text{tan. } 48^\circ\ 50$. (6)

$$\begin{aligned} \text{Log. } R + \text{log. } 39 &= 11.591065 \\ \text{Log. tan. } 48^\circ\ 50' &= \underline{10.058286} \\ \text{Log. } CD &= \ \ 1.532779 = \text{log. } 34.1 \\ CD &= 34.1. \end{aligned}$$

$$Ans. \left\{ \begin{aligned} C &= 48^\circ\ 50' \\ AC &= 51.81 \\ CD &= 34.1 \end{aligned} \right.$$

2. Given $CD = 76.84$, and $A = 51^\circ\ 42'\ 20''$.

$$Ans. \left\{ \begin{aligned} C &= 38^\circ\ 17'\ 40'' \\ AC &= 97.91 \\ AD &= 60.67. \end{aligned} \right.$$

3. Given $CD = 103.54$, and $C = 21^\circ\ 50'$.

$$Ans. \left\{ \begin{aligned} A &= 68^\circ\ 10' \\ AC &= 111.54 \\ AD &= 41.48. \end{aligned} \right.$$

4. Given $AD = 7.96$, and $C = 17^\circ\ 23'\ 12''$.

CASE IV.

Given the two sides or the base and perpendicular.

(1) To find angles,

$$AD : CD = R : \text{tan. } A, \text{ or cot. } C. \qquad (1)$$
$$90^\circ - A = C, \text{ or } 90^\circ - C = A.$$

2. To find hypotenuse,

(*a*), Apply (2), Case I.
(*b*), Apply (2), Case III.
(*c*), $\sqrt{AD^2 + CD^2} = AC$.

EXAMPLES.

1. Given $AD = 42.5$, and $CD = 59$.

Solution.

(1) $$42.5 : 59 = R : \tan. A. \qquad (1)$$

$$\begin{array}{lcl} \text{Log. } 59 + \log. R & = & 11.770852 \\ \text{Log. } 42.5 & = & \underline{1.628389} \\ \text{Log. tan. } A & = & 10.142463 \end{array}$$

$$10.142463 = \log. \tan. 54^\circ\ 14' ;\ \therefore\ 54^\circ\ 14' = A.$$

$$90^\circ - 54^\circ\ 14' = 35^\circ\ 46' = C.$$

(2.) By (2), Case I.

$$R : AC = \sin. 54^\circ\ 14' : 59$$

$$\begin{array}{lcl} \text{Log. } 59 + \log. R & = & 11.770852 \\ \text{Log. sin.} A & = & \underline{9.909237} \\ \text{Log. } AC & = & 1.861615 \end{array}$$

$$1.861615 = \log. 72.71\ \therefore\ AC = 72.71.$$

$$Ans. \begin{cases} A = 54^\circ\ 14' \\ C = 35^\circ\ 46' \\ AC = 72.71 \end{cases}$$

2. Given $AD = 34.75$, and $CD = 52.25$.

$$Ans. \begin{cases} A = 56^\circ\ 22'\ 24'' \\ C = 33^\circ\ 37'\ 36'' \\ AC = 62.75 \end{cases}$$

3. Given $AD = 102$, and $CD = 143$.

$$Ans. \begin{cases} A = 54^\circ\ 30'\ 1'' \\ C = 35^\circ\ 29'\ 59'' \\ AC = 175.65 \end{cases}$$

4. Given $AD = 17.377$, and $CD = 26.89$.

As the solution of right-angled plane triangles is so frequently required in practical mathematics, a list of practical examples is subjoined, to which the pupil may apply for himself the principles and proportions heretofore given. And the student will be fully recompensed for all time and labor expended, by the increased familiarity with these operations.

PRACTICAL PROBLEMS.

Let ABC represent any right-angled plane triangle, right-angled at B.

1. In a right-angled triangle, ABC, given the base AB, 1214, and the angle A, 51° 40′ 30″, to find the other parts.

2. Given AC, 73.26, and the angle A, 49° 12′ 20″; required the other parts.

Ans. The angle C, 40° 47′ 40″; BC, 55.46; and AB, 47.86.

3. Given AB, 469.34, and the angle A, 51° 26′ 17″, to find the other parts.

Ans. The angle C, 38° 33′ 43″; BC, 588.7; and AC, 752.9.

4. Given AB, 493, and the angle C, 20° 14′; required, the remaining parts.

Ans. The angle A, 69° 46′; BC, 1337.5; and AC, 1425.5.

5. Let $AB = 331$, and the angle $A = 49° \ 14'$; what are the other parts?

Ans. AC, 506.9; BC, 383.9; and the angle C, 40° 46′.

6. If $AC = 45$, and the angle $C = 37° \ 22'$, what are the remaining parts?

Ans. AB, 27.31; BC, 35.76; and the angle A, 52° 38′.

7. Given $AC = 4264.3$, and the angle $A = 56° \ 29' \ 13''$, to find the remaining parts.

Ans. AB, 2354.4; BC, 3555.4; and the angle C, 33°30′47″.

8. If $AB = 42.2$, and the angle $A = 31° \ 12' \ 49''$, what are the other parts?

Ans. AC, 49.34; BC, 25.57; and the angle C, 58° 47′ 11″.

9. If $AB = 8372.1$, and $BC = 694.73$, what are the other parts?

Ans. AC, 8400.9; the angle C, 85° 15′ 23″; and the angle A, 4° 44′ 37″.

10. If AB be 63.4, and AC be 85.72, what are the other parts?

Ans. BC, 57.69; the angle C, 47° 41′ 56″; and the angle A, 42° 18′ 4″.

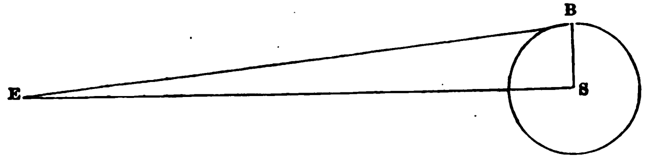
11. Given $AC = 7269$, and $AB = 3162$, to find the other parts.

Ans. $\begin{cases} BC, \ 6545.23; \text{ the angle } C, 25^\circ\ 47'\ 7''; \text{ and the angle} \\ A, \ 64^\circ\ 12'\ 53. \end{cases}$

12. Given $AC = 4824$, and $BC = 2412$, to find the other parts.

Ans. $\begin{cases} \text{The angle } A = 30^\circ\ 00', \text{ the angle } C = 60^\circ\ 00', \\ \text{and } AB = 4178. \end{cases}$

13. The distance between the earth and sun is 94,770,000 miles, and at that distance the semi-diameter of the sun subtends an angle of 16′ 6″. What is the diameter of the sun in miles? *Ans.* 887,673.5 miles.



In this example, let E be the center of the earth, S that of the sun, and EB a tangent to the sun's surface. Then the $\triangle\ EBS$ is right-angled at B, and BS is the semi-diameter of the sun. The value of $2BS$ is required.

II. OF OBLIQUE-ANGLED PLANE TRIANGLES.

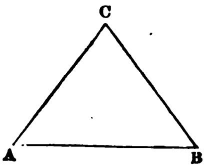
In every oblique-angled plane triangle, there are six parts; viz., three sides and three angles. Any three of these being known—provided one side at least be given—the others may be found by the preceding theorems and formulæ, as is shown in the following cases.

CASE I.

Given a side and two adjacent angles.

Let ABC be any plane triangle.

Suppose AB to be given, and the angles A and B.



(1.) To find third angle.

By (B. I., Th. 11) $180^\circ - (A + B) = C.$

(2.) To find the other sides.

By Prop. IV, $\text{Sin. } C : AB = \begin{cases} \text{sin.} A : BC, & (a) \\ \text{sin.} B : AC, & (b) \end{cases}$

EXAMPLES.

1. Given $AB = 376$, $A = 48^\circ\ 3'$, and $B = 40^\circ\ 14'$.

Solution.

(1.) $180^\circ - (48^\circ\ 3' + 40^\circ\ 14') = 91^\circ\ 43' = C.$

(2.) $\text{Sin. } 91^\circ\ 43' : 376 = \text{sin. } 48^\circ\ 3' : BC.$ (a)

$$\begin{aligned} \text{Co. log. sin. } 91^\circ\ 43' &= 0.000195 \\ \text{Log. } 376 &= 2.575188 \\ \text{Log. sin. } 48^\circ\ 3' &= 9.871414 \\ \text{Sum less } 10 &= 2.446797 \end{aligned}$$

$$2.446797 = \text{log. } 279.77 = BC.$$

$\text{Sin. } 91^\circ\ 43' : 376 = \text{sin. } 40^\circ\ 14' : AC$ (b)

$$\begin{aligned} \text{Co. log. sin. } 91^\circ\ 43' &= 0.000195 \\ \text{Log. } 376 &= 2.575188 \\ \text{Log. sin. } 40^\circ\ 14' &= 9.810167 \\ \text{Sum less } 10 &= 2.385550 \end{aligned}$$

$$2.385550 = \text{log. } 242.97 = AC.$$

$$\textit{Ans.} \begin{cases} C = 91^\circ\ 43'. \\ AC = 242.97. \\ BC = 279.76. \end{cases}$$

2. $A = 35^\circ\ 42'$, $B = 76^\circ\ 27'$, and $AB = 142$.

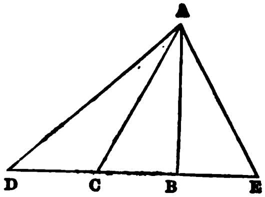
$$\textit{Ans.} \begin{cases} C = 67^\circ\ 51 \\ AC = 149.05 \\ BC = 89.47 \end{cases}$$

3. Given $B = 23^\circ\ 40'\ 22''$, $C = 69^\circ\ 39'\ 51''$, and $BC = 10$

$$\textit{Ans.} \begin{cases} \\ \\ \end{cases}$$

CASE II.

Given two sides and an angle opposite one of them.



Let ADC be a plane triangle. Suppose AD and AC to be given, and angle D opposite AC.

(1.) To find other angles.

By Prop. IV,

$$AC : \sin. D = AD : \sin. \text{ angle opposite } AD. \quad (1.)$$

Now in this proportion the fourth term is a sine; and as the sine of an angle and of its supplement are the same, the result is ambiguous.

The same ambiguity may be found in the figure; for there will be two lines AC, and AE, one on each side of the perpendicular AB, each of which will correspond with the given side numerically.

Thus, if the angle D be given opposite the shorter side AC, there will be two triangles which will contain all the required conditions. In practical cases circumstances will generally determine which of the two is to be used.

If the angle given be obtuse, as C, the other angles must be acute, and there can be no ambiguity.

AC must not be less than AB, the sine of the angle D when AD is made radius; for if so, the triangle becomes impossible.

By the proportion given above having found C and E, we have

$$180^\circ-(D+C) = DAC, \text{ and } 180^\circ-(D+E) = DAE.$$

(2.) To find third side.

By Prop. IV, $\quad \text{Sin. } D : AC = \sin. DAC : DC \quad (2)$

$\text{Sin. } D : AC = \sin. DAE : DE \quad (3)$

When there is no ambiguity, only one of the above will be used,—as only one vertical angle will be found.

EXAMPLES.

1. Given $AD=450$, $AC=309$, and $D=27^\circ\,50'$.

$$(1)\qquad 309 : \text{sin. } 27^\circ\,50' = 450 : \text{sin. } C \text{ or } E \qquad (\text{Eq. } 1).$$

$$\begin{array}{ll}
\text{Co. log. } 309 & = 7.510041 \\
\text{Log. sin. } 27^\circ\,50' & = 9.669225 \\
\text{Log. } 450 & = \underline{2.653213} \\
\text{Sum less } 10 & = 9.832479 = \text{log. sin. } C \text{ or } E.
\end{array}$$

$$9.832479 = \text{log. sin. } 42^\circ\,50'\,24'' \text{ or } 137^\circ\,9'\,36''.$$

$$C = 137^\circ\,9'\,36'',\ E = 42^\circ\,50'\,24''.$$

$$180^\circ-(27^\circ\,50'+137^\circ\,9'\,36'' = 15^\circ\,0'\,24'' = DAC. \quad (a)$$

$$180^\circ-(27^\circ\,50'+41^\circ\,50'\,24'' = 109^\circ\,19'\,36'' = DAE. \quad (b)$$

$$\text{Sin. } 27^\circ\,50' : 309 = \text{sin. } 15^\circ\,0'\,23'' : DC \qquad (2)$$

$$\begin{array}{ll}
\text{Co. log. sin. } 27^\circ\,50' & = 0.330775 \\
\text{Log. } 309 & = 2.489959 \\
\text{Log. sin. } 15^\circ\,0'\,24'' & = \underline{9.413184} \\
\text{Sum less } 10 & = 2.233918 = \text{log. } DC.
\end{array}$$

$$2.233918 = \text{log. } 171.36 \quad \therefore DC = 171.36.$$

$$\text{Sin. } 27^\circ\,50' : 309 = \text{sin. } 109^\circ\,19'\,36'' : DE.$$

$$\begin{array}{ll}
\text{Co. log. sin. } 27^\circ\,50' & = 0.330775 \\
\text{Log. } 309 & = 2.489959 \\
\text{Log. sin. } 109^\circ\,19'\,36'' & = \underline{9.974809} \\
\text{Sum less } 10 & = 2.795543 = \text{log. } DE.
\end{array}$$

$$2.795543 = \text{log. } 624.52. \quad \therefore DE = 624.52.$$

$$\textit{Ans.}\ (1)\begin{cases} C = 137^\circ\,9'\,36'' \\ DAC = 15^\circ\,0'\,24'' \\ DC = 171.36 \end{cases} \quad (2)\begin{cases} E = 42^\circ\,50'\,24'' \\ DAE = 109^\circ\,19'\,36'' \\ DE = 624.52. \end{cases}$$

2. Given, $AD = 201$, $AC = 140$, and $D = 36^\circ\,44'$.

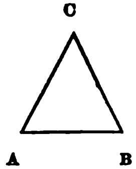
$$\textit{Ans.}\begin{cases} C = 120^\circ\,49'\,49'' \\ DAC = 22^\circ\,26'\,11'' \\ DC = 89.34. \end{cases} \quad \begin{cases} E = 59^\circ\,10'\,11'' \\ DAE = 84^\circ\,5'\,49'' \\ DE = 232.84. \end{cases}$$

3. Given, $AD = 180$, $AC = 100$, and $C = 127° 33'$.

$$Ans. \begin{cases} D = 26° \ 7' \ 59'' \\ DAC = 26° \ 19' \ 1'' \\ DC = 100.65. \end{cases}$$

CASE III.

Given two sides and the angle included by them.



In the triangle ABC, let AC and BC be given, and the angle C, which they include.

(1) To find other angles.

$$(180°—C) = A+B.$$

By Prop. VII,

$$AC+BC : AC—BC = \tan. \tfrac{1}{2}(A+B) : \tan. \tfrac{1}{2}(A—B) \quad (1).$$

$\frac{1}{2}(A—B)$ thus becomes known,

$$\left.\begin{array}{l} \tfrac{1}{2}(A+B)+\tfrac{1}{2}(A-B) = A, \\ \tfrac{1}{2}(A+B)-\tfrac{1}{2}(A-B) = B. \end{array}\right\} \quad (2).$$

(2.) To find third side.

By Prop. IV,

$$\begin{array}{l} \text{Sin. } A : BC = \text{sin. } C : AB, \text{ or} \\ \text{Sin. } B : AC = \text{sin. } C : AB. \end{array} \quad (3).$$

Which is the greater of the two angles, A and B, is determined from the sides opposite, which are known; in the above, A is assumed as the greater.

EXAMPLES.

1. $AC = 97$, $BC = 113$, and $C = 63° 41'$.

Solution.

(1) $$180°-63° 41' = 116° 19' = A+B.$$

$$\therefore \tfrac{1}{2}(A+B) = 58° \ 9' \ 30''.$$

$$113+97 = 210 = AC+BC; 113-97 = 16 = AC—BC$$

$$210 : 16 = \tan.\ 58^\circ\ 9'\ 30'' : \tan.\ \tfrac{1}{2}(A-B) \qquad (1)$$

$$\begin{array}{lcl}
\text{Co. log. } 210 & = & 7.677781 \\
\text{Log. } 16 & = & 1.204120 \\
\text{Log. tan. } 58^\circ\ 9'\ 30'' & = & \underline{10.206885} \\
\text{Sum less } 10 & = & 9.088786 = \text{log. tan. } \tfrac{1}{2}(A-B)
\end{array}$$

$$9.088786 = \text{log. tan. } 6^\circ\ 59'\ 39''.$$

$$\begin{array}{llcl}
\tfrac{1}{2}(A+B) & \ 58^\circ\ \ 9'\ 30'' & & 58^\circ\ \ 9'\ 30'' \\
\tfrac{1}{2}(A-B) & +\ \ \underline{6^\circ\ 59'\ 39''} & & -\ \ \underline{6^\circ\ 59'\ 39''} \\
 & \ 65^\circ\ \ 9'\ \ 9'' = A & & 51^\circ\ \ 9'\ 51'' = B,
\end{array} \qquad (2)$$

$$(2) \qquad \text{Sin. } 65^\circ\ 9'\ 9'' : 113 = \sin.\ 63^\circ\ 41' : AB \qquad (3)$$

$$\begin{array}{lcl}
\text{Co. log. sin. } 65^\circ\ 9'\ 9'' & = & 0.042187 \\
\text{Log. } 113 & = & 2.053078 \\
\text{Log. sin. } 63^\circ\ 41' & = & \underline{9.952481} \\
\text{Sum less } 10 & = & 2.047746 = \text{log. } AB
\end{array}$$

$$2.047746 = \text{log. } 111.62 = AB.$$

$$\textit{Ans.} \begin{cases} A = 65^\circ\ 9'\ 9'' \\ B = 51^\circ\ 9'\ 51'' \\ AB = 111.62. \end{cases}$$

2. Given $AB = 100$, $BC = 69$, and $B = 31^\circ\ 30'$.

Ans. $A = 41^\circ\ 12'\ 36''$; $C = 107^\circ\ 17'\ 24''$; $AC = 54.72$.

3. Given $AC = 233$, $BC = 396$, and $C = 49^\circ\ 40'$.

4. Given $AB = 9.75$, $AC = 11.5$, and $A = 70^\circ\ 11'\ 10.''$

CASE IV.

Given the three sides to determine the angles.

This may be solved by two methods entirely distinct, and each solution quite easily obtained.

1st method.—By Prop. VIII, we have formulæ for the cosines of one-half the angles in terms of the sides. In this case, any of these equations may be used for determining the first angle. To avoid danger of ambiguity, arising from the cosines of small arcs, it is customary to solve for the largest angle of the triangle. The following are the formulæ.

$$\text{Cos. } \tfrac{1}{2} A = \sqrt{\frac{R^2 s(s-a)}{bc}} \qquad (1)$$

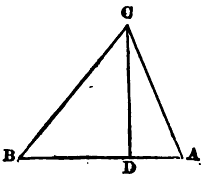
$$\text{Cos. } \tfrac{1}{2} B = \sqrt{\frac{R^2 s(s-b)}{ac}} \qquad (2)$$

$$\text{Cos. } \tfrac{1}{2} C = \sqrt{\frac{R^2 s(s-c)}{ab}} \qquad (3)$$

One angle having been obtained, the others may be found by Case II. As the largest angle is generally obtained from the formula, there is no ambiguity in the other results.

In these formulæ, the letters, a, b, c, represent the sides opposite the angles designated by the corresponding capital letters.

2d method.—In the triangle ABC, draw the perpendicular CD, dividing ABC into two right angled triangles,



By Prop. VI,

$AB : BC+AC = BC-AC : BD-AD.$ (1)

Whence, $BD-AD$ becomes known. $\tfrac{1}{2}(AB)+\tfrac{1}{2}(BD-AD) = BD$; or the greater segment, adjacent to the greater side. Also,

$$AB-BD = AD.$$

In triangle BDC, Prop. III,

$$BC : BD = R : \text{cos. } B. \qquad (2)$$

In triangle ADC,

$$AC : AD = R : \text{cos. } A. \qquad (3)$$

$$180^\circ - (A+B) = C. \qquad (4)$$

EXAMPLES.

1. Given $BC = 122$, $AC = 107$, and $AB = 98$.

Solution.—1st Method.

Since BC is the longest side, A is the largest angle. We use therefore formula (1).

$$\text{Cos. } \tfrac{1}{2}A = \sqrt{\frac{R^2 s(s-a)}{bc}} \qquad (1)$$

$$S = \tfrac{1}{2}(a+b+c) = 163.5\,; \quad s - a = 41.5.$$

$$\begin{array}{lll}
 & \text{Log. } R^2 = & 20. \\
 & \text{Log. } 163.5 = & 2.213518 \\
 & \text{Log. } 41.5 = & \underline{1.618048} \\
\text{Log. numerator,} & & 23.831566 \\
\text{Log. } b,\ 107 = 2.029384 & & \\
\text{Log. } c,\ \ 98 = \underline{1.991226} & & \underline{4.020610} = \text{Log. denom.} \\
 & \text{To extract root, } & 2)\overline{19.810956} \\
 & \text{Log. cos. } \tfrac{1}{2}A = & 9.905478 = \text{log. } 36^\circ\, 26'\, 48''.
\end{array}$$

Therefore, $A = 72^\circ\, 53'\, 36''$.

By Case II, $122 : \sin. 72^\circ\, 53'\, 36'' = 107 : \sin. B.$

$= 98 : \sin. C.$

$$\begin{array}{ll}
\text{Co. log. } 122 & = 7.913640 \\
\text{Log. sin. } 72^\circ\, 53'\, 36'' & = 9.980348 \\
\text{Log. } 107 & = \underline{2.029384} \\
\text{Log. sin. } B & = 9.923372 = \text{log. sin. } 56^\circ\, 57'\, 20'' = B. \\
 & \\
\text{Co. log. } 122 & = 7.913640 \\
\text{Log. sin. } 72^\circ\, 53'\, 36'' & = 9.980348 \\
\text{Log. } 98 & = \underline{1.991226} \\
\text{Log. sin. } C & = 9.885214 = \text{log. sin. } 50^\circ\, 9'\, 4'' = C.
\end{array}$$

$$\textit{Ans.} \begin{cases} A = 72^\circ\, 53'\, 36'' \\ B = 56^\circ\, 57'\, 20'' \\ C = 50^\circ\ \ 9'\ \ 4''. \end{cases}$$

2. Given $AB = 214$, $AC = 176$, $BC = 200$.

Solution.—2d Method.

$$214 : 376 = 24 : BD - AD. \qquad (1)$$

Log. 376 = 2.575188
Log. 24 = 1.380211
Subtract log. 214 = 2.330414
Log. $(BD - AD)$, = 1.624985; $\therefore BD - AD = 42.168$.
$\frac{1}{2}(214 + 42.168) = 128.084 = BD$, adjacent to BC.
$\frac{1}{2}(214 - 42.168) = 85.916 = AD$.

In triangle BDC,

$$200 : 128.084 = R : \cos. B. \qquad (2)$$

Co. log. 200 = 7.698970
Log. 128.084 = 2.107495
Sum + log. R − 10 = 9.806465 = log. cos. B.
Whence, B = 50° 10′ 37″.

In triangle ADC,

$$176 : 85.916 = R : \cos. A. \qquad (3)$$

Co. log. 176 = 7.754487
Log. 85.916 = 1.934074
Sum + log. R − 10 = 9.688561 = log. cos. A.
Whence, A = 60° 46′ 49″.
180° − 110° 57′ 26″ = 69° 2′ 34″ = C.

Ans. $\begin{cases} A = 60^\circ\ 46'\ 49'' \\ B = 50^\circ\ 10'\ 37'' \\ C = 69^\circ\ 2'\ 34'' \end{cases}$

3. Given $AB = 76.5$, $AC = 51.75$, and $BC = 43.25$.

Ans. $\begin{cases} A = 32^\circ\ 44'\ 31'' \\ B = 40^\circ\ 19'\ 37'' \\ C = 106^\circ\ 55'\ 52'' \end{cases}$

4. Given $AB = 34$, $AC = 48$, and $BC = 30$.

$$Ans. \begin{cases} A,\ 38^\circ\ 20'\ 33'' \\ B,\ 96^\circ\ 58'\ 57'' \\ C,\ 44^\circ\ 40'\ 30'' \end{cases}$$

Having given the theory and practice of the solution of oblique-angled plane triangles, we add the following examples, where the *student* will select and apply the proper methods to be employed.

PRACTICAL PROBLEMS.

Let ABC represent any oblique-angled triangle.

1. Given AB 697, the angle A 81° 30′ 10″, and the angle B 40° 30′ 44″, to find the other parts.

Ans. AC, 534; BC, 813; and $\angle C$, 57° 59′ 6″.

2. If $AC = 720.8$, $\angle A = 70^\circ\ 5'\ 22''$, $\angle B = 59^\circ\ 35'\ 36''$, required the other parts.

Ans. AB, 643.2; BC, 785.8; and $\angle C$, 50° 19′ 2″.

3. Given BC 980.1, the angle A 7° 6′ 26″, and the angle B 106° 2′ 23″, to find the other parts.

Ans. AB, 7283.8; AC, 7613.1; and $\angle C$, 66° 51′ 11″.

4. Given AB 896.2, BC 328.4, and the angle C 113° 45′ 20″, to find the other parts.

Ans. AC, 712; $\angle A$, 19° 35′ 46″; and $\angle B$, 46° 38′ 54″.

5. Given $AC = 4627$, $BC = 5169$, and the angle $A = 70^\circ\ 25'\ 12''$, to find the other parts.

Ans. AB, 4328; $\angle B$, 57° 29′ 56″; and $\angle C$, 52° 4′ 52″.

6. Given AB 793.8, BC 481.6, and AC 500.0, to find the angles.

$$Ans. \begin{cases} \angle\ 35^\circ\ 15'\ 32'';\ \angle B,\ 36^\circ\ 49'\ 18''; \\ \text{and } \angle C,\ 107^\circ\ 55'\ 10'. \end{cases}$$

7. Given AB 100.3, BC 100.3, and AC 100.3, to find the angles.

Ans. The angle A, 60°; the angle B, 60°; and the angle C, 60°.

8. Given AB 92.6, BC 46.3, and AC 71.2, to find the angles.

Ans. $\angle A, 29°17'22''$; $\angle B, 48°47'30''$; and $\angle C$, $101°\ 55'\ 8''$.

9. Given AB 4963, BC 5124, and AC 5621, to find the angles.

Ans. A, $57°\ 30'\ 28''$; $\angle B$, $67°\ 42'\ 36''$; and $\angle C$, $54°\ 46'\ 55''$.

10. Given AB 728.1, BC 614.7, and AC 583.8, to find the angles.

Ans. $\angle A = 54°\ 32'\ 52''$, $\angle B = 50°\ 40'\ 58''$, and $\angle C = 74°\ 46'\ 10''$.

11. Given AB 96.74, BC 88.29, and AC 111.42, to find the angles.

Ans. $\angle A = 46°\ 30'\ 45''$, $\angle B = 76°\ 3'\ 46''$, and $\angle C = 57°\ 25'\ 29''$.

12. Given AB 363.4, BC 148.4, and the angle B $102°\ 18'\ 27''$, to find the other parts.

Ans. $\angle A = 20°\ 9'\ 17''$, the side $AC = 420.8$, and $\angle C = 57°\ 32'\ 16''$

13. Given AB 632, BC 494, and the angle A $20°\ 16'$, to find the other parts, the angle C being acute.

Ans. $\angle C = 26°\ 18'\ 19''$, $\angle B = 133°\ 25'\ 41''$, and $AC = 1035.7$.

14. Given AB 53.9, AC 46.21, and the angle B $58°\ 16'$, to find the other parts.

Ans. $\angle A = 38°\ 58'$, $\angle C = 82°\ 46'$, and $BC = 34.16$.

15. Given AB 2163, BC 1672, and the angle C 112° 18′ 22″, to find the other parts.

Ans. AC, 877.2; $\angle B$, 22° 2′ 16″; and $\angle A$, 45° 39′ 22″.

16. Given AB 496, BC 496, and the angle B 38° 16′ to find the other parts.

Ans. AC, 325.1; $\angle A$, 70° 52′; and $\angle C$, 70° 52′.

17. Given AB 428, the angle C 49° 16′, and $(AC+BC)$ 918, to find the other parts, the angle B being obtuse.

Ans. $\left\{\text{The angle } A = 38° 44′ 48″\text{, the angle } B = 91° 59′ 12″, AC = 564.49\text{, and } BC = 353.5.\right.$

18. Given AC 126, the angle B 29° 46′, and $(AB-BC)$ 43, to find the other parts.

Ans. $\left\{\text{The angle } A = 55° 51′ 32″\text{, the angle } C = 94° 22′ 28″, AB = 253.05\text{, and } BC = 210.054.\right.$

19. Given AB 1269, AC 1837, and the angle A, 53° 16′ 20″, to find the other parts.

Ans. $\left\{\angle B = 83° 23′ 47″, \angle C = 43° 19′ 53″\text{, and } BC = 1482.16.\right.$

SECTION III.

OF SPHERICAL TRIGONOMETRY.

A **Spherical Triangle** contains six parts—three sides and three angles—any three of which being given, the other three may be determined.

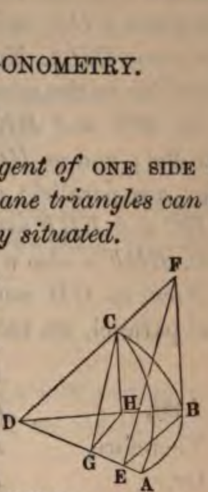
Spherical Trigonometry has for its object to explain the different methods of computing three of the six parts of a spherical triangle, when the other three are given. It may be divided into *Right-angled* Spherical Trigonometry, and

Oblique-angled Spherical Trigonometry; the first treating of the solution of right-angled, and the second of oblique-angled spherical triangles.

RIGHT-ANGLED SPHERICAL TRIGONOMETRY.

PROPOSITION I.

With the sines of the sides, and the tangent of ONE SIDE *of any right-angled spherical triangle, two plane triangles can be formed that will be similar, and similarly situated.*



Let ABC be a spherical triangle, right-angled at B; and let D be the center of the sphere. Because the angle CBA is a right angle, the plane CBD is perpendicular to the plane DBA. From C let fall CH, perpendicular to the plane DBA; and as the plane CBD is perpendicular to the plane DBA, CH will lie in the plane CBD, and be perpendicular to the line DB, and perpendicular to all lines that can be drawn in the plane DBA, from the point H (Def. 2, B. VI. Geom.)

Draw HG perpendicular to DA, and draw GC; GC will lie wholly in the plane CDA, and CHG is a right-angled triangle, right-angled at H.

We will now demonstrate that the angle DGC is a right angle.

The right-angled $\triangle CHG$, gives $CH^2 + HG^2 = CG^2$ (1)

The right-angled $\triangle DGH$, gives $DG^2 + HG^2 = DH^2$ (2)

By subtraction, $CH^2 - DG^2 = CG^2 - DH^2$ (3)

By transposition, $CH^2 + DH^2 = CG^2 + DG^2$ (4)

But the first member of equation (4) is equal to CD^2, because CDH is a right-angled triangle;

Therefore, $CD^2 = CG^2 + DG^2$

Hence, CD is the hypotenuse of the right-angled triangle DGC, (Th. 39, B. I. Geom.)

From the point B, draw BE at right angles to DA, and BF at right angles to DB, in the plane CDB extended; the point F will be in the line DC. Draw EF, and as F is in the plane CDA, and E is in the same plane, the line EF is in the plane CDA. Now we are to prove that the triangle CHG is similar to the triangle BEF, and similarly situated.

As HG and BE are both at right angles to DA, they are parallel; and as HC and BF are both at right angles to DB, they are parallel; and by reason of the parallels, the angles GHC and EBF are equal; but GHC is a right angle; therefore, EBF is also a right angle.

Now, as GH and BE are parallel, and CH and BF are also parallel, we have,

$$DH : DB = HG : BE$$

And, $DH : DB = HC : BF$

Therefore, $HG : BE = HC : BF$ (Th. 6, B. II.),

Or, $HG : HC = BE : BF.$

Here, then, are two triangles, having an angle in the one equal to an angle in the other, and the sides about the equal angles proportional; the two triangles are therefore equiangular (Geom. Cor. 2, Th. 17, B. II.); and they are similarly situated, for their sides make equal angles at H and B with the same line, DB.

Hence the proposition.

SCHOLIUM — By the definition of sines, cosines, and tangents, we perceive that CH is the sine of the arc BC, DH is its cosine, and BF its tangent; CG is the sine of the arc AC, and DG its cosine. Also, BE is the sine of the arc AB, and DE is the cosine of the same arc. With this figure we are prepared to demonstrate the following propositions.

PROPOSITION II.

In any right-angled spherical triangle, the sine of one side is to the tangent of the other side, as radius is to the tangent of the angle adjacent to the first-mentioned side.

Or, the sine of one side is to the tangent of the other side, as *the cotangent of the angle adjacent to the first-mentioned side is to the radius.*

For the sake of brevity, we will represent the angles of the triangle by A, B, C; and the sides or arcs opposite to these angles by a, b, c; that is, a opposite A, etc.

In the right-angled plane triangle EBF, we have,

$$EB : BF = R : \tan.BEF$$

That is, $\sin.c : \tan.a = R : \tan.A$,

which agrees with the first part of the enunciation. By reference to equation (5), Plane Trigonometry, we shall find that

$$\tan.A \cot.A = R^2;$$

therefore, $$\tan.A = \frac{R^2}{\cot.A}.$$

Substituting this value for tangent A, in the preceding proportion, and dividing the last couplet by R, we shall have,

$$\sin.c : \tan.a = 1 : \frac{R}{\cot.A}.$$

Or, $$\sin.c : \tan.a = \cot.A : R.$$

Or, $$R \sin.c = \tan.a \cot.A, \qquad (1)$$

which answers to the second part of the enunciation.

Cor. By changing the construction, drawing the tangent to AB in place of the tangent to BC, and proceeding in a similar manner, we have,

$$R \sin.a = \tan.c \cot.C. \qquad (2)$$

PROPOSITION III.

In any right-angled spherical triangle, the sine of the right angle is to the sine of the hypotenuse, as the sine of either of the other angles is to the sine of the side opposite to that angle.

The sine of 90°, or radius, is designated by R.

In the plane triangle CHG, we have,

$$\sin.CHG : CG = \sin.CGH : CH$$

That is, $$R : \sin.b = \sin.A : \sin.a$$

Or, $$R \sin.a = \sin.b \sin.A. \qquad (3)$$

Cor. By a change in the construction of the figure, drawing a tangent to AB, etc., we shall have,

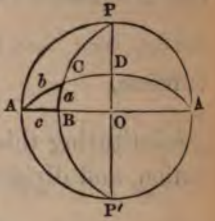
$$R : \sin.b = \sin.C : \sin.c$$

Or,
$$R \sin.c = \sin.b \sin.C. \qquad (4)$$

SCHOLIUM.—Collecting the four equations taken from this and the preceding proposition, we have,

$$\left.\begin{array}{ll}(1) & R \sin.c = \tan.a \cot.A \\ (2) & R \sin.a = \tan.c \cot.C \\ (3) & R \sin.a = \sin.b \sin.A \\ (4) & R \sin.c = \sin.b \sin.C\end{array}\right\}$$

These equations refer to the right-angled triangle, ABC; but the principles are true for any right-angled spherical triangle. Let us apply them to the right-angled triangle, PCD, the complemental triangle to ABC.



Making this application, equation

$$\begin{array}{ll}(1) \text{ becomes } R \sin.CD = \tan.PD \cot.C & (n)\\ (2) \text{ becomes } R \sin.PD = \tan.CD \cot.P & (m)\\ (3) \text{ becomes } R \sin.PD = \sin.PC \sin.C & (o)\\ (4) \text{ becomes } R \sin.CD = \sin.PC \sin.P & (p)\end{array}$$

By observing that $\sin.CD = \cos.AC = \cos.b$, and that $\tan.PD = \cot.DO = \cot.A$, etc.; and by running equations (n), (m), (o), and (p), back into the triangle ABC, we shall have,

$$\left.\begin{array}{ll}(5) & R \cos.b = \cot.A \cot.C \\ (6) & R \cos.A = \cot.b \tan.c \\ (7) & R \cos.A = \cos.a \sin.C \\ (8) & R \cos.b = \cos.a \cos.c\end{array}\right\}$$

By observing equation (6), we find that the second member refers to sides adjacent to the angle A. The same relation holds in respect to the angle C, and gives,

$$(9) \quad R \cos.C = \cot.b. \tan.a.$$

Making the same observations on (7), we infer,

$$(10) \quad R \cos.C = \cos.c \sin.A.$$

Observation 1.—Several of these equations can be deduced geometrically without the least difficulty. For example, take the figure to Proposition I. The parallels in the plane DBA give

$$DB : DH = DE : DG.$$

That is, $R : \cos.a = \cos.c : \cos.b.$

A result identical with equation (8), and in words it is expressed thus: *Radius is to cosine of one side, as the cosine of the other side is to the cosine of the hypotenuse.*

Observation 2.—The equations numbered from (1) to (10) cover every possible case that can occur in right-angled spherical trigonometry; but the combinations are too various to be remembered, and readily applied to practical use.

We can remedy this inconvenience, by taking the *complement* of the hypotenuse, and the *complements* of the two oblique angles, in place of the arcs themselves.

Thus, b is the hypotenuse, and let b' be its complement.

Then, $b+b' = 90°$; or, $b = 90°-b'$; and, $\sin.b = \cos.b'$, $\cos.b = \sin.b'$; $\tan.b = \cot.b'$.

In the same manner, if A' is the complement to A, then $\sin.A = \cos.A'$; $\cos.A = \sin.A'$; and, $\tan.A = \cot.A'$; and similarly, $\sin.C = \cos.C'$; $\cos.C = \sin.C'$; and $\tan.C = \cot.C'$.

Substituting these values for b, A, and C, in the foregoing *ten* equations (a and c remaining the same), we have,

NAPIER'S CIRCULAR PARTS.

(11) $R \sin.c = \tan.a \tan.A'$
(12) $R \sin.a = \tan.c \tan.C'$
(13) $R \sin.a = \cos.b' \cos.A'$
(14) $R \sin.c = \cos.b' \cos.C'$
(15) $R \sin.b' = \tan.A' \tan.C'$
(16) $R \sin.A' = \tan.b' \tan.c$
(17) $R \sin.A' = \cos.a \cos.C'$
(18) $R \sin.b' = \cos.a \cos.c$
(19) $R \sin.C' = \tan.b' \tan.a$
(20) $R \sin.C' = \cos.c' \cos.A'$

Omitting the consideration of the right angle, there are five parts. Each part taken as a middle part, is connected to its adjacent parts by one equation, and to its extreme parts by another equation; therefore ten equations are required for the combinations of all the parts.

These equations are very remarkable, because the first members are all composed of radius into *some sine*, and the second members are all composed of the product of *two tangents*, or *two cosines.*

To condense these equations into words, for the purpose of assisting the memory, we will refer any one of them directly to the right-angled triangle, ABC, in the last figure.

When the right-angle is left out of the question, a right-angled triangle consists of *five* parts—*three* sides, and *two* angles. Let any one of these parts be called a *middle part;* then two other parts will lie adjacent to this part, and two *opposite to it*, that is, separated from it by two other parts.

For instance, take equation (11), and call c the *middle part;* then A' and a will be adjacent parts, and C' and b' opposite parts. Again, take a as a *middle part;* then c and C' will be adjacent parts, and A' and b' will be opposite parts; and thus we may go round the triangle.

Take any equation from (11) to (20), and consider the middle part in the first member of the equation, and we shall find that it corresponds to one of the following *invariable and comprehensive rules.*

1. *The radius into the sine of the middle part is equal to the product of the tangents of the adjacent parts.*

2. *The radius into the sine of the middle part is equal to the product of the cosines of the opposite parts.*

These rules are known as Napier's Rules, because they were first given by that distinguished mathematician, who was also the inventor of logarithms.

In the application of these equations, the *accent* may be omitted if tan. be changed to cotan., sin. to cosin., etc. Thus, if equation (13) were to be employed, it would be written, in the first instance, $R \sin.a = \cos.b' \cos.A'$, to insure conformity to the rule; then, we would change it into $R \sin.a = \sin.b \sin.A$.

REMARK.—We caution the pupil to be very particular to take the *complements* of the hypotenuse, and the complements of the oblique angles.

SOLUTION OF RIGHT-ANGLED SPHERICAL TRIANGLES.

A good general conception of the sphere is essential to a practical knowledge of spherical trigonometry, and this conception is best obtained by the examination of an artificial globe. By tracing out upon its surface the various forms of right-angled and oblique-angled triangles, and viewing them from different points, we may soon acquire the power of making a natural representation of them on paper, which will be found of much assistance in the solution and interpretation of problems.

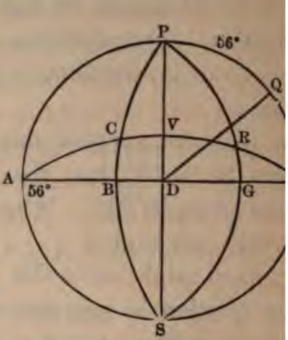
For instance, suppose one side of a right-angled spherical triangle to be 56°, and the angle between this side and the hypotenuse to be 24°. What is the hypotenuse, and what the other side and angle?

A person might solve this problem by the application of the proper equations or proportions, without really comprehending it; that is, without being able to form a distinct notion of the shape of the triangle, and of its relation to the surface of the sphere on which it is situated.

If we refer this triangle to the common geographical globe, the side 56° may be laid off on the equator, or on the meridian. In the first case, the hypotenuse will be the arc of a great circle drawn through one extremity of the side 56°, above or below the equator, and making with it an angle of 24°; the other side will be an arc of a meridian. In the second case, the side 56° falling on a meridian, the hypotenuse will be the arc of a great circle drawn through one extremity of this side, on the right or left of the meridian, and making with it an angle of 24°; the other side will be the arc of a great circle, at right angles to the meridian in which the given side lies.

Generally speaking, the apparent form of a spherical triangle, and consequently the manner of representing it on paper, will differ with the position assumed for the eye in viewing it. From whatever point we look at a sphere, its outline is a perfect circle in the axis of which the eye is uated; and when the eye is, as will be hereafter suppose an infinite distance, this circle will be a great circle of sphere. All great circles of the sphere whose planes through the eye, will seem to be diameters of the circle w represents the outline of the sphere.

We will now suppose the eye to be in the plane of the e tor, and proceed to construct our triangle on paper.



Let the great circle, $PASA'$, represent the outline of the sphere, the diameter AA' the equator, and the diameter PS the central meridian, or the meridian in whose plane the eye is situated. Let $AB = 56^\circ$ represent the given side, and AC, making with AB the angle $BAC = 24^\circ$, the hypotenuse; then will BC, the arc of a meridian, be the other side at right angles to AB, and th angle, ABC, corresponds in all respects to the given trian

Again, measure off 56° from P to Q, draw the arc make the arc $A'G$ equal to 24°, and draw the quadrant P The triangle PQR will also represent the given triang every particular.

We know from the construction that $DV = 24^\circ$ is gr than BC, and that AC is greater than AB, that is, gr than 56°.

In like manner, we know that $A' = 24^\circ$ is greater than and that PR is greater than PQ, because PR is more n equal to $PG = 90^\circ$ than PQ is to $PA = 90$.

For illustration and explanation, we also give the follo example:

In a right-angled spherical triangle there are given hypotenuse equal to 150° 33′ 20″, the angle at the base 27′ 29″, to find the base and the perpendicular. Let A

in the last figure, represent the triangle in which $A'C = 150°$ $33' 20''$, the $\llcorner BA'C = 23° 27' 29''$, and the sides $A'B$ and BC are required.

This problem presents a right-angled spherical triangle, whose base and hypotenuse are each greater than 90°; and in cases of this kind, let the pupil observe, *that the base is greater than the hypotenuse*, and the oblique angle opposite the base, is greater than a right angle. In all cases, a spherical triangle and its supplemental triangle make a *lune*. It is 180° from one pole to its opposite, whatever great circle be traversed. It is 180° along the equator, ABA', and also 180° along the ecliptic ACA'. The lune always gives two triangles; and when the sides of one of them are greater than 90°, we take the triangle having supplemental sides; hence in this case we operate on the triangle ABC.

AC is greater than AB, therefore $A'B$ is greater than the hypotenuse $A'C$.

The $\llcorner ACB$ is less than 90°; therefore the adjacent angle $A'CB$ is greater than 90°, the two together being equal to two right angles.

When a side and opposite angle are both greater or both less than 90°, they are said to be of the *same affection;* when the one is greater and the other less than 90°, they are said to be of *different affection.*

Now, if the two sides of a right-angled spherical triangle are of the *same affection*, the hypotenuse will be less than 90°; and if of *different affection*, the hypotenuse will be greater than 90°.

If, in every instance, we make a natural construction of the figure, and use common judgment, it will be impossible to doubt whether an arc must be taken greater or less than 90°.

We will now solve the triangle ACB. $AC = 180° - 150°$ $33' 20'' = 29° 26' 40''$.

To find BC, we use Eq. (3) or (13), Prop. III., thus:

$$\begin{array}{lr} b,\ \text{sin. } 29^\circ\ 26'\ 40'' & 9.691594 \\ A,\ \text{sin. } 23^\circ\ 27'\ 29'' & 9.599984 \\ \hline a,\ \text{sin. } 11^\circ\ 17'\ \ 7'' & 9.291578 \end{array}$$

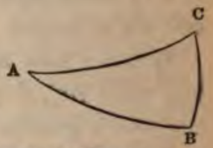
To find AB, we use equation (1) or (11), thus:

$$\begin{array}{lr} a,\ \text{tan. } 11^\circ\ 17'\ \ 7'' & 9.300016 \\ A,\ \text{cot. } 23^\circ\ 27'\ 29'' & 10.362674 \\ \hline c,\ \text{sin. } 27^\circ\ 22'\ 32'' & 9.662690 \\ \qquad 180 & \\ \hline A'B = 152^\circ\ 37'\ 28'' & \end{array}$$

REMARK.—The small letters given in the preceding equations correspond to the sides opposite the angles of like letters.

The student should familiarize himself thoroughly with the rules of Napier by careful solutions of the following

PRACTICAL PROBLEMS IN RIGHT-ANGLED SPHERICAL TRIGONOMETRY.



1. In the right-angled spherical triangle ABC, given $AB = 118^\circ\ 21'\ 4''$, and the angle $A = 23^\circ\ 40'\ 12''$, to find the other parts.

Ans. $\left\{ \begin{array}{l} AC,\ 116^\circ\ 17'\ 55''\text{; the angle } C,\ 100^\circ\ 59'\ 26''\text{; and} \\ BC,\ 21^\circ\ 5'\ 42''. \end{array} \right.$

2. In the right-angled spherical triangle ABC, given AB $53^\circ\ 14'\ 20''$, and the angle A $91^\circ\ 25'\ 53''$, to find the other parts.

Ans. $\left\{ \begin{array}{l} AC,\ 91^\circ\ 4'\ 9''\text{; the angle } C,\ 53^\circ\ 15'\ 8''\text{; and } BC, \\ 91^\circ\ 47'\ 10''. \end{array} \right.$

3. In the right-angled spherical triangle ABC, given AB $102^\circ\ 50'\ 25''$, and the angle A $113^\circ\ 14'\ 37''$, to find the other parts.

Ans. $\left\{ \begin{array}{l} AC,\ 84^\circ\ 51'\ 36''\text{; the angle } C,\ 101^\circ\ 46'\ 57''\text{; and} \\ BC,\ 113^\circ\ 46'\ 27''. \end{array} \right.$

4. In the right-angled spherical triangle ABC, given AB 48° 24′ 16″, and BC 59° 38′ 27″, to find the other parts.

Ans. { AC, 70° 23′ 42″; the angle A, 66° 20′ 40″; and the angle C, 52° 32′ 56″.

5. In the right-angled spherical triangle ABC, given AB 151° 23′ 9″, and BC 16° 35′ 14″, to find the other parts.

Ans. { AC, 147° 16′ 51″; the angle C, 117° 37′ 21″; and the angle A, 31° 52′ 49″.

6. In the right-angled spherical triangle ABC, given AB 73° 4′ 31″, and AC 86° 12′ 15″, to find the other parts.

Ans. { BC, 76° 51′ 20″; the angle A, 77° 24′ 23″; and the angle C, 73° 29′ 40″.

7. In the right-angled spherical triangle ABC, given AC 118° 32′ 12″, and AB 47° 26′ 35″, to find the other parts.

Ans. { BC, 134° 56′ 20″; the angle A, 126° 19′ 2″; and the angle C, 56° 58′ 44″.

8. In the right-angled spherical triangle ABC, given AB 40° 18′ 23″, and AC 100° 3′ 7″, to find the other parts.

Ans. { The angle A, 98° 38′ 53″; the angle C, 41° 4′ 6″; and BC, 103° 13′ 52″.

9. In the right-angled spherical triangle ABC, given AC 61° 3′ 22″, and the angle A 49° 28′ 12″, to find the other parts.

Ans. { AB, 49° 36′ 6″; the angle C, 60° 29′ 20″; and BC, 41° 41′ 32″.

10. In the right-angled spherical triangle ABC, given AB 29° 12′ 50″, and the angle C 37° 26′ 21″, to find the other parts.

Ans. { Ambiguous; the angle A, 65° 27′ 57″, or its supplement; AC, 53° 24′ 13″, or its supplement; BC, 46° 55′ 2″, or its supplement.

11. In the right-angled spherical triangle ABC, given AB

100° 10′ 3″, and the angle *C* 90° 14′ 20″, to find the other parts.

Ans. { *AC*, 100° 9′ 52″, or its supplement; *BC*, 1° 19′ 55″, or its supplement; and the angle *A*, 1° 21′ 12′, or its supplement.

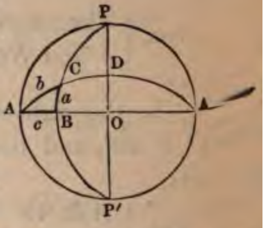
12. In the right-angled spherical triangle *ABC*, given *AB* 54° 21′ 35′, and the angle *C* 61° 2′ 15″, to find the other parts.

Ans. { *BC*, 129° 28′ 28″, or its supplement; *AC*, 111° 44′ 34″, or its supplement; and the angle *A*, 123° 47′ 44″, or its supplement.

13. In the right-angled spherical triangle *ABC*, given *AB* 121° 26′ 25″, and the angle *C* 111° 14′ 37″, to find the other parts.

Ans. { The angle *A*, 136° 0′ 5″, or its supplement; *AC*, 66° 15′ 38″, or its supplement; and *BC*, 140° 30′ 57″, or its supplement.

QUADRANTAL TRIANGLES.



The solution of right-angled spherical triangles includes, also, the solution of *quadrantal* triangles, as may be seen by inspecting the adjoining figure. *When we have one quadrantal triangle we have four, which, with one right-angled triangle, fill up the whole hemisphere.*

To effect the solution of either of the four quadrantal triangles, *APC*, *AP′C*, *A′PC*, or *A′P′C*, it is sufficient to solve the small right-angled spherical triangle *ABC*.

To the half lune *AP′B*, we add the triangle *ABC*, and we have the quadrantal triangle *AP′C;* and by subtracting the same from the equal half lune *APB*, we have the quadrantal triangle *PAC*.

When we have the side *AC*, of the same triangle, we have its supplement *A′C*, which is a side of the triangles *A′PC*,

$P'C$. When we have the side CB, of the small tri-
by adding it to 90° we have $P'C$, a side of the triangle
; and subtracting it from 90°, we have PC, a side of
ıngles APC, and $A'PC$.

PROBLEM I.

quadrantal triangle, there are given the quadrantal
°, *a side adjacent* 42° 21′, *and the angle opposite this*
'e, *equal to* 36° 31′. *Required the other parts.*

ıis enunciation we cannot decide whether the triangle
ır $AP'C$ is the one required, for $AC=42° 21'$ belongs
to both triangles. The angle $APC=AP'C=36° 31'$

ɔperate wholly on the triangle ABC. To find the angle
it the *middle part.* Then,

$$R \cos.CAB = R \sin.PAC = \cot.AC \tan.AB.$$

$$\begin{array}{lcll}
\cot.AC & = & 42^\circ\ 21' & 10.040231 \\
\tan.AB & = & 36^\circ\ 31' & \underline{\ 9.869473} \\
\cos.CAB & = & 35^\circ\ 40'\ 51'' & \ 9.909704 \\
 & & \underline{90^\circ} & \\
PAC & = & 54^\circ\ 19'\ \ 9'' & \\
P'AC & = & 125^\circ\ 40'\ 51'' &
\end{array}$$

nd the angle C, call it the *middle part.* Then,

$$R \cos.ACB = \sin.CAB \cos.AB.$$

$$\begin{array}{lcll}
\sin.CAB & = & 35^\circ\ 40'\ 51'' & 9.765869 \\
\cos.AB & = & 36^\circ\ 31' & \underline{9.905085} \\
\cos.ACB & = & 62^\circ\ \ 2'\ 45'' & 9.570954 \\
 & & \underline{180^\circ} & \\
= A'CP' & = & 117^\circ\ 57'\ 15'' &
\end{array}$$

To find the side BC, call it the *middle part.* Then,

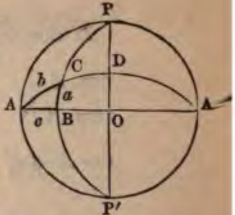
$$R \sin.BC = \tan.AB \cot.ACB.$$

$$\begin{array}{lll}
\tan.AB = & 36^\circ\ 31'\ \ 0'' & 9.869473 \\
\cot.ACB = & 62^\circ\ \ 2'\ 45'' & 9.724835 \\
\hline
\sin.BC = & 23^\circ\ \ 8'\ 11'' & 9.594308 \\
 & 90^\circ & \\
\hline
PC = & 66^\circ\ 51'\ 49'' & \\
P'C = & 113^\circ\ \ 8'\ 11'' &
\end{array}$$

We now have all the sides, and all the angles of the four triangles in question.

PROBLEM II.

In a quadrantal spherical triangle, having given the quadrantal side 90°, *an adjacent side* 115° 9′, *and the included angle* 115° 55′, *to find the other parts.*



This enunciation clearly points out the particular triangle $A'P'C$. $A'P' = 90^\circ$; and conceive $A'C = 115^\circ\ 9'$. Then the angle $P'A'C = 115^\circ\ 55' = P'D$.

From the angle $P'A'C$ take 90°, or $P'A'B$, and the remainder is the angle $OA'D = BAC = 25^\circ\ 55'$.

We here again operate on the triangle ABC. $A'C$, taken from 180°, gives $64^\circ\ 51' = AC$.

To find BC, we call it the *middle part.* Then,

$$R \sin.BC = \sin.AC \sin.BAC.$$

$$\begin{array}{lll}
\sin.AC = & 64^\circ\ 51' & 9.956744 \\
\sin.BAC = & 25^\circ\ 55' & 9.640544 \\
\hline
\sin.BC = & 23^\circ\ 18'\ 19'' & 9.597288 \\
 & 90^\circ & \\
\hline
P'C = & 113^\circ\ 18'\ 19'' &
\end{array}$$

To find AB, we call it the *middle part*. Then,

$$R \sin.AB = \tan.BC \cot.BAC.$$

$$\begin{array}{lcll}
\tan.BC & = & 23^\circ\ 18'\ 19'' & 9.634251 \\
\cot.BAC & = & 25^\circ\ 55' & 9.313423 \\
\hline
\sin.AB & = & 62^\circ\ 26'\ 8'' & 8.947674 \\
 & & 180^\circ & \\
\hline
A'B & = & 117^\circ\ 33'\ 52'' & = \text{the angle } A'P'C.
\end{array}$$

To find the angle C, we call it the *middle part*. Then,

$$R \cos.C = \cot.AC \tan.BC.$$

$$\begin{array}{lcll}
\cot.AC & = & 64^\circ\ 51' & 9.671634 \\
\tan.BC & = & 23^\circ\ 18'\ 19'' & 9.634251 \\
\hline
\cos.C & = & 78^\circ & 9.305885 \\
 & & 180^\circ\ 19'\ 53'' & \\
\hline
P'CA' & = & 101^\circ\ 40'\ 7'' &
\end{array}$$

$$\left.\begin{array}{rl}
\text{Thus, we have found the side } P'C = & 113^\circ\ 18'\ 19'' \\
\text{The angle } A'P'C = & 117^\circ\ 33'\ 52'' \\
\text{“} \quad P'CA' = & 101^\circ\ 40'\ 7''
\end{array}\right\} \textit{Ans.}$$

PRACTICAL PROBLEMS.

1. In a quadrantal triangle, given the quadrantal side, 90°, a side adjacent, 67° 3′, and the included angle, 49° 18′, to find the other parts.

Ans. The remaining side is 53° 5′ 44″; the angle opposite the quadrantal side, 108° 32′ 29″; and the remaining angle, 60° 48′ 54″.

2. In a quadrantal triangle, given the quadrantal side, 90°, one angle adjacent, 118° 40′ 36″, and the side opposite this last-mentioned angle, 113° 2′ 28″, to find the other parts.

Ans. The remaining side is 54° 38′ 57″; the angle opposite, 51° 2′ 35″; and the angle opposite the quadrantal side, 72° 26′ 21″.

3. In a quadrantal triangle, given the quadrantal side, 90°, and the two adjacent angles, one 69° 13′ 46″, the other 72° 12′ 4″, to find the other parts.

Ans. One of the remaining sides is 70° 8′ 39″, the other is 73° 17′ 29″, and the angle opposite the quadrantal side is 96° 13′ 23″.

4. In a quadrantal triangle, given the quadrantal side, 90°, one adjacent side, 86° 14′ 40″, and the angle opposite to that side, 37° 12′ 20″, to find the other parts.

Ans. The remaining side is 4° 43′ 2″; the angle opposite, 2° 51′ 23″; and the angle opposite the quadrantal side, 142° 42′ 2″.

5. In a quadrantal triangle, given the quadrantal side, 90°, and the other two sides, one 118° 32′ 16″, the other 67° 48′ 40″, to find the other parts—the three angles.

Ans. The angles are 64° 32′ 21″, 121° 3′ 40″, and 77° 11′ 6″; the greater angle opposite the greater side, of course.

6. In a quadrantal triangle, given the quadrantal side, 90°, the angle opposite, 104° 41′ 17″, and one adjacent side, 73° 21′ 6″, to find the other parts.

Ans. Remaining side, 49° 42′ 16″; remaining angles, 47° 32′ 38″, and 67° 56′ 13″.

OBLIQUE-ANGLED SPHERICAL TRIGONOMETRY.

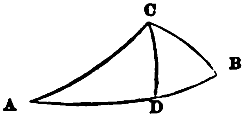
The preceding investigations have had reference to right-angled spherical trigonometry only, but the application of these principles covers oblique-angled trigonometry also; for, every oblique-angled spherical triangle may be considered as made up of the sum or difference of two right-angled spherical triangles. With this explanatory remark, we give

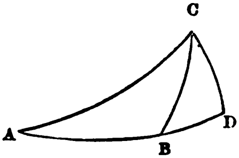
PROPOSITION I.

In all spherical triangles, the sines of the sides are to each other as the sines of the angles opposite to them.

This was proved in relation to right-angled triangles in Prop. III., Sec. 3, and we now apply the principle to oblique-angled triangles.

Let ABC be the triangle, and let CD be perpendicular to AB, or to AB produced.





Then, by Prop. III, R. A. Spher, Trig., we have,

$$R : \sin.AC = \sin.A : \sin.CD.$$

Also,

$$\sin.CB : R = \sin.CD : \sin.B.$$

By multiplying these two proportions together, term by term, and omitting the common factor R in the first couplet, and the common factor, $\sin.CD$, in the second, we have

$$\sin.CB : \sin.AC = \sin.A : \sin.B.$$

PROPOSITION II.

In any spherical triangle, if an arc of a great circle be let [illegible]l from any angle perpendicular to the opposite side as a base, or to the base produced, the cosines of the other two sides will be to each other as the cosines of the segments of the base.

By the application of equation 8, (R. A. Spher. Trig.), to the last figure, we have,

$$R \cos.AC = \cos.AD \cos.DC$$

Similarly, $$R \cos.BC = \cos.DC \cos.BD$$

Dividing one of these equations by the other, omitting common factors in numerators and denominators, we have

$$\frac{\cos.AC}{\cos.BC} = \frac{\cos.AD}{\cos.BD}$$

Or, $\cos.AC : \cos.BC = \cos.AD : \cos.BD.$

PROPOSITION III.

If from any angle of a spherical triangle a perpendicular be let fall on the base, or on the base produced, the tangents of the segments of the base will be reciprocally proportional to *the cotangents of the segments of the angle.*

By the application of Equation 2, (R. A. Spher. Trig.), to the last figure, we have,

$$R \sin.CD = \tan.AD \cot.ACD.$$

Similarly, $R \sin.CD = \tan.BD \cot.BCD.$

Therefore, by equality,

$$\tan.AD \cot.ACD = \tan.BD \cot.BCD$$

Or, $\tan.AD : \tan.BD = \cot.BCD : \cot.ACD.$

PROPOSITION IV.

The same construction remaining, the cosines of the angles at the extremities of the segments of the base are to each other as the sines of the segments of the opposite angle.

Equation 7, (R. A. Spher. Trig.), applied to the triangle ACD, gives

$$R \cos.A = \cos.CD \sin.ACD \qquad (s)$$

Also, $R \cos.B = \cos.CD \sin.BCD \qquad (t)$

Dividing equation (s) by (t), gives

$$\frac{\cos.A}{\cos.B} = \frac{\sin.ACD}{\sin.BCD}$$

Or, $$\cos.B : \cos.A = \sin.BCD : \sin.ACD.$$

PROPOSITION V.

The same construction remaining, the sines of the segments of the base are to each other as the cotangents of the adjacent angles.

Equation 1, (R. A. Spher. Trig.), applied to the triangle ACD, gives

$$R \sin.AD = \tan.CD \cot.A \qquad (s)$$

Similarly, $$R \sin.BD = \tan.CD \cot.B \qquad (t)$$

Dividing (s) by (t), gives

$$\frac{\sin.AD}{\sin.BD} = \frac{\cot.A}{\cot.B}$$

Or, $$\sin.BD : \sin.AD = \cot.B : \cot.A.$$

PROPOSITION VI.

The same construction remaining, the cotangents of the two sides are to each other as the cosines of the segments of the angle.

Equation 9, (R. A. Spher. Trig.), applied to the triangle ACD, gives

$$R \cos.ACD = \cot.AC \tan.CD \qquad (s)$$

Similarly, $$R \cos.BCD = \cot.BC \tan.CD \qquad (t)$$

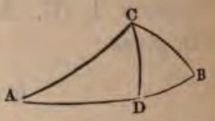
Dividing (s) by (t), gives

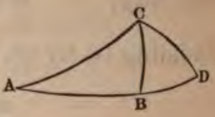
$$\frac{\cos.ACD}{\cos.BCD}=\frac{\cot.AC}{\cot.BC}$$

Or, $\qquad \cot.AC : \cot.BC = \cos.ACD : \cos.BCD.$

PROPOSITION VII.

The cosine of any side of a spherical triangle is equal to the product of the cosines of the other two sides, plus the product of the sines of those sides multivolied by the cosine of the included angle.





Let ABC be a spherical triangle, and CD a perpendicular from the angle C to the side AB, or to the side AB produced. Then, by Prop. II.,

$$\cos.AC : \cos.CB = \cos.AD : \cos.BD \qquad (1)$$

When CD falls within the triangle,

$$BD = (AB-AD);$$

and when CD falls without the triangle,

$$BD = (AD-AB).$$

Hence, $\qquad \cos.BD = \cos.(AD-AB).$

Now, $\qquad \cos.(AB-AD) = \cos.(AD-AB),$

because each of them is equal to

$\cos.AB \cos.AD+\sin.AB \sin.AD$, (Eq. 10, Prop. II., Plane Trig.).

This value of $\cos.BD$, put in proportion (1), gives

$$\cos.AC : \cos.CB = \cos.AD : \cos.AB \cos.AD+\sin.AB \sin.AD \qquad (2)$$

Dividing the last couplet of proportion (2) by $\cos.AD$, observing that

$$\frac{\sin.AD}{\cos.AD}=\tan.AD,$$

d we have

$$\cos.AC : \cos.CB = 1 : \cos.AB + \sin.AB \tan.AD \qquad (3)$$

By applying equation 6, (R. A. Spher. Trig.), to the triangle CD, taking the radius as unity, we have

$$\cos.A = \cot.AC \tan.AD \qquad (k)$$

But, $\tan.AC \cot.AC = 1$, (Eq. 5., Plane Trig.) (l)

Multiply equation (k) by $\tan.AC$, observing equation (l), d we have

$$\tan.AC \cos.A = \tan.AD.$$

Substituting this value of $\tan.AD$ in proportion (3), we ve

$$s.AC : \cos.CB = 1 : \cos.AB + \sin.AB \tan.AC \cos.A \qquad (4)$$

Multiplying extremes and means, gives

$$s.CB = \cos.AC \cos.AB + \sin.AB (\cos.AC \tan.AC) \cos.A.$$

But, $\tan.AC = \frac{\sin.AC}{\cos.AC}$; or, $\cos.AC \tan.AC = \sin.AC$.

Therefore,

$$\cos.CB = \cos.AC \cos.AB + \sin.AB \sin.AC \cos.A.$$

f the sides opposite the angles, A, B, and C, be respectively resented by a, b, and c, this equation becomes,

$$\cos.a = \cos.b \cos.c + \sin.b \sin.c \cos.A.$$

This formula conforms to the enunciation in respect to the e a. Interchanging b and a and writing B for A, in the t equation, we get the formula for $\cos.b$, which is,

$$\cos.b = \cos.a \cos.c + \sin.a \sin.c \cos.B.$$

Interchanging c and a and writing C for A, we get the mula for $\cos.c$, which is,

$$\cos.c = \cos.a \cos.b + \sin.a \sin.b \cos.C.$$

Hence, we have the three symmetrical formulæ:

$$\left.\begin{array}{l} \cos.a = \cos.b \cos.c + \sin.b \sin.c \cos.A \\ \cos.b = \cos.a \cos.c + \sin.a \sin.c \cos.B \\ \cos.c = \cos.a \cos.b + \sin.a \sin.b \cos.C \end{array}\right\} \qquad (S)$$

From these, by simple transposition and division, we deduce the following formulæ for the cosines of the angles of any spherical triangle, viz.:

$$\left.\begin{aligned}\cos.A &= \frac{\cos.a-\cos.b\ \cos.c}{\sin.b\ \sin.c}\\ \cos.B &= \frac{\cos.b-\cos.a\ \cos.c}{\sin.a\ \sin.c}\\ \cos.C &= \frac{\cos.c-\cos.a\ \cos.b}{\sin.a\ \sin.b}\end{aligned}\right\}\qquad (S')$$

By means of these equations we can find the cosine of any of the three angles of a spherical triangle in terms of the functions of the sides; but in their present form they are not suited for the employment of logarithms, and we should be compelled to use a table of natural sines and cosines, and to perform tedious numerical operations, to obtain the value of the angle.

They are, however, by the following process, transformed into others well adapted to the use of logarithms.

In Eq. 34, Plane Trig., we have

$$1+\cos.A = 2\cos.^2\tfrac{1}{2}A.$$

Therefore, $2\cos.^2\frac{1}{2}A = 1+\dfrac{\cos.a-\cos.b\cos.c}{\sin.b\ \sin.c}$; or,

$$2\cos.^2\tfrac{1}{2}A = \frac{(\sin.b\ \sin.c-\cos.b\ \cos.c)+\cos.a}{\sin.b\ \sin.c}\qquad (m).$$

But by Equation 9, Plane Trigonometry,

$$\cos.\,(b+c) = \cos.b\ \cos.c-\sin.b\ \sin.c,$$

Or, $\sin.b\ \sin.c-\cos.b\ \cos.c = -\cos.\,(b+c).$

Substituting for the first member of this equation, as found in (Eq. m), its value, $-\cos.\,(b+c)$, we have

$$2\cos.^2\tfrac{1}{2}A = \frac{\cos.a-\cos.\,(b+c)}{\sin.b\ \sin.c}.$$

Considering $(b+c)$ as one arc, and then making application of equation (18), Plane Trigonometry, we have,

$$2\cos.^2\tfrac{1}{2}A = \frac{2\sin.\left(\frac{a+b+c}{2}\right)\sin.\left(\frac{b+c-a}{2}\right)}{\sin.b\ \sin.c}.$$

But, $\frac{b+c-a}{2} = \frac{b+c+a}{2} - a$; and if we put S to represent $\frac{b+c+a}{2}$, we shall have,

$$\cos.^2\frac{A}{2} = \frac{\sin.S\ \sin.(S-a)}{\sin.b\ \sin.c}.$$

Or, $$\cos.\frac{A}{2} = \sqrt{\frac{\sin.S\ \sin.(S-a)}{\sin.b\ \sin.c}}.$$

The second member of this equation gives the value of the cosine when the radius is unity. To a greater radius, the cosine would be greater; and in just the same proportion as the radius increases, all the trigonometrical lines increase; therefore, to adapt the above equation to our tables where the radius is R, we must write R in the second member, as a factor; and if we put it under the radical sign, we must write R^2.

For the other angles, we shall have precisely similar equations.

That is, $$\left.\begin{aligned}\cos.\frac{A}{2} &= \sqrt{\frac{R^2\sin.S\ \sin.(S-a)}{\sin.b\ \sin.c}}\\ \cos.\frac{B}{2} &= \sqrt{\frac{R^2\sin.S\ \sin.(S-b)}{\sin.a\ \sin.c}}\\ \cos.\frac{C}{2} &= \sqrt{\frac{R^2\sin.S\ \sin.(S-c)}{\sin.a\ \sin.b}}\end{aligned}\right\}\quad (T)$$

To deduce from formulæ (S), formulæ for the sines of the half of each of the angles of a spherical triangle, we proceed as follows:

From Eq. 35, Plane Trig., we have

$$2\sin.^2\tfrac{1}{2}A = 1-\cos.A.$$

Substituting the value of cos. A, taken from formulæ (S), and we have,

$$2\ \sin.^2 \tfrac{1}{2}A = 1 - \frac{\cos.a - \cos.b\ \cos.c}{\sin.b\ \sin.c} =$$
$$\frac{(\sin.b\ \sin.c + \cos.b\ \cos.c) - \cos.a}{\sin.b\ \sin.c}. \quad (o)$$

But, $\cos.\ (b \sim c) = \sin.b\ \sin.c + \cos.b\ \cos.c$, (Eq. 10, Plane Trig.)

This equation reduces equation (o) to

$$2\ \sin.^2 \tfrac{1}{2}A = \frac{\cos.\ (b \sim c) - \cos.a}{\sin.b\ \sin.c}.$$

Considering $(b \sim c)$ as a single arc, and applying equation 18, Plane Trig., we have

$$2\ \sin.^2 \tfrac{1}{2}A = \frac{2\ \sin.\left(\frac{a+b-c}{2}\right) \sin.\left(\frac{a+c-b}{2}\right)}{\sin.b\ \sin.c}. \quad (o')$$

But, $\frac{a+b-c}{2} = \frac{a+b+c}{2} - c = S - c$, if we put $S = \frac{a+b+c}{2}$.

Also, $\frac{a+c-b}{2} = \frac{a+b+c}{2} - b = S - b$.

Dividing equation (o') by 2, and making these substitutions, we have,

$$\sin.^2 \tfrac{1}{2}A = \frac{\sin.\ (S-c)\ \sin.\ (S-b)}{\sin.b\ \sin.c},$$

when radius is unity.

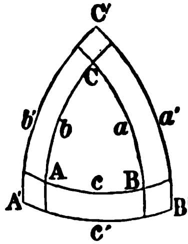
When radius is R, we have

$$\left.\begin{array}{ll} & \sin.\tfrac{1}{2}A = \sqrt{\dfrac{R^2 \sin.\ (S-c)\ \sin.\ (S-b)}{\sin.b\ \sin.c}} \\ \text{Similarly,} & \sin.\tfrac{1}{2}B = \sqrt{\dfrac{R^2 \sin.(S-a)\ \sin.(S-c)}{\sin.a\ \sin.c}} \\ \text{And,} & \sin.\tfrac{1}{2}C = \sqrt{\dfrac{R^2 \sin.(S-a)\ \sin.(S-b)}{\sin.a\ \sin.b}} \end{array}\right\} (U)$$

The preceding equations are now adapted to our tables. We shall show the application of these formulæ, and those in group (T), hereafter.

PROPOSITION VIII.

The cosine of any of the angles of a spherical triangle, is equal to the product of the sines of the other two angles multiplied by the cosine of the included side, minus the product of the cosines of these other two angles.



Let ABC be a spherical triangle, and $A'B'C'$ its supplemental or polar triangle, the angles of the first being denoted by A, B, and C, and the sides opposite these angles by a, b, c, respectively; A', B', C', a', b', c', denoting the angles and corresponding sides of the second.

By Prop. VI., Spherical Geometry, we have the following relations between the sides and angles of these two triangles.

$$A' = 180°-a, \quad B' = 180°-b, \quad C' = 180°-c;$$
$$a' = 180°-A, \quad b' = 180°-B, \quad c' = 180°-C.$$

The first of formulæ (S), Prop. VII., when applied to the polar triangle, gives

$$\cos.a' = \cos.b' \cos.c' + \sin.b' \sin.c' \cos.A'; \qquad (1)$$

which, by substituting the values of a', b', c', and A', becomes

$$\cos.(180°-A) = \cos.(180°-B)\cos.(180°-C) + \sin.(180°-B)\sin.(180°-C)\cos.(180°-a). \qquad (2)$$

But,

$$\cos.(180°-A) = -\cos.A, \text{ etc.}; \ \sin.(180°-B) = \sin.B, \text{ etc.};$$

and placing these values for their equals in eq. (2), and changing the signs of both members of the resulting equation, we get

$$\cos.A = \sin.B \sin.C \cos.a - \cos.B \cos.C,$$

which agrees with the enunciation.

By treating the other two of formulæ (S), Prop. VII., in the same manner, we should obtain similar values for the cosines of the other two angles of the triangle *ABC;* or we may get them more easily by a simple permutation of the letters A, B, C, a, etc.

Hence, we have the three equations

$$\left.\begin{aligned}\cos.A &= \sin.B \sin.C \cos.a - \cos.B \cos.C\\ \cos.B &= \sin.A \sin.C \cos.b - \cos.A \cos.C\\ \cos.C &= \sin.A \sin.B \cos.c - \cos.A \cos.B\end{aligned}\right\} \quad (V)$$

By transposition and division, these equations become

$$\begin{aligned}\cos.a &= \frac{\cos.A + \cos.B \cos.C}{\sin.B \sin.C} \qquad (3)\\ \cos.b &= \frac{\cos.B + \cos.A \cos.C}{\sin.A \sin.C}\\ \cos.c &= \frac{\cos.C + \cos.A \cos.B}{\sin.A \sin.B}\end{aligned}$$

From these we can find formulæ to express the sine or the cosine of one half of the side of a spherical triangle, in terms of the functions of its angles; thus:

Add 1 to each member of eq. (3), and we have

$$1 + \cos.a = \frac{\cos.A + \cos.B \cos.C + \sin.B \sin.C}{\sin.B \sin.C} =$$

$$\frac{\cos.A + \cos.(B - C)}{\sin.B \sin.C}$$

But, $\quad 1 + \cos.a = 2 \cos.^2 \tfrac{1}{2}a$; hence,

$$2 \cos.^2 \tfrac{1}{2}a = \frac{\cos.A + \cos.(B - C)}{\sin.B \sin.C}$$

and since $\cos.A+\cos.(B-C) = 2\cos.\frac{1}{2}(A+B-C)\cos.\frac{1}{2}(A+C-B)$, (Eq. 17, Plane Trig.), we have

$$2\cos.^2\tfrac{1}{2}a = \frac{2\cos.\frac{1}{2}(A+B-C)\cos.\frac{1}{2}(A+C-B)}{\sin.B\sin.C}$$

Make $A+B+C = 2S$; then $A+B-C = 2S-2C$, $A+C-B = 2S-2B$, $\frac{1}{2}(A+B-C) = S-C$, and $\frac{1}{2}(A+C-B = S-B$; whence

$$2\cos.^2\tfrac{1}{2}a = \frac{2\cos.(S-C)\cos.(S-B)}{\sin.B\sin.C}$$

$$\left.\begin{array}{lr} \text{or,} & \cos.\tfrac{1}{2}a = \sqrt{\dfrac{\cos.(S-C)\cos.(S-B)}{\sin.B\sin.C}} \\ \text{Similarly,} & \cos.\tfrac{1}{2}b = \sqrt{\dfrac{\cos.(S-A)\cos.(S-C)}{\sin.A\sin.C}} \\ \text{and,} & \cos.\tfrac{1}{2}c = \sqrt{\dfrac{\cos.(S-A)\cos.(S-B)}{\sin.A\sin.B}} \end{array}\right\} \quad (V')$$

To find the $\sin.\frac{1}{2}a$ in terms of the functions of the angles, we must subtract each member of eq. (3) from 1, by which we get

$$1-\cos.a = 1-\frac{\cos.A+\cos.B\cos.C}{\sin.B\sin.C}.$$

But, $1-\cos.a = 2\sin.^2\frac{1}{2}a$; hence we have,

$$2\sin.^2\tfrac{1}{2}a = \frac{(\sin.B\sin.C-\cos.B\cos.C)-\cos.A}{\sin.B\sin.C}.$$

Operating upon this in a manner analogous to that by which $\cos.\frac{1}{2}a$ was found, we get,

$$\left.\begin{array}{l} \sin.\tfrac{1}{2}a = \left\{\dfrac{-\cos.S\cos.(S-A)}{\sin.B\sin.C}\right\}^{\frac{1}{2}} \\ \sin.\tfrac{1}{2}b = \left\{\dfrac{-\cos.S\cos.(S-B)}{\sin.A\sin.C}\right\}^{\frac{1}{2}} \\ \sin.\tfrac{1}{2}c = \left\{\dfrac{-\cos.S\cos.(S-C)}{\sin.A\sin.B}\right\}^{\frac{1}{2}} \end{array}\right\} \quad (W')$$

If the first equation in (W) be divided by the first in (V'), we shall have,

$$\tan.\tfrac{1}{2}a = \left\{ \frac{-\cos.S \cos.(S-A)}{\cos.(S-B)\cos.(S-C)} \right\}^{\frac{1}{2}}$$

And corresponding expressions may be obtained for $\tan.\tfrac{1}{2}b$ and $\tan.\tfrac{1}{2}c$.

SOLUTION OF OBLIQUE-ANGLED SPHERICAL TRIANGLES.

All cases of oblique-angled spherical trigonometry may be solved by right-angled Trigonometry, except two; because every oblique-angled spherical triangle is composed of the sum, or the difference, of two right-angled spherical triangles.

When a side and two of the angles, or *an angle and two of the sides are given*, to find the other parts, conform to the following directions:

Let a perpendicular be drawn from an extremity of a given side, and opposite a given angle or its supplement; this will form two right-angled spherical triangles; and one of them will have its hypotenuse and one of its adjacent angles given, from which all its other parts can be computed; and some of these parts will become as known parts to the other triangle, from which all its parts can be computed.

To facilitate these computations, we here give a summary of the practical truths demonstrated in the foregoing propositions.

1. *The sines of the sides of spherical triangles are proportional to the sines of their opposite angles.*

2. *The sines of the segments of the bases, made by a perpendicular from the opposite angle, are proportional to the cotangents of their adjacent angles.*

3. *The cosines of the segments of the base are proportional to the cosines of the adjacent sides of the triangle.*

4. *The tangents of the segments of the base are reciprocally*

proportional to the cotangents of the segments of the vertical angle.

5. *The cosines of the angles at the base are proportional to the sines of the corresponding segments of the vertical angle.*

6. *The cosines of the segments of the vertical angle are proportional to the cotangents of the adjoining sides of the triangle.*

The two cases in which right-angled spherical triangles are not used, are,

1st. When the three sides are given to find the angles; and,

2d. When the three angles are given to find the sides.

The first of these cases is the most important of all, and for that reason great attention has been given to it, and two series of equations, (T and U, Prop. VII.), have been deduced to facilitate its solution.

As heretofore, let ABC represent any triangle whose angles are denoted by A, B, and C, and sides by a, b, and c; the side a being opposite $\angle A$, the side b opposite $\angle B$, etc.

EXAMPLES.

1. In the triangle ABC, $a = 70^\circ\ 4'\ 18''$; $b = 63^\circ\ 21'\ 27''$; and c, $59^\circ\ 16'\ 23''$; required the angle A.

The formula for this is the first equation in group (T, Prop. VII.), which is

$$\cos.\frac{A}{2}=\left(\frac{R^2\sin.S\sin.(S-a)}{\sin.b.\ \sin.c}\right)^{\frac{1}{2}}.$$

We write the second member of this equation thus:

$$\sqrt{\left(\frac{R}{\sin.b}\right)\left(\frac{R}{\sin.c}\right)(\sin.S)\sin.(S-a)},$$

showing four distinct factors under the radical.

The logarithm corresponding to $\frac{R}{\sin.b}$ is that of sin.b subtracted from 10; and of $\frac{R}{\sin.c}$ is that of sin.c subtracted from 10, which we call *sin.complement.*

$$\begin{array}{rlll}
BC = a = & 70^\circ\ \ 4'\ 18'' & & \\
AB = c = & 59^\circ\ 16'\ 23'' & \text{sin.com.} & .065697 \\
AC = b = & \underline{63^\circ\ 21'\ 27''} & \text{sin.com.} & .048749 \\
 & 2)\underline{192^\circ\ 42'\ \ 8''} & & \\
S = & 96^\circ\ 21'\ \ 4'' & \text{sin.} & 9.997326 \\
S-a = & 26^\circ\ 16'\ 46'' & \text{sin.} & \underline{9.646158} \\
 & & & 2)\underline{19.757930} \\
\frac{1}{2}A = & 40^\circ\ 49'\ 10'' & \text{cos.} & 9.878965 \\
 & \underline{\qquad\qquad\quad 2} & & \\
A = & 81^\circ\ 38'\ 20'' & &
\end{array}$$

When we apply the equation to find the angle A, we writ a first at the top of the column: when we apply the equatio to find the angle B, we write b at the top of the colum Thus,

To find the angle B.

$$\cos\tfrac{1}{2}B = \sqrt{\frac{R^2\sin.S\,\sin.(S-b)}{\sin.a\,\sin.c}}$$

$$= \sqrt{\left(\frac{R}{\sin.a}\right)\left(\frac{R}{\sin.c}\right)(\sin.S)\,\sin.(S-b)}$$

$$\begin{array}{rlll}
b = & 63^\circ\ 21'\ 27'' & & \\
c = & 59^\circ\ 16'\ 23'' & \text{sin.com.} & .065697 \\
a = & \underline{70^\circ\ \ 4'\ 18''} & \text{sin.com.} & .026875 \\
 & 2)\underline{192^\circ\ 42'\ \ 8''} & & \\
S = & 96^\circ\ 21'\ \ 4'' & \text{sin.} & 9.997326 \\
S-b = & 32^\circ\ 59'\ 37'' & \text{sin.} & \underline{9.736034} \\
 & & & 2)\underline{19.825872} \\
\frac{1}{2}B = & 35^\circ\ \ 4'\ 49'' & \text{cos.} & 9.912936 \\
 & \underline{\qquad\qquad\quad 2} & & \\
B = & 70^\circ\ \ 9'\ 38'' & &
\end{array}$$

By the other equation in formulæ (T, Prop. VII.), we can find the angle C; but, for the sake of variety, we will find the angle C by the application of the third equation in formulæ (U, Prop. VII.).

$$\sin.\tfrac{1}{2}C=\sqrt{\frac{R^2\sin.(S-b)\sin.(S-a)}{\sin.b\ \sin.a}}$$

$$=\sqrt{\left(\frac{R}{\sin.b}\right)\left(\frac{R}{\sin.a}\right)\sin.(S-b)\sin.(S-a)}$$

$$\begin{array}{rlll}
c= & 59^\circ\ 16'\ 23'' & & \\
a= & 70^\circ\ \ 4'\ 18'' & \text{sin. com.} & .026817 \\
b= & \underline{63^\circ\ 21'\ 27''} & \text{sin. com.} & .048479 \\
 & 2)\underline{192^\circ\ 42'\ \ 8''} & & \\
S= & 96^\circ\ 21'\ \ 4'' & & \\
S-a= & 26^\circ\ 16'\ 46'' & \text{sin.} & 9.646158 \\
S-b= & 32^\circ\ 59'\ 37'' & \text{sin.} & \underline{9.736034} \\
 & & & 2)\underline{19.457488} \\
\tfrac{1}{2}C= & 32^\circ\ 23'\ 17'' & \text{sin.} & 9.778744 \\
 & \underline{\qquad\qquad 2} & & \\
C= & 64^\circ\ 46'\ 34'' & &
\end{array}$$

To show the harmony and practical utility of these two sets of equations, we will find the angle A from the equation

$$\sin.\tfrac{1}{2}A=\sqrt{\left(\frac{R}{\sin.b}\right)\left(\frac{R}{\sin.c}\right)\sin.(S-b)\ \sin.(S-c)}.$$

$$\begin{array}{rlll}
a= & 70^\circ\ \ 4'\ 18'' & & \\
b= & 63^\circ\ 21'\ 27'' & \text{sin.com.} & .048749 \\
c= & \underline{59^\circ\ 16'\ 23''} & \text{sin.com.} & .065697 \\
 & 2)\underline{192^\circ\ 42'\ \ 8''} & & \\
S= & 96^\circ\ 21'\ \ 4'' & & \\
S-b= & 32^\circ\ 59'\ 37'' & \text{sin.} & 9.736034 \\
S-c= & 37^\circ\ \ 4'\ 41'' & \text{sin.} & \underline{9.780247} \\
 & & & 2)\underline{19.630727} \\
\tfrac{1}{2}A= & 40^\circ\ 49'\ 10'' & \text{sin.} & 9.815363 \\
 & \underline{\qquad\qquad 2} & & \\
A= & 81^\circ\ 38'\ 20'' & &
\end{array}$$

2. In a spherical triangle *ABC*, given the angle *A*, 38° 1 18″; the angle *B*, 48° 0′ 10″; and the angle *C*, 121° 8′ 6″; find the sides *a*, *b*, *c*.

By passing to the triangle polar to this, we have, (Pro VI., Spherical Geometry),

$A = 38° 19′ 18″$; supplement 141° 40′ 42″
$B = 48° 0′ 10″$; supplement 131° 59′ 50″
$C = 121° 8′ 6″$; supplement 58° 51′ 54″

We now find the angles to the spherical triangle, the sid of which are these supplements.

Thus,	141° 40′ 42″		
	131° 59′ 50″	sin.com.	.128909
	58° 51′ 54″	sin.com.	.067551
	2) 332° 32′ 26″		
	166° 16′ 13″	sin.	9.375375
	24° 35′ 31″	sin.	9.619253
			2) 19.191088
	66° 47′ 37½″	cos.	9.595544
	2		
Angle =	133° 35′ 15″		
Supplement =	46° 24′ 45″		

Therefore *a*, of original triangle = 46° 24′ 45″ In same manner, we find $b = 60° 14′ 25″$, and $c = 89° 1′ 14″$

It is perhaps better to avoid this indirect process of c puting the sides of a spherical triangle when the angles given, by the application of the equations in group *V′* or Prop. VIII., O. A. Spher. Trig. We will illustrate their by applying the second equation in group (*W*), for comput the side *b*. This equation is

$$\sin.\tfrac{1}{2}b = \left(\frac{-\cos.S\ \cos.(S-B)}{\sin.A\ \sin.C}\right)^{\frac{1}{2}}$$

$$\begin{array}{rl}
A = & 38^\circ\ 19'\ 18'' \\
B = & 48^\circ\ \ 0'\ 10'' \\
C = & 121^\circ\ \ 8'\ \ 6'' \\
\hline
2\,) & 207^\circ\ 27'\ 34'' \\
\hline
S = & 103^\circ\ 43'\ 47''\ -\cos.S = +\sin.13^\circ\ 43'\ 47'' = 9.375376 \\
B = & 48^\circ\ \ 0'\ 10''\ \ \cos.(S-B) = 55^\circ\ 43'\ 37'' = 9.750612 \\
\hline
(S-B) = & 55^\circ\ 43'\ 37''\qquad 2\,)\ 19.125988
\end{array}$$

$$\text{square root} = 9.562994$$

$$\begin{array}{rl}
\sin.A = & 38^\circ\ 19'\ 18'' = 9.792445 \\
\sin.C = & 121^\circ\ \ 8'\ \ 6'' = 9.932443 \\
\hline
& 2\,)\ 19.724888 \\
\hline
\text{square root} = & 9.862444 = 9.862444 \\
\hline
& \text{diff.}\ -1.700550
\end{array}$$

Add 10, for radius of the table, 10

Tabular $\sin.\frac{1}{2}b = 30^\circ\ \ 7'\ 14'' = 9.700550$

2

$b = 60^\circ\ 14'\ 28''$, nearly.

PRACTICAL PROBLEMS.

1. In any triangle, ABC, whose sides are a, b, c, given $b = 118^\circ\ 2'\ 14''$, $c = 120^\circ\ 18'\ 33''$, and the included angle $A = 27^\circ\ 22'\ 34''$, to find the other parts.

Ans. $\begin{cases} a = 23^\circ\ 57'\ 13'', \text{ angle } B = 91^\circ\ 26'\ 44'', \text{ and} \\ C = 102^\circ\ 5'\ 52''. \end{cases}$

2. Given, $A = 81^\circ\ 38'\ 17''$, $B = 70^\circ\ 9'\ 38''$, and $C = 64^\circ\ 46'\ 32''$, to find the sides a, b, c.

Ans. $\begin{cases} a = 70^\circ\ 4'\ 13'', b = 63^\circ\ 21'\ 24'', \text{ and} \\ c = 59^\circ\ 16'\ 21''. \end{cases}$

3. Given, the three sides, $a = 93° 27' 34''$, $b = 100° 4' 26''$, and $c = 96° 14' 50''$, to find the angles A, B, and C.

$$\textit{Ans.} \begin{cases} A = 94° \ 39' \ 4'', B = 100° \ 32' \ 19'', \text{and } C = 96° \\ 58' \ 35''. \end{cases}$$

4. Given, two sides, $b = 84° 16'$, $c = 81° 12'$, and the angle $C = 80° 28'$, to find the other parts.

Ans. The result is ambiguous, for we may consider the angle B as acute or obtuse. If the angle B is acute, then $A = 97° \ 13' \ 45'$, $B = 83° \ 11' \ 24''$, and $a = 96° \ 13' \ 33''$. If B is obtuse, then $A = 21° \ 16' \ 43''$, $B = 96° \ 48' \ 36''$, and $a = 21° \ 19' \ 29''$.

5. Given, one side, $c = 64° 26'$, and the angles adjacent, $A = 49°$, and $B = 52°$, to find the other parts.

$$\textit{Ans.} \begin{cases} b = 45° \ 56' \ 46'', a = 43° \ 29' \ 49'', \text{and} \\ C = 98° \ 28' \ 4''. \end{cases}$$

6. Given, the three sides, $a = 90°$, $b = 90°$, $c = 90°$, to find the angles A, B, and C.

Ans. $A = 90°$, $B = 90°$, and $C = 90°$.

7. Given, the two sides, $a = 77° 25' 11''$, $c = 128° 13' 47''$, and the angle $C = 131° 11' 12''$, to find the other parts.

$$\textit{Ans.} \begin{cases} b = 84° \ 29' \ 20'', A = 69° \ 13' \ 59'', \text{and} \\ B = 72° \ 28' \ 42''. \end{cases}$$

8. Given, the three sides, $a = 68° 34' 13''$, $b = 59° 21' 18''$, and $c = 112° 16' 32''$, to find the angles A, B, and C.

$$\textit{Ans.} \begin{cases} A = 45° \ 26' \ 38'', B = 41° \ 11' \ 30'', \\ C = 134° \ 53' \ 55''. \end{cases}$$

9. Given, $a = 89° \ 21' \ 37''$, $b = 97° \ 18' \ 39''$, $c = 86° \ 53' \ 46''$, to find A, B, and C.

$$\textit{Ans.} \begin{cases} A = 88° \ 57' \ 20'', B = 97° \ 21' \ 26'', \\ C = 86° \ 47' \ 17''. \end{cases}$$

10. Given, $a = 31^\circ\ 26'\ 41''$, $c = 43^\circ\ 22'\ 13''$, and the angle $A = 12^\circ\ 16'$, to find the other parts.

Ans. Ambiguous; $b = 73^\circ\ 7'\ 34''$, or $12^\circ\ 17'\ 40''$; angle $B = 157^\circ\ 3'\ 44''$, or $4^\circ\ 58'\ 30''$; $C = 16^\circ\ 14'\ 27''$, or $163^\circ\ 45'\ 33''$.

11. In a triangle, ABC, we have the angle $A = 56^\circ\ 18'\ 40''$, $B = 39^\circ\ 10'\ 38''$; AD, one of the segments of the base, is $32^\circ\ 54'\ 16''$. The point D falls upon the base AB, and the angle C is obtuse. Required the sides of the triangle and the angle C.

Ans. Ambiguous; $C = 135^\circ\ 25'$, or $135^\circ\ 57'$; $c = 122^\circ\ 29'$, or $123^\circ\ 19'$; $a = 89^\circ\ 40'$, or $90^\circ\ 20'$; $b = 49^\circ\ 23'\ 41''$.

12. Given, $A = 80^\circ\ 10'\ 10''$, $B = 58^\circ\ 48'\ 36''$, $C = 91^\circ\ 52'\ 42''$, to find a, b, and c.

Ans. $a = 79^\circ\ 38'\ 21''$, $b = 58^\circ\ 39'\ 16''$, $c = 86^\circ\ 12'\ 52''$.

CHAPTER III.

OF MENSURATION.

Mensuration is the measurement of extension.

Measurement is the application of a certain fixed portion of extension to that which is measured; this portion is called a *unit.*

The measure of anything—or the number expressing the result of measurement—is the ratio between the unit and that which is measured.

The quality or dimension of the unit corresponds to that which is measured; line is applied to line, surface to surface, solid to solid.

All ratios are abstract, the idea of quality disappearing in the division. Thus,

4 *feet* are contained in 12 *feet*, 3 times; or the ratio between them is 3.

4 *yards* are contained in 12 *yards*, 3 times; or the ratio between them is also 3.

Hence, though measurement is *strictly* an application of a unit of the *same* kind, yet, if we can prove the ratio between surfaces or solids to be the same as the ratio between lines, we may, by a comparison or measurement of lines, determine the measurement of surface and solidity. We shall find this frequently in use.

Mensuration is naturally divided into the measurement of lines, surfaces, and solids.

We shall call attention to these successively.

SECTION I.

OF LINES.

In the measurement of those lines which are accessible, some convenient unit of measure is directly applied.

All measurement of lines is called *linear* measurement, and units which are lines are *linear* units.

The following Tables show the standard linear units in this country.

TABLE OF LONG MEASURE.

12	inches (in.)	make	1 foot, ... ft.
3	feet	make	1 yard, ... yd.
5½	yards, or 16½ feet,	make	1 rod, ... rd.
40	rods	make	1 furlong, ... fur.
8	furlongs, or 320 rods,	make	1 statute mile, . . . mi.

The following are also in use:

6	feet	make	1 fathom, used in measuring depths at sea.
1.15	statute miles	make	1 geographic mile, used in measuring distances at sea.
3	geographic miles	make	1 league.
60 69.16	geographic miles or statute miles	make	1 degree of latitude on a meridian, or of longitude on the equator.

TABLE OF CIRCULAR MEASURE.

60	seconds (″)	make	1 minute (′)
60	minutes	make	1 degree (°)
360	degrees	make	1 circumference of circle (circ.)

SURVEYORS' LONG MEASURE.

7.92	inches (in.)	make	1 link, ... l.
25	links	make	1 rod, ... rd.
4	rods, or 66 feet,	make	1 chain, ... ch.
80	chains	make	1 mile, ... mi.

When lines are inaccessible, the principles of Geometry and Trigonometry are used to derive from accessible or known conditions, lines otherwise unknown This application is called

MENSURATION OF HEIGHTS AND DISTANCES

DEFINITIONS.

A **Vertical Line** is one formed by a line and plummet freely suspended and allowed to come to rest. Such a line is perpendicular to a tangent to the earth's surface, and is a continuation of a radius of the earth.

A **Vertical Plane** is one passing through a vertical line.

A **Horizontal Line** is one at right angles to the vertical line.

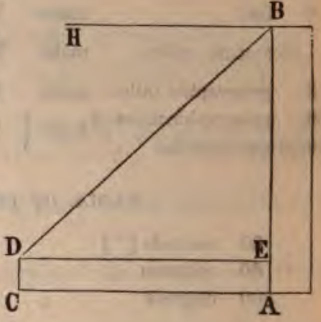
A **Horizontal Plane** is one perpendicular to the vertical line.

Angles are vertical or horizontal, as the planes of their sides are vertical or horizontal.

An **Angle of Elevation** is one, the plane of whose sides is vertical, and where one side is horizontal and the other ascending.

An **Angle of Depression** lies also in a vertical plane, but with one of its sides horizontal, and the other descending.

For example, in the figure following, EDB is an angle of elevation, having the ascending line DB; EBD is an angle of depression, having DE horizontal and BD descending.



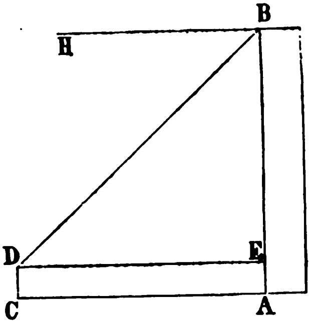
Stations are points, selected for convenience or at pleasure, from which angles and lines are measured.

A **Base Line** is one measured as a *basis* or known quantity, to be used in calculations; and with this the lines and angles to be determined are connected.

PROBLEM I.

To determine the vertical height of an object above a horizontal plane.

***ase* 1. When the object is vertical, and its base accessible.** rom the base of the object, measure on the horizontal e a line of convenient length, and at its extremity take angle of elevation.



hen if AB is the object and the base line, the instrument g placed at CD, there will be wn in the triangle DEB, $DE = AC$, and base angle B = angle of elevation.

(Prop. III, Plane Trigonome- Chap. 2.)

$R : DE = \tan. EDB : BE$.

hence BE is known; EA = = height of instrument for suring angles, $BE + EA = AB$, vertical height required.

EXAMPLES.

Required the height of an object when the line measured base to station is 110 feet, and angle of elevation is found e 54° 32′, height of instrument being 5 feet.

Solution.

In last figure $AC = DE = 110$ feet,

$$\angle EDB = 54^\circ\ 32'.$$

$$R : 110 :: \tan.\ 54^\circ\ 32' : BE.$$

$$\begin{array}{lrl} \text{By logarithms, log. } 110 & = & 2.041393 \\ \text{Log. tan. } 54^\circ\ 32' & = & \underline{10.147267} \\ & & 12.188660 \\ \text{Log. } R & = & \underline{10} \\ & & 2.188660 = \log.154.4 = BE. \end{array}$$

y condition $EA = 5$ feet: hence $BE + EA = 154.4 + 5$ 59.4 feet, height of object.

2. The distance from foot of a tower to station is found to be 109 feet, and angle of elevation 39° 22′, required the height of tower, allowing 5 feet for height of instrument.

Ans. 94.427 feet.

3. Given, base line $= 100$ feet,
Angle of elevation $= 47° 52'$,
Allowing 5 feet for instrument, required height of object.

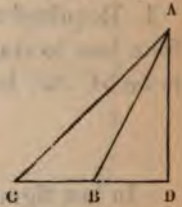
Ans. 115.54 feet.

4. Given, base line $= 80$ feet,
Angle of elevation $= 32° 42'$,
Allowing for instrument as before, required height of object.

Case 2.—When the object, or its base, is wholly inaccessible, two methods may be employed.

1*st Method.*—Two stations having been taken in a direct line towards the object, measure the distance between these stations as a base line; also, the angle of elevation of object at each station.

Then, in figure, in the triangle ABC, there will be known, BC the base line, the angle ACB, angle of elevation at first station, and angle $ABC = 180° - ABD$, angle of elevation at second station.



$$\text{Angle } CAB = (ABD - ACB) \qquad (1)$$

By Plane Trig., Chap. 2d, Sec. 2, Prop. IV,

$$\sin. CAB : BC = \sin. ACB : AB. \qquad (2)$$

Then in the right-angled triangle ABD, there are known AB from (2), and ABD.

By Plane Trig., Prop. III,

$$R : AB = \sin. ABD : AD. \qquad (3)$$

To AD add height of instrument as in Case 1, and we obtain vertical height of object.

EXAMPLES.

1. Wishing to know the vertical height of an object upon a hillside, above the horizontal plane, I took a station in the plain below the hill, at which the angle of elevation of the object was 30° 48′. I then measured toward the object 100 feet to a second station on a level with the first, where I found the angle of elevation 44° 28′. Required vertical height above the plane of stations, allowing 5 feet for instrument.

Solution.

In last figure, $BC = 100$ feet, $\angle ACB = 30^\circ\,48'$, $\angle ABD$ $44^\circ\,28'$.

$\angle ABC = 180^\circ - 44^\circ\,28' = 135^\circ\,32'$

$\angle CAB = (44^\circ\,28' - 30^\circ\,48') = 13^\circ\,40'.$ (1)

$\sin.\ 13^\circ\,40' : 100 = \sin.\ 30^\circ\,48' : AB.$ (2)

Co. log. sin. $13^\circ\,40' = 0.626586$

Log. $100 = 2.000000$

Log. sin. $30^\circ\,48' = 9.709306$

Sum less 10, $= 2.335892 =$ log. 216.72.

$AB = 216.72.$

$R : 216.72 = \sin.\ 44^\circ\,28' : AD.$ (3)

Log. $216.72 = 2.335892$

Log. sin. $44^\circ\,28' = 9.845405$

Less 10 $= 2.181297 =$ log. AD.

$2.181297 =$ log. 151.81 $\qquad 151.81 = AD$

$\qquad\qquad 5$

Ans. $= 156.81$

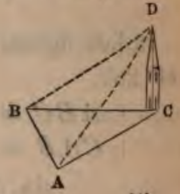
2. Wishing to ascertain the height of a church spire, I measure near its foot an angle of elevation 53° 45′; then proceeding 120 feet in a line with first station and spire, I find the angle of elevation only 34°. What is the height of spire, allowing as before for instrument. *Ans.* 165.14

3. Given, angle of elevation first station $= 60° 12'$.
Angle " second " $= 42° 25'$.
Distance between stations $= 72$ feet.

Required height of object, allowing 5 feet for instrument.
Ans. 142.98 feet.

2*d Method.*—Select two stations, from which both base and top of the object are visible, and measure distance between these for a base line. At each station measure horizontal angle between foot of object and the other station; also, at one station measure the angle of elevation of the top of the object.

Then, if CD be the object, and A and B the assumed stations, in the horizontal triangle ABC, there will be known AB, the base line, and the horizontal angles ABC and BAC.



Also, $$ACB = 180° - (ABC + BAC). \quad (1)$$

By Prop. IV, Sec. 2, Chap. 2,

$$\begin{aligned} \sin.ACB : AB &= \sin.ABC : AC, \text{ or} \\ &= \sin.BAC : BC. \end{aligned} \quad (2)$$

Then, in the right-angled triangle ACD (or BCD, if the angle of elevation be taken at B),

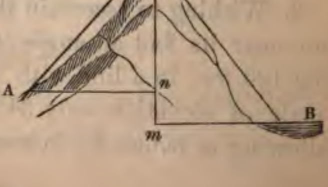
(Prop. III, Sec. 2, Chap. 2),

$$R : AC = \tan.CAD : CD, \quad (3)$$

Or, if BCD be used, $R : BC = \tan.CBD : CD$.

To CD add height of instrument as before, and the sum will be the vertical height of the object.

By an application of this method, we may compute the difference of level between two horizontal planes, if the same object is visible from both.



For example, let M be a prominent tree or rock near the top of a mountain; by observations taken at A, we can deternine the perpendicular *Mn*. By like observations taken at *B*, we can determine the perpendicular *Mm*. The difference etween these two perpendiculars is *nm*, or the difference in he elevation between the two points *A* and *B*. If the dis-ances between *A* and *n*, or *B* and *m*, are considerable, or nore than two or three miles, corrections must be made for he convexity of the earth; but for less distances, such corrections are not necessary.

EXAMPLES.

1. It is desired to determine the vertical height of a light-house near the mouth of a harbor. Two stations are selected on the shore, distant from each other 160 feet. The horizontal angle at the first station is found to be 88° 44′, and the angle of elevation at the same point 25° 56′; the horizontal angle at the second station is found to be 60° 37′. Required eight of light-house.

Solution.

In preceding figure, if *CD* be the light-house, *A* and *B* the rst and second stations, there are known $AB = 160$, $\angle CAB = 88° 44'$, and $\angle ABC = 60° 37'$.

Also, $ACB = 180° - (88° 44' + 60° 37') = 30° 39'$. (1)

$$\sin.\ 30° 39' : 160 = \sin.\ 60° 37' : AC. \qquad (2)$$

$$\begin{aligned} \text{Co. log. sin. } 30° 39' &= 0.292607 \\ \text{Log. } 160 &= 2.204120 \\ \text{Log. sin. } 60° 37' &= \underline{9.940196} \\ \text{Log. } AC &= 2.436923 = \text{log. } 273.48. \end{aligned}$$

In triangle *ACD*, $\angle CAD = 25° 56'$.

$$R : 273.48 = \tan.\ 25° 56' : CD.$$

$$\begin{aligned} \text{Log. } 273.48 &= 2.436923 \\ \text{Log. tan. } 25° 56' &= \underline{9.686898} \\ \text{Less } 10 &= 2.123821 = \text{log. } CD. \end{aligned}$$

2.123821 = log. 133 nearly. 133 + 5 = 138 feet. *Ans.*

2. The elevation of the top of a tower at one station is 19° 45′ 10″, and the horizontal angle at the same station between foot of tower and a second station is 91° 40′. At the second station, distant from first 400 feet, the horizontal angle is 51° 50′. Required height of tower.

Ans. 194.85 feet.

3. The angle of elevation of a spire from an assumed station is 23° 50′ 17″, and the horizontal angle at the same point, between the foot of the spire and a second station, distant 416 feet, is 93° 4′ 20″. At the second station the horizontal angle is 54° 28′ 36. Required height of spire.

Ans. 278.8 feet.

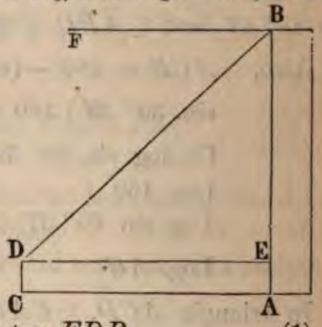
PROBLEM II.

The height of an object being known, to determine its distance from a visible station in the horizontal plane at its foot.

If the observer be at the station, let the angle of elevation be measured; if on the object, the angle of depression, which equals that of elevation.

Then, if EB is the object, there will be known in the right-angled triangle DEB, one side BE, and the angle EDB, either by measurement, or because $FBD = EDB$.

By Plane Trig., Chap. 2, Sec. 2, Prop. III,



$$DE : BE = R : \text{tan.}EDB. \tag{1}$$

Whence is known DE, the required distance.

N. B. If angle of elevation is taken, the height of the instrument should be deducted from the vertical height of the object to obtain BE.

EXAMPLES.

1. Required the distance from a given station to a spire 170 feet in height, the angle of elevation at the station being 25° 32′.

Solution.

In triangle BDE, $BE = 170-5 = 165$ feet,

$$\angle EDB = 25^\circ\ 32'.$$

$$DE : 165 = R : \text{tan. } 25^\circ\ 32'.$$

$$\begin{aligned} \text{log. } R + \text{log. } 165 &= 12.217484 \\ \text{Subtract log. tan. } 25^\circ\ 32' &= \underline{\ 9.679146} \\ \text{Log. } DE &= \ 2.538338 = \text{log. } 345.41. \\ Ans. &= 345.41 \text{ feet.} \end{aligned}$$

2. Wishing to know my distance from a building on the opposite side of a river, knowing the height of the building to be 52 feet, I measured its angle of elevation 10° 18′. What was my distance?

Ans. 258.62 feet.

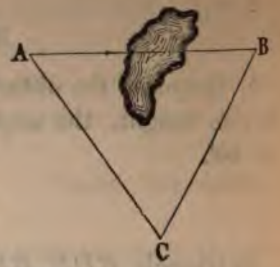
3. From the top of a mast of a vessel, 75 feet above the water, the angle of depression of another vessel's hull was found to be 18° 30′. What was the distance between the vessels?

4. Being upon the top of a tower 92 feet high, I measured the angle of depression of the bottom of a building, 5° 48′; required the distance between tower and building.

PROBLEM III.

To determine the distance between two distant objects.

Case 1.—When the objects, though separated by an impassable barrier, are themselves accessible and visible from an assumed station.



Measure the distance from each object to the assumed station, and then take the horizontal angle at the station.

If A and B represent the objects, and C the assumed station, there will be known AC, BC and $\angle C$.

By Plane Trig., Chap. 2, Sec. 2, Prop. VII.

$$AC+BC : AC-BC = \tan.\tfrac{1}{2}(A+B) : \tan.\tfrac{1}{2}(A-B) \quad (1)$$

$$\tfrac{1}{2}(A+B)+\tfrac{1}{2}(A-B) = A,$$

or larger angle, opposite greater side.

By Plane Trig. Chap. 2, Sec. 2, Prop. IV.

$$\text{Sin.}A : BC = \sin.C : AB, \text{ the required distance.} \quad (2)$$

EXAMPLES.

1. It is desired to determine the distance between two objects separated by woods and marsh. From the twc objects the distances are measured to a convenient point, 122 and 161 yards; the horizontal angle at the station is found to be 52° 42′. What is the distance?

Solution.

$$AC = 162,\ BC = 121, \text{ and } \angle ACB = 52^\circ\ 42',$$

$$A+B = 180^\circ - 52^\circ\ 42' = 127^\circ\ 18';\ \tfrac{1}{2}(A+B) = 63^\circ\ 39'.$$

$$283 : 39 = \tan.\ 63^\circ\ 39' : \tan.\tfrac{1}{2}(A-B) \quad (1)$$

Co. log. 283 = 7.548214
Log. 39 = 1.591065
Log. tan. 63° 39′ = 10.305117
Sum less 10 = 9.444396 = log. tan.$\tfrac{1}{2}(A-B)$ = log. tan. 15° 32′ 52″.

$A = 63^\circ\, 39' + 15^\circ\, 32'\, 52'' = 79^\circ\, 11'\, 52''$, since A is opposite BC, the longer side.

$$\text{Sin. } 79^\circ\, 11'\, 52'' : 161 = \text{sin. } 52^\circ\, 42' : AB.$$

$$\begin{aligned}
\text{Co. log. sin. } 79^\circ\, 11'\, 52'' &= 0.007764 \\
\text{Log. } 161 &= 2.206826 \\
\text{Log. sin. } 52^\circ\, 42'' &= \underline{9.900626} \\
& \ 2.115216 = \log. AB = 130.38.
\end{aligned}$$

Ans. 130.38 yards.

2. To ascertain the distance between objects A and B, lines are measured to station C, 178 and 212 feet; the horizontal angle is found to be 61° 40′. What is the distance?

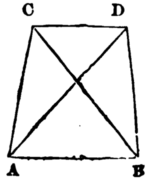
Ans. 202.01 feet.

3. From two stations, A and B, distances are measured to a third station C, 97 and 86 yards; the angle between A and B at C is 31° 50′. Required distance from A to B.

4. Wishing to know the distance between two points separated by swamp and wood, I measure to a station distances from both, and find them 120 and 133 yards; the angle I find to be 57° 10′. What is the distance?

Case 2. When the objects are not easily accessible.

Measure a base line from each extremity of which both objects are visible; at each extremity measure the horizontal angle between each object and the other station.



Then if C and D be the objects, A and B the stations, there are known AB, base line, the angles CAB, DAB, ABD and ABC.

Also, $CAD = CAB - DAB$ (1)

and $CBD = ABD - ABC$, (2)

and they are known.

Also, $ACB = 180^\circ - (CAB + ABC)$ (3)

and $ADB = 180^\circ - (ABD + DAB)$, (4)

and they are known.

Therefore, in the triangle ABC, (Chap. 2, Sec. 2, Prop. IV), we may have

$$\text{Sin.}ACB : AB = \sin.CAB : BC, \qquad (5)$$

And in ABD,

$$\text{Sin.}ADB : AB = \sin.DAB : BD. \qquad (6)$$

In the triangle CBD, $\llcorner CBD$ is known (2), and sides BC and BD (5 and 6).

By Trig., Chap. 2, Sec. 2, Prop. VII.

$$BC+BD : BC-BD = \tan.\tfrac{1}{2}(BDC+BCD) : \tan.\tfrac{1}{2}(BDC-BCD) \qquad (7)$$

$$\tfrac{1}{2}(BDC+BCD)+\tfrac{1}{2}(BDC-BCD)=BDC \qquad (8)$$

And $\quad \text{Sin.}BDC : BC = \sin.CBD : DC$, the distance required.

By using the triangles ABD and ABC, to find AD and AC, the line CD may be calculated from the triangle ACD, as well as from BCD.

EXAMPLES.

1. A man desiring to ascertain the distance between two objects from which he is separated by a river, measures a base line 200 feet long. At one extremity, (station A), he finds the horizontal angles to be 83° 47′, and 42° 32′; at the other, (station B) he finds the angles 76° 52′, and 36° 20′. What is the distance required?

Solution.

If C and D represent the objects, A and B the stations, $AB = 200$ feet, $CAB = 83^\circ\, 47'$, $DAB = 42^\circ\, 32'$, $ABD = 76^\circ\, 52'$, and $ABC = 36^\circ\, 20'$.

$$CAD = 83^\circ\, 47'-42^\circ\, 32' = 41^\circ\, 15' \qquad (1)$$

$$CBD = 76^\circ\, 52'-36^\circ\, 20' = 40^\circ\, 32' \qquad (2)$$

$$ACB = 180^\circ-(83^\circ\, 47'+36^\circ\, 20') = 59^\circ\, 53' \qquad (3)$$

$$ADB = 180^\circ-(76^\circ\, 52'+42^\circ\, 32') = 60^\circ\, 36' \qquad (4)$$

In triangle ABC,

$$\text{Sin. } 59^\circ\ 53' : 200 = \text{sin. } 83^\circ\ 47' : BC \qquad (5)$$

$\text{Co. log. sin. } 59^\circ\ 53' = 0.062981$
$\text{Log. } 200 = 2.301030$
$\text{Log. sin. } 83^\circ\ 47' = 9.997439$
$\text{Log. } BC = 2.361450 = \text{log. } 229.85 = BC.$

In triangle ABD,

$$\text{Sin. } 60^\circ\ 36' : 200 = \text{sin. } 42^\circ\ 32' : BD \qquad (6)$$

$\text{Co. log. sin. } 60^\circ\ 36' = 0.059875$
$\text{Log. } 200 = 2.301030$
$\text{Log. sin. } 42^\circ\ 32' = 9.829959$
$\text{Log. } BD = 2.190864 = \text{log. } 155.19 = BD.$

In triangle CBD,

$$\tfrac{1}{2}(180^\circ - 40^\circ\ 32') = 69^\circ\ 44' = \tfrac{1}{2}(BDC + BCD)$$

$$385.04 : 74.66 = \text{tan. } 69^\circ 44' : \text{tan.} \tfrac{1}{2}(BDC - BCD) \qquad (7)$$

$\text{Co. log. } 385.04 = 7.414494$
$\text{Log. } 74.66 = 1.873088$
$\text{Log. tan. } 69^\circ\ 44' = 10.432680$
$\text{Log. tan. } \tfrac{1}{2}(BDC - BCD) = 9.720262 = \text{log. tan. } 27^\circ\ 42'\ 18''.$
$\tfrac{1}{2}(BDC - BCD) = 27^\circ\ 42'\ 18''$
$\tfrac{1}{2}(BDC + BCD) = 69^\circ\ 44'$
$BDC = 97^\circ\ 26'\ 18''.$

Again in CBD,

$$\text{Sin. } 97^\circ\ 26'\ 18'' : 229.85 = \text{sin. } 40^\circ\ 32' : CD.$$

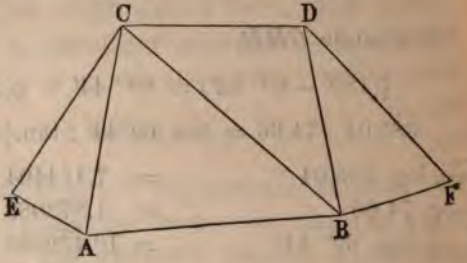
$\text{Co. log. sin. } 97^\circ\ 26'\ 18'' = 0.003670$
$\text{Log. } 229.85 = 2.361450$
$\text{Log. sin. } 40^\circ\ 32' = 9.812840$
$\text{Log. } CD = 2.177960 = \text{log. } 150.65.$
$CD = \text{distance required} = 150.65 \text{ feet.}$

2. Desiring to ascertain the distance between two objects, C and D, which are inaccessible, I select two stations, A and B, 282 feet apart. At station A I find the angle between C and B 87° 50′, between D and B 52° 40′. At station B I find angle between D and A 89° 34′, between C and A 46° 24′. What is the distance sought? *Ans.* 280.5 feet, nearly.

3. Given the following: $AB = 43$ yards, $CAB = 89° 45'$, $DAB = 39° 40'$, $ABD = 77° 10'$, and $ABC = 29° 26'$, to find the distance CD.

If it is not possible to find convenient stations from which both objects are visible, the distance between the objects may be determined by a series of triangular calculations. Thus,

Suppose C and D to be two objects, so situated that both are not visible from any station. Take station A in sight of C, and B in sight of D, A and B being in sight of each other. Measure as before, base line AB and angles BAC and ABD.



Near A take the station E, from which both A and C are visible; measure AE, and the angles EAC and AEC; ACE is found at once by subtracting from 180°. Then

$$\sin.ACE : AE = \sin.AEC : AC. \qquad (1)$$

Now, in the triangle ABC, AB and AC are known, and the angle BAC; and we have

$$AB+AC : AB-AC = \tan.\tfrac{1}{2}(ABC+ACB) : \tan.\tfrac{1}{2}(ACB-ABC). \qquad (2)$$

$$\tfrac{1}{2}(ABC+ACB) \pm \tfrac{1}{2}(ACB-ABC = ABC \text{ and } ACB. \qquad (3)$$

$$\sin.ABC : AC = \sin.BAC : BC. \qquad (4)$$

To find BD assume a station F, near B, from which B and D are visible; measure BF, BFD and FBD. As in triangle AEC,

$$\sin.BDF : BF = \sin.BFD : BD. \qquad (5)$$

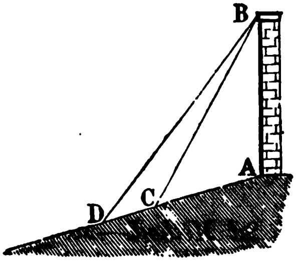
ABD is known by measurement; ABC is known from (3) $ABD-ABC = CBD$. From (4) and (5), we have BC and BD. We, therefore, have, as in the first part of the case, two sides and angle included to find the third side, which is the required distance.

PROBLEM IV.

To determine the vertical height of an object situated on an inclined plane.

1st Method.—Measure the angle at the foot of the object between it and the plane; then measuring a convenient distance to a station, take the angle between the plane and the top of the object.

Let AB be the object on an inclined plane. AC is known by measurement, as are also the angles BAC and ACB. Also, $ABC = 180° - (BAC + ACB)$. Hence,



$$\sin.ABC : AC = \sin.ACB : AB = \text{height required.}$$

EXAMPLES.

1. To ascertain the height of a vertical object situated on an inclined plane, the angle at the base is measured and found to be 102° 42′. Proceeding 100 feet, the angle between the plane and the top of the object is found to be 41° 10′. What is the height of the object?

Solution.

In the triangle ABC, $AC = 100$, $BAC = 102° 42'$, $ACB = 41° 10'$, and $ABC = 180° - (102° 42' + 41° 10') = 36° 8'$.

$$\sin. 36° 8' : 100 = \sin. 41° 10' : AB.$$

$$\begin{aligned}
\text{Co. log. sin. } 36° 8' &= 0.229394 \\
\text{Log. } 100 &= 2.000000 \\
\text{Log. sin. } 41° 10' &= 9.818392 \\
\text{Log. } AB &= 2.047786 = \text{log. } 111.63. \\
AB = \text{height} &= 111.63 \text{ feet.}
\end{aligned}$$

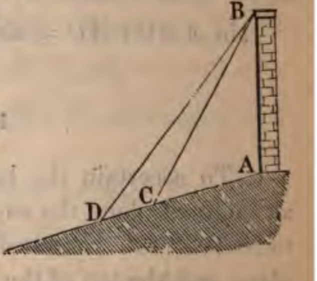
2. To determine the height of a tower on an inclined surface, there are measured the angle at the base, 107° 35', and the angle at an assumed station, 41° 54'; also, the distance from base to station, 80 feet. What is the height?

Ans. 105.21 feet.

3. To determine the height of a tree upon a hillside, I measure at the foot of the tree the angle with the plane of the hill, 105° 50', and at a station distant 40 feet, 51° 12'. Required the height of the tree. *Ans.* 79.89 feet.

2d Method.—Measure as before from the foot of the objec to a station, and then take the angle between the plane an top of object. Then measure in a line directly from the object to a second station, and then take an angle as before.

In the triangle BCD, C and D being the two stations, and AB the object, there are known DC, BDC, and $BCD = 180° - BCA$; also, $CBD = 180° - (BCD + BDC)$.



Then, $\sin. CBD : DC = \sin. BDC : BC$ (1)

In triangle ABC, BC is known (1); also, AC and ACB by measurement.

$$BC+AC : BC-AC = \tan.\tfrac{1}{2}(CAB+ABC) : \tan.\tfrac{1}{2}(CAB-ABC) \quad (2)$$

Whence, ABC and BAC are to be found,

$$\sin.ABC : AC = \sin.ACB : AB. \quad (3)$$

NOTE.—To obtain the angles at C and D, the angles of elevation should be taken, and from them the angle of inclination of the plane subtracted.

EXAMPLES.

1. To determine the height of a tower situated on a hill-side inclined 27° 48′ 11″, I measure 50 feet from the base of the tower, and take the angle of elevation, 67° 58′ 11″; then measuring in the same direction 100 feet, I find the angle of elevation 48° 0′ 11″. What is the height of the tower?

Solution.

$AC = 50$, $CD = 100$, $ACB = 67° 58' 11''-27° 48' 11'' = 40° 10'$, $CDB = 48° 0' 11''-27° 48' 11'' = 20° 12'$; also, $BCD = 180°-40° 10' = 139° 50'$, and $CBD = 40° 10'-20° 12' = 19° 58'$.

In the triangle BCD,

$$\sin.\ 19° 58' : 100 = \sin.\ 20° 12' : BC. \quad (1)$$

$$\begin{aligned} \text{Co. log. sin. } 19° 58' &= 0.466643 \\ \text{Log. } 100 &= 2.000000 \\ \text{Log. sin. } 20° 12' &= 9.538194 \\ \hline \text{Log. } BC &= 2.004837 = \text{log. } 101.12. \end{aligned}$$

In triangle ABC,

$$\tfrac{1}{2}(CAB+ABC) = \tfrac{1}{2}(180^\circ - 40^\circ\ 10') = 69^\circ\ 55'.$$

$$151.12 : 51.12 = \tan.\ 69^\circ\ 55' : \tan.\tfrac{1}{2}(CAB-ABC). \quad (2)$$

$$\begin{aligned} \text{Co. log. } 151.12 &= 7.820678 \\ \text{Log. } 51.12 &= 1.708591 \\ \text{Log. tan. } 69^\circ\ 55' &= \underline{10.436972} \\ \text{Log. tan.}\tfrac{1}{2}(CAB-ABC) &= 9.966241 = \tan.\ 42^\circ\ 46'\ 31''. \end{aligned}$$

$69^\circ\ 55' - 42^\circ\ 46'\ 31'' = 27^\circ\ 8'\ 29'' = ABC$, lesser angle, opposite AC.

$$\sin.\ 27^\circ\ 8'\ 29'' : 50 = \sin.\ 40^\circ\ 10' : AB \quad (3)$$

$$\begin{aligned} \text{Co. log. sin. } 27^\circ\ 8'\ 29'' &= 0.340856 \\ \text{Log. } 50 &= 1.698970 \\ \text{Log. sin. } 40^\circ\ 10' &= \underline{9.809569} \\ \text{Log. } AB &= 1.849395 = \text{log. } 70.696. \end{aligned}$$

Ans. = 70.696 feet.

2. From an object on a plane inclined 15° 30′ 57″, having measured 66 feet, the angle of elevation was 66° 10′ 57″; 100 feet farther on, the angle of elevation was 46° 52′ 57″. What was the height of the object?

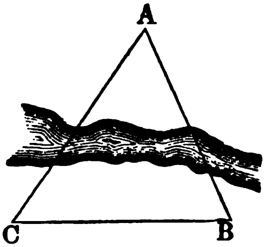
Ans. 126.41 feet.

3. Given, distance from base of object to first station 70 feet, and angle at first station 46° 40′; distance from first to second station 45 feet, and angle 38° 18′. Required height of object.

PROBLEM V.

To determine the horizontal distance from any point to an inaccessible object.

Measure from the given point a base line to some convenient station, and at each point measure the horizontal angle between the object and the other station.



Let A be the object, and B the station, from which the distance is to be found. Then BC being measured, and the angles B and C, we have $CAB = 180° - (B+C)$; and by Plane Trig., Chap. 2, Sec. 2, Prop. IV.

$$\sin. A : BC = \sin. C : AB, \text{ the required distance.}$$

EXAMPLES.

1. Desiring to ascertain the distance between two houses on opposite sides of a river, from one I measure to a station C, 100 yards; and measure also the angle at first station, 72° 41′; at the second, C, 83° 35′.

Solution.

$BC = 100$, $\angle B = 72° 41'$, $C = 83° 35'$ $\therefore$ $A = 180° - 156° 16' = 23° 44'$.

$$\text{Sin. } 23° 44' : 100 = \sin. 83° 35' : AB.$$

Co. log. sin. 23° 44′	= 0.395255	
Log. 100	= 2.000000	
Log. sin. 83° 35′	= 9.997271	
Log. AB	= 2.392526	= log. 246.9

Ans. 246.9 yards.

2. To find the distance between two objects separated by a stream, a base line is measured 210 feet to a station. The horizontal angles are then measured; at the object 81° 40′, at the station 70° 10′. What is the distance?

Ans. 418.48 feet.

3. Given a base line $BC = 160$ feet, and angles, $B = 89° 3'$, $C = 57° 56'$, to determine distances from B and C to an object A.

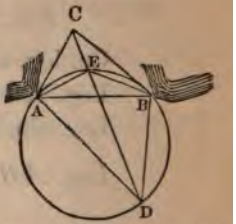
PROBLEM VI.

Given the distances between three points, and also the angles between these points from a distant object, to determine the distance from the distant object to the three points respectively.

This problem may be best understood by a careful examination of a practical example.

Coming from sea, at the point D I observed two headlands, A and B, and inland at C a steeple which appeared between the headlands. I found, from a map, that the headlands were 5.35 miles from each other; that the distance from A to the steeple was 2.8 miles, and from B to the steeple 3.47 miles; and I found, with a sextant, that the angle ADC was 12° 15', and the angle BDC, 15° 30'. Required my distance from each of the headlands, and from the steeple.

Construction.



The angle between the two headlands is the sum of 15° 30' and 12° 15', or 27° 45' Take double this sum, 55° 30'. Conceive AB to be the chord of a circle, and the arc on one side of it to be 55° 30'; and, of course, the other will be 304° 30'. The point D will be somewhere in the circumference of this circle. Consider that point as determined, and draw CD.

In the triangle ABC, we have all the sides, and of course we can find all the angles; and if the angle ACB is less than $180° - 27° 45' = 152° 15'$, then the circle cuts the line CD in a point E, and C is without the circle.

Draw *AE*, *BE*, *AD*, and *BD*. *AEBD* is a quadrilateral in a circle. and $\angle AEB + \angle ADB = 180°$.

The $\angle ADE =$ the $\angle ABE$, because both are measured by one half the arc *AE*. Also, $\angle EDB = \angle EAB$, for a similar reason.

Now, in the triangle *AEB*, its side *AB*, and all its angles, are known; and from thence *AE* can be computed. Then, having the two sides, *AC* and *AE*, of the triangle *AEC*, and the included angle *CAE*, we can find the angle *AEC*, and of course its supplement, *AED*. Then, in the triangle *AED*, we have the side *AE*, and the two angles *AED* and *ADE*, from which we can find *AD*.

Solution.

The computation, at length, is as follows:

To find *AE*.

Angle *EAB* =	15° 30′	Sin. *AEB*, 152° 15′,	9.668027
Angle *EBA* =	12° 15′	: *AB*, 5.35,	.728354
	27° 45′	:: sin. *ABE*, 12° 15′,	9.326700
	180°		10.055054
Angle *AEB* =	152° 15′	: *AE*, 2.438,	.387027

To find the angle *BAC*.

BC,	3.47		
AB,	5.35	log.	.728354
AC,	2.80	log.	.447158
	2)11.62		1.175512
S,	5.81	log.	.764176
S−*BC*,	2.34	log.	.369216
			20
			21.133392
			2)19.957880

[Forward.

2)19.957880

17° 41′ 58″ cos. 9.978940

2

Angle BAC = 35° 23′ 56″

Angle EAB = 15° 30′

Angle EAC = 19° 53′ 56″

180°

2)160° 6′ 4″

80° 3′ 2″ $= \dfrac{AEC+ACE}{2}$

To find the angles AEC and ACE.

$AC+AE$	5.238	.719165
: $AC-AE$	.362	$\bar{1}$.558709
: : tan. $\dfrac{AEC+ACE}{2}$	80° 3′ 2″	10.755928
		10.314637
: tan. $\dfrac{AEC-ACE}{2}$	21° 30′ 12″	9.595472

angle AEC, 101° 33′ 14″, sum,

angle ACE or ACD, 58° 32′ 50″, diff.

angle CDA, 12° 15′

70° 47′ 50″, supplement 109° 12′ 10″, angle CAD

35° 23′ 56″, angle CAB

73° 48′ 14″, angle BAD

To find AD.

Sin. ADC, 12° 15′, 9.326700

: AC, 2.8, .447158

: : sin. ACD, 58° 32′ 50″, 9.930985

10.378143

: AD, 11.26 miles. 1.051443

CD and BD may also readily be found.

$$Ans.\ \begin{cases} AD = 11.26, \\ BD = 11.03, \\ CD = 12.46. \end{cases}$$

The preceding problems include those most frequently met; others may arise, requiring different construction; but an acquaintance with the principles involved in the problems here given, and a knowledge of geometrical constructions and relations will soon give a key to any question arising. The miscellaneous examples which follow require mainly only the rules and constructions given in this section; whatever is required further the student will see and work out for himself with little difficulty.

PRACTICAL PROBLEMS.

1. Required the height of a wall whose angle of elevation, at the distance of 463 feet, is observed to be 16° 21′.

Ans. 135.8 feet.

2. The angle of elevation of a hill is, near its bottom, 31° 18′, and 214 yards further off, 26° 18′. Required the perpendicular height of the hill, and the distance of the perpendicular from the first station.

Ans. The height of the hill is 565.2 yards, and the distance of the perpendicular from the first station is 929.6 yards.

3. The wall of a tower which is 149.5 feet in height, makes, with a line drawn from the top of it to a distant object on the horizontal plane, an angle of 57° 21′. What is the distance of the object from the bottom of the tower?

Ans. 233.3 feet.

4. From the top of a tower which is 138 feet in height, I took the angle of depression of two objects standing in a direct line from the bottom of the tower, and upon the same horizontal plane with it. The depression of the nearer object was found to be 48° 10′, and that of the further, 18° 52′. What was the distance of each from the bottom of the tower?

Ans. Distance of the nearer, 123.5 feet; and of the further, 403.8 feet.

5. Being on the side of a river, and wishing to know the distance of a house on the opposite side, I measured 312 yards in a right line by the side of the river, and then found that the two angles, one at each end of this line, subtended by the other end and the house, were 31° 15′ and 86° 27′. What was the distance between each end of the line and the house?

Ans. 351.7, and 182.8 yards.

6. Having measured a base of 260 yards in a straight line on one bank of a river, I found that the two angles, one at each end of the line, subtended by the other end and a tree on the opposite bank, were 40° and 80°. What was the width of the river?

Ans. 190.1 yards.

7. From an eminence of 268 feet in perpendicular height the angle of depression of the top of a steeple, which stood on the same horizontal plane, was found to be 40° 3′, and of the bottom, 56° 18′. What was the height of the steeple?

Ans. 117.76 feet.

8. Wanting to know the distance between two objects which were separated by a morass, I measured the distance from each to a point from whence both could be seen; the distances were 1840 and 1428 yards, and the angle which, at that point, the objects subtended, was 36° 18′ 24″. Required their distance.

Ans. 1090.85 yards.

9. It is required to find the distance from a tower, 80 feet in height, to an object whose angle of depression from the top of the tower is 22° 41′.

Ans. 191.4 + feet.

10. The angle of elevation of a hill from a station near its foot is 29° 28′; from a station distant 100 yards, the angle of elevation is 20° 10′ 30″. Required perpendicular height of hill, allowing 5 feet for height of instrument.

Ans. 106.74 yards nearly.

11. From two stations, 300 feet apart, the horizontal angles made with a distant church are taken 88° 19′ and 89° 40′. Required distances from church to stations.

Ans. 8521.4 and 8525 feet nearly.

12. Wishing to know the distance between two inaccessible objects, C and D, I take two stations, A and B, 245 feet apart, and measure the angles as follows: $BAC = 86° 13'$, $BAD = 41° 11'$, $ABD = 80° 37'$, and $ABC = 35° 9'$. Required distance from C to D.

Ans. 204.39 feet.

13. Required the height of a wall whose angle of elevation, 100 feet from its base, is 18° 26′. *Ans.* 33.33 feet.

14. Wishing to know the height of an inaccessible object, I measure a base line AB, 190 feet, and take the horizontal angles; at A, 56° 40′; at B, 63° 11′. I measure also the angle of elevation at $A = 28° 21'$. Required the height of object.

Ans. 105.45 feet.

15. It being desired to ascertain distance between two houses, separated by swampy ground, a convenient station is selected and distances measured 472 and 560 feet. The angle between the houses at the station is found to be 63° 14′. What is the distance? *Ans.* 546.25 feet.

16. Wanting to know the breadth of a river, I measured a base of 500 yards in a straight line on one bank; and at each end of this line I found the angles subtended by the other end and a tree on the opposite bank of the river, to be 53° and 79° 12′. What was the perpendicular breadth of the river?

Ans. 529.48 yards.

17. What is the perpendicular height of a hill, its angle of elevation, taken at the bottom of it, being 46°, and 200 yards further off, on a level with the bottom, 31°?

Ans. 286.28 yards.

18. Wanting to know the height of an inaccessible tower, at the least accessible distance from it, on the same horizontal plane, I found its angle of elevation to be 58°; then going 300 feet directly from it, I found the angle there to be only 32°; required the height of the tower, and my distance from it at the first station.

Ans. Height, 307.54 feet.
Distance, 192.18 "

19. Two ships of war, intending to cannonade a fort, are, by the shallowness of the water, kept so far from it, that they suspect their guns cannot reach it with effect. In order, therefore, to measure the distance, they separate from each other a quarter of a mile, or 440 yards, and then each ship observes and measures the angle which the other ship and fort subtends; these angles are 83° 45′, and 85° 15′. What, then, is the distance between each ship and the fort?

Ans. 2292.26 yards.
2298.05 "

20. From two ships, *A* and *B*, which are anchored in a bay, two objects, *C* and *D*, on the shore, can be seen. These objects are known to be 500 yards apart. At the ship *A*, the angle subtended by the objects was measured, and found to be 41° 25′; and that by the object *D* and the other ship was found to be 52° 12′. At the other ship, the angle subtended by the objects on shore was found to be 48° 10′; and that by the object *C*, and the ship *A*, to be 47° 40′. Required the distance between the ships, and the distance from each ship to the objects on shore.

Ans. Distance between ships, 395.7 yards.
From ship *A* to object *D*, 743.5 "
From ship *A* to object *C*, 467.7 "
From ship *B* to object *D*, 590.5 "

To solve this problem, suppose the distance between the ships to be 100 yards, and determine the several distances, including the distance between the objects, *C* and *D*, under this supposition; then multiply the values thus found for the required distances by the quotient obtained by dividing the given value of *CD* by the computed value.

Full solutions of the Examples and Problems of this entire work may be found in the KEY TO ROBINSON'S GEOMETRIES AND SURVEYING.

SECTION II.

MENSURATION OF SURFACES.

The **Area** of a figure is the surface included between the lines which bound it.

Strictly, for the measurement of areas a superficial unit should be applied; but as all ratios are abstract, for practical convenience the ratio of lines is used—the quality of superficies being attached to the result.

A superficial unit is generally the square formed upon a linear unit of the same name. Thus, the square inch and square yard correspond to the linear inch and linear yard, which are the sides of the superficial units.

Roods and acres, units used in measuring land, have no corresponding linear units.

The following are the tables of superficial units.

SQUARE MEASURE.

144	square inches (sq. in.)	make	1 square foot, ...	sq. ft.
9	square feet	make	1 square yard, ...	sq. yd.
30¼	square yards	make	1 square rod, ...	sq. rd.
40	square rods	make	1 rood, ...	R.
4	roods	make	1 acre, ...	A.
640	acres	make	1 square mile, ...	sq. mi.

SURVEYORS' SQUARE MEASURE.

625	square links (sq. l.)	make	1 pole, ...	P.
16	poles	make	1 square chain, . . .	sq. ch.
10	square chains	make	1 acre, ...	A.
640	acres	make	1 square mile, ...	sq. mi.
36	square miles (6 miles square)	make	1 township, ...	Tp.

The following rules for the measurement of surfaces being *mainly* founded upon Geometry, the student is referred for their demonstration to Robinson's New Geometry, the number of the Book and Proposition being given with each rule.

PROBLEM I.

To find the area of a parallelogram.

RULE 1.—*Multiply the base by the altitude.* (Geom. Def. 54 —B. I., Th. 27.)

EXAMPLE.

Required the area of a parallelogram whose base is 23 and altitude 11 feet.

$23 \times 11 = 253$. ∴ Area required $= 253$ square feet.

NOTE.—To illustrate the transfer from linear to superficial units, let A = unit of measure, *a square*, having each side unity; and C, equal the rectangle equal in area to the parallelogram to be measured. Then from Def. 54, Geom., we may conclude, letting a and b represent altitude and base of C.

$$A : C = 1 \times 1 : a \times b, \quad \text{or} \tag{1}$$

$$1 : C = 1 \times 1 : a \times b. \quad \therefore \tag{2}$$

$$\frac{C}{1} = \frac{a \times b}{1 \times 1} \tag{3}$$

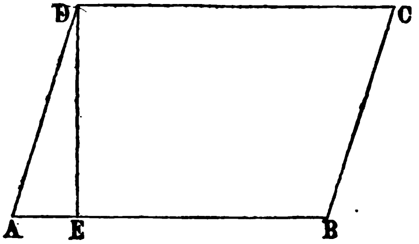
If for a and b, we place 11 and 23 as in above example, we have

$$\frac{C}{1} = \frac{11 \times 23}{1 \times 1} = 253. \tag{4}$$

That is, the unit rectangle is contained as many times in the given rectangle or parallelogram, as 1 × 1, is contained times in 11 × 23; that is, 253 times. Hence 253 = 23 × 11, expresses the ratio between the unit square foot and the surface measured; or the given surface contains *one* square foot 253 times, or 253 square feet. Here then we have two ratios—abstract numbers and equal, obtained, one by applying superficial unit to surface, the other by applying linear units to lines. We use the more convenient of these two ways of obtaining the ratios, and since the two are equal, we name and consider the result of one process as though it were the result of the other.

RULE 2.—When two sides and the angle included are known: *Multiply the product of the sides by the sine of the included angle.*

Demonstration.



Let $ABCD$ be the parallelogram, AB its base, and DE its altitude.

(RULE 1.)
Area $= AB \times DE.$ (1)

(Plane Trig., Chap. 2, Sec. 2, Prop. III,

$$R : AD = \sin. A : DE, \qquad (2)$$

$$DE = \frac{AD \times \sin. A}{R} \qquad (3)$$

Substituting for DE from (3) into (1),

$$\text{Area} = \frac{AB \times AD \times \sin. A}{R}$$

When $R=1$, Area $= AB \times AD \times \sin. A.$

If logarithms are used in the calculation, R must be considered, its logarithm being 10.

EXAMPLES.

. The sides of a parallelogram being 42 and 18 feet, and angle included 41° 11′, required the area.

Calculation.

$$\text{Area} = \frac{42 \times 18 \times \sin. 41^\circ\ 11'}{R}.$$

Log. 42	1.623249
Log. 18	1.255273
Log. sin. 41° 11′	9.818536
Sum less 10 (= log. R) =	2.697058 = log. 497.8=area.

2. Required the area of a parallelogram whose base is 11 ft. 3 in., and altitude 10 ft. 6 in. *Ans.* $118\frac{1}{8}$ sq. ft.

3. Required the area of a parallelogram whose sides are 31 and 11 feet, and included angle 31° 18′.

PROBLEM II.

To find the area of a triangle.

Rule 1.—*Take one half of the product of the base and altitude.* (Geom., B. I, Th. 33.)

Rule 2.—When two sides and angle included are known: *Take one half of the product of the two sides by the sine of the included angle, divided by radius.* (See Rule 2, Prob. 1.)

EXAMPLES.

1. What is the area of a triangle whose base is 36 and altitude 11? *Ans.* $= \frac{36 \cdot 11}{2} = 198.$

2. What is the area of a triangle two of whose sides are 45 and 31 inches, and the angle included 47° 39′?

$$\text{Area}=\frac{45\cdot 31 \text{ sin. } 47^\circ\ 39'}{2\cdot R} = 515.48 \text{ sq. inches},$$

Ans. 3 ft. 83.48 inches.

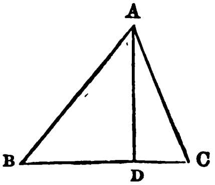
3. What is the area of a triangle, having sides 12 and 9 feet, and angle included 56° 20′?

Ans. 44.94 feet.

4. What is the area of a triangle whose sides are 42 and 60 feet, and the included angle 61° 12′?

Rule 3.—When the three sides of a triangle are known: *From one half the sum of the sides, subtract each side separately; multiply the continued product of these remainders by the half sum; the square root of the product will be the area required.*

Demonstration.



Let A represent the area of a triangle ABC, whose sides a, b, and c are known; a being considered as the base. Draw AD perpendicular to CB; it will be the altitude.

By (Geom., B. I., Th. 41.)

$$b^2 = a^2+c^2-2a\times BD \qquad (1)$$

$$BD = \frac{a^2+c^2-b^2}{2a} \qquad (2)$$

By (Geom., B. I., Th. 39), $AD^2 = c^2 - BD^2$, (3)

Substituting from (2) into (3), the value of BD,

$$AD^2 = c^2-\frac{(a^2+c^2-b^2)^2}{4a^2} \qquad (4)$$

$$AD = \frac{\sqrt{4a^2c^2-(a^2+c^2-b^2)^2}}{2a} \qquad (5)$$

By Rule 1, $$A = \frac{a \times AD}{2}, \qquad (6).$$

Substituting in (6) the value of AD from (5),

$$A = \frac{\sqrt{4a^2c^2-(a^2+c^2-b^2)^2}}{4} = \sqrt{\frac{4a^2c^2-(a^2+c^2-b^2)^2}{16.}} \qquad (7)$$

Factoring,

$$A = \sqrt{\frac{a+b+c}{2} \times \frac{b+c-a}{2} \times \frac{a+c-b}{2} \times \frac{a+b-c}{2}}, \qquad (8)$$

Since the difference of the squares of the two quantities equals the product of their sum and difference. Let $s = \frac{a+b+c}{2}$; then $s-a = \frac{b+c-a}{2}$, $s-b = \frac{a+c-b}{2}$, and $s-c = \frac{a+b-c}{2}$. Substituting these values in (8),

$$A = \sqrt{s(s-a)(s-b)(s-c)}. \qquad (9).$$

Whence the rule.

EXAMPLES.

1. Required the area of a triangle whose sides are 342, 384 and 436 feet.

Solution.

$$\begin{array}{rlrl}
a = 436 & s-a = 145\,; & \text{log.} = & 2.161368 \\
b = 384 & s-b = 197\,; & \text{“} = & 2.294466 \\
c = \underline{342} & s-c = 239\,; & \text{“} = & 2.378398 \\
2\,)\,\underline{1162} & \quad\;\; = 581\,; & \text{“} = & \underline{2.764176} \\
s = 581 & & 2\,)\, & \underline{9.598408} \\
 & & \text{Log. } A = & 4.799204
\end{array}$$

4.799204 = log. 62980.14+

Area 62980.14 sq. ft.

2. How many square yards in a triangle whose sides are 78, 82, and 100 feet?

Ans. 34.6+sq. yards.

3. Required the area of a triangle whose sides are 31, 40, and 55 rods.

Ans. 3.8 acres.

PROBLEM III.

To find the area of a trapezoid.

RULE.—*Multiply one half the sum of the parallel sides by the altitude.* (Geom. B. I., Th. 34.)

EXAMPLES.

1. What is the area of a trapezoid whose parallel sides are 23 and 11 feet, and whose altitude is 9 feet?

$$\frac{23+11}{2}\times 9 = 153.$$

Ans. 153 sq. ft.

2. Required the area of a trapezoid whose parallel sides are 178 and 146 feet, and whose altitude is 69 feet.

Ans. 41.05 sq. rods.

3. How many acres are there in a trapezoid whose bases measure 38 and 26 rods, and altitude 10 rods?

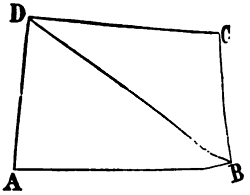
PROBLEM IV.

To find the area of a trapezium.

RULE 1.—If the sides and two opposite angles are known:—

Multiply the sine of each angle (of the two opposite) by one half the product of the sides which include it. The sum of the two products so obtained will be the area required.

Demonstration.



Let $ABCD$ be the trapezium whose sides are known, and also two angles, as A and C.

By Prob. II, Rule 2,

$$\text{Area of } ABD = \sin.A \times \frac{AB \times AD}{2} \qquad (1)$$

$$\text{Area of } BCD = \sin.C \times \frac{BC \times CD}{2} \qquad (2)$$

Hence,

$$ABCD = ABD + BCD = \sin.A \times \frac{AB \times AD}{2} + \sin.C \times \frac{BC \times CD}{2} \qquad (3)$$

Rule 2.—*If only the sides are known, a diagonal must measured; two triangles will thus be formed, whose areas may be found by Rule* 3, *Problem II. The sum of these areas w be the area of the trapezium.*

Rule 3.—*Without determining the sides, a diagonal may be measured, and also perpendiculars from the opposite angle upon that diagonal. In the two triangles formed by the diagonal, there will then be known the base and altitude, and Rule* 1, *Problem II, may be used.*

EXAMPLES.

1. Required the area of a trapezium whose sides, AB and AD, are 32 and 17 feet, and the angle A 71° 10′; sides CB and CD, 30 and 13 feet, and the angle C 108° 53′.

Solution.

Drawing diagonal BD by Rule 1st, we have,

$$\text{Area } ABD = \frac{32 \times 17 \times \sin.\ 71^\circ\ 10'}{2R} \qquad (1)$$

$$\begin{array}{lcl}
\text{Log. } 32 & = & 1.505150 \\
\text{`` } \ 17 & = & 1.230449 \\
\text{Log. sin. } 71^\circ\ 10' & = & \underline{9.976103} \\
 & & 12.711702 \\
\text{Log. } 2\ R & & \underline{10.301030} \\
\text{Log. area} & = & 2.410672 = \text{log. } 257.44.
\end{array}$$

$$\text{Area } CBD = \frac{30 \times 13 \times \sin.\ 108^\circ\ 53'}{2R} \qquad (2)$$

$$\begin{array}{lcl}
\text{Log. } 30 & = & 1.477121 \\
\text{`` } \ 13 & = & 1.113943 \\
\text{Log. sin. } 108^\circ\ 53' & = & \underline{9.975974} \\
 & & 12.567038 \\
\text{Log. } 2R & = & \underline{10.301030} \\
\text{Log. area} & = & 2.266008 = \text{log. } 184.5.
\end{array}$$

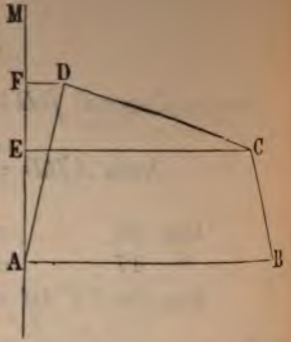
$$\begin{array}{lcl}
\text{Area } ABD & = & 257.44 \\
\text{Area } CBD & = & \underline{184.50} \\
 & & 441.94 = \text{area of trapezium.}
\end{array}$$

2. Required the area of a trapezium, whose sides are 9.5, 11, 12 and 14.8 rods, and whose diagonal from first to third station is 18 rods.

Ans. 132.25 sq. rods.

3. Required the area of a trapezium, whose diagonal measures 17.5 rods, and the perpendiculars from the angles upon that diagonal 8.4 and 4 rods.

Ans. 108½ sq. rods.



Another method still may be employed, as follows: let $ABCD$ be the trapezium. At any angle as A, draw AM perpendicular to AB. From angles C and D draw lines CE and DF perpendicular to AM, and thus parallel to AB. Then $ABCE$ and $ECDF$ will be trapezoids, and ADF a right-angled triangle. Having known AB, EC and FD, and also AF, AE and EF, the areas of these figures may be found by Prob. II., Rule 1, and Prob. III.

$$\text{Area } ABCD = ABCE + ECDF - ADF.$$

Whence is determined the area required.

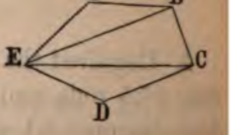
This process is the one employed in rectangular surveying, and may be applied to all polygons.

PROBLEM V.

To find the area of an irregular polygon.

RULE.—*Divide the polygon into triangles by diagonals, and draw perpendiculars from the vertical angles of these triangles upon the diagonals. Having measured the diagonals and perpendiculars, determine the areas of the triangles. The sum of these areas will be the area of the polygon.*

EXAMPLE.



To determine the area of the polygon $EABCD$, I measure the diagonals EB and EC, 60 and 68 feet. The perpendiculars I find to be as follows: from A, 10 feet; from B, 30 feet; from D, 25 feet. What is the required area?

Solution.

ob. II., Rule 1, $\frac{60\times10}{2} = 300 = EAB.$

$$\frac{68\times30}{2} = 1020 = EBC.$$

$$\frac{68\times25}{2} = 850 = EDC.$$

$$\text{Sum} = 2170 = \text{area } EABCD.$$

hat is the area of an irregular polygon whose diago- 32 and 56 feet, and perpendiculars as follows: upon diagonal, 7; upon the second, 11 and 13 feet.

Ans. $87\frac{1}{9}$ sq. yards.

PROBLEM VI.

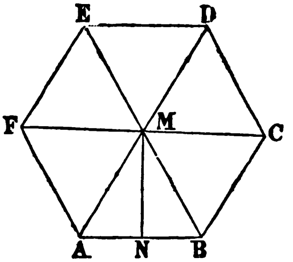
To find the area of a regular polygon.

—*Multiply one half the perimeter by the perpendic- ɩon from the center upon one of the sides.*

Demonstration.

$BCDEF$ be a regular poly- ose center is M. From M A, MB, &c., and let fall rpendicular to AB. MN the altitude of the triangle ınd by Prob. II., Rule 1,

a $ABM = \frac{1}{2}AB\times MN.$



ing the center of the polygon (Geom., B. IV, Th. 30, it is equidistant from the sides: that is, MN is equal to endicular from M upon the sides, and may represent mon altitude of the triangles ABM, BMC, &c. Hence, the areas of the triangles having for bases BC, CD, &c., will equal each one half its base into MN; and the area of the polygon, which equals the sum of the triangles, will equal

$$MN \times \frac{(AB+BC+CD+DE+EF+FA)}{2}$$

Whence the rule.

EXAMPLES.

1. What is the area of a regular hexagon whose side is 8 feet, and the perpendicular 6.92 feet.

$$\text{Perimeter} = 8 \times 6 = 48,\ \frac{48}{2} \times 6.92 = 166.08 \text{ square feet.}$$

If the perpendicular is not known, it may be determined from the following proportion, (Chap. 2, Sec. 2d. Prop. III),

$MN : AN = R : \text{tan.} AMN$. (See preceding figure.)

For (by Geom., B. IV., Th. 30, Cor. 3),

$$\text{The angle } AMB = \frac{360°}{\text{No. of sides of polygon,}}$$

And AMN is then known, being one half of AMB, since the triangle AMB is isosecles; and for the same reason AN is known, being one half of AB. Hence, AN and AMN being known, from the above proportion MN may be found.

2. What is the area of a regular polygon of eight sides, each side being 6 feet?

Solution.

$$AMN = \tfrac{1}{2}AMB = \tfrac{1}{2}\left(\frac{360}{8}\right) = 22° \ 30', \text{ and } AN = \tfrac{1}{2}AB = 3.$$

$$MN : 3 = R : \text{tan. } 22° \ 30'.$$

$$\begin{array}{ll} \text{Log. } R + \text{log. } 3 & = 10.477121 \\ \text{Less log. tan. } 22° \ 30' = & \ \ 9.617224 \\ \hline \text{Log. } MN & = \ \ 0.859897 = \text{log. } 7.243. \end{array}$$

$$\text{Area} = \tfrac{1}{2}(6 \times 8) \times 7.243 = 173.8 \text{ sq. ft., } \textit{Ans.}$$

quired the area of a regular nonagon whose side is

Ans. 890,18 sq. ft.

uired the area of a regular pentagon whose side is

Ans. 15.48 sq. ft.

2.—*Multiply the area of a regular polygon of the nber of sides, and each of whose sides is unity, by the one side of the required polygon.*

P represent the polygon whose area is required, and its sides; also, p the polygon whose side is unity, we (Geom., B. II., Th. 22),

$$p : P = 1^2 : a^2, \text{ or}$$

$$P = \frac{p \times a^2}{1}. \text{ Whence the rule.}$$

use of the above rule, the following table, giving the le polygons when the sides are unity, with their log- vill be found serviceable.

TABLE.

AMES.	SIDES.	AREAS.	LOGARITHMS.
e.........	3	0.4330127	$\bar{1}$.6365007
....	4	1.0000000	0.0000000
on........	5	1.7204774	0.2356490
n	6	2.5980762	0.4146519
on........	7	3.6339124	0.5603744
n.........	8	4.8284271	0.6838057
n	9	6.1818242	0.7911166
n.........	10	7.6942088	0.8861640
gon	11	9.3656399	0.9715375
gon.......	12	11.1961524	1.0490687

EXAMPLES.

1. What is the area of a regular pentagon whose side is 4 feet?

From the table, pentagon whose side is 1 = 1.7204774

Multiply by 4^2 = 16

Area required = 27.5276384

2. Required the area of a regular octagon whose side is 5 feet. *Ans.* 120.71 sq. ft. nearly.

3. Required the area of a regular heptagon whose side is 7 feet.

PROBLEM VII.

To determine the circumference of a circle from the radius or diameter.

RULE.—*Multiply the diameter by* 3.14159. (Geom., B. V., Th. 6.)

As π is always used to express the above 3.14159, the rule may be given analytically,

$$C = 2\pi R.$$

EXAMPLES.

1. What is the circumference of a circle whose radius is 5 feet?

2. What is the circumference of a circle whose diameter is 18 feet?

PROBLEM VIII.

To determine the diameter of a circle from the circumference.

RULE.—*Divide the circumference by* 3.14159; *or multiply by* .31831.

From Prob. VII, $C = 2\pi R \therefore 2R = \frac{C}{\pi}$.

EXAMPLES.

quired the diameter of a circle whose circumference feet. *Ans.* 12.67 feet, nearly.

hat is the radius of a circle whose circumference is iches?

hat is the diameter of a circle whose circumference is feet.

PROBLEM IX.

To determine the area of a circle.

1.—*Multiply the circumference by one half the radius.* B. V, Th. 1.)

2.—*Multiply the square of the radius by* 3.14159.

y Prob. VII., $C = 2\pi R$,

ule 1, $\text{Area} = C \times \frac{R}{2}$.

$$\text{Area} = 2\pi R \times \frac{R}{2} = \pi R^2$$

the analytical expression of the rules.

EXAMPLES

hat is the area of a circle whose radius is 9 feet?
Ans. $9 \times 9 \times 3.14159 = 254.47$ sq. ft., nearly.

hat is the area of a circle whose diameter is 12 rods?

hat is the area of a circle whose radius is 11 feet?

PROBLEM X.

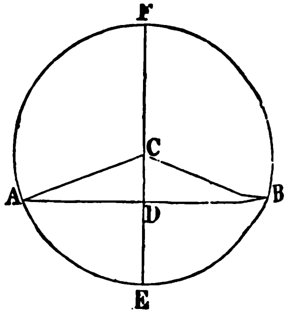
To determine the length of a circular arc of any number of degrees.

RULE.—*Multiply the circumference of the circle by the ratio between the number of degrees in the arc, and* 360°.

For (Geom., B. I., Def. 53, and Th. 2, Cor. 2),

$$360° : \text{circumference} = \text{number of degrees in arc} : \text{arc}$$

$$\text{Arc} = \text{circumference} \times \frac{\text{No. of degrees in arc}}{360°}$$



A. If the chord of the arc be given, and its height, the diameter may be readily found.

For (Geom. B. III., Th. 17, Cor.) AB being the chord, and DE the height of the arc, we have

$$DE \cdot DF = AD^2$$

$$DF = \frac{AD^2}{DE}$$

and $$FE = DF + DE.$$

B. If the diameter of the circle is known, and either the chord or height of the arc, the number of degrees in the arc may be determined.

By (Trig., Chap. 2, Sec. 2, Prop. III),

$$R : AC = \cos.ACD : CD \qquad (1)$$

$$R : AC = \sin.ACD : AD \qquad (2)$$

When $AC =$ radius of the circle, $CD =$ radius less t height of the arc, and $AD =$ one half the chord; ACD bei one half the angle subtended by the chord. From (1) havi radius of circle and height of arc, ACD may be found; a from (2) having radius AC and chord AB, the same an becomes known. Hence, we find the half arc and arc itsel

EXAMPLES.

1. Required the length of an arc of 22°, in a circle whose dius is 5 feet.

Solution.

Prob. VII, $3.14159 \times 10 = 31.4159 =$ circumference.

$$\text{Arc} = 31.4159 \times \frac{22}{360} = 1.92, \text{ nearly.}$$

2. What is the length of an arc whose chord is 12 feet in a rcle, whose radius is 14 feet?

Solution.

$$AC = 14\,;\ AD = \tfrac{1}{2}AB = \tfrac{12}{2} = 6.$$

From B, (2) $R : 14 = \sin.\ ACD : 6.$

$$\begin{aligned} \text{Log. } R + \text{log. } 6 &= 10.778151 \\ \text{Log. } 14 &= \underline{1.146128} \\ \text{Log. sin.} ACD &= 9.632023 = \sin.\ 25^\circ\ 22'\ 37'' \end{aligned}$$

$$\tfrac{1}{2} \text{ arc} = 25^\circ\ 22'\ 37'' \ \therefore \ \text{arc} = 50^\circ\ 45'\ 14''$$

Prob. VII., Circumference $= 3.14159 \times 28 = 87.96452$

$$50^\circ\ 45'\ 14'' = 50.75389^\circ.$$

$$\textit{Ans.}\ \left\{ \text{Arc} = 87.96452 \times \frac{50.75389^\circ}{360^\circ} = 12.4015. \right.$$

3. What is the length of an arc of 78° in a circle whose radius is 16 feet?

4. What is the length of an arc whose chord is 20 feet, in circle whose radius is 35 feet.

PROBLEM XI.

To find the area of a sector of a circle.

Rule.—*Multiply the arc of the sector by one half the dius.* (Geom., B. V, Th. 1.)

EXAMPLES.

1. What is the area of a sector of 20°, in a circle whose radius is 13 feet?

Solution.

Prob. VII, Circumference $= 3.14159 \times 26 = 81.68134$

Prob. X, Arc $= 81.68134 \times \frac{20}{360} = 4.53785$

Sector $= 4.53785 \times \frac{13}{2} = 29.496$ sq. ft.

Ans. 29.496 sq. ft.

2. Required the area of a sector of 32°, whose radius is 20 feet?

3. Required the area of a sector of 18°, whose radius is 1.5 feet? *Ans.* 0.35343 sq. ft.

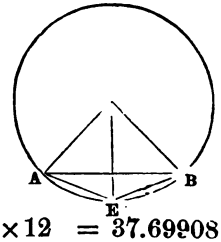
PROBLEM XII.

To find the area of a segment of a circle.

Rule.—*Determine the area of a sector included between the arc of the sector and radii; also the area of a triangle formed by the radii with the chord of the segment. If the segment be greater than a semicircle take the sum; if less, the difference, of these areas: the result will be the area required.*

EXAMPLES.

1. Required the area of the segment AEB, whose arc is 120°, where the radius of the circle is 6 feet.



Solution.

By Prob. VII. Circumference $= 3.14159 \times 12 = 37.69908$

By Prob. X. Arc $AEB = 37.69908 \times \frac{120}{360} = 12.56636$

By Prob. XI. Sector $AEBC = 12.56636 \times \frac{6}{2} = 37.69908$

By Prob. II., R. 2, Trian. $ACB = \frac{6 \times 6 \times \sin.120^\circ}{2R} = 15.58854$

Subtracting, since arc is less than 180°, segment $= 22.11054$

Area of segment 22.11054

2. Required the area of a circular segment, whose chord is 8 feet in a circle whose radius is 10 feet?

Ans. 4.48 feet, nearly.

3. What is the area of a circular segment whose chord is 20 and height 2 feet?

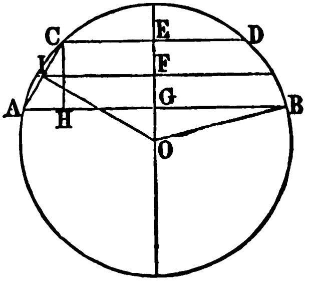
PROBLEM XIII.

To find the area of a zone included between two parallel chords.

RULE.—*Take the difference between the areas of the segments subtended by the upper and lower bases of the zone, which will be the area required.*

If only bases of zone and its height are known, the radius of the circle may be found as follows:

Let AB and CD, the bases, and EG, the height, be known. Draw AC a chord, and from the center O a perpendicular OI. $AI = IC$. (Geom. B. III, Th. 1.)



Draw also CH parallel to EG, and hence its equal; and IF parallel to AG and CE, and hence equal to

$$\tfrac{1}{2}(AG + CE),$$

since I is the middle point of AC.

In the similar triangles ACH and IOF (Geom. B. II, Th. 17, Cor. 1),

$$CH : AH = IF : FO, \qquad (1)$$

Or, $$EG : AG - CE = \frac{AG + CE}{2} : FO \qquad (2)$$

Whence $$FO = \frac{AG^2 - CE^2}{2EG} \qquad (3)$$

Now, $FG = \frac{1}{2}EG$, and $GO = FO - FG$. Hence,

$$GO = \frac{AG^2 - CE^2}{2\,EG} - \frac{EG}{2} = \frac{AG^2 - (CE^2 + EG^2)}{2\,EG} \qquad (4)$$

Radius of circle $= OB^2 = GO^2 + BG^2$ (or AG^2). Substituting for GO its value from (4),

$$\text{Radius} = OB = \sqrt{\left(\frac{AG^2 - (CE^2 + EG^2)}{2\,EG}\right)^2 + AG^2} \qquad (5)$$

Expressed in words, equation (5) will give the following

RULE.

To find radius when two parallel chords and their perpendicular distance are given:

From the square of half the greater chord, subtract the sum of the squares of half the lesser chord, and of the height; divide the remainder by twice the height; to the square of this quotient add the square of one half the greater chord, and extract the square root of the whole expression. The result will be the value of radius.

EXAMPLES.

1. Required the area of a zone whose bases are 80 and 60, and their perpendicular distance apart 18.94 feet.

Solution.

Taking equation (5) and substituting $AG = 40$, $CE = 30$, and $EG = 18.94$,

$$\text{Radius} = \sqrt{\left(\frac{1600 - (900 + 358.72)}{37.88}\right)^2 + 40^2} = 41.$$

By Prob. VII., circumference $= 3.14159 \times 82 = 257.61$.

To find greater segment.

From (Prob. X., B. Eq. 2),

$$R : 41 = \sin.\tfrac{1}{2}\text{ arc} : 40 \therefore$$

$$\tfrac{1}{2}\text{ arc} = 77^\circ\ 19'\ 11''. \quad \text{Arc} = 154^\circ\ 38'\ 22''.$$

By Prob. X., Length of arc $= 257.61 \times \frac{154.64}{360} = 110.65$

" XI., Sector $= 110.65 \times \tfrac{1}{2}.41 = 2268.46$

" II., Rule 2, triangle =

$$\frac{41 \times 41 \times \sin.154^\circ\ 38'\ 22''}{2\ R} = 359.996$$

Greater segment $=$ sector—triangle $= 1908.464$

To find lesser segment.

As before, $R : 41 = \sin.\tfrac{1}{2}\text{ arc} : 30$

$$\tfrac{1}{2}\text{ arc} = 47^\circ\ 1'\ 47'' \therefore \text{arc} = 94^\circ\ 3'\ 34''.$$

Prob. X., Length of arc $= 257.61 \times \frac{94.0594}{360} = 67.31$

" XI., Sector $= 67.31 \times \tfrac{1}{2}41 = 1379.85$

" II., Rule 2, triangle $= \frac{41^2 \times \sin.\ 94^\circ\ 3'\ 34''}{2\ R} = 838.39$

Lesser segment $= 541.46$

Zone=difference of segments=1908.464—541.46=1367.00.

2. Required the area of a zone whose bases are 96 and 60 inches, and altitude 26 inches.

Ans. 2136.75 sq. inches.

PROBLEM XIV.

To determine the area of an ellipse.

Rule.—*Multiply the product of the semi-axes by* 3.14159.

(For demonstration, see Conic Sections, Ellipse, 16th Theorem.)

EXAMPLES.

Required the area of an ellipse whose axes are 12 and 8.

$$6 \times 4 \times 3.14159 = 75.40 \text{ nearly.}$$

2. What is the area of an ellipse whose semi-axes are 25 and 20 feet.

Ans. 1570.8 sq. ft.

3. What is the area of an ellipse whose semi-axes are 12 and 9.

PROBLEM XV.

To determine the area of a parabola.

RULE.—*Take two thirds of the product of the base and perpendicular height.* (For demonstration, see Conic Sections, Parabola, Prop. 19th.)

1. What is the area of a parabola, the base being 20, and the altitude 12.

Ans. $\frac{2}{3}.20 \times 12 = 160$.

2. What is the area of a parabola when the base is 30, and the altitude 20 feet?

SECTION III.

MENSURATION OF SOLIDS.

In the mensuration of solids, the unit supposed to be applied is a cube, receiving its name from the name of one of its edges—as, a cubic inch, cubic foot, cubic yard.

As with surfaces, the ratio of lines is substituted for the ratio of solids, and by linear measurements we determine solidity.

The standards for solidity are given in the following

TABLE OF CUBIC OR SOLID MEASURES.

1728	cubic inches make	1 cubic foot.
27	cubic feet	1 cubic yard.
166⅜	cubic yards	1 cubic pole.
64000	cubic poles	1 cubic furlong.
512	cubic furlongs	1 cubic mile.

NOTE.—The measurement of the surfaces of solid bodies is included in this section for convenience.

PROBLEM I.

To determine the convex surface of a regular pyramid.

RULE.—*Multiply the perimeter of the base by one half the slant height.* (Geom., B. VII., Th. 17).

EXAMPLES.

1. What is the convex surface of a regular hexagonal pyramid, whose slant height is 12, and each side of its base 5 feet? *Ans.* 180 sq. ft.

2. What is the convex surface of a regular octagonal pyramid, whose slant height is 20 feet, and each side of the base 7 feet? *Ans.* 560 sq. ft.

PROBLEM II.

To determine the solidity of a pyramid.

RULE.—*Multiply the area of the base by one third of the altitude.* (Geom., B. VII., Th. 15.)

EXAMPLES.

1. What is the solidity of an octagonal pyramid, the sides of the base being each 8 feet, and the altitude 15 feet?

Solution.

By Sec. 2, Prob. VI., Rule 2,

$$\text{Area of base} = 4.8284271 \times 64 = 309.02$$

$$\textit{Ans.}\ 309.02 \times 5 = 1545.10 \text{ cu. ft.}$$

2. Required the solidity of a pentagonal pyramid, the altitude being 21 feet, and each side of the base 3 feet.

Ans. 108.39 cu. ft.

PROBLEM III.

To determine the convex surface of a right prism.

Rule.—*Multiply the perimeter of the base by the altitude* (Geom., B. VII., Th. 3.)

EXAMPLE.

1. What is the convex surface of a pentagonal prism, whose altitude is 12 feet; and each side of whose base is 2 feet?

Ans. 120 sq. ft.

2. What is the *entire* surface of a hexagonal prism, having an altitude of 7 feet, and each side of whose base is 3.5 feet?

Note.—For *entire* surface, the two bases must be included.

PROBLEM IV.

To determine the solidity of a prism.

Rule.—*Multiply the area of the base by the altitude* (Geom., B. VII., Th. 11.)

EXAMPLES.

1. Required the solidity of the octagonal prism, the altitude being 12 feet, and each side of the base 8 feet.

Solution.

By Sec. 2, Prob. VI., Rule 2,

$$\text{Area of base} = 4.8284271 \times 64 = 309.02 \text{ sq. ft.}$$
$$309.02 \times 12 = 3708.24 \text{ cu. ft.} = \text{solidity.}$$

2. Required the solidity of an heptagonal prism, each side of the base being 10 feet, and the altitude 30 feet.

3. Required the solidity of an octagonal prism, whose altitude is 5 feet, and each side of the base 4 inches.

PROBLEM V.

To determine the convex surface of a frustum of a regular pyramid.

Rule.—*Multiply the sum of the perimeters of the bases by one half the slant height of the frustum.* (Geom., B. VII., Th. 18.)

EXAMPLES.

1. What is the convex surface of a frustum of a regular octagonal pyramid; the sides of the bases being 5 and 3 feet respectively, and the slant height 6 feet.

Solution.

Lower base perimeter 40,
Upper base perimeter 24, $64 \times \frac{6}{2} = 192$ sq. ft.

2. What is the convex surface of a frustum of a regular

pentagonal pyramid, the slant height being 12, and the sides of the upper and lower bases 5 and 7.

NOTE.—In Problems I., III., and V., if the entire surface is required, the area of the bases must be added to the convex surface.

PROBLEM VI.

To determine the solidity of a frustum of a pyramid.

RULE.—*To the sum of the areas of the bases, add their mean proportional; multiply the sum by one third of the altitude; the product will be the required solidity.* (Geom., B. VII., Th. 16.)

EXAMPLES.

1. Required the solidity of a frustum of a pentagonal pyramid, the side of the bases being 6 and 4 feet, and the altitude 9 feet.

Solution.

Sec. 2, Prop. VI., R. 2, Upper base $= 1.7204774 \times 16 = 27.53$
Sec. 2, Prob. VI., R. 2, Lower base $= 1.7204774 \times 36 = 61.94$
Their mean proportional $= 1.7204774 \times 24 = 41.29$
Sum $= 130.76$

Ans. $130.76 \times 3 = 392.28$-

2. Required the solidity of a frustum of an hexagonal pyramid whose altitude is 15 feet, the sides of the bases being 5 and 2 feet. *Ans.* 506.65 cu. ft. nearly.

3. Required the solidity of a frustum of a triangular pyramid whose altitude is 6 feet, the side of the bases being 3 and 2 feet. *Ans.* 16.45 cu. ft. nearly.

PROBLEM VII.

To determine the solidity of a wedge.

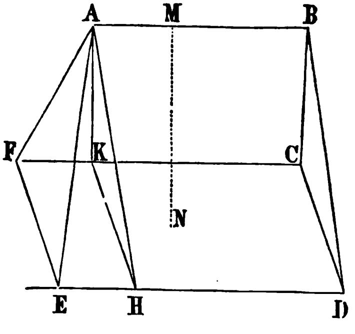
Definitions.—A wedge is a solid, bounded by five faces, viz.: a rectangle, two trapezoids, forming a plane angle, and two triangular ends. The common section of the two trapezoids is called the edge.

The base is the rectangular face.

The altitude is a perpendicular let fall from the edge upon the plane of the base.

RULE.—*To the edge add twice the length of the base, and multiply the sum by one sixth the product of the altitude and breadth of the base.*

Demonstration.



Let $AB - CDEF$, be a wedge. Through A pass a plane parallel to the plane of BCD, making AKH, equal to BCD. It is then clear that the wedge will be divided into two sections; viz.: $BCD-AKH$, a triangular prism, and $A-KHEF$, a quadrangular pyramid. If CF, the length of the base, be longer than AB, the edge, the wedge will be equal to the sum of these two sections; if CF be the shorter, the wedge will equal their difference.

Now let MN, the altitude $= a$,
AB, the edge $(=KC)$ $= E$,
CF or ED, length of base $= L$,
EF, or KH, or CD, breadth of base $= b$; KF will then equal $L-E$.

It is evident that the prism $BCD-AKH$ is equivalent to one half a parallelopiped, whose base is $CDHK$ and altitude MN; hence we have

$$\text{Solidity of } BCD-AKH=\tfrac{1}{2}(CD\cdot KC\cdot MN)=\tfrac{1}{2}(b\times E\times a) \quad (1)$$

By Problem II.,

$$\text{Solidity } A-KHEF = \tfrac{1}{3}ab(L-E) \quad (2)$$

But

$$\tfrac{1}{2}(b\times E\times a) = \tfrac{3}{6}abE = \tfrac{1}{6}ab\times 3E \quad (3)$$

and

$$\tfrac{1}{3}ab(L-E) = \tfrac{2}{6}abL-\tfrac{2}{6}abE = \tfrac{1}{6}ab\times(2L-2E) \quad (4)$$

Adding values for prism and pyramid as obtained in (3) and (4), and we have

$$\text{Wedge} = \tfrac{1}{6}ab\times(2L-2E+3E) = \tfrac{1}{6}ab(2L+E) \quad (5)$$

Whence the rule. The same result will be obtained when E is greater than L.

EXAMPLES.

1. Required the solidity of a wedge, when the edge is 9 feet, its altitude 10 feet, the breadth of the base 6 feet, and length of the same 14 feet. *Ans.* 370 cu. ft.

2. Required the solidity of a wedge, whose edge is 11 feet, its altitude 9 feet, the breadth of base 4, and length 20 feet. *Ans.* 306 cu. ft.

3. Required the solidity of a wedge, edge being 8, altitude 12, breadth of base 5, and length 4 feet.

PROBLEM VIII.

To determine the surface of a regular polyedron.

Rule 1.—*Multiply the area of one face by the number of faces.*

For, each face is a regular polygon, whose area may be found from the length of one edge; and the faces are also equal.

Rule 2.—*Multiply the surface of a polyedron of the same number of faces, whose edge is unity, by the square of an edge of the given polyedron.* (Geom., B. II., Th. 22.)

ırface of the polyedron whose edge is unity must be . by Rule 1. For the convenience of the student in ɔf Rule 2, we give a table of the surfaces and their ns.

TABLE.

NAME.	NO. OF FACES.	SURFACE.	LOGARITHMS.
dron..........	4	1.73205+	0.2385607
ꞁron...........	6	6.00000	0.7781513
.ron...........	8	3.46410+	0.5395907
ıedron.........	12	20.64573−	1.3148302
lron...........	20	8.66025+	0.9375307

EXAMPLES.

ıat is the surface of an octaedron, each of whose edges es?

Solution.

ɾ Sec. 2, Prob. VI., Rule 2,

of each face $= 0.4330127 \times 4^2 = 6.9282+$

$6.9282 \times 8 = 55.4256.$

ɾ Rule 2, $3.46410 \times 4^2 = 55.4256.$ *Ans.*

ıat is the surface of a dodecaedron, each of whose 2.5 inches?

PROBLEM IX.

termine the solidity of a regular polyedron.

1.—*Multiply the surface by one third of the perpen- let fall from the centre upon one of the faces.*

Demonstration.

By planes passed through the edges of the polyedron and its center, the solid will be divided into a number of pyramids whose bases will be the faces of the solid, and whose altitude will be the perpendicular from the centre to those faces. Each of these pyramids will be equal (Prob. II.) to its base into one third of its altitude; and the sum of the pyramids, that is, the polyedron, will equal the sum of the bases, that is, the surface into one third the common altitude, which is the perpendicular from center to face.

By Rule 1, the solidities of the regular polyedrons having *unity* for each edge have been calculated, and as (Geom., B. VII., Th. 19, Cor. 3,) polyedrons are as the cubes of their homologous edges, we have the following:

RULE 2. *Multiply the solidity of a polyedron whose edge is unity, and which has the same number of faces, by the cube of the edge of the required polyedron.*

For reference we give the solidities of the regular polyedrons, as determined by Rule 1, with their logarithms, in the following

TABLE.

NAME.	NO. OF FACES.	SOLIDITY.	LOGARITHM.
Tetraedron.........	3	0.11785	$\bar{1}.0713344$
Hexaedron.........	6	1.00000	0.0000000
Octaedron	8	0.47140	$\bar{1}.6733937$
Dodecaedron.......	12	7.66312	0.8844056
Icosaedron.........	20	2.18169	0.3387940

EXAMPLES.

1. Required surface and solidity of a regular octaedron, one of whose edges is 3 feet.

Solution.

$$\text{Surface} = 3.46410 \times 9 = 31.1769$$
$$\text{Solidity} = 0.47140 \times 27 = 12.7278.$$

2. Required the surface and solidity of a regular dodecaedron, each of whose edges is 5 feet.

Ans. $\begin{cases} \text{Surface} = 516.143 \text{ sq. ft.} \\ \text{Solidity} = 957.89 \text{ cub. ft.} \end{cases}$

3. Required the surface and solidity of an icosaedron, each of whose edges is 7 inches.

Ans. $\begin{cases} \text{Surface, } 424.35 \text{ sq. in.} \\ \text{Solidity, } 748.32 \text{ cu. in.} \end{cases}$

PROBLEM X.

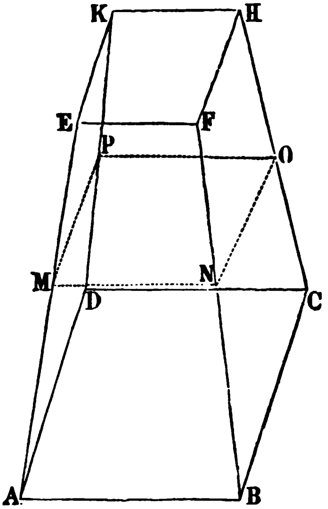
To determine the solidity of a prismoid.

Definition.—A prismoid is a solid bounded by six plane faces, two of which are rectangles and parallel, the other four being trapezoids. The rectangles are the bases of the figure.

Rule.—*To the areas of the bases, add four times the area of a section midway between them; multiply the sum by one sixth the altitude: the product will be the solidity required.*

Demonstration.

Let $ABCD-EFHK$ be a prismoid. Let a represent the altitude; l and b, length and breadth of upper base; L and B, length and breadth of lower base. If a plane be passed through $CD-EF$, the prismoid will be



divided into two wedges, having for common altitude a, the altitude of the prismoid, and for bases the upper and lower bases of the prismoid.

By Prob. VII., we have the solidity of these wedges respectively:

Solidity of $CD-EFHK = \frac{1}{6}ab\,(2l+L) =$
$$\tfrac{1}{6}a\,(2bl+bL). \quad (1)$$

Solidity of $EF-ABCD = \frac{1}{6}aB\,(2\,L+l) =$
$$\tfrac{1}{6}a\,(2BL+Bl) \quad (2)$$

Therefore adding (1) and (2), we have
$$\text{Prismoid} = \tfrac{1}{6}a\,(2BL+2\,bl+Bl+bL) \qquad (3)$$

Let m and n be the length and breadth of a section midway between the bases. Then $m=\frac{1}{2}(L+l)$, and $n=\frac{1}{2}(B+b)$,
$$mn = \tfrac{1}{4}(BL+bl+Bl+bL), \text{ and}$$
$$4\,mn = (BL+bl+Bl+bL). \qquad (4)$$

Substituting from (4) into (3), $4\,mn$ for its equal, we have,
$$\text{Prismoid} = \tfrac{1}{6}a\,(BL+bl+4\,mn). \qquad (5)$$

Whence the rule.

EXAMPLES.

1. Required the area of a prismoid, whose bases are 14 by 9 and 10 by 5, and whose altitude is 18.

$$\tfrac{1}{6}\times 18\big(14\times 9+10\times 5+4(12\times 7)\big) = 1536. \textit{ Ans.}$$

2. What is the solidity of a prismoid, whose bases are 7 by 5 and 3 by 3, and whose altitude is 3 feet?

Ans. 62 cubic feet.

3. Required the solidity of a prismoid, whose bases are 17 by 10 and 5 by 2, and whose altitude is 12 feet.

PROBLEM XI.

To determine the convex surface of a cone.

.—*Multiply the circumference of the base by one half* *t height.* (Geom. B. VII., Th. 20, Cor. 2.)

= height, we have analytically,

$$\text{Convex surface} = \pi RH.$$

EXAMPLES.

quired the convex surface of a cone, the radius of the ng 3, and the slant height 11 feet.

ec. 2, Prob. VII), circumference=$3.14159 \times 6 = 18.84$

$$18.84954 \times \frac{11}{2} = 103.67. \textit{ Ans.}$$

quired the convex surface of a cone, the radius of ase is 2, and slant height 6 feet.

quired the convex surface of a cone, the radius of ase is 5 inches, and slant height 12 inches.

PROBLEM XII.

To determine the solidity of a cone.

.—*Multiply the area of the base by one third of the* . (Geom. B. VII., Th. 21.)

tically, if A = altitude, we have,

$$\text{Solidity} = \tfrac{1}{3}\pi R^2 A.$$

EXAMPLES.

quired the solidity of a cone whose altitude is 9 feet, radius of the base 2 feet.

Solution.

By (Sec. 2, Prob. IX., Rule 2), area of base $= 3.14159 \times 4 = 12.566+$. $12.566 \times 3 = 37.70$. *Ans.*

2. Required the solidity of a cone, the radius of whose base is 5 feet, and altitude 12 feet.

3. Required the solidity of a cone, the radius of the base being 3 inches, and the altitude 8 inches.

PROBLEM XIII.

To determine the convex surface of a cylinder.

RULE.—*Multiply the circumference of the base by the altitude.* (Geom., B. VII., Th. 20, Cor. 1.)

If A represent the altitude and R the radius of the base, we have analytically,

$$\text{Convex surface} = 2\pi RA.$$

EXAMPLES.

1. What is the convex surface of a cylinder, the radius of the base being 4, and the altitude 10.

$$2\pi RA = 2 \times 3.14159 \times 4 \times 10 = 251.3272. \quad \textit{Ans.}$$

2 What is the convex surface of a cylinder whose altitude is 5 feet, and the radius of the base 2 feet?

3. What is the convex surface of a cylinder whose altitude is 3 feet, and the diameter of the base 9 inches?

PROBLEM XIV.

To determine the solidity of a cylinder.

RULE.—*Multiply the area of the base by the altitude.* (Geom., B. VII., Th. 22, Cor. 1.)

Expressed analytically, Solidity $= \pi R^2 A$.

EXAMPLES.

1. Required the solidity of a cylinder whose base has a radius of 3 feet, and whose altitude is 10 feet.

$$\pi R^2 A = 3.14159 \times 9 \times 10 = 282.7431 \text{ cu. ft. } Ans.$$

2. Required the solidity of a cylinder whose altitude is 8 feet, and the radius of the base 5 feet.

PROBLEM XV.

To determine the convex surface of the frustum of a cone.

RULE.—*Multiply the sum of the circumferences of the bases by one half the slant height of the frustum.* (Geom., B. VII., Th. 20.)

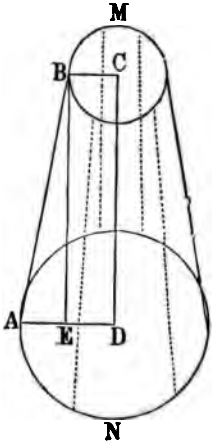
If R and r represent the radii of upper and lower bases, and H the slant height, we have analytical expressions.

$$\text{Convex surface} = \pi H(R+r).$$

If the radii of the bases and the altitude of the frustum are known, the slant height may be obtained by the following

RULE.—*Add the square of the altitude to the square of the difference between the radii, and extract the square root of the sum.*

Demonstration.



Let MN be the frustum, AB the slant height, AD and BC radii of the bases, and CD the altitude. Draw BE parallel to CD. Then $ED = BC$ and $AE = AD - BC$. Also $BE = CD$.

In right-angled triangle AEB,

$$AB^2 = BE^2 + AE^2,$$

or substituting and extracting root

$$AB = \sqrt{CD^2 + (AD-BC)^2}$$

Whence the rule.

EXAMPLES.

1. Required the convex surface of a frustum of a cone, the radii of the bases being 9 and 5 inches, and the altitude 3 inches.

Solution.

$$\text{Slant height} = \sqrt{9+(9-5)^2} = \sqrt{25} = 5.$$

By (Sec. 2, Prob. VII.),

Circumference upper base $= 3.14159 \times 10 = 31.4159$

Circumference lower base $= 3.14159 \times 18 = 56.5486$

Sum $= 87.9645$

Multiplied by $\frac{5}{2} = 219.911$. *Ans.*

2. Required the convex surface of a frustum of a cone, the radii of whose bases are 2 and 3 feet, and the slant height 6 feet.

3. Required the convex surface of a frustum of a cone, the radii of whose bases are 4 and 2, and the altitude 3 feet.

NOTE.—In Probs. XI., XIII., and XV., to obtain the entire surface, the areas of base or bases, must be included.

PROBLEM XVI.

To determine the solidity of a frustum of a cone.

RULE.—*Add the areas of the bases and a mean proportional between them; and multiply the sum by one third the altitude of the frustum.* (Geom., B. VII., Th. 22.)

Expressed analytically, A representing altitude,

$$\text{Solidity} = \tfrac{1}{3}A\pi(R^2+r^2+rR).$$

EXAMPLES.

1. Required the solidity of a frustum of a cone, the radii of whose bases are 3 and 4 feet, and whose altitude is 6 feet.

Solidity $= \frac{1}{3} \times 6 \times 3.14159\ (16+9+12) = 232.48-$. *Ans.*

2. Required the solidity of a frustum of a cone, the radii of whose bases are 5 and 7 feet, and altitude 9 feet.

3. Required the solidity of a frustum of a cone, the radii of whose bases are 10 and 13 inches, and whose altitude is 1 foot.

PROBLEM XVII.

To determine the surface of a sphere.

RULE.—*Multiply the circumference of a great circle by the diameter of the sphere.* (Geom., B. VII., Th. 25.)

By (Sec. 2, Prob. VII.), the circumference of a great circle $= 2\pi R$, or πD.

Multiply by $2R$ or D, and

$$\text{Surface} = 4\pi R^2, \text{ or } \pi D^2.$$

EXAMPLES.

1. Required the surface of a sphere whose radius is 5 feet.

Solution.

$$3.14159 \times 100 = 314.159$$

2. Required the surface of a sphere whose diameter is 2 feet.
Ans. 12.566.

3. Required the surface of a sphere whose radius is 11 feet.

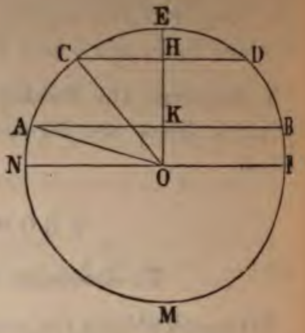
PROBLEM XVIII.

To determine the surface of a spherical zone.

RULE.—*Multiply the circumference of a great circle by the altitude of the zone.* (Geom., B. VII., Th. 25, Cor. 1.)

If A = altitude, we have

$$\text{Surface of zone} = 2\pi R \cdot A$$



REMARK 1.—If the radii of the section forming the zone, be known, and the radius of the sphere, the altitude of the zone may easily be found. In the figure, representing section of a sphere, AO and CO = radius of sphere, and AK and CH are known as radii respectively of sections forming the zone. Then (Geom., B. I., Th. 39,) $\sqrt{AO^2-AK^2} = KO$ (1), and $\sqrt{CO^2-CH^2} = HO$ (2). Also $HO-KO = HK$, the altitude of zone.

REMARK 2.—If the arcs of a great circle subtended by the diameters of the sections as chords be known, the altitude may also be found. For (in figure above), the arcs CE and AE would be known, being halves of the arcs CD and AB. Also arc $AN = 90° -$ arc AE. Hence the angles at the centre COE and $AON = OAK$, would be known.

Also the angle OCH, in the $R.A.$ triangle $COH = 90° - COE$.

Then in the triangles COH and AOK, by (Chap. 2, Sec. 2. Prop. III),

$$R : AO = \text{sin. } OAK : OK \qquad (1)$$

$$R : CO = \text{sin. } OCH : OH \qquad (2)$$

As before $OH-OK = HK$, the altitude of the zone.

EXAMPLES.

1. Required the surface of a spherical zone on a spher whose radius is 5 feet, and when the radii of the sections ar 4 and 3 feet.

Solution.

To find altitude of zone, AO or $CO = 5$, $AK = 4$, $CH = 3$, $HO = \sqrt{5^2 - 3^2} = 4$, $KO = \sqrt{5^2 - 4^2} = 3$. $\therefore HK = 1 = A$.

$$2\pi RA = 2 \times 3.14159 \times 5 \times 1 = 31.4159 \text{ sq. ft.} \quad \textit{Ans.}$$

2. Required the surface of a zone of a sphere whose radius is 9 feet, when the height of the zone is 3 feet.

3. Required the surface of a zone, on a sphere whose radius is 11 feet, where the arcs of the segments whose difference forms the zone, are 122° and 58°.

PROBLEM XIX.

To determine the solidity of a sphere.

RULE.—*Multiply the surface of the sphere by one third its radius.* (Geom., B. VII., Th. 29).

By Prob. XVII., surface $= 4\pi R^2$ or πD^2

Multiplying by $\frac{1}{3}R$, or $\frac{1}{6}D$, Solidity $= \frac{4}{3}\pi R^3$, or $\frac{1}{6}\pi D^3$.

EXAMPLES.

1. What is the solidity of a sphere whose radius is 2 inches?
Ans. 33.51.

2. What is the solidity of a sphere whose diameter is 40 inches?
Ans. 33510.4 cu. in.

3. What is the solidity of a sphere whose circumference is 24 inches?

PROBLEM XX.

To determine the solidity of a spherical segment.

RULE.—*Multiply the sum of the areas of the bases by one half the altitude of the segment, and to the product add the solidity of a sphere having this altitude as a diameter.* (Geom., B. VII., Th. 32.)

If R and r represent the radii of bases, and A the altitude of the zone, we have

$$\text{Solidity of segment} = \frac{A}{2}(\pi R^2 + \pi r^2) + \tfrac{1}{6}\pi A^3 =$$

$$\frac{\pi A}{2}(R^2 + r^2 + \tfrac{1}{3}A^2) \qquad (1)$$

If the segment have but one base, $r = 0$, and (1) becomes

$$\text{Solidity} = \frac{\pi A}{2}(R^2 + \tfrac{1}{3}A^2) \qquad (2)$$

EXAMPLES.

1. Required the solidity of a spherical segment whose bases have as radii 10 and 7 inches, and whose altitude is 3.113 inches.

$$\frac{\pi A}{2}(R^2 + r^2 + \tfrac{1}{3}A^2) = \frac{3.14159 \times 3.113}{2}(100 + 49 + 3.23) = 744.6.$$

Ans. 744.6 cu. in.

2. Required the solidity of a spherical segment whose bases have radii of 5 and 3 feet, and where the radius of the sphere is 6 feet.

REMARK.—The altitude of the segment will be found from two right-angled triangles, of which radius of the sphere will be hypothenuse, and the radii of the bases a side in each. The sum or difference of the third sides of these triangles will be the altitude of the zone, according as the sections are of different sides, or of the same side of the center of the sphere.

3. Required the solidity of a spherical segment of one base, whose radius is 3 feet, the altitude of the segment being 1.6 feet.

PROBLEM XXI.

To determine the area of a spherical triangle.

RULE.—*Multiply the area of the tri-rectangular triangle, or one-eighth of the surface of the sphere, by the excess of the angles of the given triangle over two right angles, and divide the product by* 90. (Geom., Part II., Sec. 1, Prop. 16).

If A, B, and C, represent the angles of the given triangle, $R.A.$ a right angle, and T the tri-rectangular triangle, we have

$$\text{Area} = \frac{(A+B+C-2\cdot R.A.)}{90}T.$$

The division by 90 is necessary in consequence of taking a right angle, or 90°, as the *unit*, instead of 1 degree. (Geom., Part II., Sec. 1, Th. 15, Cor. 2.)

EXAMPLES.

1. Required the area of a spherical triangle whose angles are 62°, 75°, and 102°, on a sphere whose radius is 9 feet.

Solution.

$$\text{Tri-rectangular triangle} = \tfrac{1}{8}\times 4\pi R^2 = 127.234 = T.$$

$$\frac{(A+B+C-2R.A.)}{90^\circ}\times T = \frac{62^\circ+75^\circ+102^\circ-180^\circ}{90^\circ}\times 127.234 =$$

$$\tfrac{59}{90}\times 127.234 = 83.47.$$

Ans. 83.41.

2. Required the area of a spherical triangle on the same sphere, whose angles are 81°, 92°, and 108°.

3. What is the area of a spherical triangle whose angles are 70°, 55°, and 87°, on a sphere whose radius is 3 feet?

PROBLEM XXII.

To determine the area of a spherical polygon.

RULE.—*From the sum of the angles of the polygon, subtract twice as many right angles as the figure has sides, less two; multiply the remainder by the tri-rectangular triangle, and divide by* 90. (Geom., Part II., Sec. 1, Prop. 17).

If $S =$ sum of the angles, and $n =$ the number of sides of the polygon,

$$\text{Area} = \frac{S-(n-2)2 \cdot R.A.}{90} \times T.$$

EXAMPLES.

1. Required the area of a spherical polygon of 6 sides, the sum of whose angles is 750°, on a sphere whose radius is 6 feet.

$\frac{1}{8}$ surface of sphere $=$ tri-rectangular triangle $= 56.56 = T$.

$$\left(\frac{S-(n-2)2 \cdot R.A.}{90}\right)T = \frac{750-720}{90} \times 56.56 = 18.85. \quad \textit{Ans.}$$

2. Required the area of a spherical polygon of 5 sides, where the sum of the angles is 765, on a sphere having a radius of 10 inches.

RECAPITULATION.

For convenience, as reference, we give the following *résumé* of the expressions for the surface and solidity most commonly in use.

Diameter is represented by D; radii by R and r; altitude by A; slant height by h.

The tri-rectangular triangle is represented by T, and the constant 3.14159 by π.

Circumference of circle $= 2\pi R$ or πD

Area " " $= \pi R^2$ or $\frac{1}{4}\pi D^2$

Arc of circle $= 2\pi R \times \frac{\text{angle}}{360^\circ}$

Convex surface of cone $= \pi R \cdot h.$

Entire surface of “ $= \pi Rh + \pi R^2.$

Solidity of “ $= \frac{1}{3}\pi R^2 \cdot A.$

Convex surface of cylinder $= 2\pi R \cdot A.$

Entire “ “ “ $= 2\pi RA + 2\pi R^2.$

Solidity “ “ “ $= \pi R^2 \cdot A.$

Convex surface of frustum $= \pi h(R+r).$

Entire “ “ “ $= \pi h(R+r) + \pi(R^2+r^2).$

Solidity “ “ “ $= \frac{1}{3}\pi A(R^2+r^2+Rr).$

Surface of sphere $= 4\pi R^2$ or $\pi D^2.$

Solidity of sphere $= \frac{4}{3}\pi R^3$ or $\frac{1}{6}\pi D^3.$

Surface of zone $= 2\pi R \cdot A.$

Solidity of zone (or segment) $= \frac{\pi A}{2}\left(R^2 + r + \frac{A^2}{3}\right)$

Area of spherical triangle $= \left(\frac{A+B+C-180^\circ}{90^\circ}\right)T.$

CHAPTER IV.

LAND SURVEYING.

SECTION I.

One of the most important applications of mathematics, for men in all departments of life, is Land Surveying. For the measurement of the areas of land many processes may be given, some exceedingly simple, to be applied to triangular and rectangular fields, and corresponding exactly with the plain rules of mensuration; others more intricate, and mainly interesting as mere mathematical processes. We shall give only the more practical, explaining several methods, but dwelling mainly on what is called the *rectangular method* of computing areas, the method most generally in use, and the one best adapted for application in all cases. Before proceeding to the rules the attention of the student is called to the definition of terms as used by surveyors, and to the explanation of the traverse table.

DEFINITIONS.

The unit of measure for land is the acre, which contains 10 square chains, or 160 square rods, the surveyor's chain being 4 rods in length.

The **Magnetic Meridian** is the direction of the magnetic needle, or a North and South line; and a line perpendicular to the magnetic meridian is called an East and West line.

The **Bearing of a Line** is the angle it makes with the magnetic meridian, and is sometimes called the course. The bearing is read from the nearest end of the needle. Thus a line that runs so as to make an angle of 40° with the direction of the needle, and is on the right hand, is said to be North 40° East; if it lies on the left hand, it will read North 40° West.

The **Length** of a line is the horizontal distance between its extreme points.

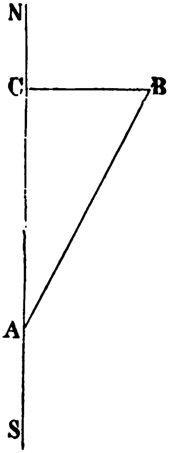
The **Northing** or **Southing** of a line, or its difference of latitude, is the distance between the East and West lines that pass through its extremities.

The **Easting** or **Westing** of a line, or its departure, is the distance between the meridians passing through its extremities

If AB represent any distance whose bearing is the angle CAB, then will AC be the difference of latitude, and BC the departure corresponding to that distance.

The distance is always the hypothenuse of a right-angled triangle, of which the latitude and departure are the other two sides, and the bearing is the angle opposite the departure.

Hence, if we multiply the distance by the sine of the bearing, the product will be the departure.



And if we multiply the distance by the cosine of the bearing, the product will be the difference of latitude.

Example 1.—If AB bears N. 22° 30′ E., 65.27 chains, what is the difference of latitude and the departure?

$$\begin{aligned} \text{Log. } 65.27 &= 1.814714 \\ \text{Cosine } 22^\circ\ 30' &= \underline{9.965615} \\ \text{Log. } 60.30 &= 1.780329 \end{aligned}$$

Whence AC, the difference of latitude, is 60.30 chains north.

Log. 65.27 = 1.814714
Sine 22° 30′ = 9.582840
Log. 24.98 = 1.397554

Whence BC, the departure, is 24.98 chains east.

Example 2.—A line bears N. 75° 45′ W., 49.50 chains. Required the difference of latitude and the departure.

Log. 49.50 = 1.694605
Cosine 75° 45′ = 9.391206
Log. 12.18 = 1.085811

Whence the northing is 12.18 chains.

Log. 49.50 = 1.694605
Sine 75° 45′ = 9.986427
Log. 47.98 = 1.681032

Whence the westing is 47.98 chains.

If we use the table of natural sines and cosines, we shall get the difference of latitude and departure by simple multiplication, as in the following examples:

Example 3.—The bearing of a certain line is N. 35° 18′ E.; distance 12 chains; what is the corresponding latitude and departure?

Angle 35° 18′	N. cos.	.81614	N. sin.	.57786
Dis. (multiplier)		12		12
Diff. lat.		9.79368	Dep.	6.93432

Example 4.—A certain line runs S. 4° 50′ E.; distance 74.40; what is the corresponding latitude and departure?

Angle 4° 50′	N. cos.	.9964	N. sin.	.0843
Distance		74.4		74.4
		39856		3372
		39856		3372
		69748		5901
Lat.		74.13216	Dep.	6.27192

In this way, by computing for various distances, the latitude and departure for each degree and quarter degree, or for each point and quarter point of the quadrant, and tabulating the results, we shall form what is called the

TRAVERSE TABLE.

This is a table much used by surveyors and navigators. By means of it, we can, with very little labor, find the latitude and departure of any distance and bearing within the limits of the table. Thus, in Example 1, if we look under 22° 30′, we find,

Latitude for 65 = 60.05; Departure for 65 = 24.87
Latitude for .27 = .25; Departure for .27 = 10
Latitude for 65.27 = 60.30; Departure for 65.27 = 24.97

Whence we have 60.30 chains northing,
and 24.97 chains easting.

Example 5.—A line bears S. 43° 30′ W., distance 80.25 chains. Required the difference of latitude and departure.

In the traverse table, under the angle 43° 30′, we find,

Latitude for 80 = 58.03; Departure for 80 = 55.07
Latitude for .25 = .18; Departure for .25 = .17
Latitude for 80.25 = 58.21; Departure for 80.25 = 55.24

Whence we have 58.21 chains southing,
and 55.24 chains westing.

Example 6.—A line bears N. 71° 30′ W., distance 35.18 chains. Required the latitude and departure.

In the table, over 71° 30′, we find,

Latitude for 35 = 11.11; Departure for 35 = 33.19
Latitude for .18 = .06; Departure for .18 = .17
Latitude for 35.18 = 11.17; Departure for 35.18 = 33.36

Whence we have 11.17 chains northing,
and 33.36 chains westing.

Example 6.—A line bears S. 28° E., distance 155.27 chains. Required the latitude and departure.

In the traverse table, under the angle 28°, we find

Latitude for 100 = 88.29 ; Departure for 100 = 46.95
Latitude for 55 = 48.56 ; Departure for 55 = 25.82
Latitude for .27 = .24 ; Departure for .27 = .13
Latitude for 155.27 = 137.09 ; Departure for 155.27 = 72.90

Example 7.—A line bears N. 48° 30′ W., distance 187.61 chains. Required the corresponding latitude and departure.

Ans. { Latitude = 124.31 chains N.
Departure = 140.51 " W.

Example 8.—A line bears S. 81° W., distance 76.87 chains. Required the corresponding latitude and departure.

Ans. { Latitude = 12.02 chains S.
Departure = 75.92 " W.

A traverse table computed to two places of decimals will answer for the ordinary calculations in land surveying. Where greater accuracy is required, and especially where the bearing does not agree with any angle in the table, the latitude and departure should be obtained by trigonometry, as in Examples 1 and 2.

SECTION II.

MEASUREMENT OF LINES AND ANGLES.

1. *To measure a line with a chain.*

To measure with a chain requires the assistance of two men; a fore chain-man and a hind chain-man. A picket or flag-staff should be set up in the direction of the line to be measured. The fore chain-man takes ten pins, and straightens out the chain; the hind chain-man puts his end of the chain at the point on the line where the measurement is to begin, and by calling *right* or *left*, he keeps the fore chain-man in line direct toward the flag-staff. When the chain is straight and horizontal, the hind chain-man calls *down*. Then the fore chain-man puts into the ground a pin precisely at his end of the chain; as soon as the pin is securely fixed, he calls *up*. Then they advance until the hind chain-man comes to the pin; after seeing that the fore chain-man is in line, the hind chain-man brings his end of the chain carefully to the pin, and when the chain is straight, he calls *down*. The fore chain-man then puts in another pin at his end of the chain and calls *up*. The hind chain-man then takes up the pin at his end of the chain, and they advance in this way until the pins are all down, or the end of the line is reached.

If the pins are all down, a tally must be made, and the ten pins again handed to the fore chain-man, when he advances as before. This operation must be repeated until the line is measured. Great care should be taken that no mistake be made in the tally, and that the links are correctly counted at the end of the line.

If the line to be measured is obstructed in any way so as to render its measurement difficult, offsets may be made, and pickets set up at equal distances from the line; then the distance required can be determined by measuring a line in the direction of the pickets or flag-staff, and this line will be parallel and equal to the line required to be measured.

2. *To find the bearing of a line with the surveyor's compass.*

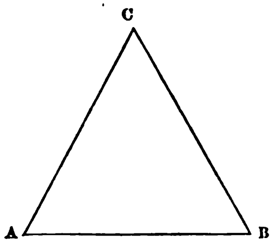
Place the compass firmly on its support, directly over a point in the line; set up a flag-staff at another distant point in the line; bring the compass carefully to a level; turn the sights accurately to the flag-staff; after the needle has settled to its position, read the bearing from the end of the needle nearest the direction of the line. If the view along the line is obstructed so that the flag-staff cannot be seen through the sights of the compass, then place the compass at some measured distance from the line, and set up the flag-staff at the same distance from the line, and the bearing of the flag-staff will be the bearing required.

SECTION III.

MEASUREMENT OF AREAS.

1. *To survey a triangular field.*

Measure the three sides of the field with a chain; or measure two sides, and with the compass measure the included angle. Then compute the area by the rules given in Mensuration.

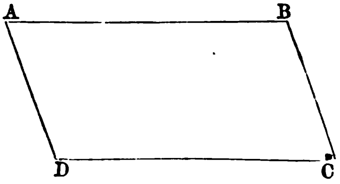


Example.—Let ABC be a triangular field; measure $AB = 24$ chains, measure $AC = 19.30$ chains, and measure the angle BAC, equal to 42° 30′. To find the area.

$$\begin{array}{ll} \text{Log. } 19.30 & = 1.285557 \\ \text{Log. } 24 & = 1.380211 \\ \text{Sin. } 42^\circ\ 30' & = 9.829683 \\ \hline \text{Log. } 312.932 & = 2.495451 \end{array}$$

Whence the double area in chains is 312.932. Divide by 2, and we have 156.466, which is the area in chains; move the decimal point one place, and we have 15.6466, which is the area of the field in acres and decimals of an acre.

2. *To survey a field in the form of a parallelogram.*



Measure two adjacent sides and the angle included by them. The area will be found by multiplying the two sides, and the sine of the included angle.

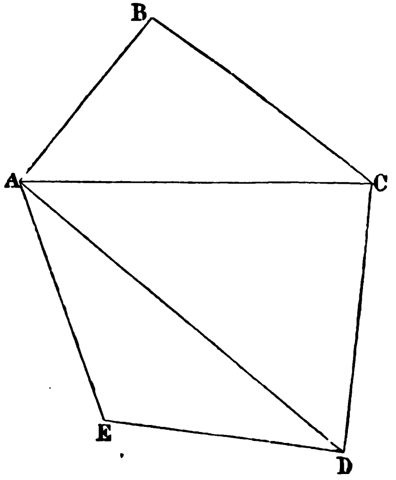
Example.—Let $ABCD$ be a field in the form of a parallelogram: the side AB was found to be 46 chains; the side AD was found to be 26 chains, and the angle at A was 82°. To find the area, we have

$$\begin{array}{ll} \text{Log. } 46 & = 1.662758 \\ \text{Log. } 26 & = 1.414973 \\ \text{Sin. } 82^\circ & = \underline{9.995753} \\ \text{Log. } 1184.36 & = 3.073484 \end{array}$$

Therefore, the area is 1184.36 chains,

Or, 118.436 acres. *Ans.*

3. *To survey a field where from one corner each of the other corners can be seen.*



In the diagram, B, C, D, E, are corners visible from the corner A. Measure the lines AB, AC, AD and AE, and take their bearings; then in each triangle, there will be two sides and the included angle to find the area.

Example. — Find the area from the following notes:

	BEARINGS.	CHAINS.
AB	$N\,40°\,E$	15
AC	E	25
AD	$S\,50°\,E$	30
AE	$S\,20°\,E$	18

Whence the angle $BAC = 50°$; $CAD = 40°$; $DAE = 30°$. To find the area of ABC, we have

$$\begin{aligned} \text{Log. } 15 &= 1.176091 \\ \text{Log. } 25 &= 1.397940 \\ \text{Sin. } 50° &= \underline{9.884254} \\ \text{Log. } 287.27 &= 2.458285 \end{aligned}$$

Whence the double area of ABC is 287.27 chains, which gives 14.3635 acres for the area.

To find the area of CAD, we have

$$\begin{aligned} \text{Log. } 25 &= 1.397940 \\ \text{Log. } 30 &= 1.477121 \\ \text{Sin. } 40° &= \underline{9.808067} \\ \text{Log. } 482.09 &= 2.683128 \end{aligned}$$

Whence the double area of CAD is 482.09 chains, or the area is 24.104 acres.

To find the area of DAE, we have

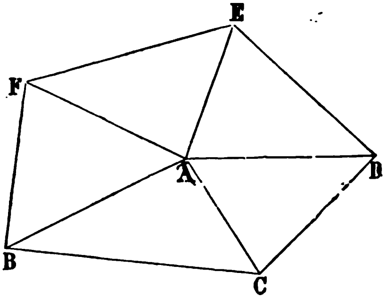
$$\begin{aligned} \text{Log. } 30 &= 1.477121 \\ \text{Log. } 18 &= 1.255273 \\ \text{Sin. } 30° &= \underline{9.698970} \\ \text{Log. } 270 &= 2.431364 \end{aligned}$$

Whence the double area of DAE is 270 chains, or the are is 13.50 acres.

$$\begin{aligned} \text{Therefore, the area of } ABC &= 14.3635 \\ \text{the area of } ACD &= 24.1040 \\ \text{the area of } ADE &= \underline{13.5000} \\ & 51.9675 \text{ acres,} \end{aligned}$$

which is the area of the field.

4. *To survey a field from a point within, from which each of the corners can be seen.*



Let $BCDEF$ be a field, and A a point from which all the corners can be seen.

Measure from the point A to each of the corners of the field, and also measure the angle contained by each two lines; then in each triangle there will be two sides, and the included angle to find the area.

Example.—Let $AB = 22$ chains,
$AC = 15$ "
$AD = 20$ "
$AE = 14$ "
$AF = 18$ "

Let the angles $BAC = 91°$
$CAD = 60°$
$DAE = 70°$
$EAF = 89°$
$FAB = 50°$

To find the area of ABC, we have,

$$\begin{array}{ll} \text{Log. } 22 & = 1.342423 \\ \text{Log. } 15 & = 1.176091 \\ \text{Sin. } 91° & = \underline{9.999934} \\ \text{Log. } 329.95 & = 2.518448 \end{array}$$

Whence the double area of ABC is 329.95 chains.

To find the area CAD, we have,

$$\begin{array}{ll} \text{Log. } 15 & = 1.176091 \\ \text{Log. } 20 & = 1.301030 \\ \text{Sin. } 60° & = \underline{9.937531} \\ \text{Log. } 259.81 & = 2.414652 \end{array}$$

Whence the double area of CAD is 259.81 chains.

To find the area of *DAE*, we have,

Log. 20 = 1.301030
Log. 14 = 1.146128
Sin. 70° = 9.972986
Log. 263.11 = 2.420144

Whence the double area of *DAE* is 263.11 chains.

To find the area of *EAF*, we have,

Log. 14 = 1.146128
Log. 18 = 1.255273
Sin. 89° = 9.999934
Log. 251.96 = 2.401335

Whence the double area of *EAF* is 251.96 chains.

To find the area of *FAB*, we have

Log. 18 = 1.255273
Log. 22 = 1.342423
Sin. 50° = 9.884254
Log. 303.35 = 2.481950

Whence the double area of *FAB* is 303.35 chains.

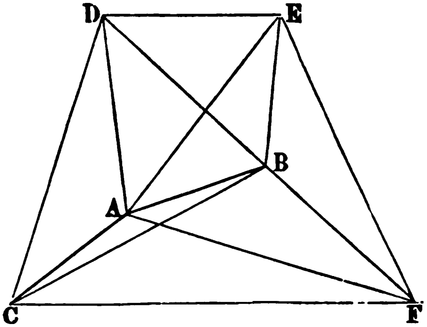
Therefore the double area of *ABC* is 329.95
" *CAD* " 259.81
" *DAE* " 263.11
" *EAF* " 251.96
" *FAB* " 303.35
2) 1408.18

The area of *BCDEF* = 70.409 acres.

5. *To survey a field from two stations within it.*

Measure the distance between the stations. Then measu
the angle between the line joining the two stations, and th
line from each station to each corner of the field. There wi

then a set of triangles, in each of which there will be one le and all the angles, determine the other les; after these sides e computed, there will a set of triangles about ch station, in each of hich there will be nown the two sides and e included angle to etermine the area; the m of the areas of the triangles of either set will give the area the field.



Example.—In the diagram let A and B be the stations, d C, D, E, F, be the corners of the field. Also suppose AB is und to be 25 chains, and the angles,

$BAD = 81^\circ\ 20'$ $ABD = 60^\circ$
$BAE = 35^\circ\ 15'$ $ABE = 115^\circ$
$BAF = 35^\circ$ $ABF = 120^\circ$
$BAC = 159^\circ$ $ABC = 11^\circ$

hen will the angles subtended by the line joining the stations e as follows:

$ADB = 38^\circ\ 40'$
$AEB = 29^\circ\ 45'$
$AFB = 25^\circ\ 0'$
$ACB = 10^\circ\ 0'$

We shall also have the angles,

$DAE = 46^\circ\ 5'$; $DBE = 55^\circ\ 0'$
$EAF = 70^\circ\ 15'$; $EBF = 125^\circ\ 0'$
$FAC = 124^\circ\ 0'$; $FBC = 109^\circ\ 0'$
$CAD = 119^\circ\ 40'$. $CBD = 71^\circ\ 0'$

In the triangles, we have,

Log. 25	=	1.397940	Log. 25	=	1.397940
Sin. 60°	=	9.937531	Sin. 81° 20′	=	9.995013
		11.335471			11.392953
Sin. 38° 40′	=	9.795733	Sin. 38° 40′	=	9.795733
Log. *AD*	=	1.539738	Log. *BD*	=	1.597220
Log. 25	=	1.397940	Log. 25	=	1.397940
Sin. 115°	=	9.957276	Sin. 35° 15′	=	9.761285
		11.355216			11.159225
Sin. 29° 45′	=	9.695671	Sin. 29° 45′	=	9.695671
Log. *AE*	=	1.659545	Log. *BE*	=	1.463554
Log. 25	=	1.397940	Log. 25	=	1.397940
Sin. 120°	=	9.937531	Sin. 35°	=	9.758591
		11.335471			11.156531
Sin. 25°	=	9.625948	Sin. 25°	=	9.625948
Log. *AF*	=	1.709523	Log. *BF*	=	1.530583
Log. 25	=	1.397940	Log. 25	=	1.397940
Sin. 11°	=	9.280599	Sin. 159°	=	9.554329
		10.678539			10.952269
Sin. 10°	=	9.239670	Sin. 10°	=	9.239670
Log. *AC*	=	1.438869	Log. *BC*	=	1.712599

It is obvious that the area of the field is the same as th area of the triangles about each station; that is, the triangle *DAE*, *EAF*, *FAC*, *CAD*, about the station *A*, form the are of the field. Also, the triangles *DBE*, *EBF*, *FBC*, *CB* about the station *B* form the area of the field.

To find the area of the triangle DAE, we have,

Log. AD = 1.539738
Log. AE = 1.659545
Sin. DAE = 9.857543
Log. 1139.8 = 3.056826

Therefore 1139.79 is the double area DAE.

For the triangle EAF, we have,

Log. AE = 1.659545
Log. AF = 1.709523
Sin. 70° 15′ = 9.973671
Log. 2201.6 = 3.342739

Therefore the double area of EAF is 2201.6 chains.

For the triangle FAC, we have,

Log. AF = 1.709523
Log. AC = 1.438869
Sin. FAC = 9.918574
Log. 1166.72 = 3.066966

Therefore the double area of FAC is 1166.72 chains.

For the triangle CAD, we have,

Log. AC = 1.438869
Log. AD = 1.539738
Sin. CAD = 9.938980
Log. 827.15 = 2.917587

Therefore the double area of CAD is 827.15 chains.

For the triangle DBE, we have,

Log. BD = 1.597220
Log. BE = 1.463554
Sin. 55° = 9.913365
Log. 942.19 = 2.974139

Therefore the double area of DBE is 942.19.

For the triangle EBF, we have,

Log. BE = 1.463554
Log. BF = 1.530583
Sin. 125° = 9.913365
Log. 808.17 = 2.907502

Therefore the double area of EBF is 808.17 chains.

For the triangle FBC, we have,

Log. BF = 1.530583
Log. BC = 1.712599
Sin. 109° = 9.975670
Log. 1655.2 = 3.218852

Therefore the double area of FBC is 1655.21 chains.

For the triangle CBD, we have,

Log. CB = 1.712599
Log. BD = 1.597220
Sin. 71° = 9.975670
Log. 1929,7 = 3.285489

Therefore the double area of CBD is 1929.7 chains.

Hence, the triangles about the station A give

$$\begin{array}{rl} DAE = & 1139.79 \\ EAF = & 2201.6 \\ FAC = & 1166.72 \\ CAD = & 827.15 \\ \hline 2\,)\,\, & 5335.26 \\ \hline & 266.763 \end{array}$$

266.763 acres, the area of the field.

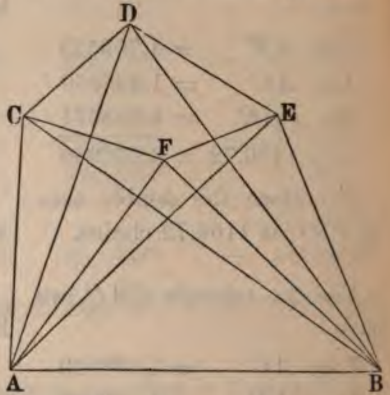
The triangles about the station B give

$$\begin{array}{rl} DBE = & 942.19 \\ EBF = & 808.17 \\ FBC = & 1655.21 \\ CBD = & 1929.70 \\ \hline 2\,)\,\, & 5335.27 \\ \hline & 266.763 \end{array}$$

266.763 acres,

the area of the field, which agrees with the above.

6. *To survey a field from two stations without the field.*



Measure the distance between the two stations. Take the bearing of each corner of the field from each of the stations, and also the bearing of one station from the other. Then there will be a set of triangles in each of which there will be known one side, and all the angles, to determine the other sides—then there will be a set of triangles for each station, in which triangles there will be known two sides, and the included angle of each, to determine the area.

Example.—Let $CDEF$ be a field, and A and B two stations without it. Measure AB, and suppose it be found 20 chains, and suppose the angles are found as below,

$$\begin{array}{ll@{\qquad\qquad}ll}
BAC = & 88^\circ & ABC = & 36^\circ \\
BAD = & 70^\circ & ABD = & 54^\circ \\
BAE = & 43^\circ & ABE = & 68^\circ \\
BAF = & 53^\circ & ABF = & 44^\circ
\end{array}$$

Then we shall have

$$\begin{array}{ll@{\qquad\qquad}ll}
CAD = & 18^\circ & CBD = & 18^\circ \\
DAE = & 27^\circ & DBE = & 14^\circ \\
EAF = & 10^\circ & EBF = & 24^\circ \\
FAC = & 35^\circ & FBC = & 8^\circ
\end{array}$$

We have also the angles

$$\begin{array}{ll}
ACB = & 56^\circ \\
ADB = & 56^\circ \\
AEB = & 69^\circ \\
AFB = & 83^\circ
\end{array}$$

Then to find AC and BC, we have

$$\begin{array}{lr@{\qquad\qquad}lr}
\text{Log. } 20 = & 1.301030 & \text{Log. } 20 = & 1.301030 \\
\text{Sin. } 36^\circ = & 9.769219 & \text{Sin. } 88^\circ = & 9.999735 \\
\cline{2-2}\cline{4-4}
 & 11.070249 & & 11.300765 \\
\text{Sin. } 56^\circ = & 9.918574 & \text{Sin. } 56^\circ = & 9.918574 \\
\cline{2-2}\cline{4-4}
\text{Log. } AC = & 1.151675 & \text{Log. } BC = & 1.382191
\end{array}$$

To find AD and BD, we have

$$\begin{array}{lr@{\qquad\qquad}lr}
\text{Log. } 20 = & 1.301030 & \text{Log. } 20 = & 1.301030 \\
\text{Sin. } 54^\circ = & 9.907958 & \text{Sin. } 70^\circ = & 9.972986 \\
\cline{2-2}\cline{4-4}
 & 11.208988 & & 11.274016 \\
\text{Sin. } 56^\circ = & 9.918574 & \text{Sin. } 56^\circ = & 9.918574 \\
\cline{2-2}\cline{4-4}
\text{Log. } AD = & 1.290414 & \text{Log. } BD = & 1.355442
\end{array}$$

To find AE and BE, we have

Log. 20 = 1.301030
Sin. 68° = 9.967166
11.268196
Sin. 69° = 9.970152
Log. AE = 1.298044

Log. 20 = 1.301030
Sin. 43° = 9.833783
11.134813
Sin. 69° = 9.970152
Log. BE = 1.164661

To find AF and BF, we have

Log. 20 = 1.301030
Sin. 44° = 9.841771
11.142801
Sin. 83° = 9.996751
Log. AF = 1.146050

Log. 20 = 1.301030
Sin. 53° = 9.902349
11.203379
Sin. 83° = 9.996751
Log. BF = 1.206628

We now have the logarithms of the sides of the several triangles at each station.

To find the area of the triangle ACD, we have

Log. AC = 1.151675
Log. AD = 1.290414
Sin. CAD = 9.489982
Log. 85.52 = 1.932071

Therefore the double area of CAD is 85.52 chains.

To find the area DAE, we have,

Log. AD = 1.290414
Log. AE = 1.298044
Sin. 27° = 9.657047
Log. 176 = 2.245505

Therefore the double area of DAE is 176 chains.

To find the area of CBD we have

Log. BC = 1.382191
Log. BD = 1.355442
Sin. 18° = 9.489982
Log. 168.89 = 2.227615

Therefore the double area of CBD is 168.9 chains.

To find the area of DBE, we have,

Log. BD = 1.355442
Log. BE = 1.164661
Sin. 14° = 9.383675
Log. 80.13 = 1.903778

Therefore the double area o
DBE is 80.13 chains.

To find the area of *EAF*, we have,

$$\begin{array}{lcl} \text{Log. } AE & = & 1.298044 \\ \text{Log. } AF & = & 1.146050 \\ \text{Sin. } 10^\circ & = & 9.239670 \\ \hline \text{Log. } 48.28 & = & 1.683764 \end{array}$$

Therefore the double area of *EAF* is 48.28 chains.

To find the area of *FAC*, we have,

$$\begin{array}{lcl} \text{Log. } AF & = & 1.146050 \\ \text{Log. } AC & = & 1.151675 \\ \text{Sin. } 35^\circ & = & 9.758591 \\ \hline \text{Log. } 113.85 & = & 2.056316 \end{array}$$

Therefore the double area of *FAC* is 113.85 chains.

To find the area of *EBF*, we have,

$$\begin{array}{lcl} \text{Log. } BE & = & 1.164661 \\ \text{Log. } BF & = & 1.206628 \\ \text{Sin. } 24^\circ & = & 9.609313 \\ \hline \text{Log. } 95.63 & = & 1.980602 \end{array}$$

Therefore the double area of *EBF* is 95.63 chains.

To find the area of *FBC*, we have,

$$\begin{array}{lcl} \text{Log. } BF & = & 1.206628 \\ \text{Log. } BC & = & 1.382191 \\ \text{Sin. } 8^\circ & = & 9.143555 \\ \hline \text{Log. } 54 & = & 1.732374 \end{array}$$

Therefore the double area of *FBC* is 54 chains.

It is obvious that if from the sum of the areas of the triangles *CAD* and *DAE*, we subtract the sum of the areas of the triangles *EAF* and *FAC*, we shall have the area of the field. Also, if from the sum of the areas of the triangles *CBD* and *DBE*, we subtract the sum of the triangles *EBF* and *FBC*, we shall also have the area of the field.

Therefore, since the double area of

$$\begin{array}{rcr} CAD & = & 85.52 \\ DAE & = & 176.00 \\ \hline & & 261.52 \\ \\ EAF & = & 48.28 \\ FAC & = & 113.85 \\ \hline & & 162.13 \\ \hline & 2\,) & 99.39 \text{ chains.} \\ \hline \text{Area of the field} & = & 4.9695 \text{ acres.} \end{array}$$

Again, the double area of

$$\begin{array}{rr l}
CBD = & 168.89 & \\
DBE = & 80.13 & \\
\hline
 & 249.02 & \\
EBF = & 95.63 & \\
FBC = & 54.00 & \\
\hline
 & 149.63 & \\
\hline
2\,) & 99.39 & \text{chains.} \\
\hline
 & 49.695 & \text{acres.}
\end{array}$$

the area of the field as before.

SECTION IV.

RECTANGULAR SURVEYING.

1. *To survey a field with a chain and compass.*

Begin at any convenient corner of the field to be surveyed, take the bearing of the first side with the compass, and enter it in degrees and minutes in a note book as the first course; measure the length of the side with the chain, and enter it in chains and decimals, or in chains and links, in the note book opposite the first course. Then keeping the field on the right hand, proceed to the second side, take its bearing and measure its length, which measurements enter in the note book; and so proceed until each side of the field has been measured. The entries made in the note book are called field-notes. Any mark which may distinguish either a side or a corner of the field should be carefully entered in its proper place in the note book, since it is from these notes that the area must be determined, the diagram drawn, and the survey bill written out.

find the area of a field whose sides have been meas-

e we have the following field notes:

1	N. 23° E.	17	chains.
2	N. 83° E.	11	"
3	S. 14° E.	23	"
4	N. 77° W.	23.73	"

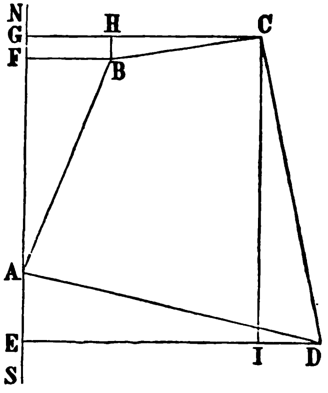


diagram let *ABCD* re- he field whose measure- re been taken. Through ı north and south line ı *B*, *C* and *D* draw the ulars *BF*, *CG* and *DE*. ious that if from the *CDEG* we take the *AE*, the triangle *ABF* rapezoid *FBCG*, there in the field *ABCD*. ake from the traverse latitude and departure for each course and distance, ge all as in the following tablet.

E.	DISTANCE.	N.	S.	E.	W.	MERIDIAN DIST.	DOUBLE MERID. DIST.	N. A.	S. A.
E.	17	15.65		6.64		6.64	6.64	103.9160	
E.	11	1.34		10.92		17.56	24.20	32.4280	
E.	23		22.32	5.56		23.12	40.68		907.9776
W.	23.73	5.33			23.12	0	23.12	123.2296	
								259.5736	907.9776
									259.5736

Double area in chains = 2) 648.4040

Area in acres = 32.42020

In the tablet we see that $AF = 15.65$, $BH = 1.34$, $CI = 22.32$, and $EA = 5.33$; also $FB = 6.64$, $HC = 10.92$, $DI = 5.56$, and $DE = 23.12$. In the right column, the first number 6.64 is BF; the second number 17.56 is CG, found by adding FB and HC; the third number 23.12 is DE, found by adding CG and DI. The ninth column contains multipliers, found by adding the numbers of the eighth column. The first number 6.64 is FB; the second number 24.20 is the sum of FB and CG; the third number is the sum of CG and DE; the fourth number is DE. The first number in the tenth column is the double area of the triangle ABF; the second number is the double area of the trapezoid $FBCG$; the third number is the double area of the triangle AED. The number in the eleventh column is the double area of the trapezoid $CDEG$.

If we subtract the sum of the numbers in the tenth column from that of the eleventh, we shall find 648.4040, which is the double area of $ABCD$ in square chains. If we divide by 2, and move the decimal point one place to the left, we shall get 32.4202 acres for the area of the field.

From the above example, we give the following summary for finding the area of any field.

RULE.—1. *Prepare a table headed as in the example, namely, Bearings, Distance, North, South, East, West, Meridian distance, Double meridian distance, North areas, South areas.*

2. *Begin at the most western point of the field, and conceive a meridian to pass through that point.*

Find, by the traverse table or by trigonometry, the northings, southings, eastings, and westings of the several sides of the field, and set them in the table opposite their respective stations, under their proper letters, N., S., E., or W.

3. *For the first meridian distance take the departure of the first line; for the second, take the first meridian distance and*

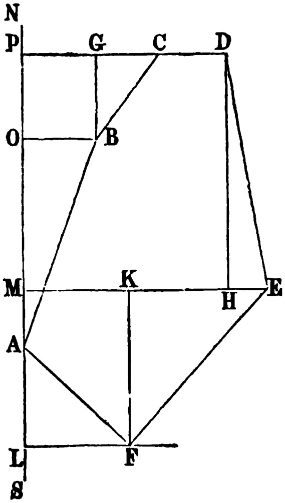
add to it the departure of the second line, if the departure is east, or subtract if west, &c.

4. *Add each two adjacent meridian distances, and set their sum opposite the last of the two in the column of double meridian distances.*

5. *Multiply each double meridian distance by the latitude to which it is opposite, and set the product in the column of N. areas if the latitude is north, and in that of S. areas if the latitude is south.*

6. *Subtract the sum of the N. areas from that of the S. areas, and take half the remainder, which will be the area of the field in square chains. Dividing this by* 10 *gives the acres.*

Example.—It is required to find the area of the field *ABCDEF* from the following notes.



1	*AB*	N. 20° E.	= 17.87 chains.
2	*BC*	N. 30° E.	= 8.40 "
3	*CD*	East.	= 6.32 "
4	*DE*	S. 10° E.	= 19.20 "
5	*EF*	S. 40° W.	= 16.80 "
6	*FA*	N. 50° W.	= 12.00 "

Take from the traverse table the latitude and departure for each side of the field, and arrange them as in the following tablet.

	BEARING.	DISTANCE.	N.	S.	E.	W.	MERIDIAN DIST.	DOUBLE MERID. DIST.	N. A.	S. A.
1	N. 20° E.	17.87	16.79		6.13		6.13	6.13	102.9227	
2	N. 30° E.	8.40	7.28		4.20		10.33	16.46	119.8288	
3	E.	6.32			6.32		16.65	26.98		
4	S. 10° E.	19.20		18.91	3.33		19.98	36.63		692.6733
5	S. 40° W.	16.80		12.87		10.79	9.19	29.17		375.417
6	N. 50° W.	12.00	7.71			9.19	0	9.19	70.8549	
									293.6064	1068.091
										293.606
										774.48
										38.724

Comparing the tablet with the diagram, we find

Latitudes.

$AO = 16.79$
$BG = 7.28$
$DH = 18.91$
$KF = 12.87$
$LA = 7.71$

Departures.

$OB = 6.13$
$GC = 4.20$
$CD = 6.32$
$EH = 3.33$
$EK = 10.79$
$FL = 9.19$

Meridian Distances.

$BO = 6.13$
$CP = 10.33$
$DP = 16.65$
$EM = 19.98$
$FL = 9.19$

Double Meridian Distances.

$BO = 6.13$
$BO + CP = 16.46$
$CP + CD = 26.98$
$DP + EM = 36.63$
$EM + FL = 29.17$
$FL = 9.19$

From the tenth column, we find

That the double area of $AOB = 102.9227$ chains,
" " " $OBCP = 119.8288$ "
" " " $ALF = 70.8549$ "

293.6064

the eleventh column,

the double area of $PDEM = 692.6733$ chains,

" " $MEFL = 375.4179$ "

1068.0912

fore, we have the double area of

$PDEFL = 1068.0912$ chains,

louble area of $PCBAFL = 293.6064$

acting, we get 774.4848

the double area of $ABCDEF$, and dividing by 2 and ve get the area 38.72424 acres.

ple.—Required the area of a field from the following

1.	N. 33° 30′ E.	= 35.30 chains,
2.	N. 76° E.	= 16.00 "
3.	S.	= 9.00 "
4.	S. 10° W.	= 11.29 "
5.	S. 75° W.	= 13.70 "
6.	S. 20° 30′ W.	= 10.30 "
7.	W.	= 16.20 "

ING.	DIST.	N.	S.	E.	W.	MERIDIAN DIST.	DOUBLE MERID. DIST.	N. A.	S. A.
30′ E.	35.30	29.44		19.49		19.49	19.49	573.7856	
E.	16.00	3.87		15.52		35.01	54.50	210.9150	
	9.00		9.00			35.01	70.02		630.1800
W.	11.29		11.12		1.97	33.04	68.05		756.7160
W.	13.70		3.54		12.24	19.80	52.84		187.0536
30′ W.	10.30		9.65		3.60	16.20	36.00		347.4000
V.	16.20				16.20	0.0	16.20		
								784.7006	1921.3496
									784.7006
									1136.6490
					Area in acres				56.83245

EXAMPLES.

Required the areas of the fields whose sides and bearings are given in the following tablets.

(1.)

	BEARINGS.	CHAINS.
1	S.	27.00
2	N. 87° W.	14.00
3	N. 4° 13′ E.	46.92
4	S. 27° 15′ E.	23.00

Ans. 47 acres.

(2.)

	BEARINGS.	CHAINS.
1	N. 20° 30′ E.	11.66
2	S. 79° 45′ E.	20.30
3	S. 27° 30′ W.	18.90
4	N. 63° 15′ W.	16.56
5	N. 15° 30′ W.	2.08

Ans. 29.896 acres.

(3.)

	BEARINGS.	CHAINS.
1	S. 80° E.	3.45
2	S. 69° E.	38.19
3	S. 15° 45′ W.	15.00
4	N. 66° 45′ W.	3.15
5	N. 49° 24′ W.	42.26

Ans. 34.35 acres.

(4.)

	BEARINGS.	CHAINS.
1	S. 31° W.	8.70
2	N. 70° 45′ W.	26.76
3	S. 41° 45′ W.	6.24
4	N. 63° W.	12.54
5	N. 27° 15′ E.	28.26
6	S. 49° 26′ E.	42.30

Ans. 73.849 acres.

(5.)

	BEARINGS.	CHAINS.
1	N. 29° 50′ W.	10.61
2	N. 62° 45′ E.	9.25
3	S. 36° E.	7.60
4	S. 45° 30′ W.	10.40

Ans. 8.81 acres.

(6.)

	BEARINGS.	CHAINS.
1	N. 45° E.	40.12
2	S. 30° W.	25.00
3	S. 5° E.	36.00
4	W.	29.60
5	N. 20° E.	31.00

Ans. 85.58 acres.

(7.)

	BEARINGS.	CHAINS.
1	N. 58° E.	19.00
2	S. 84° E.	20.00
3	S. 17° W.	20.00
4	W.	20.00
5	N. 42° 19′ W.	15.07

Ans. 54.95 acres.

(8.)

	BEARINGS.	CHAINS.
1	S. 46° 30′ E.	20.00
2	S. 51° 45′ W.	16.29
3	W.	21.25
4	N. 56° W.	27.60
5	N. 33° 15′ E.	18.80
6	S. 77° 13′ E.	32.92

Ans. 112.90 acres.

3. *To balance the work when the survey is slightly incorrect.*

If the field notes have been accurately taken, and the latitudes and departures accurately computed, the sum of the northings will equal the sum of the southings, and the sum of the eastings will equal the sum of the westings. This is a good test of the accuracy of the work. If the northings do not equal the southings, the difference is called the error in latitude; and if the eastings do not equal the westings, the difference is called the error in departure. When these errors are small they may be *distributed* by the proportion:

As the sum of the sides of the field is to the error in latitude or departure, so is each side to the correction belonging to that side.

In most cases the latitudes or the departures may be made equal by taking half the error from the numbers in that column which gave the greater sum, and adding half the error to the numbers in the column which gave the smaller sum; and the area computed from the corrected latitudes and departures will be near the truth.

When any of the sides are more difficult to be measured accurately than others, the surveyor must use his judgment in applying the corrections.

Example.—Required the area of a piece of land, of which the following are the *field-notes.*

	BEARINGS.	CHAINS.
1	N. 40° E.	20.00
2	S. 50° E.	30.00
3	S. 40° W.	40.00
4	N. 16¼° W.	36.05

From the traverse table, we find the following tablet.

	BEARINGS.	CHAINS.	LATITUDES.		DEPARTURES.	
			N.	S.	E.	W.
1	N. 40° E.	20.00	15.32		12.86	
2	S. 50° E.	30.00		19.28	22.98	
3	S. 40° W.	40.00		30.64		25.71
4	N. 16¼° W.	36.05	34.61			10.08
		126.05	49.93	49.92	35.84	35.79

The error in the latitudes is one link, and the error in the departure is 5 links. As these are small errors, they may be so distributed as to make the latitudes and the departures balance by the following Rule.

As the sum of all the sides is to the error in latitude or departure, so is each side to the correction for that side.

Thus, we have the following proportions:

126.05 : 5 : : 20 : 1, the correction for the first side in departure.

126.05 : 5 : : 30 : 1, for the second side.

126.05 : 5 : : 40 : 2, " third side.

126.05 : 5 : : 36.05 : 1, for the fourth side.

In this example, the error in latitude being only one link, may be applied to the southing of the third side, or the orthing of the fourth side.

And as the eastings are greater than the westings, the corection for the first and second sides must be subtracted, and ose for the third and fourth sides must be added.

The corrected latitudes and departures are as follows:

	BEARINGS.	CHAINS.	N.	S.	E.	W.			N. A.	S. A.
1	N. 40° E.	20.00	15.32		12.85		12.85	12.85	196.8620	
2	S. 50° E.	30.00		19.28	22.97		35.82	48.67		938.3576
3	S. 40° W.	40.00		30.65		25.73	10.09	45.91		1407.1415
4	N. 16¼° W.	36.05	34.61			10.09	0.0	10.09	349.2149	
									546.0769	2345.4991 546.0769

2) 1799.4222

89.97111

hence the area is 89.97 acres.

It is not always necessary to work out a proportion for each rrection. The latitudes and departures may be balanced by btracting half the error from the numbers in that column hich gives the greater sum, and adding half the error to the umbers in the lesser column.

In this method, we usually distribute the half error in prortion to the latitudes or departures. The surveyor should so use his judgment in applying the corrections to those des difficult to be measured accurately, so as to make greater rrections where errors are most likely to arise.

Again, the errors may be supposed to arise *in part* from correct measurement of the angles, in taking the bearings. nd it should be borne in mind that when the angle is small, e error in its measurement will affect the *departure* mainly; ut when the angle is large, the error will be chiefly felt in he *latitude*.

EXAMPLES.

In the following examples correct the latitudes and departures, and compute the areas.

(1.)

	BEARINGS.	CHAINS.
1	S. 10° W.	38.00
2	N. 71° W.	30.50
3	N. 37° 45′ E.	38.00
4	S. 78° E.	12.50

Ans. 78.66 acres.

(2.)

	BEARINGS.	CHAINS.
1	N. 12° 45′ E.	24.26
2	S. 71° 55′ E.	15.59
3	S. 34° E.	9.17
4	S. 66° 15 W.	27.69

Ans. 31.31 acres nearly.

(3.)

	BEARINGS.	CHAINS.
1	N. 20° E.	15.00
2	E.	10.10
3	S. 10° E.	20.00
4	S. 50° W.	13.50
5	N. 30° W.	16.40

Ans. 35.42 acres.

(4.)

	BEARINGS.	CHAINS.
1	S. 32° W.	15.38
2	N. 62° W.	14.26
3	N. 52° E.	21.26
4	S. 30° E.	8.20

Ans. 19.5 acres.

4. *To find the bearing and length of a side that has been omitted in the survey, and to compute the area.*

If for special reasons the surveyor leaves one side of a field unmeasured, the difference between the northings and southings of the measured sides will give the latitude of the unmeasured side, and the difference between the eastings an westings of the measured sides will give the departure of th unmeasured side; and from these we can get the area of th field; also, the length and bearing of the unmeasured side, as in the following example.

	BEARINGS.	CHAINS.
1	S. 40° 30′ E.	31.80
2	N. 54° E.	2.08
3	N. 29° 15′ E.	2.21
4	N. 28° 45′ E.	35.35
5	N. 57° W.	21.10
6	....	....

Ans. 92.87 acres nearly.

In the above example the sixth side is unmeasured. To find the area, take from the traverse table the latitudes, and departures of the five measured sides, and arrange them as below.

	BEARINGS.	DISTANCES.	N.	S.	E.	W.	MERIDIAN DIST.	DOUBLE MER. DIST.	N. AREA.	S. AREA.
1	S. 40° 30′ E.	31.80		24.18	20.65		20.65	20.65		499.3170
2	N. 54° E.	2.08	1.22		1.68		22.33	42.98	52.4356	
3	N. 29° 15′ E.	2.21	1.92		1.08		23.41	45.74	87.8208	
4	N. 28° 45′ E.	35.35	31.00		17.00		40.41	63.82	1978.4200	
5	N. 57° W.	21.10	11.49			17.69	22.72	63.13	725.3637	
6				21.45		22.72	0.0	72.72		487.3440
									2844.0401	986.6610
									986.6610	

2)1857.3791

92.86895 acres.

In the tablet we find that the northings exceed the southings by 21.45 chains; this we place in the column of southings, as the southing of the unmeasured side. We also find that the eastings exceed the westings by 22.72 chains; this we place in the column of westings, as the westing of the unmeasured side. With these numbers the area is computed as in preceding examples. To find the bearing of the unmeasured side,

$$\begin{aligned}
\text{Log. } 22.72 &= 1.356408 \\
\text{Log. } 21.45 &= \underline{1.331427} \\
\text{Tan. } 46^\circ\, 39' &= 10.024981
\end{aligned}$$

whence the bearing is S. 46° 39′ W.

To find the distance

$$\begin{aligned}
\text{Log. } 22.72 &= 1.356408 \\
\text{Sin. } 46^\circ\, 39' &= \underline{9.861638} \\
\text{Log. } 31.24 &= 1.494770
\end{aligned}$$

Whence the unmeasured side is 31.24 chains.

In the following notes the sixth side is unmeasured. Required the area of the field:

	BEARINGS.	CHAINS.
1	S. 85° W.	11.60
2	N. 53° 30′ W.	11.60
3	N. 36° 30′ E.	19.20
4	N. 22° E.	14.00
5	S. 76° 30′ E.	12.00
6	....	....

Ans. 55.08 acres, nearly.

The bearing of the unmeasured side is S. 13° 18′ W., and its length is 32.38 chains.

In the two following examples which are parts of the same tract, the 8th side is common, and was not measured. Required, the area of each part, also the bearing and length of the unmeasured side.

EXAMPLE.

	BEARINGS.	CHAINS.
1	N. 85° W.	7.65
2	N. $26^\circ\frac{1}{4}$ E.	27.65
3	S. 87° E.	29.99
4	S. 3° W.	26.80
5	S. 85° E.	9.28
6	S. 6° W.	11.61
7	N. 85° W.	19.37
8	....	....

Ans. 128.985 acres.

Bearing N. $58^\circ\ 15'\frac{1}{3}$ W.
Distance 25.81 chains.

EXAMPLE.

	BEARINGS.	CHAINS.
1	S. $5^\circ\frac{3}{4}$ W.	10.09
2	N. $85^\circ\frac{3}{4}$ W.	1.89
3	S. 26° W.	7.20
4	N. $85^\circ\frac{1}{2}$ W.	18.07
5	N. 26° E.	7.17
6	N. 85° W.	2.97
7	N. 5° E.	21.96
8	....	....

Ans. 48.975 acres.

Bearing S. $58^\circ\ 15'\frac{1}{3}$ E.
Distance 25.81 chains.

In forming the meridian distance column for the first part, begin at the 6th side and add the westings, or begin at the 2d side, and add the eastings; for the second part begin at the 1st side and add the westings.

5. *To draw a plan of a field that has been measured.*

Draw on a paper a line as a meridian passing through the first corner of the field, which corner we assume as the starting point; from this, with any scale of equal parts, set off along the meridian the northing or southing of the first side of the field, as given in the tablet from which the area was computed; there make an offset equal to the first number in the eighth column of the tablet, and it will determine the position of the second corner of the field. Then from where the latitude of the first side terminated, measure on the meridian the northing or southing of the second side, and make an offset equal to the second number in the eighth column, and it will determine the position of the third corner of the field. In the same manner the other corners can be determined. Lines joining these points will represent the sides of the field.

Example—It is required to draw a plan from the following field-notes.

	BEARINGS.	CHAINS.
1	N. 20° E.	10.00
2	S. 80° E.	9.60
3	S. 11° E.	10.00
4	S. 43° W.	12.00
5	N. 31° 29′ W.	12.73

Arrange the latitudes and departures as in the tablet below.

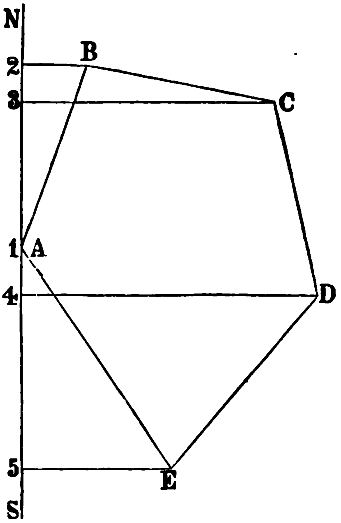
	BEARING.	DISTANCE.	N.	S.	E.	W.	MERID. DISTANCE.	DOUBLE MERID. DIST.	N. A.	S. A.
1	N. 20° E.	10.00	9.40		3.42		3.42	3.42	32.1480	
2	S. 80° E.	9.60		1.66	9.45		12.87	16.29		27.0414
3	S. 11° E.	10.00		9.82	1.91		14.78	27.65		271.5230
4	S. 43° W.	12.00		8.78		8.13	6.65	21.43		188.1554
5	N. 31° 29′ W.	12.73	10.86			6.65	0.0	6.65	72.2190	
									104.3670	486.7198 104.3670

2) 382.3528

Area = 19.11764 acres.

Draw *NS* as a meridian, take *A* as the first corner of the field, set off from *A* to 2 the northing of the first side, 9.40 chains; at 2 make an offset of 3.42 chains, which will determine the point *B* the second corner of the field. From 2 set off 1.66 chains, the southing at the second side, and at 3 make an offset of 12.87 chains, which will determine the point *C* the third corner of the field; from 3 set off the southing of the third side, 9.82 chains to 4, and at that point make an offset of 14.78 chains, and it will determine the point *D* the fourth corner. Then set off from 4 to 5 the southing of the fourth side, 8.78 chains, and at 5 make an offset of 6.65 chains, and it will determine the point *E* the fifth corner of the field.

Then draw the lines *AB*, *BC*, *CD*, *DE* and *EA*, and the plan will be completed.

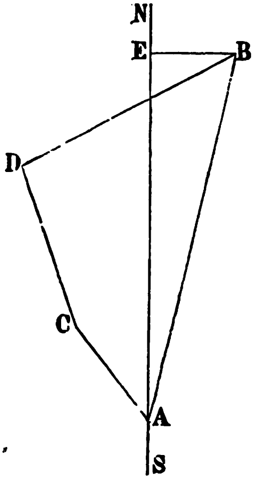


From the following notes it is required to draw a plan of the field, and compute its area.

	BEARINGS.	CHAINS.
1	N. 20° 30′ E.	10.00
2	S. 70° E.	13.50
3	S. 33° 30′ W.	20.00
4	N. 23° 21′ W.	13.00

Ans. 17.634 acres nearly.

6. *To determine the bearing and distance from one point to another, when there are obstructions that render it difficult to to take the bearing, or measure the distance directly.*



Begin at one of the points, run on several courses in succession, which courses must be determined by the nature of the ground. Take the bearing and distance of each line run, until the other point is reached. The difference between the sum of the northings and the sum of the southings of the lines run, will be the northing or southing of the line required; and the difference between the sum of the eastings and the sum of the westings, will be the easting or westing of the required line; and from these the line and its bearing can be determined.

Example.—To find the bearing and distance from *A* to *B*, we make the following measurement:

	BEARINGS.	CHAINS.
AC	N. 40° W.	6.30
CD	N. 20° W.	8.50
DB	N. 60° E.	12.20

Arrange the latitudes as in the tablet below,

	BEARINGS.	CHAINS.	N.	S.	E.	W.
AC	N. 40° W.	6.30	4.83			4.05
CD	N. 20° W.	8.50	7.99			2.91
DB	N. 60° E.	12.20	6.10		10.56	
AB				18.92		3.60

Whence we see that 18.92 is the southing from *B* to *A*, and 3.60 is the westing.

To find the bearing,

$$\begin{aligned} \text{Log. } 3.60 &= .556303 \\ \text{Log. } 18.92 &= \underline{1.276921} \\ \text{Tan. } 10^\circ 46' &= 9.279382 \end{aligned}$$

Whence the bearing from *B* to *A* is S. 10° 46′ W., and from *A* to *B*, N. 10° 46′ E.

To find the distance,

$$\begin{aligned} \text{Log. } 3.60 &= .556303 \\ \text{Sin. } 10^\circ 46' &= \underline{9.271400} \\ \text{Log. } 19.27 &= 1.284903 \end{aligned}$$

Whence the distance from *A* to *B* is 19.27 chains.

To determine the bearing and distance of a point on the osite side of a thicket, a surveyor runs the following lines necting the point with his station, namely:

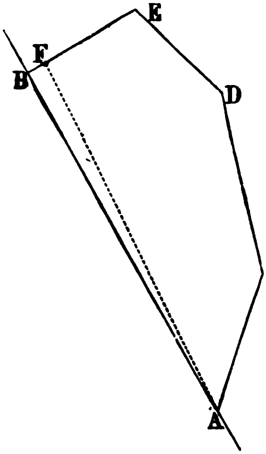
	BEARINGS.	CHAINS.
1	N. 42° E.	22.40
2	N. 14° E.	21.00
3	N. 24° W.	32.00
4	N. 56° W.	36.00
5	S. 50° W.	16.00

Required the bearing and distance to the point.

Ans. N. 24° 44′ W = bearing.
83.80 chains = distance.

A surveyor running a line north twenty seven degrees west ets a thicket so dense that he cannot see his way through he makes a detour, and takes the following measurent:

	BEARINGS.	CHAINS.
AC	N. 20° E.	12.00
CD	N. 10° W.	15.00
DE	N. 45° W.	10.00
EF	S. 63° W.	9.00



From these notes the surveyor shes to find his line.

Let *AB* be a portion of the line nning N. 27° W., from the beargs and distances, *AC*, *CD*, *DE*, d *EF*, the bearing and distance *F* must be computed.

Arrange the latitudes and departures of these lines as in e following tablet:

	BEARINGS.	CHAINS.	N.	S.	E.	W.
AC	N. 20° E.	12.00	11.28		4.10	
CD	N. 10° W.	15.00	14.77			2.60
DE	N. 45° W.	10.00	7.07			7.07
EF	S. 63° W.	9.00		4.09		8.02
FA				29.03	13.59	

From this we see that the latitude of *FA* is 29.03 chains, and the departure of *FA* is 13.59 chains. Then to find the bearing,

$$\begin{array}{ll} \text{Log. } 13.59 & = 1.133219 \\ \text{Log. } 29.03 & = 1.462847 \\ \hline \text{Tan. } 25^\circ\ 5'\ 10'' & = 9.670372 \end{array}$$

Whence from *A* to *F* is N. 25° 5′ 10″ W. Subtracting this bearing from the bearing of the line *AB*, which is N. 27° W., we have the angle *BAF* equal 1° 54′ 50″. To find *AF*, we have,

$$\begin{array}{ll} \text{Log. } 13.59 & = 1.133219 \\ \text{Sin. } 25^\circ\ 5'\ 10'' & = 9.627345 \\ \hline \text{Log. } 32.05 & = 1.505874 \end{array}$$

To find *FB*, we have,

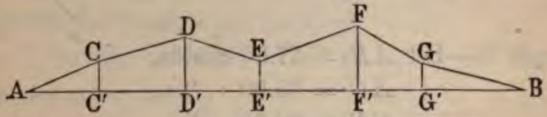
$$\begin{array}{ll} \text{Log. } 32.05 & = 1.505874 \\ \text{Sin. } 1^\circ\ 54'\ 50'' & = 8.523713 \\ \hline \text{Log. } 1.07 & = 0.029587 \end{array}$$

Therefore the point *F* is 1.07 chains from the line; and as in this example the line *EF* is at right angles to the line that is to be found, measure on in the direction *BF* one chain and seven links, and then drive a stake; it will be on the line, and from that the line can be continued. To find the distance from *A* to *B*, we have,

$$\begin{array}{ll} \text{Log. } 32.05 = AF & = 1.505874 \\ \text{Cosine } 1^\circ\ 54'\ 50' & = \underline{9.999778} \\ \text{Log. } 32.04 & = 1.505652 \end{array}$$

Whence the distance from A to B is 32.04 chains. If the surveyor had crossed his line, the bearing of AF would come out more than the bearing of the line which he was running; that is, in the present example the bearing of AF is not quite 27°, therefore the surveyor has not quite reached his line at the point F

IRREGULAR BOUNDARIES.



When the boundary of a field is irregular, it is often advisable to run a convenient base line, and from this measure offsets to the prominent points of the irregular boundary. These offsets form the parallel sides of trapezoids, and as we measure the distance from one offset to another, we can compute the area included between the base line and the irregular boundary. In the diagram, if $ACDEFGB$ represent an irregular boundary of a field, take the bearing and distance from A to B; at C', D', E', &c., measure offsets $C'C$, $D'D$, $E'E$, &c.; also measure AC', $C'D'$, $D'E'$, &c., from which we can compute the area included between AB and the irregular line. If the boundary is curvilinear like the bank of a river, make the offsets equally distant from each other, and the area will be more easily obtained.

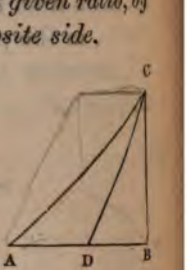
The area included by the base line will be computed as in the preceding cases.

SECTION V.

DIVIDING AND LAYING OUT LAND.

PROBLEM I.

To divide a triangle into two parts having a given ratio, by a line drawn from one of the angles to its opposite side.



Let ABC represent the triangle; divide its base into two parts corresponding to the given ratio, and let AD be one of the parts. Stake out the line from D to C, and it will divide the triangle as required.

Example 1.—Let $AB = 37.50$ chains,
$AC = 35.00$ "
$CB = 32.50$ "

It is required to run the line CD so that the triangle ACD shall contain 10 acres. Compute the area of the triangle whose sides are given above, it will be found 52.5 acres. Then

$$52.5 : 10 :: 37.50 : AD = 7.14 \text{ chains.}$$

Or, without computing the area of the triangle ABC, we may determine AD so that the triangle ACD shall contain the required amount of land.

We have $\sin. A \cdot AC \cdot AD = 2ACD.$ But in this example, the angle A is 53° 8′, and the side $AC = 35$ chains, and the triangle ACD is 10 acres or 100 chains. Therefore, we have,

$$35 \sin.53^\circ 8' \cdot AD = 200 \cdot$$

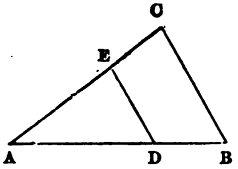
$$\text{Or,} \quad AD = \frac{200}{35 \sin.53^\circ 8'} = 7.14 \text{ chains.}$$

Example 2.—A triangular field, whose sides are 20, 18, and 16 chains, is to have a piece of 4 acres in content fenced off from it, by a right line drawn from the most obtuse angle to the opposite side. Required the length of the dividing line, and its distance from either extremity of the line on which it falls.

Ans. Length of the dividing line, 13 chains 89 links, if run nearest the side 16. Distance it strikes the base from the next most obtuse angle is 5.85 chains.

PROBLEM II.

To divide a triangle into two parts having a given ratio, by a line parallel to one of its sides.



Let ABC be the given triangle, and let DE divide the triangle as required, then if $n : 1$ be the ratio of ADE to the whole, we must have

$$AD : AB :: \sqrt{n} : 1,$$

since similar triangles are to each other as the squares of their homologous sides. Therefore, if we take AD, having to the line AB the ratio of $\sqrt{n} : 1$, and from D run a line parallel to BC, it will divide the triangle as required.

Example 1.—In the triangle ABC, if $AB = 46$ chains, $AC = 54.75$ chains, and $BC = 36.8$ chains, it is required to cut off 20 acres by a line parallel to the side BC.

The area of the triangle ABC will be found 83.8 acres; then we shall have

$$AD = 46\left(\frac{20}{83.8}\right)^{\frac{1}{2}} = \frac{46}{(4.19)^{\frac{1}{2}}} = 22.47 \text{ chains.}$$

Whence, measure from A 22.47 chains, and then run a line with the same bearing as BC; and the line will cut off 20 acres.

Example 2.—The three sides of a triangle are 5, 12, and 13. If two-thirds of this triangle be cut off by a line drawn parallel to the longest side, it is required to find the length of the dividing line, and the distance of its two extremities from the extremities of the longest side.

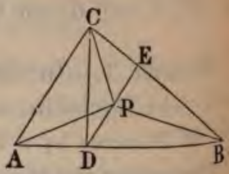
Ans. Distance from the extremity of 5 is $5\left(\frac{\sqrt{3}-\sqrt{2}}{\sqrt{3}}\right)$; of 12, it is $12\left(\frac{\sqrt{3}-\sqrt{2}}{\sqrt{3}}\right)$. The division line is $13\sqrt{\frac{2}{3}}$.

Example 3.—Two sides of a triangle, which include an angle of 70°, are 14 and 17. It is required to divide it into three equal parts, by lines drawn parallel to its longest side.

Ans. The first division line on the side 17, cuts that side at distance $\frac{17}{\sqrt{3}}$; the second division line, $\frac{17\sqrt{2}}{\sqrt{3}}$. The side 14 is cut at $\frac{14}{\sqrt{3}}$ and $\frac{14\sqrt{2}}{\sqrt{3}}$.

PROBLEM III

To divide a triangle into three equal parts by lines drawn from the angles to some point within the triangle.



Let ABC be the triangle whose sides are given. Take AD one third of the base AB, draw DE parallel to AC, and take P the middle of DE; then lines drawn from P to A, B, and C will divide the triangle into three equal triangles.

AD being one third of AB, ACD is one third of ACB; but $ACP = ACD$, since DE is parallel to AC; therefore ACP is one third of ACB. It is also obvious that CPB and APB are equal. The lines AP, BP, and CP are easily found, since AD, DP, and the angle at D are known; whence AP will be known, and so of the other lines. Or as the angle at D equals the angle at A, we shall have

$$AP^2 = AD^2 + DP^2 + 2AD \cdot DP \cdot \cos. A,$$

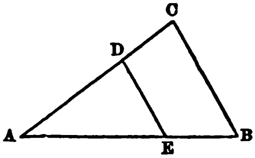
which gives AP, since DP is one third of AC.

Example.—The sides of a triangle are 17.51 chains, 12.575 iains, and 23.645 chains. This triangle is to be divided into iree equal parts by lines drawn from the angles to some oint within the triangle. Required the length of the lines.

Ans. The line from the angle opposite the side 12.575 is 13.2242 chains; and the line from the angle opposite the side 17.51 is 11.19 chains.

PROBLEM IV.

To divide a triangle into two parts having a given ratio, by line running in a given direction.



Let ABC be the given triangle, DE the dividing line, and $1 : n$ the ratio of the triangle ADE to the whole triangle. Put $AB = c$, $AC = b$, $AE = x$; then since the position of DE is given, the angles at D and E are known; therefore we shall have $AD = \frac{\sin. E \cdot x}{\sin. D}$, and the area of the triangle ADE will equal $\frac{\sin. A \ \sin. E x^2}{2 \sin. D}$; also the area of ABC will equal $\frac{\sin. A \cdot b \cdot c}{2}$. Therefore by the conlitions we have

$$\frac{\sin. A \ \sin. E \cdot x^2}{2 \sin. D} = \frac{\sin. A \cdot b \cdot c}{2 \cdot n}.$$

Whence . $$x = \left(\frac{\sin. D \cdot b \cdot c}{n \sin. E}\right)^{\frac{1}{2}}.$$

which determines the point E, from which stake out the line running in the given direction, and it will divide the triangle as required.

Example.—In the triangle ABC we have $AB = 15$ chains; $AC = 12$ chains; the angle $A = 67°$. It is required to divide this triangle into two equal parts by a line DE, which makes an angle of 65° with AC, and an angle of 48° with AB.

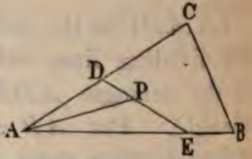
In this example $n = 2$, and

$$x = \left(\frac{\sin. 65^\circ \cdot 12 \cdot 15}{2\sin. 48^\circ}\right)^{\frac{1}{2}} = 10.477 \text{ chains,}$$

for the line AE, and $AD = 8.59$ chains.

PROBLEM V.

To divide a triangle into two parts having a given ratio, by a line passing through a given point.



Let ABC be the given triangle, P the given point; and let DE be the dividing line. Put $AE = x$, $AD = y$, $AB = c$, $AC = b$; join AP, and put P and P' for the perpendicular distance of the given point from AB and AC respectively. Then we shall have

$$ABC = \frac{\sin. A \cdot b \cdot c}{2}$$

$$ADE = \frac{\sin. A \cdot x \cdot y}{2}$$

$$APE = \frac{Px}{2}$$

$$APD = \frac{P'y}{2}$$

Then if $1 : n$ is the ratio of ADE to ABC, we shall have

$$xy = \frac{bc}{n} \qquad (1)$$

And since ADE is composed of the two triangles, APE and APD, we have

$$P \cdot x + P' \cdot y = \frac{\sin. A \cdot b \cdot c}{n} \qquad (2)$$

Eliminating y from (1) and (2), we get

$$x = \frac{\text{Sin.}A\cdot b\cdot c}{2nP} \pm \left(\frac{\text{Sin.}^2A\cdot b^2\cdot c^2}{4n^2P^2} - \frac{P'bc}{nP}\right)^{\frac{1}{2}} \qquad (3)$$

When the given point is outside the triangle, the sign between the terms within the parenthesis will be positive.

When the given point is on one of the sides, as on AC, then $P' = 0$, and

$$x = \frac{\text{sin.}A\cdot b\cdot c,}{nP.}$$

Again, it is sometimes more convenient to use co-ordinates of the given point than perpendiculars; and if we take the origin at A, we can measure a line from P parallel to AC, and another from P parallel to AB. Call these lines x' and y'; put $AE = x$. Then will $AD = \frac{y'x}{x-x'.}$ And the area of ADE will be $\frac{\text{sin.}A\cdot y'\cdot x^2}{2(x-x')}$, whence we shall have,

$$\frac{\text{sin.}A\cdot y'\cdot x^2}{2(x-x')} = \frac{\text{sin.}A\cdot b\cdot c}{2n} \qquad (4)$$

$$\therefore \quad ny'x^2 - bcx = -bcx', \qquad (5)$$

From which we get,

$$x = \frac{bc \pm (bc)^{\frac{1}{2}}(bc - 4nx'y')^{\frac{1}{2}}}{2ny'} \qquad (6)$$

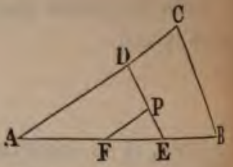
Which determines the point E.

From the above value of x, we see that in some cases there may be two lines drawn, each of which will solve the problem. When bc is less than $4nx'y'$, the problem is impossible, or when the triangle ADE is less than 4 times the triangle formed by the co-ordinates of the given point and the line AP, the problem is impossible: when $bc = 4nx'y'$, then $x = 2x'$. And then the triangle ADE will be the least that can be cut off from ABC by a line running through the given point P. When the given point is on one of the sides of the given triangle, as on AC, then will $x' = 0$, in which case equation (6) becomes

$$x = \frac{bc}{ny'}.$$

Example 1.—In the triangle ABC let

$AB = 30$ chains,
$AC = 25$ "
$BC = 20$ "



There is a spring of water at P; it is required to divide the triangle into equal parts by a line running through the spring.

From the spring measure PF parallel to AC; suppose it to be found equal 4 chains. And measure AF; suppose it 14 chains. Then in equation (6), we shall have $b = 25$; $c = 30$; $n = 2$; $x' = 14$; $y' = 4$.

Therefore, equation (6) gives

$$x = 17.13 \text{ chains, which is } AE.$$

And since $EF : FP :: AE : AD$, we shall find

$$AD = 21.89 \text{ chains.}$$

Example 2.—In the triangle ABC, the angle at A is found to be 75° 56′, and the co-ordinates of a spring at P are found to be $AF = 6.40$ chains, $FP = 5.10$ chains. It is required to run a line through the spring at P that shall cut off 7 acres of land.

From equation (4), we have,

$$\text{Sin.}75° \, 56' \cdot \frac{5.10x^2}{x-6.40} = 140,$$

this being the double area to be cut off in chains. This equation gives two values of x; one $x = 18.5206$, the other $x = 9.7794$. The first value, that is $AE = 18.5206$, will give $AD = 7.7929$; the other value of x, or $AE = 9.7794$, gives $AD = 14.7585$ chains. Both values are applicable to the problem.

If it had been required to run a line through the spring so as to cut off the least quantity of land, we should make FE equal to AF, and run the line EPD. The line AE would be 12.80 chains, using the numbers in the last example; and AD would be 10.20 chains, and the triangle ADE thus cut off would contain 6.3322 acres.

Again, if it were required to cut off 7 acres, and include the spring by the shortest line DE, we should make $AE = AD$; then we should have,

$$\text{Sin.} 75^\circ\ 56' \cdot \overline{AE}^2 = 140 \text{ chains},$$

From which we get,

$$AE = 12.014 \text{ chains.}$$

Therefore, if we measure 12.014 chains for AE and AD each, the line DE will be the shortest that will cut off 7 acres.

Example 3.—It is required to find the length and position of the shortest possible line which shall divide into two equal parts a triangle whose sides are 25, 24, and 7 respectively.

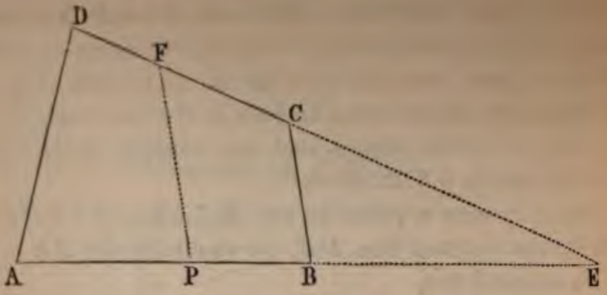
REMARK.—It is obvious that the division line must cut the sides 25 and 24; and to make it the shortest line possible, the triangle cut off must be isosceles.

Ans. The division line makes an angle with the sides 25 and 24 of 81° 52′ 10″, and its length is 4.899.

PROBLEM VI.

To divide a quadrilateral into two given parts by a line passing through a given point in one of the sides.

Let $ABCD$ be a quadrilateral; it is required to run a line from P, a given point on the side AB, so as to divide the quadrilateral into parts such that each shall contain a given area. 1st. Measure the sides of the quadrilateral, and compute its area. Then extend the two sides as AB and DC until they



meet in E; and since the angles B and C of the quadrilateral are known, the angles of the triangle EBC are known, and the side BC is known; then compute the area of the triangle EBC, and also its sides EB and EC. 2*d*. The point P is given in position, therefore BP will be known; add BP to BE, and EP will be known. Also, to the area of the triangle EBC, add the area of the part $PBCF$, and the area of the triangle EPF will be known.

Then in the triangle EPF we have the area, the angle at E, and the side EP, to find the side EF.

Therefore by mensuration we have

$$EP \cdot EF \cdot \sin.E = 2EPF.$$

Hence,
$$EF = \frac{2EPF}{EP \cdot \sin.E}$$

Then subtract EC from EF, and CF will remain. Then measure from C towards D the value of CF, and there drive a stake. The work will be finished by staking out the line PF. If the flag-staff at F cannot be seen from P, the bearing of the line must be determined from the angle EPF, and the line run with the compass. In such cases the surveyor should be careful to preserve stakes at equal intervals on the line, so that if his bearing does not bring him precisely to the point F, when he reaches the line CD he can measure his distance from F, and by proportion determine how much each stake must be moved to mark out a straight line from P to F

Example.—Let $ABCD$ be a field with the side AB along a highway; it is required to divide the field into two equal parts by a line running from P, a point at the middle of the side AB. The following are the field notes:

	BEARINGS.	CHAINS.
AD	N. 12° E.	24.60
DC	S. 72° E.	24.00
CB	S. 10° E.	16.91
BA	W.	30.88

	BEARING.	DIST.	N.	S.	E.	W.			N. A.	S. A.
1	N. 12° E.	24.60	24.07		5.11		5.11	5.11	122.9971	
2	S. 72° E.	24.00		7.42	22.83		27.94	33.05		245.2310
3	S. 10° E.	16.91		16.65	2.94		30.88	58.82		979.3530
4	W.	30.88				30.88	0.0	30.88		
									122.9971	1224.5840
										122.9971
										2)1101.5869
								Area in acres,		55.07934

Hence the field contains 55.08 acres; and as it is to be divided into equal parts, each part must contain 27.54 acres.

Produce the sides AB and DC until they meet at E. From the bearings of the sides AB and BC, we find the angle $EBC = 100°$; from the bearing of the sides BC and CD, we find the angle $ECB = 62°$; therefore the angle at E is 18°. And since the side BC is 16.91 chains, we have the angles and one side of the triangle EBC. to find the other sides and the area.

To find EC, we have

$$\begin{array}{lcr} \text{Sin. } 100^\circ & = & 9.993351 \\ \text{Log. } 16.91 & = & \underline{1.228144} \\ & = & 11.221495 \\ \text{Sin. } 18^\circ & = & \underline{9.489982} \\ \text{Log. } 53.89 & = & 1.731513 \end{array}$$

Hence $EC = 53.89$ chains.

To find EB we have

$$\begin{array}{lcr}
\text{Sin. } 62^\circ & = & 9.945935 \\
\text{Log. } 16.91 & = & \underline{1.228144} \\
 & & 11.174079 \\
\text{Sin. } 18^\circ & = & \underline{9.489982} \\
\text{Log. } 48.317 & = & 1.684097
\end{array}$$

Hence $EB = 48.317$ chains.

Since $AB = 30.88$ chains, and the point P is at the middle of AB, we have $PB = 15.44$ chains; therefore EP, the sum of EB and BP, will be 63.757 chains.

To find the area of the triangle, we have

$$\begin{array}{lcr}
\text{Log. } 53.89 & = & 1.731513 \\
\text{Log. } 48.317 & = & 1.684097 \\
\text{Sin. } 18^\circ & = & \underline{9.489982} \\
\text{Log. } 804.62 & = & 2.905592
\end{array}$$

which is the double area in chains. Hence, the area of the triangle is 40.231 acres.

The area of the part $PBCF = 27.54$ acres; therefore the area of the triangle EPF will be 67.771 acres. Then in the triangle EPF, we have the side EP, the angle at E, and the area to find the side EF; we shall have

$$EF = \frac{1355.42}{63.757 \sin. 18^\circ}.$$

$$\begin{array}{lcrr}
 & & \text{Log. } 1355.42 = & 3.132074 \\
\text{Log. } 63.757 & = & 1.804528 & \\
\text{Sin. } 18^\circ & = & \underline{9.489982} & \\
 & & 1.294510 & \underline{1.294510} \\
\text{Log. } 68.796 & & = & 1.837564
\end{array}$$

Therefore $EF = 68.796$ chains. We found $EC = 53.89$; subtracting we get $CF = 14.91$ chains, which determines where the dividing line intersects the side CD; subtracting CF from CD, we get $FD = 9.09$ chains.

d the bearing and length of the dividing line, we will the area of one of the parts, say *PADF*, and thr e work.

RINGS.	DIST.	N.	S.	E.	W.			N. A.	S. A.
W	15.44				15.44	15.44	15.44		
2° E.	24.60	24.07		5.11		10.33	25.77	620.2839	
2° E.	9.09		2.81	8.65		1.68	12.01		33.7481
			21.26	1.68		0.0	1.68		35.7168
								620.2839 69.4649	69.4649

2)550.8190

27.54 acres.

one half the field.

d the bearing of *PF*, we have

Log. 1.68 = 0.225309
Log. 21.26 = 1.327563
Tan. 4° 31′ = 8.897746

F bears N. 4° 31′ W. To find the length of *PF*, we have

Log. 1.68 = 0.225309
Sin. 4° 31′ = 8.896246
Log. 21.33 = 1.329063

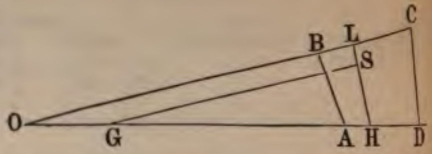
, *PF* = 21.33 chains.

PROBLEM VII.—(GUMMERE'S).

e of land is bounded as follows:

	BEARINGS.	CHAINS.
1	N. 14° W.	15.20
2	N. 70° 30′ E.	20.43
3	S. 6° E.	22.79
3	N. 86° 30′ W.	18.00

Within this lot there is a spring; the course to it from the second corner is S. 75° E., 7.90 chains. It is required to cut off ten acres from the west side of this lot, by a line running through the spring. Where will the dividing line meet the sides of the lot?



Let $ABCD$ be the piece of land, and let S be the position of the spring; extend the lines DA and CB until they meet at O. From the bearings of these lines, we find in the triangle AOB, $BAO = 72^\circ\ 30'$, $ABO = 84^\circ\ 30'$, and $AOB = 23^\circ$; the side $AB = 15.20$ chains, $AO = 38.72$ chains, and $BO = 37.10$ chains. The area $AOB = 280.67$ chains. Take the origin at O, and consider OG and GS as coördinates of the spring. Call $OG = x'$ and $GS = y'$; and since $BS = 7.90$ chains, and the angle $SBL = 34^\circ\ 30'$, found from the bearing of BS and BC, we can find $OG = x' = 11.452$ chains, and $GS = y' = 33.0691$ chains. Then put $x = OH$. LH being the dividing line; and as GS is parallel to OL, we shall have

$$x-x' : y' :: x : OL = \frac{y'x}{x-x'}.$$

Therefore, we have,

$$\frac{\sin.23^\circ \cdot y' \cdot x^2}{2(x-x')}$$

for the area of the triangle OLH; but the area of the triangle AOB is found to be 280.67 chains, and by the Problem the area of $ABLH$ is to be 10 acres or 100 chains. Therefore we have,

$$\frac{\sin.23^\circ \cdot y' \cdot x^2}{2(x-x')} = 380.67,$$

Or,
$$\frac{x^2}{x-x'} = \frac{761.34}{\sin.23^\circ \cdot y'} \qquad (1)$$

But,

$$\begin{array}{lr} \text{Log. } 761.34 & = 2.881579 \\ \text{Log. } y' \,(33.0691) & = 1.519422 \\ \text{Sin. } 23^\circ & = \underline{9.591878} \\ & \underline{1.111300} \\ \text{Log. } 58.922 & = 1.770279 \end{array}$$

Therefore equation (1) becomes

$$\frac{x^2}{x-x'} = 58.922 \qquad (2)$$

We have found $x' = 11.452$ chains; this value substituted for x' in (2) will give,

$$x^2 - 58.922\,x = -674.77. \qquad (3)$$

Solving equation (3), we get,

$$x = 29.461 \pm 13.899$$

Taking the positive sign, we have,

$$x = 43.36 \text{ chains,}$$

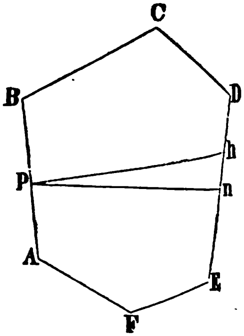
Which is the distance from O to H where the dividing line meets the side DA. If we subtract OA, which is 38.72 chains, we have left 4.64 chains for the distance from A to H. We also find $OL = \frac{y'x}{x-x'} = 44.94$ chains, therefore subtracting OB, which is 37.10 chains, we have $BL = 7.84$ chains.

Also the dividing line LH bears S. 2° 58′ E., and from L to H is 17.67 chains.

The area of $ABCD$ = 35.6877 acres, and
" $ABLH$ = 10 acres nearly.

PROBLEM VIII.

To cut off a given quantity of land from a field of several sides, by a line running from a given point in one of the sides of the field.



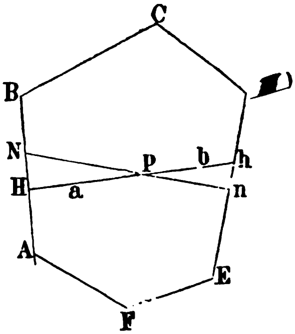
Let *ABCDEF* be the field, and *P* the given point on the side *AB*. From *P* run a random line cutting off the required quantity as near as may be. Measure *PB*, *BC*, *CD*, and *Dh*. Compute the area, considering *Ph* as the closing side. Also, find the bearing and distance of *Ph*. Then if *Pn* is the true dividing line, the triangle *Phn* will equal the difference between the area cut off by the random line *Ph*, and the quantity required to be cut off; put this difference equal *D*, then will

$$Ph\cdot hn \sin.h = 2D.$$

Therefore
$$hn = \frac{2D}{Ph\cdot \sin.h}.$$

PROBLEM IX.

To cut off from a field of several sides a given quantity of land, by a line running through a given point within the field.



Let *ABCDEF* be the proposed field, the sides of which should be measured in the usual way. Let *P* be the given point; run the line *HPh* perpendicular to *AB* at *H*; compute the area of *HBCDh*, and find how much it differs from the quantity required to be cut off; let *D* equal the difference; let $HP = a$, and $Ph = b$.

Then, if we draw *NPn* so that the difference of the triangles *Pnh* and *PNH* shall equal *D*, *NPn* will divide the field as required, or will cut off the quantity of land required.

the triangle PHN, we have $PN = \frac{a}{\cos. P}$.

erefore the area of $PHN = \frac{a^2 \sin. P}{2 \cos. P} = \frac{a^2}{2 \cot. P}$. (1)

the triangle Phn, we have $Pn = \frac{b \sin. h}{\sin. (P+h)}$.

erefore the area of

$$Phn = \frac{b^2 \sin. h \ \sin. P}{2 \sin. (P+h)} = \frac{b^2}{2 \ (\cot. P + \cot. h)}. \qquad (2)$$

nce we get

$$\frac{b^2}{\cot. P + \cot. h} - \frac{a^2}{\cot. P} = 2D. \qquad (3)$$

d this reduces to

$$\cot.^2 P + \left(\frac{a^2 - b^2}{2D} + \cot. h\right) \cot. P = -\frac{a^2 \cot. h}{2D}. \qquad (4)$$

om this equation we get the angle P, and thus determine osition of the dividing line NPn.

is Problem can be conveniently solved as follows:

tend the sides that are intersected by the dividing line they meet in some point which call O; compute the area e triangle AOE, and add the quantity to be cut off, and out the area of the triangle AFE, and we shall have the of the triangle ONn. When NPn is the dividing line, is area equal A; let $x'y'$ be the co-ordinates of the point e origin being taken at O; these co-ordinates can be mined from the position of the point P, the bearings of ides BA and DE being given. Then put $x = On$; then $\frac{y'x}{x-x'} = ON$.

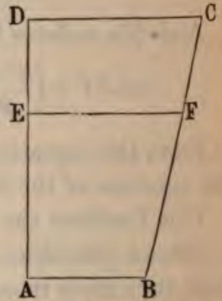
erefore the area of $OnN = \frac{y'x^2 \sin. O}{2(x-x')} = A$.

om the last equation, we can find x, which is the distance and since $ON = \frac{y'x}{x-x'}$, we have both On and ON. We also have OE and OA; therefore by subtracting, we have En and AN. Hence the position of the dividing line is determined.

When the given point is without the field, x' becomes negative, and we shall have $ON = \frac{y'x}{x+x'}$.

PROBLEM X.

Let ABCD be a trapezoid; it is required to cut off a given quantity of land by a line parallel to AB or CD.



Produce the lines that are not parallel until they meet, compute the sides and area of the triangle thus formed outside the trapezoid, to the area thus formed add the area to be cut off, and we shall have the areas of two similar triangles and the sides of one of them; and as the areas are as the squares of their sides, we can find the sides of the other; and from these we can determine the points of division.

Example 1.—Let $ABCD$ be a trapezoid, $AB = 4.50$ chains; the angle at A is a right angle; the angle at B is equal to 106°.

It is required to cut off six acres of land by a line parallel to AB.

Produce DA and CB until they meet, then will AB tan.B $= 4.50$ tan. $74° = 15.693$ chains, which is the distance from the point where the sides meet. This will be the altitude of a triangle whose base is 4.50 chains, and its area is 35.309 chains; to this add the six acres reduced to chains, and we shall get 95.309 chains for the area of the other triangle; then we can say

35.309 : 95.309 :: $(15.693)^2$: the square of the distance from the point where the sides meet to the point of division; whence we get the distance equal to 25.783 chains. From this subtract 15.693 chains, and and we have left $AE = 10.09$ chains.

Therefore measure from A 10.09 chains, and run a line EF at right angles to AD, and it will cut off six acres.

Again, if we put $x =$ the required line AE, $a = AB$, then EF will equal $a + \frac{x}{\tan.B}$; and hence the area of $ABFE$ equals $ax + \frac{x^2}{2.\tan.B}$. Therefore putting A for the area to be cut off, we have $\frac{x^2}{\tan.B} + 2ax = 2A$.

Or, $$x = -a \tan.B \pm (2A \tan.B + a^2 \tan.^2 B)^{\frac{1}{2}},$$

Applying to this equation the value given in the example, we get

$$x = 10.09 \text{ chains, as before.}$$

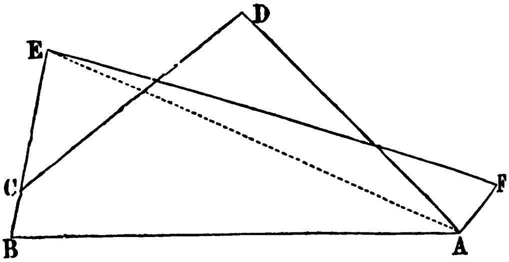
Example 2.—There is a farm containing 64 acres; commencing at its south westerly corner, the first course is N. 15° E., distance 12 chains, the second is N. 80° E. (distance lost), the third S. (distance lost), the fourth is N. 82° W. (distance lost), to the place of beginning. It is required to determine the distances lost.

NOTE.—Extend the northern and southern boundary westward, and thus form a triangle on the west side of 12.

Ans. The 2d side is 35.81 chains
" 3d " 23.21 "
" 4th " 38.76 "

PROBLEM XI.

The bearings and distances of the sides of the field ABCD, in the diagram are as follows:



	BEARINGS.	CHAINS.
AB	S. 15°44′ W.	13.80
BC	N. 63° W.	1.40
CD	N. 25° W.	9.00
DA	N. 63° E.	9.86

AF bears N. 25° W, and E is taken on the line of BC distant from C 4.60 chains. It is required to run a line from E to intersect AF, so that ABEF shall contain the same quantity of land as ABCD.

	BEARINGS.	CHAINS.	N.	S.	E.	W.	MERIDIAN DIST.		N. A.	S. A.
1	S. 15° 44′ W.	13.80		13.28		3.74	3.74	3.74		49.6672
2	N. 63° W.	1.40	0.64			1.25	4.99	8.73	5.5872	
3	N. 25° W.	9.00	8.16			3.80	8.79	13.78	112.4448	
4	N. 63° E.	9.86	4.48		8.79		0.0	8.79	39.3792	
									157.4112	49.667
									49.6672	

2)107.7440

Area of *ABCD* = 53.8720 chains.

From the bearings of *AB* and *BE* we find the angle *ABE* = 78° 44′, *AB* = 13.80 chains, and *BE* = 6 chains.

thence we find the area of the triangle $ABE = 40.6$ chains. This subtracted from 53.872, the area of $ABCD$, will leave 13.272 chains, which must be the area of the triangle AEF. We also find $AE = 13.93$ chains, and from the bearings of AE and AF we get the angle $EAF = 114° 17'$; and since we have

$$AF = \frac{2AEF}{AE\,\text{sin.}AEF} = \frac{26.544}{13.93\,\text{sin.}114° \; 17'} = 2.09 \text{ chains.}$$

Therefore measure 2.09 chains from A to F. Then drive a stake, and run a line from E to the stake at F.

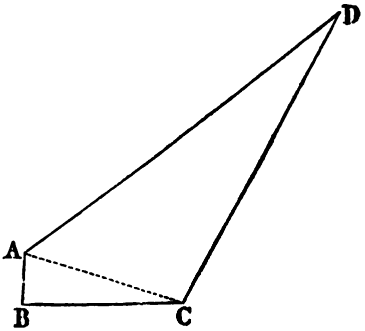
To verify this result compute the area of $ABEF$, and compare it with the area of $ABCD$ as before determined.

When the ground is favorable for staking out parallels, the position of the dividing line can be quite easily determined in the following manner.

From the corner D run a line parallel to the diagonal AC, and where this parallel intersects the line BCE, drive a stake, from which run a line parallel to the diagonal AE, and this parallel will intersect the line AF at the point F, and thus determine that point; and a line running from E to F will be the dividing line required.

PROBLEM XII.

In the diagram, AB was found to run north 2 chains; BC west 6.40 chains; CD was a highway running S. 40° W. It was required to run a line from A to intersect the highway at some point as at D, so as to inclose 5 acres of land.



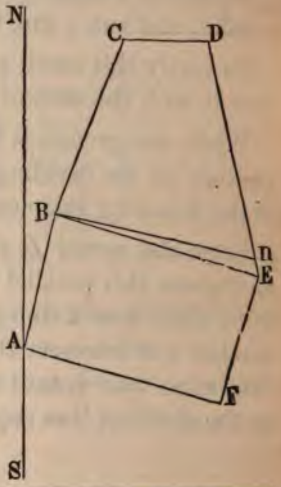
The area of the triangle ABC is 6.40 chains; this taken from the 5 acres leaves the triangle $ACD = 43.60$ chains. AC is found to be 6.71 chains, and the angle $ACB = 17° 21' 15''$; but the angle $BCD = 130°$; therefore $ACD = 112° 38' 45''$.

Now, $$CD = \frac{2ACD}{AC \text{ sin.} ACD} = 14.09 \text{ chains.}$$

Then measure along the road 14 chains and 9 links, and drive a stake. A line from A to the stake will inclose the required quantity of land.

PROBLEM XIII.

It is required to divide the field ABCDEF into two equal parts, by a line running from B, the second corner of the field.



Measure the sides of the field, and arrange them as in the following tablet.

	BEARINGS.	CHAINS.	N.	S.	E.	W.	MERID. DISTANCE.	MULT.	N. A.	S. A.
AB	N. 15° E.	14.00	13.52		3.62		3.62	3.62	48.9424	
BC	N. 20° E.	20.00	18.79		6.84		10.46	14.08	264.5632	
CD	E.	8.00			8.00		18.46	28.92		
DE	S. 10° E.	25.00		24.62	4.34		22.80	41.26		1015.8212
EF	S. 15° W.	15.30		14.78		3.96	18.84	41.64		615.4392
FA	N. 69° 23' W.	20.13	7.09			18.84	0.0	18.84	133.5756	
									447.0812	1631.2604
										447.0812

2) 1184.1792

592.0896

Therefore the area of the field is 592.0896 chains.

Next arrange the latitudes and departures of the sides *EF*, *FA*, *AB*, and consider *BE* as the closing line, as in the following tablet.

	BEARINGS.	CHAINS.	N.	S.	E.	W.	MERIDIAN DIST.	MULT.	N. A.	S. A.
EF	S. 15° W.	15.30		14.78		3.96	3.96	3.96		58.5288
FA	N. 69° 23′ W.	20.13	7.09			18.84	22.80	26.76	189.7284	
AB	N. 15° E.	14.00	13.52		3.62		19.18	41.98	567.5696	
BE				5.83	19.18		0.0	19.18		111.8194
									757.2980	170.3482
									170.3482	
									586.9498	
									293.4749	

Whence the area of *EFAB* is 293.4749 chains; the area to be cut off is 296.0448 chains, and the difference is 2.5699 chains, which is the area of the triangle *BEn*.

To find the bearing of *BE*, we have,

$$\begin{aligned} \text{Log. } 19.18 &= 1.282849 \\ \text{Log. } 5.83 &= .765669 \\ \text{Tan. } 73^\circ\ 5\tfrac{1}{2}' &= 10.517180 \end{aligned}$$

Whence *BE* is S. 73° 5½′ E.

To find the distance, we have,

$$\begin{aligned} \text{Log. } 19.18 &= 1.282849 \\ \text{Sin. } 73^\circ\ 5\tfrac{1}{2}' &= 9.980808 \\ \text{Log. } 20.05 &= 1.302041 \end{aligned}$$

From the bearing of *BE* and *DE*, we find the angle *BED* equals 63° 5½′.

If *Bn* is the dividing line, we shall have,

$$\frac{BE \cdot En \ \sin. BEn}{2} = 2.5699,$$

And,
$$En = \frac{5.1398}{BE \ \sin. BEn}.$$

But, Log. 5.1398 $= 0.710947$

$$\begin{array}{lrl} \text{Sin.}BEn \text{ or } 65^\circ\ 5\tfrac{1}{2}' & = & 9.950234 \\ \text{Log. } BE & = & 1.302041 \\ \hline & & 1.252275 \end{array}$$

$$\begin{array}{lrl} & & 1.252275 \\ \text{Log. } .2875 & = & \bar{1}.458672 \end{array}$$

Therefore En is nearly 29 links.

The bearing of Bn is S. 73° 49′ E., and the distance is 19.92 chains.

PROBLEM XIV.

A rectangular farm, 50 *chains in length, and* 40 *chains in breadth, containing* 200 *acres of land, was purchased by two men, each paying* \$4,000. *The land on one side of the farm was found to be worth one dollar per acre more than that on the other. The surveyor was required to divide this farm equitably between the two purchasers, by a line parallel to the longest side.*

Let $x =$ the price per acre of the land on one side, the $x+1$ will be the price of the other; and $\frac{4000}{x}$ will express th number of acres at one price; also, $\frac{4000}{x+1}$ will express the number of acres at the other price. These expressions must equa the number of acres in the farm; therefore we have

$$\frac{4000}{x} + \frac{4000}{x+1} = 200. \qquad (1)$$

This reduces to

$$x^2 - 39x = 20. \qquad (2)$$

From which we get

$$x = 39.506 \text{ nearly.}$$

This is the price per acre in dollars of the land on one side of the farm, and 40.506 will be the price of the land on the other side; and $\frac{4000}{39.506} = 101.25$ acres, which is the part belonging to one purchaser.

And $\frac{4000}{40.506} = 98.75$ acres, which is the part belonging to the other purchaser.

Also, $\frac{1012.5}{50} = 20.25$ chains, the width of one part.

And, $\frac{987.5}{50} = 19.75$ chains, the width of the other part.

Therefore, the dividing line will be 19.75 chains from one corner, and 20.25 chains from the other.

PROBLEM XV.

A rectangular farm, 50 *chains in length and* 40 *chains in breadth, is to be divided into two parts of equal value, by a line parallel to the longest side, on the supposition that the value of the land increases uniformly from one side to the other.*

Measuring from the side where the land is of the least value, we have

$\frac{40}{\sqrt{2}} = 28.284$ chains to the dividing line; the part on that side will contain 141.42 acres; the other part will contain 58.58 acres.

PROBLEM XVI.

A triangular field, whose base is 35 *chains and whose altitude is* 20 *chains, is to be divided by a line parallel to its base into two parts of equal value, on the supposition that the land* *increases uniformly in value from the vertex to the base of the triangle.*

Ans. The altitude of the triangle will be $\frac{20}{\sqrt[3]{2}} = 14.142$ chains, and the altitude of the trapezoid will be 5.858 chains.

PROBLEM XVII.

There is a piece of land bounded as follows: Beginning at the westernmost point of the field; thence,

	BEARINGS.	CHAINS.
1	N. 35° 15′ E.	23.00
2	N. 75° 30′ E.	30.50
3	S. 3° 15′ E.	46.49
4	N. 66° 15′ W.	49.64

It is required to divide this field into four equal parts, by two lines, one running parallel to the third side, the other cutting the first and third sides.

Find the distance of the parallel line from the first corner measured on the fourth side, and the bearing of the other line, and its distance from the first corner measured on the first side.

Ans. Distance to the parallel = 32.50 chains. Bearing of the other division line, S. 88° 22′ E. Distance, 5.99 chains.

TO LOCATE A LINE.

In running a line that is to be permanent, two flag-staffs should be used, so as to allow back-sights to be taken at each station. Permanent monuments or marks should be established at each end of the line, such as a stone, or a stake of some durable wood, surrounded by stones.

Trees directly on the line should be marked as line trees, by hewing the bark with an ax on the opposite side of the tree in the direction of the line, and then cutting distinct notches in the place hewed. Trees not on the line, but near it, may be marked by hewing the bark on the side toward the line in two places, more or less distant, according as the tree is nearer or farther from the line. The corners or points where lines intersect should be distinctly marked or indicated by the bearing and distance of objects near.

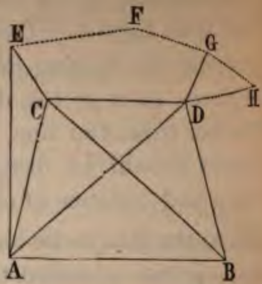
When the line to be located has two points known, or there are two points admitted to be on the line, begin at one of the known points, and run on the bearing of the line, if that is known; or if the bearing of the line is not known, run as near the true line as may be. Drive stakes at equal distances on the line run, as at every 5 or 10 chains, according to the length of the line and the condition of the ground. If the line thus run does not come to the other given point, measure the perpendicular distance from the given point to the line run, and by proportion compute the distance each stake is off the true line. Then move each stake its corresponding distance, and the line required will be marked out by the stakes.

SECTION VI.

TRIANGULAR SURVEYING.

Triangular Surveying is a method of finding the distance between remote points by measuring, as a base line, one side of the first of a series of triangles, of which each consecutive two have a common side, and observing the angles of all the triangles in the series.

Some of the other lines, however, should be measured after being computed, as a test of the accuracy or inaccuracy of the operations.



Let AB represent a base line, which must be very accurately measured, for any error in AB will cause a proportional error in every other line.

If at A we measure the angles BAC, BAD, and at B we measure *or observe* the angles ABC, ABD, we then have sufficient data to determine the points C and D, and the line CD.

With the same facility with which we determine the point C, we can determine E, or F, or G, or any other *visible* point.

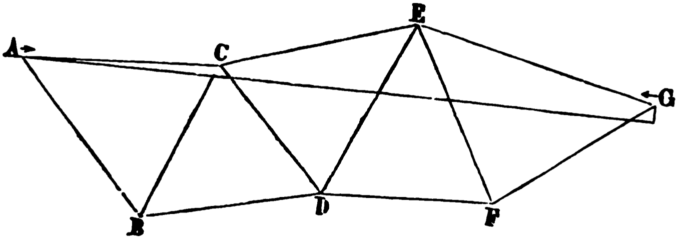
Thus we may determine all the sides and angles of the figure $CEFGHD$, or any *visible* part of it, by triangulating from the base AB.

The lines forming the triangles are not drawn, except those to the points C and D; we omitted to draw others to *avoid confusion*.

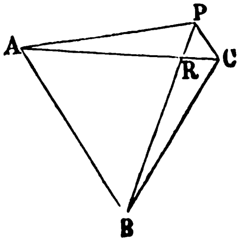
After any line, as FG, has been computed, it is well to measure it, and if the measurement corresponds with computation, or nearly so, we may have full confidence in the accuracy of the work as far as it has been carried.

We may take CD as the base, and determine any number of points visible, as A, B, H, F, G, &c.; trace any figure and determine its area; or show the relative positions and distances of objects from each other, such as buildings, monuments, trees, &c.

But to make the computation, triangle after triangle, for the sake of making a map, would be very tedious; and to measure every side and angle would be as tedious; and to facilitate this kind of operation we may have an instrument called the PLANE TABLE.



To determine the distance from A to G, two points remote from each other, measure the base AB; then with a theodolite measure the angles of the triangle ABC, the station C being selected so as to be visible from A and B; then compute the sides AC and BC, and measure the angles of the triangle BCD, the station D being visible from B and C; then compute the sides BD and CD. Thus continue until the point G is reached, when the whole system of triangles will be known, and the distance and bearing of the two points A and G will be known.



It sometimes happens that the theodolite cannot be placed directly over the station, as at C in the diagram; then it should be placed at P as near to C as may be. Measure the line PC, and the angles APB and BPC; then

$$ARB = APB + PAC,$$

Also,

$$ARB = ACB + PBC$$

Therefore, we get

$$ACB = APB + PAC - PBC.$$

From the triangle PAC, we have

$$\text{Sin.}PAC = \frac{PC \sin.APC}{AC};$$

from the triangle PBC, we have

$$\text{Sin.}PBC = \frac{PC \sin.BPC}{BC}.$$

Since PC is small compared with AC, we may take the arc for the sine; so also in the triangle PBC. Then substituting these values in the above, we get

$$ACB = APB + PC\left(\frac{\sin. APC}{AC} - \frac{\sin. BPC}{BC}\right)$$

AC and BC can be computed from the angle APB, instead of ACB, the base AB being known, and the angle APB being nearly equal to ACB. The correction above must be reduced to arc by dividing by the sine of $1''$; then we shall have

$$ACB = APB + \frac{PC}{\sin. 1''}\left(\frac{\sin. APC}{AC} - \frac{\sin. BPC}{BC}\right)$$

and the correction will be positive or negative according to the position of the point P with reference to the station C. When the point P is on the circumference of a circle passing though the stations A, B, and C, the correction will be nothing.

In this method the stations are selected so as to avoid the introduction of either very large or very small angles in any of the fundamental triangles, and the line selected for the base must admit of being measured with the greatest accuracy.

After the triangulation has been carried to considerable extent, a line connected with this system, and called a base of verification, is selected and measured; the computed length compared with the measured length is a test of the accuracy of the work.

In the French Trigonometric Survey under Mechain and Delambre, a base of verification was measured and found to differ less than one foot from the computed length, depending upon a system of triangles extending to the fundamental base 400 miles distant.

In the English Survey, General Roy measured a base of verification on Romney Marsh, in Kent, and the measured length differed only 28 inches from the length computed from a system of triangles extending to the fundamental base on Hounslow Heath, sixty miles distant.

In the United States survey, a base was measured on Kent Island, in Chesapeake Bay, and another one on Long Island, nearly 200 miles distant. The length of one side of a triangle, nearly 12 miles, as deduced from one of these bases, differed but 20 inches from the length deduced from the other base.

By computing a system of triangles in this way, we can determine the relative positions of places accurately, and give great precision to the geography of the country.

An important application of this method is found in the measurement of arcs of the terrestrial meridian, in different latitudes, from the results of which we deduce the true figure of the earth.

HARBOR SURVEYING.

When the triangulation includes coasts and harbors, where it is necessary that the depth of water should be indicated, as well as the position of rocks, shoals, &c., signals should be anchored on the shoals and rocks, and their bearings from each end of a known base must be taken. Then in each triangle there will be known all the angles, and one side to determine the triangle, and thus the position of the rocks and shoals will become known. To indicate the depth of water, soundings must be made, and the bearings of signals must be taken from the extremities of some known base, when, as before, there will be known all the angles and one side of each triangle to determine its vertex, which will define the position of the sounding.

Another method is to measure with a sextant the angles included between lines drawn from the place of a sounding to three distant objects whose places have been previously determined. Then the position of the soundings can be determined by Pothenot's Problem, or the problem of three points.

In trigonometrical surveying, on shore, the observer is supposed to take his angles from the extremities of a base line; but in trigonometrical surveying on water, the observer can take his angles only from single points which may be connected together by distant base lines on the shore.

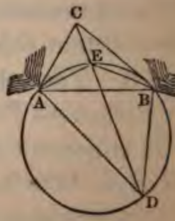
Important points along the shore are determined by taking latitude and longitude, and intermediate places, by regular land surveying.

The localities of rocks and shoals are also determined by astronomical observations, establishing latitude and longitude, in case no land is in sight, or they are far from the shore; but in the vicinity of the land, the determination of a point is commonly effected by the *three point problem.*

The three point problem is the determination of any point from observations taken at that point, on *three* other distant points, where the distances of these three points from each other are known.

It is immaterial how those points are situated, provided the three points and the observer are not in the same right line, the middle one may be nearest or most remote from the observer, or two of them may be in one right line with the observer, or all three may be in one right line, provided the observer be not in that line. The following example will illustrate the principle.

Coming from sea, at the point D, I observed two headlands, A and B, and inland, C, a steeple, which appeared between the headlands. I found, from a map, that the headlands were 5.35 miles from each other; that the distance from A to the steeple was 2.8 miles, and from B to the steeple 3.47 miles; and I found with a sextant, that the angle ADC was 12° 15′, and the angle BDC 15° 30′. Required my distance from each of the headlands, and from the steeple.



If the direction of AB is known, the direction of AC is equally well known.

The case in which the three objects, A, C, and B, are in one right line, may require illustration.

At the point A, make the angle $BAE=$

the observed angle *CDB*; and at *B*, make the angle *ABE* = the observed angle *ADC*.

Describe a circle about the triangle *ABE*, join *E* and *C*, and produce that line to the circumference in *D*, which is the point of observation. Join *AD*, *BD*. The angle *ADB* is the sum of the observed angles, and *AEB* added to it, must make 180°.

The Trigonometrical Analysis.—In the triangle *ABE*, we have the side *AB* and all the angles; *AE* and *EB* can therefore be computed.

In the triangle *AEC*, we now have *AC*, *AE*, and the angle *CAE*, from which we can compute *ACE*; then we know *ACD*.

Now in the triangle *ACD*, we have *AC* and all the angles; whence we can find *AD* and *CD*.

SECTION VII.

CANAL AND ROAD SURVEYING.

Surveys of roads or highways are taken in nearly the same manner as the sides of fields are measured. The bearing and distance of each portion must be taken, and entered in a note book, which will define the position of the main lines; then offsets must be made to determine the position of the sides of the highway, and the limits of private property. A map must be made, on which the principal lines shall be delineated, and such permanent monuments referred to, as will enable a surveyor to recover the original lines and limits of the highway, should any of them be lost.

CANAL SURVEYING.

The preliminary surveys of canal routes are conducted in the same manner as the survey of roads. A base line is measured and its bearings taken, from which offsets are made to determine the width and position of the canal, and also its various embankments. In the re-survey of the New York canals, the inner line of the towing path was established as the base line. This is called on the maps the red line. The outer line of the towing path, determined by offsets from the base line, is called the blue line, and this line marks the boundary between the property of the state and that of individuals adjacent to the canals throughout the state.

PUBLIC LANDS.

Soon after the organization of the present government, several of the States ceded to the United States large tracts of unoccupied land, and these, with other lands since acquired by treaty and purchase, constitute what is called the public lands.

Previous to 1802, there was no general plan for surveying the public lands, or in fact, no surveys were made; and when grants were made the titles often conflicted with each other, and in some cases different grants covered the same premises.

In the year 1802, Colonel I. Mansfield, then Surveyor General of the North-western Territory, adopted the following method;

Through the middle, or about the middle of the tract to be surveyed, a meridian is to be run, called the *principal meridian*. At right angles to this, and near the middle of it, an east and west line is to be run, and called the *principal parallel*.

Other meridians are to be run, six miles distant from the principal meridian, both east and west.

Also, parallels of latitude are to be run, six miles from the principal parallel, both north and south.

When this is done (and it has been on all the public lands east of the Mississippi river), the whole country is divided into squares, six miles on a side, called *townships*.

Each township contains 36 square miles. Each square mile is called a section, and it contains 640 acres. Sections are divided into half sections, quarter sections, and eighths. But these divisions are only made on paper.

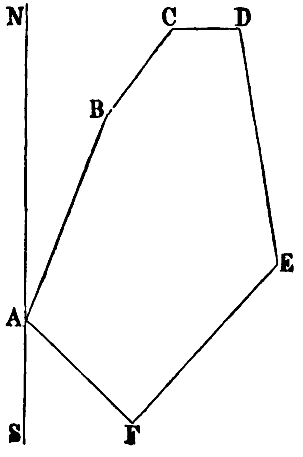
Townships which lie along a meridian are called a *range*, and numbered to distinguish them from each other.

Sections are regularly numbered in every township; and to designate any particular one, we say, section 13, in township number 4 north, in range 3 east.

This shows that the third range of townships east of the principal meridian, in township No. 4 north of the principal parallel, is the township, and the thirteenth section of this township is the one sought.

SURVEY BILL.

Beginning at a stake and stones, thence running north 20° east 17.87 chains; thence north 30° east 8.40 chains, to an elm tree; thence east 6.32 chains to stake and stones; thence south 10° east 19.20 chains; thence south 40° west 16.80 chains; thence north 50° west 12 chains to the place of beginning: containing by computation 38.72 acres of land.



The survey bill of every piece of land measured should be carefully written, for the description of the premises in the title deed is a copy of the Surveyor's statement.

Permanent objects near the corners, such as trees, &c., should be referred to; names of the owners of adjacent lands should be stated; also roads and streams of water should be so mentioned as clearly to define the premises.

SECTION VIII.

VARIATION OF THE COMPASS.

As the true meridian is an astronomical line, we must find it by astronomical observations; and then by comparing the meridian of the compass with it, we shall have the variation of the compass.

When the sun is on the equator, it rises due east, and sets directly in the west. Should we then observe the direction of its center, just as it was rising or setting, at the time it had no declination, and trace that line a short distance on the ground, we should have a due east and west line.

If from any point in that line we draw another line at right angles, we should then have the true meridian.

If we now put the compass on this meridian, and make the sight-vanes range with it, the needle will also range with it, if there is no variation. But if the north point of the needle is to the west of the sight-vane, the variation is westerly; if to the east, easterly; and the number of degrees and parts of a degree that the needle deviates from the direction of the sight-vanes shows the amount of the variation.

But it is not to be supposed that any particular observer can be at the points and places, where the sun is either rising or setting just at the time the sun is on the equator. We must have a broader basis, and in fact by means of the latitude of the observer and the declination of the sun, any observer has the means of knowing the precise direction in which the sun will rise or set, any day in any year.

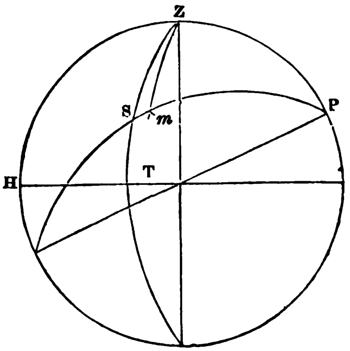
Let us suppose that the sun on a certain day, observed from a certain place, must have risen S. 81° E., but by the compass it was observed to rise S. 79° E., the variation of the compass was therefore 2° west.

These observations are called taking an azimuth. Azimuths are often taken at sea to determine the variation of the compass.

On land, however, the horizon is rarely visible and very few observations on sunrise or sunset can be made; besides there are other objections arising from atmospherical refraction. It is therefore best, most convenient, and more conducive to accuracy, to take the sun when up 10°, 15°, or 25° above the horizon, observe its direction per compass, and compare the result with the computed bearing for the same moment, and if the two results agree the compass has no variation; if they disagree the amount of such disagreement is the amount of the variation of the compass.

The true bearing of the sun can be determined when the observer knows his latitude, the sun's declination, and the altitude of the sun.

In the diagram let *Z* be the zenith of the observer, *P* the north pole, and *S* the place of the sun when its altitude was taken. Then will *PZ* be the observer's co-latitude; *PS* will be the sun's co-declination, and *ZS* will be the sun's co-altitude, and the angle *PZS* will give the sun's bearing or azimuth.



In the spherical triangle PZS, the three sides will be known, and to find an angle, we have the equation,

$$\text{Cos.}PS = \cos.PZ \cos.SZ + \sin.PZ \sin.SZ \cos.Z \quad (1)$$

If we put $\Delta =$ the sun's declination, $L =$ the observer's latitude, and $A =$ the sun's altitude; then since Δ is the complement of PS, L that of PZ, and A that of SZ, the above equations will become

$$\text{Sin.}\Delta = \sin.L \sin.A + \cos.L \cos.A \cos.Z. \qquad (2)$$

from which we can determine the angle Z by its cosine.

Example.

In latitude 39° 6′ 20″ north the sun's declination was 12° 3′ 10″ north, and the true altitude of the sun's center was observed to be 30° 10′ 40″. What was the sun's azimuth?

In this example $\Delta = 12° 3' 10''$, $L = 39° 6' 20''$, and $A = 30° 10' 40''$; with these values we get $PZS = 99° 17'$, or $HZS = 80° 43'$. Hence the bearing of the sun is S. 80° 43′ E.

If at the time of taking the altitude of the sun another observer had taken its bearing by the compass, and found it to be S. 80° 43′ E., then the compass would have no variation, and whatever it differed from that would be the amount of variation.

If a line were run along the ground, direct toward the center of the sun, at the time the altitude was taken, and sufficiently marked, that would be a standing line of known direction; and if from any point in that line, we could draw another line, making an angle with it of 99° 17′ on the north, or 80° 43′ on the south, such a line definitely marked, would be a permanent meridian line for all time to come, on which we could at any time place a compass, and observe its variation.

tead of equations (1) and (2) we may use the equation

$$\text{Cos.}\tfrac{1}{2}Z = \left(\frac{\text{sin.}S\,\text{sin.}(S-PS)}{\text{sin.}PZ\ \text{sin.}SZ}\right)^{\frac{1}{2}}$$

which we get Z by the cosine of half Z, where S is half m of the sides.

e $PZ = 50° 53' 40''$; $PS = 77° 56' 50''$; $ZS = 59° 49' 20''$
l $S = 94° 19' 55''$, and $S-PS = 16° 23' 5''$.

ice $\text{Sin.}S = +9.998758$
$\text{Sin.}(S-PS) = +9.450381$
$\text{Sin.}PZ = -9.889853$
$\text{Sin.}ZS = -9.936750$
$2)19.622536$
$\text{Cos.}\,49° 38' 36' = 9.811268$

refore $Z = 99° 17' 12''$ nearly as before.

equation is adapted to logarithms; see Spherical Trig-try.

OATE A MERIDIAN LINE FROM OBSERVATIONS UPON THE NORTH STAR WITH A THEODOLITE.

north star, Polaris, is now 1863, about 1° 25′ distant the north pole, and the star apparently makes a circle the pole in a sidereal day, making two transits across eridian, one above and the other below the pole—a on to it, at these times, would be a true meridian line. find these times, *subtract the right ascension of the sun the right ascension of the star*; increasing the latter by o render the subtraction possible, when necessary.

difference will be the time of the upper transit, and nd 59m. from that time will be the time of the transit. The right ascension of the sun is to be found in the Nautical Almanacs, for every day in the year; and it is nearly the same, for the same day, in every year.

For example. At what time will the north star make its transits over the meridian on the first day of July, 1853.

	H.	M.	S.
∗ *R. A.* +24h....................	25	6	0
⊙ *R. A.*.........................	6	41	16
	18	24	44

This result shows that the upper transit will occur about 6h. 24m., in the morning of the 2d of July. I say *about*, because I took the sun's right ascension for the morning of July 1, and from that time to 6, next morning, is 18 hours; and during this time the right ascension of the sun will increase full 3 minutes—therefore the upper transit will take place 6h. 21m. in the morning, and the previous lower transit 11h. 59m. previous, or at 6h. 22m., evening.

The time when the north star is on the meridian may be known approximately, since the star in the handle of the dipper nearest the four stars that form the dipper, passes the meridian nearly at the same time as the north star. Having obtained the time the pole star will be on the meridian, direct the telescope so that at that moment the star shall be upon the middle spider line, and the line of the telescope will indicate the true meridian; and this line permanently marked will enable the surveyor to ascertain the variation of his compass at any time.

Or knowing his latitude, and having from the Almanac the north star's polar distance, and its time of passing the meridian, the surveyor can find when the pole star will be at its greatest elongation east or west from the equation

$$\text{Cos.}P = \text{tan.}L\,\text{tan.}\Delta,$$

Where L is the latitude of the place, and Δ is the north star polar distance, and P is the time angle, which angle reduced to time by allowing 15° for one hour, will give the time of the star's greatest elongation. This may be approximately known by the position of the dipper; the first star in the handle of the dipper will be in a horizontal line with the north star. Direct the telescope to the star a little before this time, and follow the star until it ceases to move in the same direction. Then mark the direction of the telescope.

Compute the star's azimuth from the equation

$$\sin.\Delta = \cos.L \cdot \sin.Z,$$

Where Δ is the star's polar distance, L is the latitude, and Z the angle of azimuth.

Then with the theodolite upon the line of greatest elongation, set off the angle Z as determined from the above equation, and the line thus run will be the true meridian.

Example.

In 1863, the polar distance of the north star is about 1° 25′. Required its azimuth for latitude 43° 3′.

From the last equation, we have,

$$\text{Sin}.Z = \frac{\sin.\Delta}{\cos.L},$$

And since $\Delta = 1°\ 25'$, and $L = 43°\ 3'$, we have,

$$\begin{aligned} \text{Sin. } 1°\ 25' &= 8.393101 \\ \text{Cos. } 43°\ 3' &= \underline{9.863774} \\ \text{Sin. } 1°\ 56'\ 20'' &= 8.529327 \end{aligned}$$

Which is the angle Z, or the azimuth of the pole star at that time. If the direction of the star at the time of its greatest elongation has been marked out, then with the theodolite mark out another line intersecting the first at an angle of 1° 56′ 20″, and it will be the meridian.

By placing a compass on any well defined and true meridian, we can determine its variation by simple observation.

The declination of the needle, or the variation, as it is called, is the angle between the true and the magnetic meridian.

In the United States, the magnetic needle points west of north at all places in the eastern and middle states, and east of north in the western states.

Those places where the true and magnetic meridian coincide, or where the needle points directly north, are said to be on the line of no declination; and those places where the angle between the true and magnetic meridian is the same, are said to be on lines of equal declination.

At the close of the last century, the western declination in the United States was decreasing, and the eastern declination was increasing; this is now reversed, the western declination is increasing, and the eastern is decreasing. In the New England States, the western declination is increasing from 5′ to 7′ annually. In the middle states, the western declination is increasing at the rate of from 3′ to 4′ annually; and in the southern and western states at the rate of about 2′ annually.

The change of declination is not constant at the same place, and at different places is quite unequal. In 1835, Charlottesville, in Virginia, was on the line of no declination, and the line of no declination then struck Lake Erie, not far from Erie in Pennsylvania. In 1840, the line of no declination was west of Charlottesville, so the declination of that place was 19′ west while the line struck Lake Erie, not far east of Cleveland, in Ohio, the declination of that place being then 19′ east.

In the 34th and 39th volumes of the American Journal of Science, Professor Loomis published charts with lines of equal declination for the greater part of the United States, arranged for the years 1838 and 1840.

In the Coast Survey Report for 1856, under the direction of Dr. Bache, a chart with lines of equal magnetic declination was published. This chart embraced the Pacific Coast, and the lines were arranged for the year 1850.

The following table shows the magnetic declination of several places in the United States.

TABLE OF DECLINATIONS.

PLACE.		DECLINATION.	DATE.
Maine	N. E. angle	19° 12′ W.	1838
Cambridge	Mass.	9° 18′ W.	1840
Burlington	Vt.	9° 45′ W.	1837
New Haven	Ct.	6° 10′ W.	1845
Columbia College	N. Y.	6° 25′ W.	1845
Albany	N. Y.	7° 54′ W.	1855
Washington	D. C.	5° 44′ W.	1855
Buffalo	N. Y.	1° 25′ W.	1837
Philadelphia	Pa.	4° 8′ W.	1840
Pittsburg	Pa.	0° 33′ W.	1845
Charlottesville	Va.	0° 19′ W.	1840
Hudson	Ohio	0° 52′ E.	1840
Raleigh	N. C.	0° 44′ E.	1854
Charleston	S. C.	2° 30′ E.	1849
Cincinnati	O.	4° 26′ E.	1840
Detroit	Mich.	2° 00′ E.	1840
Mobile	Ala.	7° 05′ E.	1850
Nashville	Ten.	7° 07′ E.	1835
Alton	Ill.	7° 45′ E.	1840
St. Louis	Mo.	8° 37′ E.	1840
Natchez	Miss.	9° 00′ E.	1802
San Francisco	Cal.	15° 27′ E.	1852

The change of declination can be ascertained from the recorded bearings of old lines, as the division lines of farms. Place the compass upon the line whose bearing is given, and direct the sights to a flag-staff upon another distant point of the same line; the reading of the compass compared with the recorded bearing of the line will give the change of declination.

To retrace lines from the bearings given in "ancient deeds." First, ascertain the change of declination since the dates of the record; then if the change has been west, add the change to the S. W. and N. E. bearings, and subtract the change from the N. W. and S. E. bearings; if the change has been east, then subtract the change from the S. W. and N. E. bearings, and add it to the N. W. and S. E. bearings. The bearings thus corrected will give the included angle at each corner of the field the same as the old bearings.

Example.

In an old deed the following bearings were given:

	BEARINGS.
1	S. 10° W.
2	N. 71° W.
3	N. 37° E.
4	S. 53° E.

The change of declination was found to be 3° 30′ west. What will be the bearings of the sides?

	BEARINGS.
1	S. 13° 30′ W.
2	N. 67° 30′ W.
3	N. 40° 30′ E.
4	S. 49° 30′ E.

Ans.

If at the time the above bearings were taken the declination of the needle were 3° 30′ west, what would be the bearings of the sides referred to the true meridian?

	BEARINGS.
1	S. 6° 30′ W.
2	N. 74° 30′ W.
3	N. 33° 30′ E.
4	S. 56° 30′ E.

Ans.

The lines of an old survey may be retraced by moving the the vernier of the compass through an arc equal to the change in the declination of the needle since the old survey was made; then with the compass thus adjusted, run the lines according to the bearing given in the notes of the old survey.

Or place the compass on a well marked line of the old survey, and move the vernier until the needle indicates the same bearing as given for that line in the notes of the old survey; then the compass will retrace the lines of the survey from the original bearings, and the reading of the vernier will indicate the change of declination since the original survey was made.

Any land mark to the corner of a lot laid down by the original surveyors, must remain; subsequent surveyors can straighten lines between point and point, and decide what the true courses are, and how many acres the lot contains.

When a surveyor is called to survey any farm or estate that has been previously surveyed, he must find some corner as a place of commencing, and from this run a *random* line, as near the true line as his judgment permits; and if he strikes another corner he has run the true course; if not, he corrects his course, as taught in Chapter IV. Thus he must go round the field from corner to corner. He has a right to *establish corners* only where no corners are to be found, and no evidence can be obtained as to the existence and locality of a former land mark.

It may be the case that a surveyor is called to survey a lot where no corners are to be found. If a fence or line exists, which has been the undisputed boundary for a long time, that boundary cannot be changed, and the surveyor must establish a corner by ranging some other line to meet the first. Sometimes corners may be found to some neighboring lot, from which lines can be run to establish a corner to the lot we wish to survey.

Lines of lots in the same town are generally parallel; and a surveyor who offers his services to the public, must make himself acquainted with the general directions of the lines of lots, over that section of country where his services are required.

When a surveyor is called to divide a piece of land, he is then an original surveyor, and not liable to be embarrassed by old lines and old traditions; he has then only his mathematical problem before him.

Owing to the inaccuracies of original surveys, and the impossibility of leaving proper land marks, in consequence of the great haste in which lands were originally surveyed, great confusion has followed, in some sections of our country, in respect to lines, and it has been no uncommon thing to have whole neighborhoods at variance, if not in law, in reference to the boundaries of their lands.

CHAPTER V.

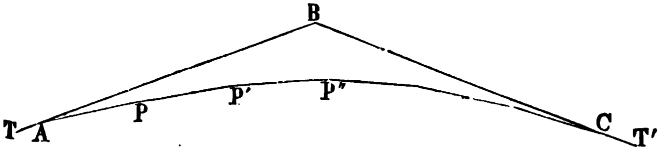
TOPOGRAPHICAL SURVEYING.

SECTION I.

LOCATING CURVES.

PROBLEM I.

To stake out a curve with the Compass or Transit.



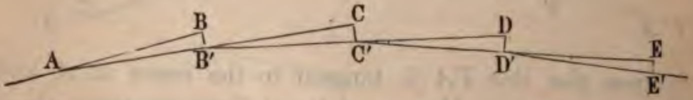
Suppose the line TA is tangent to the curve at A and C is tangent at C. Measure AB and determine the angle at then will r, the radius of the required curve, be equal to B tan. $\frac{1}{2}B$, and the angle BAP will be found from the ation $\frac{c}{2r} = \sin.BAP$, where c is the engineer's chain; n with the transit at A, make an angle BAP as deteried by the above equation, and from A measure one chain to where put a pin; make the angle BAP' double the angle AP, and measure one chain from P to range with AP'; a pin at P. Make the angle BAP'' three times the angle AP; measure from P' one chain in range with AP'', and put a pin at P'', and so on; the pins at P, P', P'', &c., will be in the circumference of a circle.

If it is not convenient to measure AB, take the bearing and distance from A to C; then will the radius of the required curve be $\frac{\frac{1}{2}AC}{\sin. BAC} = r$, whence we can get the angle BAP as before. When $AB = BC$, the lines are tangents at A and C, but otherwise not. By the last method the curve must pass through the given point C, but may not be so that the given line will be tangent at the point C; when the point C is not given, we may assume any convenient radius, and then stake out the curve.

PROBLEM II.

To locate a curve with a chain.

Let r be the radius of the required curve, and c the length of the chain in feet; then will $\frac{c^2}{2r}$ be the versed sine of the arc whose chord is the given chain.



Suppose the straight line AB is tangent to the curve at A. Put a pin at A, and extend the chain its length from the pin along the line AB; deflect the chain into the position AB', so that the versed sine $\frac{c^2}{2r}$ shall measure the distance of B' from the line AB. Put a pin at B', extend the chain along the line AB' to C; then deflect the chain to C', so that CC' shall be double the versed sine $\frac{c^2}{2r}$, or double the deflection at B'. Put a pin at C', then extend the chain along the line $B'C'$ to leflect to D' making the deflection DD' equal to CC', n.

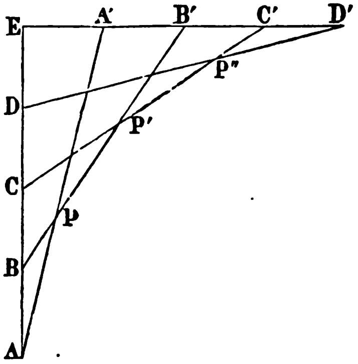
ins at A, B', C' and D', will be in the circumference e, and AB', $B'C'$, $C'D'$, &c., will be equal chords in vhose radius is r.

the curve is again to unite with a straight line as at next deflection, as at E, must be half that at D', or e as at the first point B'; that is, the deflection must e given versed sine.

example, the radius of the required curve is 1,000 chain being 100 feet, then $\frac{c^2}{2r}$ will equal 5 feet, the n at B'; at C', the deflection will be 10 feet, while e deflection will be 5 feet, and $D'E'$ will be tangent rve at E'.

PROBLEM III.

ke out a parabola to which two given lines shall be



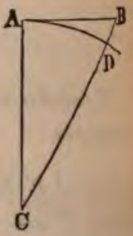
E and ED' be the es meeting at E. off equal spaces, as C, &c., on the line stakes at the points D, &c. Also meas- equal spaces on the , and put stakes as ', C', &c.

out AA' and BB', a stake at the inter- f the ranges at P; then range out CC', and put a P where the range intersects that of BB'; range out d at P'' put a stake where DD' intersects CC'. The stakes at P, P', P'', will be on the arc of a parabola, and the line AE will be tangent at A, and ED' will be tangent at D'; this method will apply whether $AE = ED'$ or not.

SECTION II.

LEVELING.

The surface of tranquil water is called a level surface; a line whose points are all equally distant from a surface of tranquil water is called a line of true level; a straight line tangent to the true level at a given point is called the line of apparent level with reference to that point.



Let C be the center of the earth, and A a point at its surface; then AD is the line of true level, and AB, the tangent at the point A, is the line of apparent level, and BD is the difference between the true and apparent level for the distance AB.

To compute BD, we will let $AC = r$, $AB = d$, and $BD = h$; then will $BC = r+h$. From the right-angled triangle BAC, we have $(r+h)^2 = r^2+d^2$, from which we get,

$$2rh+h^2 = d^2.$$

But since BD is small, compared with AC, the radius of the earth, we may neglect h^2, whence we shall have,

$$2rh = d^2,$$

Or, $$h = \frac{d^2}{2r}.$$

Since $2r$ is constant the equation $h = \frac{d^2}{2r}$ shows that the ence between the true and apparent level varies as the of the distance.

n the above equation we put for $2r$ the mean diameter earth 7,912 miles, and take $d = 1$ mile, we shall get inches; hence, at the end of one mile, the true level is nches below the apparent level.

ve take any distance in miles, and multiply its square ve shall get in inches the difference between true and nt level for distance taken; thus, for 3 miles we multi- y 8, and get 72 inches, or 6 feet, the correction for 3

ind the correction for 2 chains, or 200 feet, we have,

$$
\begin{array}{lcr}
\text{Log. } 200 & = & 2.301030 \\
\text{Log. } 5280 & = & 3.722634 \\
\hline
 & & \bar{2}.578396 \\
 & & 2 \\
\hline
 & & \bar{3}.156792 \\
\text{Log. } 8 & = & 0.903090 \\
\hline
\text{Log. } .01148 & = & \bar{2}.059882
\end{array}
$$

shows that for 200 feet the correction is but little over an inch.

find the distance at which an object, whose height is can be seen from the surface of the earth.

d and d' be any two distances, and h and h' their cor- ding heights; then we shall have,

$$d^2 = 2rh$$

$$d'^2 = 2rh'.$$

refore,

$$\frac{d^2}{d'^2} = \frac{h}{h'}.$$

we know that when $d' = 3$ miles, h' will be 6 feet.

$$\text{Therefore, } \frac{d^2}{9} = \frac{h}{6}, \text{ or } \frac{d^2}{3} = \frac{h}{2}.$$

$$\text{Whence, } \quad d = \sqrt{\frac{3h}{2}},$$

Which gives the distance in miles when the height is given in feet.

Example 1.

The lantern of the old Eddystone Light-house was 92 feet above the water. How far could its light be seen?

Put $h = 92$ feet, and we get,

$$d = \sqrt{\tfrac{3}{2} \cdot 92} = \sqrt{138} = 11.75 \text{ miles.}$$

Example 2.

A spring of water is found to be on an apparent level with a given point, and distant from it 15,000 feet. What is the fall from the spring to the given point?

Solution.—Log. 15,000	= 4.176091
Subtract Log. 5280 to reduce to miles	= 3.722634
	0.453457
Multiply by 2 to square distance	2
	0.906914
Add log. $\frac{8}{12}$ correction for 1 mile in feet	= $\bar{1}.823909$
Log. 5.38 feet	= 0.730823

which is the fall from the spring to the given point.

PROBLEM I.

To find the difference of level between any two stations with the theodolite.

Place the theodolite at one of the stations, say the lower, and take the angle of elevation and measure the distance from one station to the other; then multiply the measured distance by the sine of the angle of elevation; the product will be the elevation of one station above the line of apparent level passing through the other.

The same distance multiplied by the cosine of the angle of elevation will give the horizontal distance, which reduced to miles, squared, and multiplied by 8, will give the correction in inches for true level.

If the horizontal distance is measured, we must multiply by the tangent of the angle of elevation for the difference of level.

Example.

At a given station an object 6000 feet distant gave with the theodolite an angle of elevation of 5° 10′. What was its true altitude?

Solution. Sin. 5° 10′ = 8.954499
Log. 6000 = 3.778151
Log. 540.32 = 2.732650

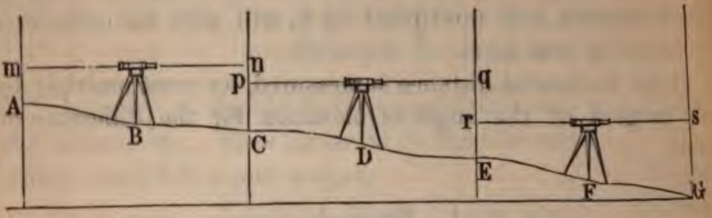
which gives the elevation of the object above the line of apparent level, 540.32 feet.

And cos. 5° 10′ = 9.998232
Log. 6000 = 3.778151
Log. 5975.6 ft. = 3.776383
To reduce to miles, Log. 5280 = 3.722634
0.053749
Square 2
0.107498
Log. $\frac{8}{12}$ $\bar{1}.823909$
Log. .8539 ft. $\bar{1}.931407$

Whence we may take .85 feet as the correction for true level; this added to 540.32 will give 541.17 feet for the altitude of the object.

PROBLEM II.

To find the difference of level between any two points on the earth's surface.



Let A and G be two proposed points, to find the elevation of A above G. Measure from A toward G any convenient distance, say two chains to C; put a pin at A, and one at C; set up the engineer's level at B, midway between A and C; on the pins at A and C set up the leveling rods; direct the telescope of the level to the target at m, read off from the rod the elevation of m above A, and record it in feet and tenths as a *back sight*; then direct the telescope to the target at n, read off from the rod the elevation of n above c, and record it in feet and tenths as a *fore sight*. From C measure toward G, a distance CE, equal to AC, and put a pin at E, set up the level at D, midway between C and E, and move the rod from A to the pin at E, direct the telescope to the target at P, and read off from the rod the elevation of P above C, and record it as a *back sight;* then direct the telescope to the target at q, and read off the elevation of q above E, and record it as a *fore sight*. Proceed in this way until it is convenient to set up a rod on a pin at G, then find the sum of the back sights and and the sum of the fore sights. The difference of these sums will give the elevation of one point above the other.

A horizontal line passing through either of the proposed points is called a "datum line," and any point carefully determined with reference to other points is called a "bench." It is convenient to record the field notes in the form of a tablet as follows:

STATIONS.	BACK-SIGHTS.	FORE-SIGHTS.	DIFFERENCE.	FROM DATUM LINE	FROM GRADE LINE.
B	3.2	6.0	2.8	2.8	1.33
D	5.1	9.0	3.9	6.7	1.56
F	4.2	9.9	5.7	12.4	0.00

The first column shows the several stations; the second column shows the back-sights at each station; the third column shows the fore-sights; the fourth column shows the difference of elevation between each two stations; the fifth column shows the distance of each pin from the *datum line;* the sixth column shows the distance of each pin from the *grade line.*

If at station *B* we find *Am* equal 3.2 feet, and *Cn* equal 6.0 feet; and if at station *D* we find *Cp* equal 5.1 feet, and *Eq* equal 9.0 feet, and at station *F* if *Er* equal 4.2 feet, and *Gs* equals 9.9 feet, then will *C* be 2.8 feet below *A*, and *E* will be 3.9 feet below *C*, and *G* will be 5.7 feet below *E*. The numbers in the fifth column show that *C* is 2.8 feet below the *datum line* that passes through *A*, and that *E* is 6.7 feet below the same line, and that *G* is 12.4 feet below the same line.

The numbers in the sixth column show that the pin at *C* is 1.33 feet above a grade line from *A* to *G*, and that the pin at *E* is 1.56 feet above the same grade.

The numbers in the fourth column are found by subtracting the back sights from the fore sights; the numbers in the fifth column are found by adding the numbers in the fourth column.

To find the numbers in the sixth column, compute the distance from the *datum line* to the *grade line* at each of the pins; this can easily be done since we know the position of the lines, and the distance from one pin to another. The difference between these computed distances, and the corresponding numbers in the fifth column, will give the required numbers in the sixth column. In the above example, the fore sights exceed the back sights; if at any station the fore sight is less than the back sight, the difference in the fourth column must be marked, so that in using it we shall get correct numbers for the fifth column.

Example 1.

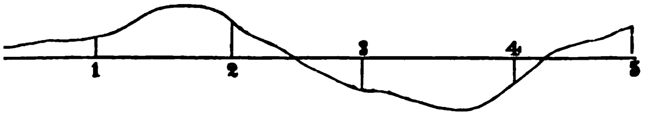
From the following field-notes it is required to find the difference of level, to exhibit the section, and to reduce the same to grade.

STATIONS.	BACK SIGHTS.	FORE SIGHTS.	DIFF. LEVEL.	FROM DATUM.	FROM GRADE.
1	8.2	5.4	+ 2.8	+2.8	+2.0
2	12.1	9.2	+ 2.9	+5.7	+4.1
3	2.0	12.1	−10.1	−4.4	−6.8
4	7.4	8.8	− 1.4	−5.8	−9.0
5	12.4	2.6	+ 9.8	+4.0	0.0

Find the numbers in the fourth column by taking the difference of the fore and back sights, making the remainder positive when the back sights are the larger, and negative when the back sights are the smaller.

Find the numbers in the fifth column by adding the numbers in the fourth column, according to their signs, as follows: 2.8, the first number in the fourth column, is the first number in the fifth column; 5.7, the second number in the fifth column, is the sum of 2.8 and 2.9; −4.4, the third number, is the sum of 5.7 and −10.1; −5.8, the fourth number, is the sum of −4.4 and −1.4; and +4.0, the last number in the column, is the sum of −5.8 and +9.8.

To exhibit the section from the above, draw a datum line through *A*, as the first point; on this line, with any scale of equal parts, set off the distances of the several pins as at 1, 2, 3, 4, 5. The numbers in the fifth column of the above tablet



ss the distance of the pins above or below the datum line, ding as they are positive or negative. Hence, if at the s 1, 2, 3, 4, 5, with any convenient scale, we make off- corresponding to the numbers in the fifth column, a line n through the extremities of the offsets will exhibit the tions in the surface of the ground.

a grade line be drawn from *A* to the pin at 5, it will be above 1 in the datum line, 1.6 above 2, 2.4 above 3, 3.2 above 4, when the pins are equally distant from each . These numbers, combined with the numbers in column give the numbers in column sixth, which show the posi- of the pins with reference to the grade line.

Example 2.

FIELD NOTES.

STATIONS.	BACK SIGHTS.	FORE SIGHTS.
1	3.35	2.25
2	4.40	1.80
3	2.00	6.50
4	3.25	4.00
5	4.00	5.00
6	5.10	7.20

rom the above field-notes, required the difference of level he several points, and the cutting necessary to carry a grade from the first to the last pin.

Example 3.

FIELD NOTES.

STATIONS.	BACK SIGHTS.	FORE SIGHTS.
1	4.32	7.21
2	5.22	8.17
3	9.18	6.27
4	6.27	6.12
5	6.12	3.76
6	9.81	11.62
7	8.47	9.02
8	2.64	8.91
9	1.07	7.38
10	4.29	5.32
11	5.32	4.85
12	4.85	3.17
13	8.22	1.53

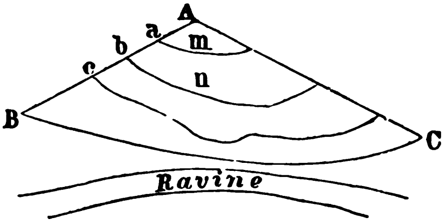
From the above field-notes it is required to determine the difference in the elevations of the several points, and also to reduce them to a grade line passing from the first to the last pin.

CONTOUR OF GROUND.

Contour of ground is shown on maps, by marking where equi-distant parallel planes meet the surface. We shall give only the general principle.

Let A be the top of a hill, whose contour we wish to delineate; measure any convenient line AB, up or down hill, and by the level or theodolite, ascertain the relative elevations of a, b, c, d, &c., as many planes as we wish to represent.

At a, place the level or theodolite, and level it ready for observation; measure the height of the instrument, and put the target on the rod at that height.



Send the rod-man d axe-man round e hill, on the same vel as the instru- ent. Let the rod- an set the rod; the veler will sight to it rough the telescope, and if the target is below the level, he ill motion the rod-man up the hill, if too high, down the hill; length he will get the same level, and there the ax-man ill drive a stake. In the same manner we will establish nother stake further on; and thus proceed from point to oint. To get round the hill, it may be necessary to move e instrument several times. The plane thus established, is presented by the curve *am*.

In the same manner, by placing the instrument at *b*, we can stablish the next plane *bn*.

Then the next, and the next, as many as we please. Where e hill is more steep, two of these parallel planes will be earer together in the figure; where less steep, they will ppear at a greater distance asunder; and this, with the proper ading, will give a true representation of the ground.

Another method is to select an elevated point in the field hose contour is to be represented, and from that point run iverging lines; then with the theodolite or level, determine e difference of level between all the important points on ese lines; then by proportion, ascertain where pins must be riven to mark the intersections of these lines by equi-distant arallel planes. Curves drawn through the points marked by e pins will indicate the contour of the field.

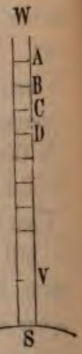
Another method is to ascertain the difference of level on everal parallel sections running through the field.

The sections plotted will give the contour of the surface ore or less exactly, according to the number of the sections nd the nature of the surface.

ELEVATIONS DETERMINED BY ATMOSPHERIC PRESSURE, AS INDICATED BY THE BAROMETER.

The higher we ascend above the level of the sea, the less is the atmospheric pressure (other circumstances being the same), and therefore we can determine the ascent, provided we can accurately measure the pressure, and know the law of its decrease.

The pressure of the atmosphere at any place, is measured by the height of a column of mercury it sustains in the barometer tube.



It is found *by experiment*, that air is compressible, and the amount of compression is always in proportion to the amount of the compressing force.

Now, suppose the atmosphere to be divided into an indefinite number of strata, of the *same thickness*, and so small that the density of each stratum may be considered as uniform.

Commence at an indefinite distance above the surface of the earth, as at A, and let w represent the weight of the whole column of atmosphere resting on A. Let the small and indefinite distances between AB, BC, CD, &c., be equal to each other, and we shall call them *units* of some unknown magnitude.

The weight of the column of atmosphere supposed to rest on B, is greater than w, by some indefinite part of w, say the nth part. Then the weight on B, must be expressed by $\left(w+\frac{w}{n}\right)$ or $\left(\frac{n+1}{n}\right)w$.

In the same manner, the weight or pressure resting on C must be the weight above B, increased by its nth part; that is, it must be $\left(\frac{n+1}{n}\right)w+\left(\frac{n+1}{n^2}\right)w$, which by addition is $\frac{(n+1)^2w}{n^2}$.

In the same manner, we find that the weight resting on D, must be $\frac{(n+1)^3}{n^3}w$, and so on. For the sake of perspicuity, we recapitulate.

The pressure on A is	w;	units from A	0
“ “ on B is	$\left(\frac{n+1}{n}\right)w$;	“ “	1
“ “ on C is	$\frac{(n+1)^2}{n^2}w$;	“ “	2
“ “ on D is	$\frac{(n+1)^3}{n^3}w$;	“ “	3
“ “ on E is	$\frac{(n+1)^4}{n^4}w$;	“ “	4
“ on F is	$\frac{(n+1)^5}{n^5}w$;	“ “	5

Here we observe the series which represents the pressure of the atmosphere, at the different points A, B, C, &c., is a series in *geometrical progression*, and it corresponds with another series in *arithmetical progression*; therefore, by the nature of logarithms, the numbers in the arithmetical series may be taken as the logarithms of the numbers in the geometrical series.

But this system of logarithms may not be *hyperbolic* nor tabular; indeed it is neither. The *base of this system* is as yet unknown; but our investigations will soon lead to its discovery.

Now, let the number of units from A to S (the surface of the sea), or *to the lower of two stations*, be represented by x; then the expression for the pressure of the air would be $\left(\frac{n+1}{n}\right)^x w$. But this is neither more nor less than the weight of the column of mercury in the barometer, which is sustained by this pressure.

By calling this b, and designating the logarithms of this unknown system by L' we shall have

$$L'b = x. \qquad (1)$$

Taking y to represent the number of units from A to V, and $b_{,}$ to represent the pressure of the air at that point, we shall have

$$L'b_{,} = y. \tag{2}$$

Subtracting (2) from (1), we shall have

$$L'b - L'b_{,} = x - y = SV.$$

That is, a certain *peculiar logarithm* of the barometer column at the lower station, diminished by the logarithm of the barometer column at the upper station will give the difference of level of the two stations. But still all is indefinite and unknown, because we know nothing of these logarithms.

In algebra, we learn that the logarithms of one system can be converted into another by multiplying them by a constant multiplier called the *modulus* of the system, therefore

Assume Z to be the modulus or constant that will convert common logarithms into these peculiar logarithms.

Then, $$Z(\log.\ b - \log.\ b_{,}) = SV. \tag{3}$$

Here $\log.\ b$ denotes the common logarithms of the barometer column.

Equation (3) is general, and determines nothing until we know SV in some particular case.

Taking SV some *known elevation*, and observing the altitude of the barometer column at both stations, then equation (3) will give Z once for all.

Putting h to represent the *known elevation*, we have, in general,

$$Z = \frac{h}{\log.b - \log.b_{,}}. \tag{4}$$

Example.—At the bottom and top of a tower, whose height was 200 feet, the mercury stood in the barometer as follows:

At the bottom, 29.96 inches $= b$
At the top, 29.74 inches $= b_{,}$,

the temperature of the air being 49° of Fahrenheit's thermometer.

Whence,

$$Z = \frac{200}{\log. 29.96 - \log. 29.74} = \frac{200}{0.003201} = 62500 \text{ nearly.}$$

"But this multiplier is constant only when the mean temperature of the air at the two stations is the same; and for a lower temperature the multiplier is less, and for a higher it is greater. *A correction, however, may be applied for any deviation from an assumed temperature, by increasing or diminishing (according as the temperature is higher or lower) the approximate height by its 449th part for each degree of Fahrenheit's thermometer.* We can moreover change the multiplier to a more convenient one by assuming such a temperature as shall reduce this number to 60000 instead of 62500. Now 62500 exceeds 60000 by its 25th part; and, since 1° causes a change of one 449th part, the proportion

$$\tfrac{1}{449} : 1^\circ :: \tfrac{1}{25} : 17.9,$$

gives 18° nearly for the reduction to be made in the temperature of the air at the time of the above observations, in order to change the constant multiplier from 62500 to 60000, or to 10000, by calling the height fathoms instead of feet. Thus, instead of the thermometer standing at 49°, we may suppose it to stand at 49°—18° or 31°; and then, we take 10000 as the multiplier, and apply a correction additive for the 18° excess of temperature."

The same observations, for example, being given, to find the height of a tower.

$$\begin{array}{lcl}
\text{Log. } 29.96 & = & 1.47654 \\
\text{Log. } 29.74 & = & \underline{1.47334} \\
\text{Diff. of log.} & = & 0.00320 \\
\text{Multiplier} & = & \underline{10000} \\
\text{Product} & = & 32
\end{array}$$

Then the height of the tower is 32 fathoms, or 32 × 6 = 192 feet, on the supposition that the temperature of the air was

31° in place of 49°. But it being 49°, we must increase 192 by its $\frac{1}{449}$ part for each degree above 31°, that is, by $\frac{18}{449}$ or $\frac{1}{25}$ nearly of its approximate height, which gives nearly 8 feet to add to 192, making 200 feet for the height of the tower.

The same method is applicable to other cases whatever be the temperature of the air at the two stations, provided it be the same or nearly the same at both stations, or provided we take the mean temperature of the two stations. We can find the difference of levels of two stations to considerable accuracy by the following

RULE.

1st. *Take the difference of the logarithms of the two barometer columns, and remove the decimal point four places to the right. This is the approximate difference of levels in fathoms.*

2d. *Add* $\frac{1}{449}$ *of the approximate height for each degree of temperature above* 31°, *and* SUBTRACT *the same for each degree below* 31°; *the result cannot be far from the truth.*

PRACTICAL APPLICATIONS.

Example 1.—The barometer at the base of a mountain stood at 29.47 inches, and taking it to the top it fell to 28.93 inches. The mean temperature of the air was 51°. What was the height of the mountain in feet? *Ans.* 503.34 feet.

$$\begin{aligned} \text{Log. } 29.47 &= 1.469380 \\ \text{Log. } 28.93 &= \underline{1.461348} \\ &\ 0.008032 \end{aligned}$$

Approximate height in fathoms, 80.32

Correction.—Add $\frac{20}{449}$ of the 80.32 to itself, that is, add 3.58

$$\begin{aligned} \text{Height, in fathoms} &= \ 83.9 \\ \text{Multiply by} &\ \underline{6} \\ \text{Height in feet} &= 503.4 \end{aligned}$$

The average height of the barometer, at the level at the sea, is 30.09 inches; and now, if we know the average height of the barometer at any other place, and the average temperature, it is equivalent to knowing the elevation of the latter place above the level of the sea.

For example, the mean height of the barometer at Albany Academy is 29.96, and the mean temperature is 49°. How high is the academy above the tide water?

Ans. 117.3 feet.

$$\begin{array}{rrl} \text{Log. } 30.09 = & 1.478422 & 49^\circ \\ \text{Log. } 29.96 = & \underline{1.476542} & \underline{31} \\ & 0.001880 & 18^\circ \end{array}$$

$$\begin{array}{lr} \text{Approximate height} = & 18.80 \text{ fathoms.} \\ \text{Add } \frac{18}{449} \text{ or } \frac{1}{25}, & \underline{75} \\ & 19.55 \times 6 = 117.3 \text{ feet} \end{array}$$

When the difference of temperatures at the two stations is considerable, the result must be affected by it.

When the upper station is the coldest, which is generally the case, the mercurial column will be shorter than it otherwise would be, and consequently indicate too great a height.

If the temperature of the upper station is taken for the temperature of the lower, the mercurial column at the lower station would not be high enough, and the deduced result would be too small, as is the case in example 5.

The contraction of mercury being about one 10000th part for each degree of cold, or 0.0025 in a column of 25 inches, it would require 4° difference of temperature to produce an effect amounting to one division on the scale of a common barometer, where the graduation is to hundredths of an inch.

This correction is combined with the former in the following equation, in which t and t' represent the temperatures of the air at the two stations (t at the lower station), q and q' the temperatures of the mercury at the two stations, as indicated by the *attached* thermometer

The fraction 0.00223 is equal to $\frac{1}{449}$ nearly; h = the height sought, b and $b_{\prime}$ represent the observed heights of the mercurial columns.

$$h = 10000 \left\{ 1 + 0.00223 \left(\frac{t+t'}{2} - 31 \right) \right\} \log. \frac{b}{b_{\prime}(1+.0001)(q-q')}$$

Beside the corrections previously considered, regard is sometimes had to the effect of the variation of gravity in different latitudes, and at different elevations above the earth's surface. The latter, however, is too small to require any notice in an elementary work. The former may be found by multiplying the approximate height by 0.0028371 × cos. 2 lat. It is additive, when the latitude it less than 45°, and subtractive when greater. Or it may be taken from the following table.

Latitude.	Correction.
0°	$+\frac{1}{352}$ of the app. height.
5°	$+\frac{1}{358}$
10°	$+\frac{1}{375}$
15°	$+\frac{1}{407}$
20°	$+\frac{1}{460}$
25°	$+\frac{1}{548}$
30°	$+\frac{1}{705}$
35°	$+\frac{1}{1030}$
40°	$+\frac{1}{2030}$
45°	0
50°	$-\frac{1}{2030}$
55°	$-\frac{1}{1030}$
60°	$-\frac{1}{705}$
65°	$-\frac{1}{548}$
70°	$-\frac{1}{460}$
75°	$-\frac{1}{407}$
80°	$-\frac{1}{375}$
85°	$-\frac{1}{358}$
90°	$-\frac{1}{352}$

mple 2.—Given, the pressure of the atmosphere at the
of a mountain, equal to 29.68 in. of mercury, and that
ummit, equal to 25.28 in., the mean temperature being
find the elevation.

Ans. 727.2 fathoms, or 4363.2 feet.

nple 3.—The following observations were taken at the
d summit of a mountain, namely,

he foot,

ır. 29.862; attach. therm. 78°; detach. therm. 71°.

ıe summit,

ır. 26.137; attach. therm. 63°; detach. therm. 55°.

quired to find the elevation.

Ans. 612.9 fathoms, or 3677.4 feet.

nple 4.—It is required to find the height of a mountain
ude 30°, the observations with the barometer and ther-
er being as follows: namely,

ıe foot,

r. 29.40; attach. therm. 50°; detach. therm.* 43°.

ıe summit,

r. 25.19; attach. therm. 46°; detach. therm. 39°.

Ans. 683.27 fathoms, or 4097.62 feet.

–If we assume any temperature, for instance 45°, and the height
rometer at the level of the sea, at 30.09 inches, we can compute
tion of the point, where it would be 29.99, 29,89, 29.79, 29.69, &c.,
nd thus we might form a table, showing the elevations that would
d to any assumed height of the barometer at that temperature.
found, that the first fall of $\frac{1}{10}$ of an inch will correspond to about
elevation; but every subsequent tenth will require a greater and
evation.

ıple 5.—At a certain station the average reading of
ımeter, reduced to a temperature of 32°, was found to

---

attached thermometer measures the temperature of the mercury
ometer, and the detached thermometer, that of the surrounding

be 28.130 inches. What is the elevation of the station above tide water? *Ans.* 1755 feet.

Example 6.—Where the average reading of the barometer, reduced to 32°, is 28.980 inches, what is the elevation above the sea? *Ans.* 979 feet.

Example 7.—On a mountain the barometer indicated 24.860 inches, and the thermometer stood at 68°. What was the elevation of the mountain. *Ans.* 5386 feet.

CHAPTER VI.

NAVIGATION.

SECTION I.

DEFINITIONS.

gation is the art of determining the position of a ship ocean.

Axis of the earth is the line about which it revolves; emities of the axis are called poles.

Equator is a circle whose plane is perpendicular to the the earth.

lians are great circles passing through the poles of the .

itude is measured on the equator from an assumed n.

ude is measured on a meridian north or south of the .

lels of Latitude are small circles parallel to the .

ence of Latitude is the arc of a meridian between two s of latitude.

rture is distance measured on a parallel of latitude, west from a given meridian.

In Navigation the surface of the ocean is assumed to be spherical.

The **Course** of a ship is the angle its path makes with a meridian.

A ship is said to sail on the same course when its path crosses the meridians at the same angle.

The **Rhumb Line** is the path of a ship pursuing a uniform course on the surface of the ocean.

Nautical Distance is the portion of the Rhumb line intercepted between two points.

When a ship sails on several courses, the course and distance from the point left to the point arrived at are called the course and distance *made good.*

The several courses and distances spoken of together are called a *traverse;* and computing the course and distance made good, is called working a *traverse.*

The **Horizon** of a place is a circle whose plane touches the earth at the place.

The **Zenith** is the upper pole of the horizon.

Vertical Circles are those circles that pass through the poles of the horizon.

The **Altitude** of a body is the arc of a vertical circle intercepted between the horizon and the body.

The **Ecliptic** is the great circle in whose plane the earth performs its revolution around the sun.

The **Equinoctial Points** are the intersections of the ecliptic and equator.

One is called the *vernal,* the other the *autumnal* equinox.

Right Ascension is measured on the equator eastward from the vernal equinox.

Declination is measured on a meridian north or south of the equator.

The **Meridian** of any place is the great circle that passes through the poles of the equator, and the poles of the horizon of the place.

The course of a ship is ascertained by the *Mariner's Compass*, which differs from the surveyor's compass only in its graduation and adjustments.

LEEWAY.

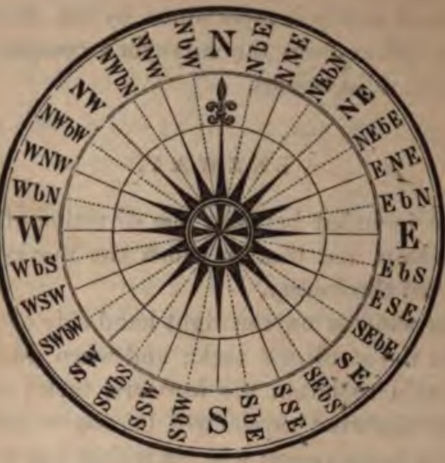
The angle included between the direction of the fore and aft line of a ship, and that in which she moves through the water, is called the *leeway*.

When the wind is on the right hand side of a ship, she is said to be on the *starboard* tack; and when on the left hand side, she is said to be on the *larboard* tack; and when she sails as near the wind as she will lie, she is said to be *close hauled*. Few large vessels will lie within less than six points to the wind, though small ones will sometimes lie within about five points, or even less; but, under such circumstances, the real course of a ship is seldom precisely in the direction of her head; for a considerable portion of the force of the wind is then exerted in driving her to leeward, and hence her course through the water is in general found to be leeward of that on which she is steered by the compass. Therefore to determine the point toward which the ship is actually moving, the leeway must be allowed *from the wind*, or toward the *right* of her apparent course when she is on the *larboard* tack; but toward the *left*, when she is on the *starboard* tack.

It is only when a ship crowds to the wind, that leeway is made.

It is seldom that two ships on the same course make precisely the same leeway; and it not unfrequently happens, that the same ship makes a different leeway on each tack. It is the duty of the officer of the watch to exercise his best skill in determining or estimating how much this deviation from the apparent course amounts to.

CARD OF THE MARINER'S COMPASS.



The card attached to the needle of the mariner's compass is divided into thirty-two equal parts, called points. There are eight points in each quadrant; they are counted from the meridian NS, as in the diagram; thus N.b.E. is one point east of north, and is read north by east; the angle is one-eighth of 90°, or 11° 15′. And N.N.E. is two points east of north, or 22° 30′ east, and is read north, north east. In the same manner the courses in the other quadrants are read. Each point is usually subdivided into quarter points of 2° 48′ 45″ each. Seamen take the course of their ship to the nearest quarter point, and for their convenience in practical navigation, the traverse table is arranged so as to give for various distances the latitudes and departures for points and quarter points, and on the plane scale the line of chords, called the line of rhumbs, is marked for the same angles.

TABLE.

ving the degrees and minutes corresponding to each nd quarter point of the compass.

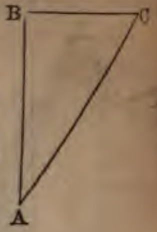
	S.	S.	N.	POINTS.	ANGLES.
	S.¼E.	S.¼W.	N.¼W.	.¼	2° 48′ 45″
	S.½E.	S.½W.	N.½W.	.½	5° 37′ 30″
	S.¾E.	S.¾W.	N.¾W.	.¾	8° 26′ 15″
	S.bE.	S.bW.	N.bW.	1	11° 15′ 0″
.¼E.	S.bE.¼E.	S.bW.¼W.	N.bW.¼W.	1¼	14° 3′ 45″
.½E.	S.bE.½E.	S.bW.½W.	N.bW.½W.	1½	16° 52′ 30″
.¾E.	S.bE.¾E.	S.bW.¾W.	N.bW.¾W.	1¾	19 41′ 15″
E	S.S.E.	S.S.W.	N.N.W.	2	22° 30′ 0″
E.¼E.	S.S.E.¼E.	S.S.W.¼W.	N.N.W.¼W.	2¼	25° 18′ 45″
E.½E.	S.S.E.½E.	S.S.W.½W.	N.N.W.½W.	2½	28° 7′ 30″
E.¾E.	S.S.E.¾E.	S.S.W.¾W.	N.N.W.¾W.	2¾	30° 56′ 15″
N.	S.E.bS.	S.W.bS.	N.W.bN.	3	33° 45′ 0″
N.	S.E.¾S.	S.W.¾S.	N.W.¾N.	3¼	36° 33′ 45″
N.	S.E.½S.	S.W.½S.	N.W.½N.	3½	39° 22′ 30″
N.	S.E.¼S.	S.W.¼S.	N.W.¼N.	3¾	42° 11′ 15″
	S.E.	S.W.	N.W.	4	45° 0′ 0″
E.	S.E.¼E.	S.W.¼W.	N.W.¼W.	4¼	47° 48′ 45″
E.	S.E.½E.	S.W.½W.	N.W.½W.	4½	50° 37′ 30″
E.	S.E.¾E.	S.W.¾W.	N.W.¾W.	4¾	53° 26′ 15″
E.	S.E.bE.	S.W.bW.	N.WbW.	5	56° 15′ 0″
E.¼E.	S.E.bE.¼E.	S.W.bW.¼W.	N.W.bW.¼W.	5¼	59° 3′ 45″
E.½E.	S.E.bE.½E.	S.W.bW.½W.	N.W.bW.½W.	5½	61° 52′ 30″
E.¾E.	S.E.bE.¾E.	S.W.bW.¾W.	N.W.bW.¾W.	5¾	64° 41′ 15″
	E.S.E.	W.S.W.	W.N.W.	6	67° 30′ 0″
¾N.	E.bS¾S.	W.bS.¾S.	W.bN.¾N.	6¼	70° 18′ 45″
½N.	E.bS.½S.	W.bS.½S.	W.bN.½N.	6½	73° 7′ 30″
¼N.	E.bS.¼S.	W.bS.¼S.	W.bN.¼N.	6¾	75° 56′ 15″
	E.bS.	W.bS.	W.bN.	7	78° 45′ 0″
	E.¾S.	W.¾S.	W.¾N.	7¼	81° 33′ 45″
	E.½S.	W.½S.	W.½N.	7½	84° 22′ 30″
	E.¼S.	W.¼S.	W.¼N.	7¾	87° 11′ 15″

SECTION II.

PLANE SAILING.

e **Sailing** is a method of determining the position of a at sea, from the properties of plane triangles.

e the path of the ship crosses the meridians at the same the *distance*, *departure*, and difference of latitude have the same relation to each other as the sides of a plane right-angled triangle, in which the course is the angle opposite the departure and the distance is the hypotenuse.



In the triangle ABC, if AC represent the distance, and the angle at A is the course, then will AB represent difference of latitude, and BC will represent departure; any two of these quantities being given, we can determine the others by trigonometry. (See Chap. 2, Sect. II., Prop. 3). Thus we have

$$R : AC :: \sin.A : BC,$$

$$\text{or } R : \text{distance} :: \text{sin. course} : \text{departure}; \qquad (1)$$

$$R : AC :: \cos.A : AB,$$

$$\text{or } R : \text{distance} :: \text{cos. course} : \text{diff. lat.}; \qquad (2)$$

$$R : \tan.A :: AB : BC,$$

$$\text{or } R : \text{tan. course} :: \text{diff. lat.} : \text{departure}. \qquad (3)$$

EXAMPLES.

1. If a ship sail from Cape St. Vincent in lat. 37° 2′ 54″ N., 148 miles on a course S. 39° 22½′ W, required her latitude and departure.

By proportion (1), we have

$$\begin{aligned} &\text{Sin. } 39^\circ\ 22\tfrac{1}{2}, && = 9.802359 \\ &\text{Log. } 148 && = \underline{2.170262} \\ &\text{Log. } 93.89 = \text{log. depart.} && = 1.972621 \end{aligned}$$

By proportion (2), we have

$$\begin{aligned} &\text{Cos. } 39^\circ\ 22\tfrac{1}{2}' && = 9.888185 \\ &\text{Log. } 148 && = \underline{2.170262} \\ &\text{Log. } 114.4 && = 2.058447 \end{aligned}$$

Whence the difference of latitude is 114.4 miles, which is 1° 54′ 24″. Hence

$$\begin{aligned} &\text{Latitude left} && = 37^\circ\ \ 2'\ 54''\ \text{N.} \\ & && \quad\ \underline{1^\circ\ 54'\ 24''\ \text{S.}} \\ &\text{Latitude arrived at} && = 35^\circ\ \ 8'\ 30''\ \text{N.} \end{aligned}$$

2. A ship sails from latitude 40° 28′ N., E. S. E. 21 miles. Required her latitude and departure.

Ans. Latitude 40° 20′ N.; Departure 19.4 miles.

3. A ship sails from Oporto, in lat. 41° 9′ N., N. 47° 48¾′ W. 315 miles. Required her departure and latitude.

Ans. Dep. 233.4 miles; Lat. 44° 41′ N.

4. A ship sails from lat. 55° 1′ N., S. 33° 45′ E., till her departure is 45 miles. Required her latitude, and the distance sailed. *Ans.* Dist. 81 miles; Lat. 53° 54′ N.

5. A ship from lat. 36° 12′ N. sails south-westward, until she arrives at lat. 35° 1′ N., having made 76 miles departure. Required her course and distance.

Ans. Course S. 46° 57′ W.; Dist. 104 miles.

6. A ship sails from Halifax, in lat. 44° 44′ N., S. 50° 37½′ E., until her departure is 128 miles. Required her latitude, and the distance sailed.

Ans. Lat. 42° 59′; Dist. 165.6 miles.

7. A ship leaving Charleston light, in latitude 32° 43′ 30″ N., sails north eastward 128 miles, and is then found 39 miles north of the light. Required her course, latitude, and departure. *Ans.* Latitude 33° 22′ 30″ N.; Course N. 72° 16′ E.; Departure 122 miles.

8. A ship from Cape St. Roque, in latitude 5° 10′ south, sails N. E. ½ N. 7 miles an hour, from 3 P. M. until 10 A. M. Required her distance, departure, and latitude.

Ans. Dist. 133 miles; Dep. 84.4 miles; Lat. 3° 27′ S.

7. A ship from latitude 41° 2′ N. sails N. N. W. ¾ W. 5½ miles an hour, for 2½ days; required her distance, departure, and latitude arrived at.

Ans. Dist. 330 miles; Dep. 169.7 miles; Lat. 45° 45′ N.

When a ship has sailed on several different courses, the reduction of them to a single course and distance is called working the traverse. This is most readily done by taking from the traverse table the latitude and departure of each distance, and arranging the numbers in columns in a tablet ruled for the purpose. Then the difference between the sum of the northings and the sum of the southings, will be the latitude of the distance made good; and the difference between sum of the eastings and sum of the westings, will be the departure of the distance made good.

A ship makes the following courses and distances.

	BEARINGS.	MILES.
1	S.bW.	23
2	W.S.W.	40
3	S.W.¾W.	18
4	W.½N.	28
5	S.bE.	12
6	S.S.E.¼E.	16

Required her course and distance made good, her departure and difference of latitude.

From the traverse table, we obtain the numbers in the following tablet.

	COURSES.		POINTS.	MILES.	N.	S.	E.	W.
1	S.bW.	S. 11° 15′ W.	1	23		22.56		4.49
2	W.S.W.	S. 67° 30′ W.	6	40		15.31		36.96
3	S.W.¾W.	S. 53° 26¼′ W.	4¾	18		10.72		14.46
4	W.½N.	N. 84° 22½′ W.	7½	28	2.74			27.87
5	S.bE.	S. 11° 15′ E.	1	12		11.77	2.34	
6	S.S.E.¼E.	S. 25° 18¾′ E.	2¼	16		14.46	6.84	
					2.74	74.82	9.18	83.78
						2.74		9.18
						72.08		74.60

Whence we have the departure 74.60 miles, and the difference of latitude 72.08 miles.

To find the course,

Log. 74.60 = 1.872739
Log. 72.08 = 1.857815
Tan. 45° 59′ = 10.014924

Whence the course is S. 45° 59′ W.

To find the distance,

Log. 74.60 = 1.872739
Sin. 45° 59′ = 9.856812
Log. 103.7 = 2.015927

Whence the distance is 103.7 miles.

10. A ship makes the following courses and distances:

	BEARINGS.	MILES.
1	S.S.W.	18
2	S.W.	15
3	S.W.bS.	20
4	W.	9
5	W.S.W.	14

Required her course and distance made good, the departure and difference of latitude.

	COURSES.		POINTS.	MILES.	N.	S.	E.	W.
1	S.S.W.	S. 22° 30′ W.	2	18		16.63		6.89
2	S.W.	S. 45° W.	4	15		10.61		10.61
3	S.W.bS.	S. 33° 45′ W.	3	20		16.63		11.11
4	W.	West.		9		0.0		9.00
5	W.S.W.	S. 67° 30′ W.	6	14		5.36		12.93
						49.23		50.54

Whence we see that the departure is 50.54, and the difference of latitude is 49.23.

To find the course,

Log. 50.54 = 1.703635
Log. 49.23 = 1.692230
Tan. 45° 45′ = tan. course, 10.011405

To find the distance,

Log. 50.54 = 1.703635
Sin. 45° 45′ = 9.855096
Log. 70.56 = log. distance, 1.848539

11. A ship makes the following courses and distances.

	BEARINGS.	MILES.
1	S.S.W.	42
2	S.W.	18
3	W.S.W.	24
4	W.	11
5	N.W.	108

Required her course and distance made good, her depar and difference of latitude.

Ans. Course, N. 83° 32′ W.; Distance, 139.3 miles; De ture, 138.4 miles; Diff. lat., 15.7 miles.

12. A ship on the equator sails as follows:

	BEARINGS.	MILES.
1	E.bS.	90
2	E.½S.	76
3	E.N.E.	41
4	N.E.	82

Required her position.

Ans. Course, N. 79° 23′ E.; Distance, 264.3 miles; D ture, 259.8 miles; and the ship is 48.7 miles north of the equ ship makes the following courses and distances:

	BEARINGS.	MILES.
1	W.	28
2	S.W.bW.	30
3	S.W.bS.	46
4	E.S.E.	28

ired her course and distance made good.

Ans. Course, S. 38° 43′ W.; Distance, 84.1 miles.

ship from latitude 42° north makes the following and distances,

	BEARINGS.	MILES.
1	S.S.W.	48
2	S.bE.	34
3	S.W.$\frac{1}{4}$W.	26
4	E.	17

d the latitude arrived at, and the course and distance od.

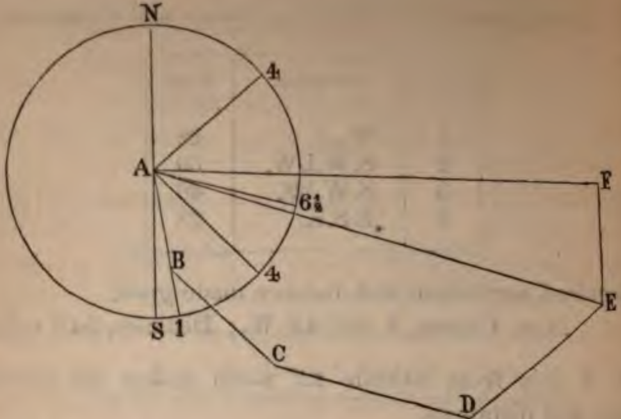
Lat. 40° 25′ N.; Course S. 8° 22′ W.; Dist. 96.2 miles.

in course of the day a ship has sailed on several difacks, seamen often determine approximately the course ance made good by drawing a diagram with a scale iders, as in the following example:

ship makes the following courses and distances.

1	S.bE.	20 miles
2	S.E.	30 "
3	E.bS.$\frac{1}{2}$S.	42 "
4	N.E.	36 "

d the course and distance made good, by construction.



About *A* as a center, describe a circle with a radius equal to the chord of 60°, taken from the line of chords on the plane scale. Draw *NAS* as a meridian; then from *S* set off *S*1, with the chord of the first course, taken from the line of rhumbs; then set off *S*4 with the chord of the second course, taken from the same line; then set off *S*6½ with the chord of the third course; then from *N* set off *N*4 in the northeast quadrant with the chord of the fourth course taken from the same line of rhumbs; then draw the lines *A*1, *A*4, *A*6½, and *A*4. On *A*1 set off the first distance 20 miles, taken from any scale of equal parts; suppose it extends to *B*. Then through *B* draw a line parallel to *A*4, and on it set off *BC* equal to 30 miles, the second distance; through *C* draw a line parallel to *A*6½; on it set off *CD* equal to 42 miles, the third distance; through *D* draw a line parallel to *A*4 in the northeast quadrant, and from the same scale of equal parts set off *DE* equal to 36 miles, the fourth distance. Then draw the line *AE*, and it will represent the distance made good; applying it to the scale, we find for the above example it equals 95 miles. For the course, extend the dividers from *S* to where the line *AE* cuts the circle, and then apply the dividers to the line of chords, and we shall get the bearing of *AE* equal to S. 73° 10′ E., nearly.

In plane sailing it is not assumed that the surface of the ocean is a plane, or nearly so, for short distances. But the properties of the *rhumb line* are such, that crossing the meridians each at the same angle, the length of the *rhumb line*, the *difference of latitude*, and the *departure*, have the same relation to each other as the sides of a plane triangle.

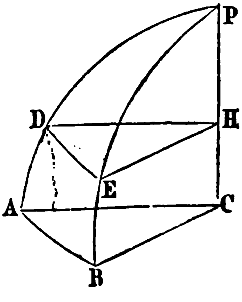
The rhumb line is a spiral; the difference of latitude is an arc of a great circle; the departure is an arc of a parallel of latitude, a small circle. It is assumed that these lines are drawn upon the surface of a sphere, and in consequence ot the above relation, we get the difference of latitude and departure accurately for a single course, whether the distance is long or short.

When a ship sails on several courses the sum of the departures is not precisely equal to the departure for the same distance on a single course.

Thus, when we work a traverse we get the difference of latitude accurately, and the departure approximately. Plane sailing does not give difference of longitude.

SECTION III.

TO FIND THE DIFFERENCE OF LONGITUDE.



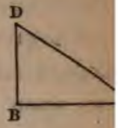
Let C be the center of the earth, P the pole, PC the axis of the earth, PDA and PEB meridians, AB a portion of the equator, DE a corresponding portion of a parallel of latitude. Then will AD be latitude; and if DH is parallel to AC, it will be the cosine of the latitude to a radius AC; DE will be departure, and AB will be differ-

ence of longitude. But we have from similar sectors, *DE*
and *ABC*,

$$DH : AC :: DE : AB \quad \text{or,}$$

(1) Cos. lat. : R :: departure : diff. longitude.

This proportion can be represented by a triangle as *BC*
where *BC* is departure.



The angle *BCD* is equal to the latitude, and the hypotenuse *DC* is the difference of longitude.

From plane sailing, we have

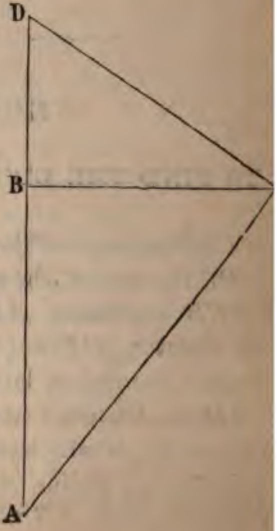
Sin. course : R : : departure : distance.

This combined with the preceding proportion so as to elimin
departure, will give

(2) Cos. lat. : distance : : sin. course : diff. longitude.

Also, from plane sailing, we have,

Diff. latitude : departure : : R : tan. course.



And this when combined with proportion (1) so as to eliminate departure will give,

(3) Cos. lat. : diff. lat. : : tan. course : diff. longitude.

If we put the triangle for plane sailing with the triangle for longitude, we shall have the diagram in the margin, in which *AC* is the distance, the angle at *A* is the course, *AB* is difference of latitude, *BC* is departure, the angle *BCD* is the latitude, the angle at *D* is co-latitude, and *DC* is the difference of longitude.

The triangle DAC gives the second proportion, since we have,

$$\text{Sin.}D : AC :: \sin.A : DC,$$

which is equivalent to the second proportion. The third is derived by using AB and tan.A as equivalent to BC.

Whence we have three propositions for finding longitude.

1. *Cosine of latitude is to radius as departure is to difference of longitude.*

2. *Cosine of latitude is to distance as the sine of the course is to difference of longitude.*

3. *Cosine of latitude is to difference of latitude as the tangent of the course is to the difference of longitude.*

The latitude in these proportions for longitude is the arithmetical mean of the latitude left and arrived at; it is obtained by taking half the sum when both latitudes are north or south, and half the difference when one is north and the other south. It is assumed that, measured on the parallel of this mean latitude, the departure is equal to the meridian distance; this is nearly so when the difference of latitude is small, and it may be rendered quite exact by corrections taken from a table prepared for the purpose, and first published by Mr. Workman in 1805.

When a ship sails on the parallel of latitude, the distance equals the departure, and proportion (1) gives the difference of longitude; this is called *parallel sailing.* When the ship does not sail on a parallel, but changes its latitude, and the difference of longitude is determined by proportions (2) and (3), the method is called *middle latitude sailing.*

EXAMPLE UNDER PROPORTION 1.

1. What difference of longitude corresponds to 47 miles departure in the latitude of 37° 23′? *Ans.* 59.15 miles.

Let x = the difference of longitude required.

Then, $\cos. 37° 23' : \text{R.} :: 47 : x = \dfrac{47 \text{ R}}{\cos. 37° 23'}$

$$\begin{array}{ll} \text{Log. } 47\,R & = 11.672098 \\ \text{Cos. } 37° 23' & = 9.900144 \\ \hline \text{Log. Diff. lon. } 59.15 = & 1.771954 \end{array}$$

2. How many miles, or how much departure, corresponds to a degree in longitude on the parallel of 42° of latitude?
Ans. 44.59 miles.

Here the longitude of one degree is given.

$$R : \cos. 42° :: 60 : x = \frac{60 \cos. 42°}{R}$$

$$\begin{array}{ll} \text{Log. } 60 & = 1.778151 \\ \text{Cos. } 42° & = 9.871073 \\ \hline \text{Log. } 44.59 & = 1.649224 \end{array}$$

3. A ship sails east from Cape Race, 212 miles; required her longitude. The latitude of the cape is 46° 40′ N., longitude 53° 3′ 15″ west. *Ans.* Lon. 47° 54′ west.

Cos 46° 40′ [illegible]

4. Two places in lat. 50° 12′ differ in longitude 34° 48′; required their distance asunder in miles. *Ans.* 1336.

5. How far must a ship sail W. from the Cape of Good Hope that her course to Jamestown, St. Helena, may be due north?
Ans. 1193 miles.

Co 34° 29′ R [illegible]

NOTE.—Cape { lat. 34° 29′ S. / lon. 18° 23′ E. Jamestown { lat. 15° 55′ S. / lon. 5° 43′ 30″ W.

6. How far must a ship sail E. from Cape Horn to reach the meridian of the Cape of Good Hope? The latitude of Cape Horn being 55° 58′ 30″ S., lon. 67° 21′ W., and the latitude and longitude of the Cape of Good Hope being as stated in the above note. *Ans.* 2878 miles.

7. In what latitude will the difference of longitude be three times its corresponding departure? *Ans.* 70° 31′ 44′.

The following examples are designed to illustrate the principles of Section 3.

Example 1.

A ship from Cape Clear, Ireland, in latitude 51° 25′ N. and longitude 9° 29′ W., sails as follows:

	BEARINGS.	MILES.
1	S.S.E.¼E.	16
2	E.S.E.	23
3	S.W.bW.½W.	36
4	W.¾N.	12
5	S.E.bE.¼E.	41

Required her course, distance, difference of latitude, and difference of longitude.

TRAVERSE TABLE.

COURSES.	POINTS.	DIST.	DIFF. LAT.		DEPARTURE.	
			N.	S.	E.	W.
S.S.E.¼E.	2¼	16		14.5	6.8	
E.S.E.	6	23		8.8	21.2	
S.W.bW.½W.	5½	36		17.0		31.7
W.¾N.	7¼	12	1.8			11.9
S.E.bE.¼E.	5¼	41		21.1	35.2	
			1.8	61.4	63.2	43.6
				1.8	43.6	
Result,				59.6	19.6	

Lat. left = 51° 25′ N.
Diff. lat. = 1° 00′ S.
Lat. in = 50° 25′ N. Mid. lat. 50° 55′.

To find the course and distance, by trigonometry,

As diff. lat., 59.6 miles,	1.775246
: Radius 90°	10.000000
: : Dep., 19.6 miles,	1.292256
: Tan. course, 18° 12′,	9.517010
As sin. course 18° 12′	9.494621
: Dep., 19.6 miles,	1.292256
: : Radius	10.000000
: Dist. 62.75 miles,	1.797635

To find the difference of longitude.

As cos. 50° 55′	9.799651
: Radius	10.000000
: : Dep., 19.6,	1.292256
: Diff. lon., 31.09 miles,	1.492605

Longitude left = 9° 29′ west
Diff. lon. = 31′ east
Lon. in = 8° 58′ west.

Thus, we have found the course 18° 12′; distance, 62.75 miles; diff. longitude, 31′ E.; lat. in, 50.25 N.; lon., 8° 58′ W.

If these be the distances run in a day, from noon to noon again, then the preceding operation is called working a day's work; otherwise it is called working a traverse.

Example 2.

A ship sails from lat. 37° 2′ north, and longitude 9° 2′ west, and makes the following courses and distance.

	BEARINGS.	MILES.
1	E.S.E.	45
2	S.W.bW.	43
3	S.E.bS.	64
4	N.N.E.	22

uired the latitude and longitude arrived at, and the course distance made good.

ake the northings, southings, eastings, and westings, from traverse table, and arrange them as in the following tablet:

	COURSES.	POINTS.	DIST.	N.	S.	E.	W.
1	E.S.E.	6	45		17.2	41.6	
2	S.W.bW.	5	43		23.9		35.8
3	S.E.bS.	3	64		53.2	35.6	
4	N.N.E.	2	22	20.3		8.4	
				20.3	94.3	85.6	35.8
					20.3	35.8	
					74.0	49.8	

Whence the difference of latitude is 74 miles south, ich is 1° 14′.

And the given latitude is 37° 2′ N.
Difference of latitude, 1° 14′ S.
Latitude arrived at, 35° 48′ N.

The departure is 49.8 miles; the mean latitude is 36° 25′, f the sum of the two above given; hence by Proportion we have

$$\text{Cos. } 36^\circ\ 25' : R :: 49.8 : \text{diff. lon.}$$

Therefore,

$$\begin{aligned} \text{Log. } 49.8 &= 1.697229 \\ \text{Cos. } 36^\circ\ 25' &= 9.905645 \\ \text{Log. } 61.88 &\quad 1.791584 \end{aligned}$$

And we have 61.88, or nearly 62, miles for the difference of gitude, which is equal to 1° 2′.

Therefore, longitude given = 9° 2′ W.
Difference of longitude = 1° 2′ E.
Longitude arrived at = 8° 0′ W.

To find the course, we have

Log. 49.8 = 1.697229
Log. 74.0 = 1.869232
Tan. 33° 56′ 9.827997

Whence the course is S. 33° 56′ E.

To find the distance, we have

Log. 49.8 = 1.697229
Sin. 33° 56′ = 9.746812
Log. 89.2 1.950417

Whence the distance is 89.2 miles.

Example 3.

A ship in latitude 33° 56′ south, and longitude 18° 23′ east, sails

1. N.W.bN. 12 miles.
2. N.W. 36 "
3. N.W.bW. 140 "

Required her latitude and longitude, and the course and distance made good.

Ans. Lat. 32° 3′ S.; Lon. 15° 26′ E.; Course, N. 52° 41′ W.; Dist. 187 miles.

Example 4.

A ship in latitude 42° 40′ N., longitude 59° W., sails S.E.bS. 600 miles. Required the latitude and longitude arrived at.

Ans. Lat. 34° 21′ N.; Lon. 51° 53′ W.

Example 5.

A ship in latitude 51° 18′ N., longitude 11° 15′ W., sailed S.E.¼S. 480 miles. Required the latitude and longitude arrived at. *Ans.* Lat. 45° 22′ N.; Lon. 3° 10′ W.

Example 6.

A ship finds by observations upon the light at Sandy Hook that her latitude is 40° 25′ N., and her longitude is 74° W. She then sails S.bW. 520 miles; it is required to find her course and distance thence to Nassau in latitude 25° 4′ N., and longitude 77° 18′ W.

Ans. Course, S. 8° 45′ W.; Dist. 416 miles.

Example 7.

Required the course and distance from Land's End, in latitude 50° 6′ N., and longitude 6° W., to Bermuda, in latitude 31° 20′ N., longitude 64° 48′ W.

Ans. Course, S. 66° 56′ W.; Dist. 2874 miles.

Example 8.

Required the course and distance from latitude 37° 48 N., and longitude 25° 13′ W., to latitude 50° 13′ N. and longitude 3° 38′ W.

Ans. Course, N. 51° 11′ E.; Distance, 1189 miles.

Example 9.

A ship in latitude 37° 48′ N. and longitude 58° 12′ W., sails on the following courses:

	BEARINGS.	MILES.
1	S. 67° 30′ E.	12
2	S.	6
3	S. 67° 30′ W.	6
4	N. 50° 37½′ E.	32

Required the latitude and longitude arrived at.

Ans. Latitude, 37° 55′ N.; Longitude, 57° 34′ W.

Example 10.

A ship in latitude 43° 25′ N., and longitude 65° 35′ W., sails on the following courses:

	BEARINGS.	MILES.
1	S.W.bS.	63
2	S.S.W.½W.	45
3	S.bE.	54
4	S.W.bW.	74

Required her course and distance thence to Sandy Hook light, in latitude 40° 27½′ N. and longitude 74° 1½′ W.

Ans. Course, N. 88° 14′ W.; Distance, 276 miles.

Example 11.

A ship sails from latitude 50° 8′ N. and longitude 4° 24′ W., on the following courses.

	BEARINGS.	MILES.
1	S. 19° 41¼′ W.	18
2	S. 75° 56¼′ W.	22
3	S. 53° 26¼′ W.	58

Required the latitude and longitude arrived at.

Ans. Lat. 49° 11′ N.; Lon. 6° 18′ W.

Example 12.

A ship from Cape Clear, latitude 51° 55′ N., longitude 9° 29′ W., sails as follows:

	BEARINGS.	MILES.
1	S.bW.	23
2	W.S.W.	40
3	S.W.¾W.	18
4	W.½N.	28
5	S.b.E.	12
6	S.S.E.¾E.	16

red her course, and distance made good; also, latitude itude arrived at.

Course, S. 45° 47′ W.; Distance, 102.4 miles; Latitude, 50° 44′ N.; Longitude, 11° 25′ W.

Example 13.

in latitude 41° 12′ N., longitude 37° 21′ W., sails as

	BEARINGS.	MILES.
1	S.W.bW.	21
2	S.W.½S.	31
3	W.S.W.½S.	16
4	S.¾E.	18
5	S.W.¼W.	14
6	W.½N.	30

red her course, distance, latitude and longitude.

Course, S. 52° 49′ W.; Distance, 111.7 miles; Latitude, 40° 5′ N.; Longitude, 39° 18′ W.

Example 14.

oon we were in latitude 28° 46′ S., and longitude 32° since then we have sailed by the log,

	BEARINGS.	MILES.
1	S.W.¾W.	62
2	S.bW.	16
3	W.¼S.	40
4	S.W.¾W.	29
5	S.bE.	30
6	S.¾E.	14

Required the direct course and distance, and our present latitude and longitude.

Ans. Course, S. 43° 14′ W.; Distance, 158 miles; Latitude, 30° 41′ S.; Longitude, 34° 24′ W.

Example 15.

A ship from Toulon, latitude 43° 7′ N., longitude 5° 56′ E. sailed,

	BEARINGS.	MILES.
1	S.S.W.	48
2	S.bE.	34
3	S.W.¼W.	26
4	E.	17

Required her course and distance to Port Mahon, latitude 39° 52′ N., and longitude 4° 18′ 30″ E.

Ans. Latitude of ship, 41° 32′ N.; Longitude, 5° 37′ E.

Course to Port Mahon, S. 30° 45½′ W. nearly; and distance, 116.4 miles.

Example 16.

On leaving the Cape of Good Hope for St. Helena, we took our departure; Cape Town bearing S. E. by S. 12 miles, after running N. W. 36 miles, and N. W. by W. 140 miles.

Required our latitude and longitude, and the course and distance made.

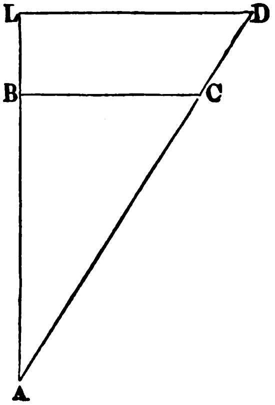
N. B. Latitude of Cape Town, 33° 56′ S. Longitude, 18° 23′ E.

Latitude of St. Helena, 15° 55′ S. Longitude, 5° 43′ 30″ W.

Ans. Latitude, 32° 3′ S.; Longitude, 15° 25′ E.; Course, N. 52° 41′ W.; Distance, 187 miles.

SECTION IV.

MERCATOR'S SAILING.



Mercator's Sailing is a method of determining difference of longitude derived from the following principle.

In the figure, let AC be distance, AB difference of latitude, and BC departure. Now, if we take AL greater than AB in the ratio of radius to the cosine of the latitude of BC, and draw LD parallel to BC, it will represent the difference of longitude for the two points A and C; for

$$LD : BC :: AL : AB.$$

Therefore,

$$LD : BC :: R : \text{Cosine latitude.}$$

But from Proportion 1 we have

Difference of longitude : Departure : : R : Cosine latitude.

Therefore, if BC is departure, LD must be difference of longitude.

AL is called the meridional difference of latitude, to distinguish it from AB, the proper difference of latitude.

To find AL, the meridional difference of latitude, a table called a Table of Meridional Parts has been computed. If we take any small portion of the meridian AB, and divide it by the cosine of its latitude, or multiply it by the secant of its latitude, radius being unity, we shall get a corresponding portion of the increased meridian AL; and taking a nautical mile as the unit of the table, beginning at the equator, we shall get secant 1′, secant 2′, secant 3′, secant 4′, and so on, for the several minutes of the increased meridian. Adding these secants, we shall get the numbers called meridional parts for the latitudes 1′, 2′, 3′ 4′, and so on.

Thus, Secant 1′
Secant 1′+secant 2′
Secant 1′+secant 2′+secant 3′
Secant 1′+secant 2′+secant 3′+secant 4′, etc.,

give the numbers of the table in nautical miles. These numbers express the distance from the equator to the corresponding parallel of latitude, measured on the increased meridian. From this table we can take the meridional parts corresponding to each latitude, and by subtracting one number from the other when both latitudes are north or south, or by adding them when one is north and the other south, we shall obtain the meridional difference of latitude in numbers.

In the figure we have

1. $AB : AL :: BC : LD$; or

The proper difference of latitude is to the meridional difference of latitude as the departure is to the difference of longitude.

2. $R : \tan.BAC :: AL : LD$; or

Radius is to the tangent of the course as the meridional difference of latitude is to the difference of longitude.

Example 1.

A ship from latitude 32° 30′ N. and longitude 18° 20′ W., makes the following courses and distances:

1. N.W.bW. 150 miles.
2. W.N.W. 124 "
3. S.S.W. 41 "

Required the latitude and longitude arrived at, and the course and distance made good.

Take the latitudes and departures from the traverse table, and arrange them as in the tablet.

	COURSES.	DIST.	N.	S.	E.	W.
1	N.W.bW.	150	83.3			124.7
2	W.N.W.	124	47.5			114.6
3	S.S.W.	41		37.9		15.7
			130.8	37.9		255.0
			37.9			
			92.9 = diff. of latitude.			

Whence, 32° 30′ N., latitude given,
1° 33′ N., difference of latitude.
34° 3′ N., latitude arrived at.

To find the longitude, take from the table the meridional parts for 34° 3′, which will be 2175

Also the parts for 32° 30′, " " " 2064

Subtracting we get the meridional diff. of latitude = 111

Then from the tablet, we see that the departure is 255 miles, the proper difference of latitude is 93 miles nearly; and since proper difference of latitude is to meridional differe f latitude, as is departure to the difference of longitude, we have

$$\begin{array}{ll}
\text{Log. } 255 & = 2.406540 \\
\text{Log. } 111 & = \underline{2.045323} \\
 & 4.451863 \\
\text{Log. } 93 & = \underline{1.968483} \\
\text{Log. } 304.4 & = 2.483380
\end{array}$$

which gives the difference of longitude equal to 304 nearly, or 5° 4′ west.

$$\begin{array}{ll}
\text{And} & 18^\circ\ 20'\ \text{W., longitude given,} \\
 & \underline{5^\circ\ 4'\ \text{W.,}}\ \text{difference of longitude,} \\
 & 23^\circ\ 24'\ \text{W., longitude arrived at.}
\end{array}$$

To find the course, we have

$$\begin{array}{lll}
\text{Log. } 255 & = & 2.406540 \\
\text{Log. } 93 & = & \underline{1.968483} \\
\text{Tan. } 69^\circ\ 58' & & 10.438057
\end{array}$$

Therefore the course is N. 69° 58′ W.

To find the distance we have

$$\begin{array}{ll}
\text{Log. } 255 & = 2.406540 \\
\text{Sin. } 69^\circ\ 58' & = \underline{9.972894} \\
\text{Log. } 271.4\ \text{miles} & = 2.433646
\end{array}$$

In determining difference of longitude from the proportion,

Cos. lat. : 1 :: departure : diff. longitude,

when the ship sails on an oblique course, we assume that the departure is the same as would have been made on that parallel, which is the arithmetical mean of the latitude left and arrived at. This assumption is not true. The mean latitude found in that way does not always give the true difference of longitude.

From the proportion,

Diff. lat. : meridional diff. lat. : : departure : diff. lon.

we get

$$\frac{\text{diff. lat.}}{\text{meridional diff. lat.}} = \frac{\text{departure}}{\text{diff. lon.}} \qquad (1)$$

If we put ψ for the latitude of the parallel that will give the true longitude, we have

Cos. ψ : 1 : : departure : diff. lon.

Therefore $$\text{Cos. } \psi = \frac{\text{departure}}{\text{diff. lon.}} \qquad (2)$$

From 1 and 2, we get

$$\text{Cos. } \psi = \frac{\text{diff. lat.}}{\text{meridional diff. lat.}} \qquad (3)$$

Hence, we see that the proper difference of latitude divided by the meridional difference of latitude will give the cosine of the required latitude, and this compared with the arithmetical mean of the given latitudes will give the correction to be added to the mean latitude.

Example 2.

Suppose the given latitudes are 30° and 40°, the proper difference of latitude will be 10° or 600 miles; the meridional difference will be

Meridional parts for 40°	= 2622.7
Meridional parts for 30°	= 1888.4
Meridional difference of lat.	= 734.3

Therefore, $\cos. \psi = \frac{600}{734.3}$

And

Log. 600	= 2.778151
Log. 734.3	= 2.865874
Cos. 35° 12′	= 9.912277

The mean of 40° and 30° is 35°, hence the correction is 12′.

In this manner the following table may be computed:

Table of corrections in minutes to be added to the arithmetical mean to find the true mean latitude.

MEAN LAT.	DIFFERENCE OF LATITUDE. 2°	3°	4°	5°	6°	7°	8°	9°	10°	11°	12°	13°	14°	15°	16°	17°	18°	19°	20°
	′	′	′	′	′	′	′	′	′	′	′	′	′	′	′	′	′	′	′
15°	1	2	3	5	7	9	12	15	18	22	26	31	36	41	47	52	59	65	72
16°	1	2	3	4	6	9	11	14	18	21	25	30	34	39	44	50	56	62	69
17°	1	2	3	4	6	8	11	14	17	20	24	28	33	38	43	48	54	60	66
18°	1	1	3	4	6	8	10	13	16	20	23	27	32	36	41	46	52	58	64
19°	1	1	3	4	6	8	10	13	16	19	22	26	30	35	40	45	50	56	61
21°	1	1	2	4	5	7	10	12	15	18	22	25	29	34	38	43	48	54	60
23°	1	1	2	3	5	7	9	11	14	17	20	23	27	31	35	40	45	50	55
25°	1	1	2	3	5	7	9	11	13	16	19	23	26	30	34	39	43	48	53
30°	1	1	2	3	5	6	8	10	13	15	18	21	25	28	32	36	41	45	50
35°	0	1	2	3	4	6	8	10	12	15	18	21	24	28	32	36	40	45	49
40°	1	1	2	3	5	6	8	10	13	15	18	21	25	28	32	36	41	45	50
45°	1	1	2	3	5	6	8	11	13	16	19	22	26	30	34	38	43	48	53
50°	1	1	2	4	5	7	9	11	14	17	20	24	28	32	36	41	46	51	57
55°	1	1	2	4	6	8	10	13	16	19	22	26	31	35	40	45	51	57	63
60°	1	2	3	4	6	9	11	14	18	22	26	30	35	40	46	52	58	65	72
62°	1	2	3	5	7	9	12	15	19	23	27	32	37	43	49	55	62	70	77
64°	1	2	3	5	7	10	13	16	20	24	29	34	40	46	52	59	67	75	83
66°	1	2	3	5	8	11	14	18	22	26	32	37	43	50	57	64	72	81	90
68°	1	2	4	6	8	12	15	19	24	29	34	40	47	54	62	70	79	89	99
70°	1	2	4	6	9	13	16	21	26	32	38	44	52	60	68	78	88	98	110
71°	1	2	4	7	10	13	17	22	27	33	40	47	55	63	72	82	93	104	116
72°	1	3	5	7	10	14	18	23	29	35	42	49	58	67	76	87	98	111	124
73°	1	3	5	8	11	15	19	25	31	37	44	52	61	71	81	93	105	118	133

Examples.

1. A ship from Cape Finisterre, in lat. 42° 56′ N., and longitude 8° 16′ W., sailed S. W. ¼ W. till her difference of longitude is 134 miles; required the distance sailed, and the latitude in.

As radius	10.000000
: diff. lon., 134 miles,	2.127105
: : cot. course, 4¼ points,	9.957295
: mer. diff. lat., 121.5 miles,	2.084400

Lat. Cape Finisterre 42° 56′ N.;	Mer. parts	2858
	Mer. diff.	121
Lat. 41° 27′ N., corresponding to		2737 in table.

As cosine course	9.827085
: proper diff. lat., 89 miles,	1.949390
: : radius	10.000000
: dist. 132.5 miles,	2.122305

2. A ship from lat. 40° 41′ N., lon. 16° 37′ W., sails in the N. E. quarter till she arrives lat. 43° 57′ N., and has made 248 miles departure; required her course, distance, and longitude in.

Ans. Course N. 51° 41′ E.; Dist. 316 miles; Lon. in 11° W.

3. How far must a ship sail N. E. ¾ E. from lat. 44° 12′ N., lon. 23 W., to reach the parallel of 47° N.; and what from that point will be the bearing and distance of Ushant, which is in lat. 48° 28′ N., and lon. 5° 3′ W.?

Ans. She must sail 264.8 miles, and her course to Ushant will then be N. 80° 32′ E., and distance 535 miles.

4. A ship from the Cape of Good Hope steers E. ½ S. 446 miles; required her place, and her course and distance to Kerguelen's Land, in lat. 48° 41′ S., and lon. 69° E.

Ans. Lat. 35° 13′ S., lon. 27° 21′ E.; course to Kerguelen's Land, S. 66° 25′ E., and distance 2018 miles.

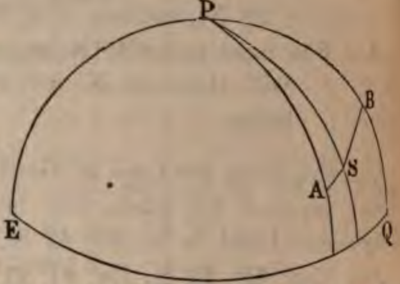
5. By observation, a ship was found to be in lat. 41° 50′ S., lon. 68° 14′ E. She then sailed N. E. 140 m., and E. ½ S. 76 m.; required her place, and her course and distance to the island of St. Paul, which is in lat. 38° 42′ S., and in lon. 77° 18′ E. *Ans.* Lat. 40° 18′ S., lon. 72° 6′ E.; course to St. Paul N. 68° 15′ E., and dist. 259 miles, nearly.

DIRECT METHOD OF COMPUTING MERIDIONAL PARTS.

This presentation of Mercator's Sailing is thought sufficient for all practical purposes. But it may be desirable to have a method of computing the Table of Meridional Parts directly for any degree of latitude without the preceding computations, especially if we wish to test the accuracy of any part of the tables. It may also be interesting to the mathematical student to examine the Theory of Mercator's Sailing in a manner differing entirely from the preceding.

It will be seen in what follows, that from the definition of the rhumb line, we can derive an equation that will give the difference of longitude when we have the latitude left, the latitude arrived at, and the course known, without a table of meridional parts.

Also, that from the hypothesis of Mercator's Sailing, we can derive an equation that gives directly the meridional parts for any latitude.



Let EQ be the equator, and P its pole; let ASB be the rhumb line or track of a ship, sailing from A to B; put C for the course of the ship, and let PS equal θ, the co-latitude of the ship, and ϕ equal the angle APS, which is the longitude of the ship reckoned from the meridian passing through A. Then we shall have,

$$\frac{d\phi \sin.\theta}{d\theta} = \tan. C, \qquad (1)$$

whence we get,

$$d\phi = \frac{\tan. C d\theta}{\sin.\theta}. \qquad (2)$$

Integrating, we get,

$$\phi = \tan. C \log. \tan.\tfrac{1}{2}\theta.$$

Taking the limits PA and PB, we get,

$$\phi = \tan. C\,(\log. \tan.\tfrac{1}{2}\theta' - \log. \tan.\tfrac{1}{2}\theta'') \qquad (3)$$

where θ' is the co-latitude of the place left, and θ'' is the co-latitude of the place arrived at. The logarithms in equation (3) are Naperian, and if we use the common tables, the right hand member of (3) must be divided by the modulus of our sys-

hich is .4342944819. And to obtain ϕ in nautical miles,
st multiply by $\frac{180^\circ \cdot 60'}{\pi}$, which will give,

$$\phi = 7915.7 \tan. C \, (\log. \tan. \tfrac{1}{2}\theta' - \log. \tan. \tfrac{1}{2}\theta'') \qquad (4)$$

ation (4) gives the difference of longitude when the lati-
f the places, and the course, are given.

Example.

ip in latitude 32° 38′ N. and longitude 16° 55′ W., sails
37′ W. until she reaches the parallel of 40° 2′ N. Re-
the longitude arrived at.
quation (4), we must put $C = 79^\circ\ 37'$, $\theta' = 57^\circ\ 22'$,
$= 49^\circ\ 58'$, and we shall get
915.7 tan. 79° 37′ (log. tan. 28° 41′—log. tan. 24° 59′).

Tan. 28° 41′ = 9.738071
Tan. 24° 59′ = 9.668343
.069728

,

Log. .069728 = $\bar{2}.843407$
Tan. 79° 37′ = 10.736995
Log. 7915.7 = 3.898489
Log. 3012 = 3.478891

efore, $\phi = 3012$ miles, or 50° 12′. Hence the longi-
rived at is 67° 7′ W.
ompute a table of meridional parts, we may put θ for
itude of any parallel, and ψ for the distance of the same
l from the equator; then from Mercator's theory, we
ave,

$$d\psi = \frac{d\theta}{\cos.\theta} \qquad (1)$$

integral of this equation gives

$$\psi = \log. \tan. (45^\circ + \tfrac{1}{2}\theta). \qquad (2)$$

common logarithms and nautical miles as the unit, we must multiply the right hand number of (2) by 7915. whence we get,

$$\psi = 7915.7 \text{ log. tan.}\left(45^\circ + \frac{\theta}{2}\right) \qquad (3)$$

Example 1.

Required the meridional parts for 20° of latitude.
Here $\theta = 20^\circ$, whence,

$$\psi = 7915.7 \text{ log. tan. } 55^\circ.$$

Tan. 55° = 10.154773; and

$$\begin{array}{lcr} \text{Log. } .154773 & = & -1.189696 \\ \text{Log. } 7915.7 & = & 3.898489 \\ \hline \text{Log. } 1225.1 & = & 3.088185 \end{array}$$

Therefore $\psi = 1225.1$ miles, which is the number found the table of meridional parts for 20°.

Example 2.

Required the meridional parts for latitude 78° 52′.
Here $\theta = 78^\circ\ 52'$, and equation (3) becomes

$$\psi = 7915.7 \text{ log. tan. } 84^\circ\ 26'.$$

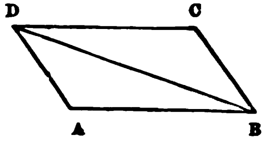
Tan. 84° 26′ = 11.011158; and we have

$$\begin{array}{lcr} \text{Log. } 1.011158 & = & .004819 \\ \text{Log. } 7915.7 & = & 3.898489 \\ \hline \text{Log. } 8004 & = & 3.903308 \end{array}$$

Whence $\psi = 8004$ miles, the meridional parts for the gi latitude, 78° 52′.

SECTION V.

SAILING IN CURRENTS.



ship at B, sailing in the direction BA, were in a cur- hich would carry her from B to C, in the same time still water she would sail from 1, then, by the joint action of rrent and the wind, she would same time describe the diagonal ' the parallelogram $ABCD$. For her being carried by rent in a direction parallel to BC, would neither alter rce of the wind, nor the position of the ship, nor the ith respect to it; the wind would therefore continue to the ship in a direction parallel to AB, in the same man- if the current did not exist. Hence, as she would be to the line CD by the independent action of the cur- n the same time that she reached the line AD by the ndent action of the wind on her sails, she would be at D, the point of intersection of the lines AD and CD, moved along the diagonal BD.

lems relating to the oblique action of a current upon a ay be resolved by the solution of a plane triangle, as in the preceding figure, where, if BA represent the dis- a ship would sail in still water, and AD the drift of rrent in the same time, BD will be the actual dis- ailed, and ABD the change in the course produced by rrent.

EXAMPLES.

f a ship sail W. 28 miles, in a current which in the same arries her N. N. W. 8 miles, required her true course stance.

Conceive the current to be one course and distance, and with the other course find the course and distance made good.

Thus, by the traverse table:

COURSE.	DIST.	DIFF. LATITUDE.		DEPARTURE.	
		N.	S.	E.	W.
W.	28				28
N.N.W.	8				
		7.39			3.06
		7.39			31.06

$7.39 : R :: 31.06 : \tan.\ 76^\circ\ 37'$, the course,

$\text{Sin. } 76^\circ\ 37' : R :: 31.06 : 31.93$, the distance.

2. If a ship sails E. 7 miles an hour by the log, in a current setting E. N. E. 2.5 miles per hour, required her true course and hourly rate of sailing.

Ans. Course, N. 84° 8′ E.; rate, 9.358 per hour.

3. A ship has made by the reckoning N. $\frac{1}{2}$ W. 20 miles, but by observation it is found that, owing to a current, she has actually gone N. N. E. 28 miles. Required the setting and drift of the current in the time which the ship has been running. *Ans.* Setting, N. 64° 48′ E.; drift, 14.1 miles.

4. A ship's course to her port is W. N. W., and she is running by the log 8 miles an hour; but meeting with a current setting W. $\frac{1}{2}$ S. 4 miles an hour, what course must she steer in the current that her true course may be W. N. W.?

Ans. Course, N. 53° 52′ 2″ W.

5. In a tide running N. W. b W. 3 miles an hour, I wished to weather a point of land which bore N. E. 14 miles. What course must I steer so as to clear the point, the ship sailing 7 miles an hour by the log, and what time shall I be in reaching the point?

Ans. Course, N. 69° 51′ E.; time, 2 hours 25 minutes.

6. From a ship in a current, steering W. S. W. 6 miles an ur by the log, a rock was seen at 6 in the evening, bearing W. ½ S. 20 miles. The ship was lost on the rock at 11 P. M. equired the setting and drift of the current.

Ans. Setting, S. 75° 10′ E.; drift, 3.11 miles per hour.

PARALLAX.

To obtain the true altitude of a body from its apparent alti-de, as given by an instrument, certain corrections are neces-ry.

These corrections are for *semi-diameter*, *dip*, *refraction* and *arallax*. The correction for semi-diameter is obvious.

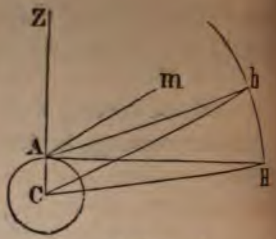
At sea, the visible horizon (from which all observed alti-des are taken) is where the sea and sky apparently meet; d when the eye of the observer is above the water, this visi-e horizon is below the *sensible* horizon, and the amount of e depression is called the *dip of the horizon.* Its correction always subtractive, and its amount is to be found in Table V.

Refraction is to be found in Table VII. It is always sub-active; for the reason, see some treatise on natural phil-ophy.

Parallax is always additive. Conceive two lines drawn to a avenly body, one from an observer at the circumference of e earth, and the other from the center of the earth. The in-ination of these two lines is parallax; and when the body is the horizon its parallax is greatest, and it is then called rizontal parallax.

Parallax always tends to depress the object; but the parallax any celestial object, except that of the moon, is so small, at we shall pay attention to lunar parallax only. This is important to navigation that we shall give it a full explana-on.

The moon's horizontal parallax is given in the Nautical Al-anac for every noon and midnight of Greenwich time, and om the horizontal parallax we must deduce the parallax



corresponding to any other altitude.

Let AC be the radius of the earth, A the position of an observer, Z his zenith, and suppose H to be the moon in the horizon; then the angle AHC is the moon's horizontal parallax, and the angle AhC is the parallax corresponding to the apparent altitude hAH. Draw Am parallel to Ch; then mAH will be the *true altitude.*

From this figure we draw the following definition for horizontal parallax.

The horizontal parallax of any body is the angle under which the semi-diameter of the earth would appear as seen from that body. Of course, then, when the body is at a great distance, its horizontal parallax must be small; hence the sun and the remote planets have very little parallax, and the fixed stars none at all.

Let CH and Ch be each represented by R. Put $p =$ the horizontal parallax, and $x =$ the parallax in altitude, or the angle mAh or AhC.

Now in the triangle ACH, right-angled at A, we have,

$$1 : \sin.p :: R : AC.$$

In the triangle ACh, we have,

$$\sin.\ CAh : \sin.x :: R : AC.$$

By comparing these two proportions, we perceive that

$$1 : \sin.p :: \sin.CAh : \sin.x.$$

Whence, $$\sin.x = \sin.p \sin.CAh.$$

But $\sin.CAh = \cos.hAH$, for the sine of any arc greater than 90° is equal to the cosine of the excess over 90°; hence,

$$\sin.x = \sin.p \cos.hAH.$$

The lunar horizontal parallax is rarely over a degree, commonly less, and the sine of a degree does not materially differ rom the arc itself; hence, the preceding equation becomes, without any essential error the following:

$$x = p \text{ cos. altitude.}$$

Or, in words, *the parallax in altitude is equal to the horizontal parallax multiplied by the cosine of the apparent altitude* (radius being unity).

EXAMPLES.

1. The apparent altitude of the moon's center, after being corrected for dip and refraction, was 31° 25′; and its horizontal parallax at that time, taken from a nautical almanac, was 57′ 37″; what was the correction for parallax, and what was the true altitude as seen from the center of the earth?

$$p = 57' \, 37'' = 3457''; \quad \text{log. } 3457'' = 3.538699$$
$$\text{cos. } 31^\circ \, 25' = \underline{9.931152}$$
$$\text{Log. } 2950 = 49' \, 10'' = x = 3.469851$$

Ans. Cor. for parallax, 49′ 10″; true altitude, 32° 14′ 10″.

2. The apparent altitude of the moon's center on a certain ccasion was 42° 17′, and its horizontal parallax at the same ime was 58′ 12″; what was the parallax in altitude, and what was the moon's true altitude?

Ans. Parallax in altitude, 43′ 4″; true altitude, 43° 0′ 4″.

SECTION VI.

LATITUDE.

1. *To find the latitude of a place by the sun at noon.*

The latitude of a place may be determined from the meriian altitude of the sun.

The altitude taken with a sextant must be corrected for semi-diameter, parallax, dip, and refraction. The correction for semi-diameter is found in the almanac, and it must be subtracted or added, according as the upper or lower limb of the sun was observed.

The correction for parallax is found by multiplying the sun's parallax by the cosine of the observed altitude; it must always be added.

The corrections for dip and refraction are found in tables, and must be subtracted to give the true altitude.

Then from the true altitude subtract the sun's declination found in the almanac for that time, and the remainder will be the co-latitude. Or subtract the true altitude from 90°, and get the zenith distance.

Then if the sun and observer are on the same side of the equator, to the zenith distance add the sun's declination to obtain the latitude; if the sun and observer are on different sides of the equator, from the zenith distance subtract the sun's declination to obtain the latitude.

EXAMPLES.

1. On a certain day, the meridian* altitude of the sun's lower limb was observed to be 31° 44′, bearing south. At that time its declination was 7° 25′ 8″ south, semi-diameter 16′ 9″, index error + 2′ 12″, height of the eye 17 feet. What was the latitude? *Ans.* 50° 38′ north.

---

* To obtain the meridian altitude of the sun, the observer commences observations before noon, while the sun is still rising, driving the index forward as fast as the image appears to rise; and there will come a time, a few minutes in succession, in which the image appears to rest on the horizon, neither rising nor falling; but at length the image will fall; then the observer knows that noon has passed, and the greatest apparent altitude will be shown by reading the index.

Observed altitude = 31° 44′ 0″
Semi-diameter . +16′ 9″
32° 0′ 9″
Index error = + 2′ 12″
32° 2′ 21″
Dip = − 4′ 4″
31° 58′ 17″
Refraction = − 1′ 32″
31° 56′ 45″
Parallax + 7″
True altitude = 31° 56′ 52″
Zenith distance = 58° 3′ 8″
Declination = 7° 25′ 8″
Latitude north = 50° 38′ 0″

2. The meridian altitude of the sun's upper limb was 40° 42′ bearing north; the declination was 23° 22′ south; semi-diameter was 16′ 17″; height of the observer was 16 feet. Required the latitude.

Corrections:
Sun's semi-diameter = −16′ 17″
Dip = − 8′ 56″
Refraction = − 1′ 6″
Parallax in altitude = + 7″
−21′ 10″
Observed altitude of limb = 40° 42′ 0″
True-altitude of sun's center = 40° 20′ 50″
Zenith distance = 49° 39′ 10″
Declination = 23° 22′ 0′
Latitude south = 73° 1′ 10″

In this example the semi-diameter is subtracted because the upper limb was observed; the dip and refraction are always subtracted, and parallax is added.

3. The meridian altitude of the sun's lower limb was 60° 25′

bearing south, semi-diameter 16′ 8″, height of the observer 16 feet, and the sun's declination 9° 22′ north. What was the latitude?

Corrections:

Sun's semi-diameter = +16′ 8″
Dip = − 3′ 56″
Refraction = − 0′ 33″
Parallax in altitude = + 4″
+11′ 43″
Observed altitude = 60° 25′ 0″
True altitude of sun's center = 60° 36′ 43″
Zenith distance = 29° 23′ 17″
Declination = 9° 22′ 0″
Latitude north = 38° 45′ 17″

Find the latitude from each of the following meridian observations:

	OBJECT.	ALT. OB.	DIREC.	S. D.	HEIGHT.	DECLINATION.	LATITUDE.
1	Sun *L.L.*	45° 27′	South	16′ 15″	20 feet	17° 19′ 31″ S.	27° 2′ 51″ N.
2	Sun *L.L.*	81° 43′	South	15′ 47″	14 "	22° 13′ 7″ N.	30° 18′ 10″ N.
3	Sun *L.L.*	87° 29′	South	16′ 17″	16 "	22° 9′ S.	19° 50′ 12″ S.
4	Sun *L.L.*	15° 46′	South	16′ 0″	16 "	4° 43′ S.	69 23′ 16″ N.

Navigators usually add 12′ to the observed altitude of the sun's lower limb as a correction for the sun's semi-diameter, parallax, and dip; then subtract the refraction due to the altitude as given in the tables of refraction. The remainder will give the true altitude nearly, when the observation is taken upon the deck of a common sized vessel.

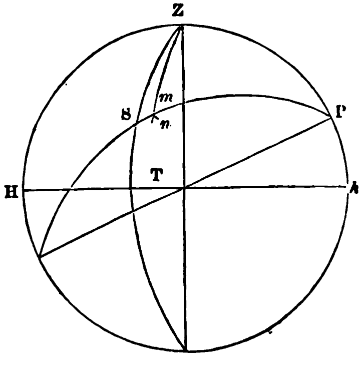
The following table gives the correction for the sun's semi-diameter, dip, and refraction, when the sun's lower limb is observed.

CORRECTION TO BE ADDED TO THE OBSERVED ALTITUDE OF THE SUN'S LOWER LIMB TO FIND THE TRUE ALTITUDE.

HEIGHT OF THE EYE ABOVE THE SEA IN FEET.

6	8	10	12	14	16	18	20	22	24	26	28	30	32	34
′	′	′	′	′	′	′	′	′	′	′	′	′	′	′
3.8	3.5	3.1	2.8	2.5	2.3	2.1	1.8	1.6	1.4	1.2	1.0	0.8	0.6	0.5
5.3	4.9	4.6	4.3	4.0	3.7	3.5	3.3	3.0	2.8	2.6	2.4	2.2	2.1	1.9
6.4	6.0	5.7	5.4	5.1	4.8	4.6	4.4	4.1	3.9	3.7	3.5	3.3	3.2	3.0
7.2	6.8	6.5	6.2	5.9	5.7	5.4	5.3	5.0	4.8	4.6	4.4	4.2	4.0	3.9
7.9	7.5	7.2	6.9	6.6	6.4	6.1	5.9	5.7	5.5	5.3	5.1	4.9	4.7	4.5
8.5	8.1	7.8	7.5	7.2	6.9	6.7	6.5	6.2	6.0	5.8	5.6	5.4	5.3	5.1
8.9	8.6	8.2	7.9	7.6	7.4	7.2	6.9	6.7	6.5	6.3	6.1	5.9	5.7	5.6
9.3	9.0	8.7	8.3	8.0	7.8	7.6	7.3	7.1	6.9	6.7	6.5	6.3	6.2	6.0
9.9	9.6	9.2	8.9	8.7	8.4	8.2	7.9	7.7	7.5	7.3	7.1	6.9	6.8	6.6
10.4	10.1	9.7	9.4	9.1	8.9	8.7	8.4	8.2	8.0	7.8	7.0	7.4	7.2	7.1
10.8	10.4	10.1	9.8	9.5	9.3	9.0	8.8	8.6	8.4	8.2	8.0	7.8	7.6	7.5
11.1	10.7	10.4	10.1	9.8	9.6	9.3	9.1	8.9	8.7	8.5	8.2	8.1	7.9	7.7
11.4	11.0	10.7	10.4	10.1	9.8	9.6	9.4	9.1	8.9	8.7	8.5	8.3	8.2	8.0
11.7	11.4	11.0	10.7	10.5	10.2	10.0	9.7	9.5	9.3	9.1	8.9	8.7	8.6	8.4
12.0	11.7	11.3	11.0	10.8	10.5	10.3	10.0	9.8	9.6	9.4	9.2	9.0	8.9	8.7
12.3	11.9	11.6	11.3	11.0	10.7	10.6	10.3	10.1	9.9	9.7	9.4	9.2	9.2	9.0
12.5	12.2	11.8	11.5	11.3	11.0	10.8	10.5	10.3	10.1	9.9	9.7	9.5	9.4	9.2
12.7	12.4	12.0	11.7	11.5	11.2	11.0	10.7	10.5	10.2	10.1	9.8	9.7	9.6	9.4
12.8	12.5	12.2	11.9	11.6	11.3	11.1	10.9	10.6	10.4	10.3	10.0	9.8	9.7	9.5
13.0	12.6	12.3	12.0	11.7	11.5	11.2	11.0	10.7	10.5	10.3	10.1	9.9	9.8	9.6
13.1	12.7	12.4	12.1	11.8	11.6	11.3	11.1	10.9	10.6	10.4	10.2	10.1	9.9	9.7
13.2	12.8	12.5	12.2	11.9	11.7	11.4	11.2	11.0	10.7	10.5	10.3	10.1	10.0	9.8
13.3	12.9	12.6	12.3	12.0	11.8	11.5	11.3	11.0	10.8	10.6	10.4	10.2	10.1	9.9
13.4	13.1	12.7	12.4	12.1	11.9	11.7	11.4	11.2	11.0	10.8	10.6	10.4	10.2	10.1
13.6	13.2	12.9	12.6	12.3	12.0	11.8	11.6	11.3	11.1	10.9	10.7	10.5	10.4	10.2

thly Correction	Jan. +0′.3	Feb. +0′.2	Mar. +0′.1	April. 0′.0	May. —0′.1	June. —0′.2
for s Semi-diameter.	July. —0′.3	Aug. —0′.2	Sept. —0′.1	Oct. +0′.1	Nov. +0′.2	Dec. +0′.3



To find the latitude by un at any given time.

ke the altitude of the note the time, correct bserved altitude for dip, diameter, and refrac- also, take the declina- rom the Almanac. Then e triangle *ZPS*, *ZS* will ıe complement of the altitude, PS the complement of declination, and the time at which the observation was taken subtracted from 12^h, if the observation was taken before noon, will measure the angle at P. Therefore, we shall have ZS and PS, and the angle P, to find PZ, which is the co-latitude. If we put θ for the arc from P to where the perpendicular falls from S, we shall have $\cos.P = \cot.PS \tan.\theta$; from which we get θ. And we also have,

$$\text{Cos.}PS : \cos.ZS :: \cos.\theta : \cos.\theta',$$

where θ' is the arc from Z to where the perpendicular meets PZ produced. The difference of these arcs gives PZ, the co-latitude.

Example 1.

At 8^m afternoon, the true altitude of the sun's center was found to be 70° 58′, the declination of the sun being 21° N. Required the latitude.

In this example,

$$ZS = 19° \; 2'$$
$$PS = 69° \; 0'$$
$$P = 2° \; 0'$$

If we form a right-angled triangle, with PS as hypotenuse and θ for its base, we shall have $\cos.\ 2° = \cot.\ 69° \ \tan.\theta$. Therefore, $\tan.\theta = \dfrac{\cos.\ 2°}{\cot.\ 69°}$; hence $\theta = 68°\ 59'\ 18''$.

Again, we have $\cos.\ 69° : \cos.\ 19°\ 2' :: \cos.\theta : \cos.\theta'$, where θ' is the base of the triangle whose hypotenuse is 19° 2′. Therefore, $\cos.\theta' = \dfrac{\cos.\ 19°\ 2' \cdot \cos.\ 68°\ 59'\ 18''}{\cos.69°}$;

hence $\theta' = 18°\ 56'\ 43''$.

And,

$$\begin{array}{r} 68°\ 59'\ 18'' \\ 18°\ 56'\ 43'' \\ \hline PZ = 50°\ \ 2'\ 35'' \end{array}$$

Hence the latitude is 39° 57′ 25″

Example 2.

At 32^m before noon, the sun's true altitude was found to be 19° 41′ bearing south, the sun's declination being 20° south. What was the latitude of the place of observation?

32 minutes converted to arc gives 8° for the angle at *P*; then we shall have,

$$\begin{aligned} P &= 8^\circ \\ ZS &= 70^\circ\ 19' \\ PS &= \frac{\pi}{2}+20^\circ \end{aligned}$$

Let θ = the arc which is the base of the triangle whose hypotenuse is *PS*, and let θ' be the base of the triangle whose hypotenuse is *ZS*; then we shall have,

$$\text{Cos. } 8^\circ = \text{cot.}\left(\frac{\pi}{2}+20^\circ\right)\text{tan.}\theta.$$

From which we get,

$$\theta = 110^\circ\ 10'\ 49''.$$

Again, we have

$$\text{Cos. }\left(\frac{\pi}{2}+20^\circ\right) : \text{cos. } 70^\circ\ 19' : : \text{cos. } 110^\circ\ 10'\ 49'' : \text{cos.}\theta'$$

From which we get,

$$\theta' = 70^\circ\ 8'\ 21''$$

But $\theta - \theta' = PZ =$ co-latitude.

$$\begin{array}{lr} \text{Therefore,} & 110^\circ\ 10'\ 49'' \\ & \underline{70^\circ\ \ \ 8'\ 21''} \\ \text{Co-latitude} = & 40^\circ\ \ \ 2'\ 28'' \\ \text{Latitude} = & 49^\circ\ 57'\ 32'' \end{array}$$

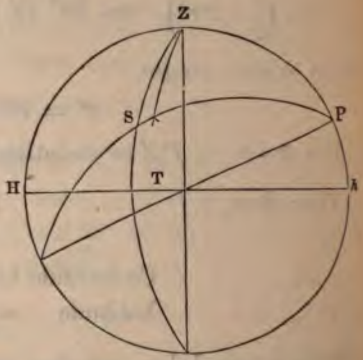
This method does not give good results when the sun is far from the meridian at the time the altitude is taken. A small error in the angle at *P* occasions a large error in the co-latitude *PZ*.

SECTION VII.

LONGITUDE.

Longitude, from celestial observations, is measured by time. A place 15° west of another will have noon one hour of absolute time later; if 30° west, noon will be two hours later, &c., &c.; 15° corresponding always to an hour in time. Therefore, if we have any way of determining the times at two places, corresponding to the same absolute instant, the difference of such times will correspond to the difference of longitude between the two places, at the rate of 15° to an hour, or 4 minutes to a degree.

Hence if we have a chronometer set to Greenwich mean time, and we know the rate of the chronometer, we can determine the longitude of any place whose local time can be ascertained. The difference between the Greenwich and local times is the longitude of the place, which will be east or west, according as the local time is earlier or later than the Greenwich time, as shown by the chronometer.



Having the latitude of a place, the local time can be found from an observed altitude of the sun; the declination of the sun being taken from the almanac.

In the diagram, let Z be the zenith of the place, P the north pole, S the place of the sun when its altitude was observed. PZ will be co-latitude, PS co-declination, and ZS will be co-altitude. In the triangle PZS, we have all the sides to find the angle at P, which is the angular distance of the sun from the meridian of the place where the altitude was taken. Hence, if we compute the angle ZPS, and convert it to time by allowing one hour for fifteen degrees, we shall have the time at which the altitude was taken.

Let $S =$ the half sum of the sides of the triangle PZS, then from Spherical Trigonometry, we have

$$\text{Cos.}\ \tfrac{1}{2}P = \left(\frac{\sin. S \sin.(S-ZS)}{\sin. PZ \sin. PS}\right)^{\frac{1}{2}}$$

Example 1.

In latitude 39° 6′ 20″ north, the sun's declination being 12° 3′ 10″ north, the true altitude of the sun's center was found to be 30° 10′ 40″ rising. What was the time?

In this example

$PZ = 50° 53' 40''$
$PS = 77° 56' 50''$
$ZS = 59° 49' 20''$

Hence, $S = 94° 19' 55''$
And $S-ZS = 34° 30' 35''$

$$\begin{array}{lll}
\text{Therefore,} & \text{Sin.}\ S & = 9.998758 \\
 & \text{Sin.}(S-ZS) = & \underline{\ 9.753235} \\
 & & 19.751993 \\
 & \text{Sin.}\ PZ & = 9.889853 \\
 & \text{Sin.}\ PS & = \underline{\ 9.990319} \\
 & & 19.880172 \\
 & & 2\overline{)19.871821} \\
\text{Cos.}\ \tfrac{1}{2}P = \text{cos. } 30° 22' & = & 9.935910 \\
\text{Therefore } \tfrac{1}{2}P = & 30° 22' & \\
\text{And } P = & 60° 44' &
\end{array}$$

This, converted to time, gives $4^h\ 2^m\ 56^s$, or the altitude was taken at $7^h\ 57^m\ 4^s$ in the morning. This is local apparent time. The equation of time found in the almanac for the day on which the observation was taken will correct this for local mean time; and the difference between local, and Greenwich, mean time, will be the longitude.

Example 2.

In latitude 43° 30′ north at, $7^h\ 43^m$ in the morning by the watch, the altitude of the sun's lower limb was taken 32° 4′, the height of the observer being 16 feet, the sun's declination being 19° 50′ 47″ north, semi-diameter 15′ 49″, the equation of time $-3^m\ 51^s$, and the chronometer indicating $9^h\ 0^m\ 46^s$ Greenwich mean time. What was the longitude?

Observed altitude lower limb	=	32° 4′ 0″
Semi-diameter	=	+15′ 49″
Dip	=	− 3′ 56″
Refraction	=	− 1′ 30″
True altitude of center	=	32° 14′ 23″

In this example we have

$PZ = 46° 30′ 0″$
$PS = 70° 9′ 13″$
$ZS = 57° 45′ 37″$
Hence, $S = 87° 12′ 25″$
And $S-ZS = 29° 26′ 48″$
Therefore,

$$
\begin{aligned}
\text{Sin.}S &= +9.999483\\
\text{Sin.}(S-ZS) &= +9.691623\\
\text{Sin.}PZ &= -9.860562\\
\text{Sin.}PS &= -9.973408\\
& \quad 2)\overline{19.857136}\\
\text{Cos. } 31° 58′ 8″ &= \quad 9.928568 = \cos \tfrac{1}{2}P
\end{aligned}
$$

Therefore $\frac{1}{2}P = 31° 58′ 8″$
And $P = 63° 56′ 16″$

This value of P converted to time gives $4^h\ 15^m\ 45^s$, which is the time before noon when the altitude was taken, which gives $7^h\ 44^m\ 15^s$ for the local apparent time; but since the equation of time is $-3^m\ 51^s$, we have

$$\begin{array}{rr} & 7^h\ 44^m\ 15^s \\ & -3^m\ 51^s \\ \hline & 7^h\ 40^m\ 24^s = \text{local mean time.} \\ \text{Watch time} = & \underline{7^h\ 43^m\ \ 0^s} \\ & 2^m\ 36^s\ \text{watch too fast.} \end{array}$$

$$\begin{array}{lr} \text{Greenwich mean time by chronometer} = & 9^h\ \ 0^m\ 46^s \\ \text{Time by observation} & 7^h\ 40^m\ 24^s \\ \hline & 1^h\ 20^m\ 22^s \end{array}$$

which is the longitude of the place of observation; and it is west, the local time being behind Greenwich time.

Example 3.

In latitude 54° 12′ north, at $5^h\ 33^m$ afternoon by the watch, the true altitude of the sun's center was found to be 16° 26′ 52″. The sun's declination was 15° 26′ 50″ north, and the equation of time was $+5^m$; the chronometer indicated $7^h\ 12^m\ 45^s$, Greenwich mean time. What was the error of the watch, and what was the longitude of the place of observation?

In this example, we have,

$$\begin{array}{lll} & PZ & = 35^\circ\ 48'\ \ 0'' \\ & PS & = 74^\circ\ 33'\ 10'' \\ & ZS & = 73^\circ\ 33'\ \ 8'' \\ \text{Hence we find} & S & = 91^\circ\ 57'\ \ 9'' \\ \text{And} & S-ZS & = 18^\circ\ 24'\ \ 1'' \end{array}$$

$$\begin{array}{lr} \text{Sin.}S & = +\ 9.999747 \\ \text{Sin.}(S-ZS) & = +\ 9.499210 \\ \text{Sin.}PZ & = -\ 9.767124 \\ \text{Sin.}PS & = -\ 9.984021 \\ \hline & 2)19.747812 \\ \hline \text{Cos. } 41^\circ\ 34'\ 55'' = & 9.873906 \end{array}$$

Hence, $\frac{1}{2}P = 41^\circ\ 34'\ 55''$
And $P = 83^\circ\ 9'\ 50''$

This gives in time $5^h\ 32^m\ 39^s$
Applying equation of time, $+5$
$5^h\ 37^m\ 39^s$

which is the local mean time.

Greenwich mean time by chronometer $= 7^h\ 12^m\ 45^s$
Local time by observation $= 5^h\ 37^m\ 39^s$
$1^h\ 35^m\ 6^s$

which is the longitude required.

Local time by observation $= 5^h\ 37^m\ 39^s$
Watch time $= 5^h\ 33^m\ 0^s$
Error of watch $= 4^m\ 39^s$

Example 4.

In latitude 21° 36′ north, the true altitude of the sun's
ter was found to be 30° 24′ 40″, the sun's declination be
21° 41′ 40″ south, equation of time $+ 8^m\ 31^s$, chronom
indicating $6^h\ 0^m\ 21^s$ P. M. Greenwich mean time. Requ
the longitude of the place of observation.

In this example, we have

$PZ = 68^\circ\ 24'\ 0''$
$PS = 111^\circ\ 41'\ 40''$
$ZS = 59^\circ\ 35'\ 20''$
Therefore, $S = 119^\circ\ 50'\ 30''$
And $S - ZS = 60^\circ\ 15'\ 10''$

$\text{Sin.}S = +\ 9.938221$
$\text{Sin.}(S - ZS) = +\ 9.938631$
$\text{Sin.}PZ = -\ 9.968379$
$\text{Sin.}PS = -\ 9.968094$
2) 19.940379
$\text{Cos. } 20^\circ\ 59'\ 14'' = 9.970189$

fore, $\frac{1}{2}P = 20^\circ\ 59'\ 14''$

$P = 41^\circ\ 58'\ 28''$

gives, $2^h\ 47^m\ 54^s$ local apparent time.

ation of time, $8^m\ 31^s$

$2^h\ 56^m\ 25^s$ local mean time

er.wich mean time $= 6^h\ 0^m\ 21^s$

$3^h\ 3^m\ 56^s$ longitude west.

Example 5.

tude 0° 41′ south, the true altitude of the sun's center
d to be 32° 31′ 52″ rising, the declination of the sun
″ south, the equation of time $+9^m\ 53^s$; the chrono-
dicated $11^h\ 27^m\ 41^s$ A. M., Greenwich mean time.
as the longitude by chronometer?

we have,

$$\begin{aligned} PZ &= 89^\circ\ 19'\ 0'' \\ PS &= 68^\circ\ 57'\ 24'' \\ ZS &= 57^\circ\ 28'\ 8'' \end{aligned}$$

,

$$\begin{aligned} S &= 107^\circ\ 52'\ 16'' \\ S-ZS &= 50^\circ\ 24'\ 8'' \end{aligned}$$

$$\begin{aligned} \text{Sin.}S &= +\ 9.978522 \\ \text{Sin.}(S-ZS) &= +\ 9.886794 \\ \text{Sin.}PZ &= -\ 9.999969 \\ \text{Sin.}PS &= -\ 9.970025 \\ & \quad 2)\ 19.895322 \\ \text{Cos. } 27^\circ\ 34'\ 4'' &= \quad 9.947661 \end{aligned}$$

fore, $\frac{1}{2}P = 27^\circ\ 34'\ 4''$

$P = 55^\circ\ 8'\ 8''$

This changed to time gives	$3^h\ 40^m\ 33^s$
The time of the day will be	$8^h\ 19^m\ 27^s$ apparent time.
Equation of time,	$+9^m\ 53^s$
	$8^h\ 29^m\ 20^s$ local mean time.
Greenwich mean time,	$11^h\ 27^m\ 41^s$
	$2^h\ 58^m\ 21^s$ = lon. required.

SECTION VIII.

LUNAR OBSERVATIONS.

A good and well-tried chronometer is a valuable and reliable instrument for finding the longitude at sea, during short runs; but still it is but an instrument, and is not one of the reliable works of nature. Near the end of a long voyage the best of chronometers very frequently give false longitude; and in such cases good navigators always resort to lunar observations, which, from the hands of a good observer, can be relied upon to within 10 or 12 minutes of a degree. Indeed, they usually come within 5 or 6 miles, and sometimes even more exact; but that is accidental and unfrequent.

To comprehend the theory of lunars, we must call to mind the fact that the moon moves through the heavens, apparently among the stars, at the rate of more than 13° in a day, and any angular distance it may have from the sun or any star corresponds to some moment of Greenwich time.

About three days before and after the change of the moon, she is too near the sun to be visible; but at all other times her distance from the sun, some of the larger planets, and certain bright fixed stars, called lunar stars,* which lie near her path, are computed and put down in the nautical almanac, for every third hour of mean Greenwich time, commencing at noon.

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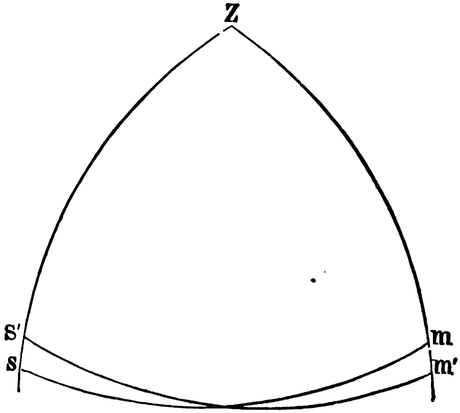
* There are nine lunar stars, Arietis, Aldebaran, Pollux, Regulus, Spica, Antares, Aquilæ, Fomalhaut, and Pegasi.

For any particular day, the distances are given to such objects only, east and west of her, as will be convenient to measure with the common instruments.

The distances put down in the nautical almanac are such as would be seen if viewed from the center of the earth; but observers are always on the surface of the earth, and the distances thence observed must always be reduced to equivalent distances seen from the center by the application of spherical trigonometry. This reduction is called *working a lunar.*

The moon is never seen by an observer in its *true place*, unless the observer is in a line between the center of the earth and the moon, that is, unless the moon is in the zenith of the observer; in all other positions the moon is depressed by parallax, and appears nearer to those stars that are below her, and further from those stars that are above her, than she would appear from the center of the earth. Therefore the apparent altitudes of the two objects must be taken at the same time that their distance asunder is measured. The altitudes must be corrected for parallax and refraction, thus obtaining the true altitudes.

FIRST METHOD OF WORKING A LUNAR.



Let Z be the zenith of an observer, S' the apparent place of a star, and S its true place. Also, let m' be the apparent place of the moon, and m its true place, as seen from the center of the earth. Here $ZS'm'$ and ZSm are two spherical triangles.

The apparent altitudes subtracted from 90° degrees give ZS' and Zm', and $S'm'$ is the apparent distance; with these three sides the angle Z can be found. Correcting the altitudes and subtracting them from 90° will give the sides ZS and Zm; these two sides, and their included angle at Z, will give the side Sm which is the true distance.

The definite true distance must have a definite Greenwich time, which can readily be found; and this, compared with the local time deduced from an altitude of the sun, will give the longitude.

Let S' = the apparent altitude of a star,
and S = the true altitude.
Let m' = the apparent altitude of the moon,
and m = the true altitude.
Also let d = the apparent distance of the moon from the star,
and x = the true distance.

Then from the fundamental equations of Spherical Trigonometry, we have the following,

$$\text{Cos. } Z = \frac{\cos.d - \sin.S' \sin.m'}{\cos.S' \cos.m'}$$

Also $$\text{Cos. } Z = \frac{\cos.x - \sin.S \sin.m}{\cos.S \cos.m}$$

Whence, $$\frac{\text{Cos.}d - \sin.S' \sin.m'}{\cos.S' \cos.m'} = \frac{\cos.x - \sin.S \sin.m}{\cos.S \cos.m}$$

By adding unity to each member, we have

$$1 + \frac{\cos.d - \sin.S' \sin.m'}{\cos.S' \cos.m'} = 1 + \frac{\cos.x - \sin.S \sin.m}{\cos.S \cos.m}$$

$$\frac{(\text{Cos.}S' \cos.m' - \sin.S' \sin.m') + \cos.d}{\cos.S' \cos.m'} =$$
$$\frac{(\cos.S \cos.m - \sin.S \sin.m) + \cos.x}{\cos.S \cos.m}$$

By observing equation 9, Plane Trigonometry, we perceive hat the preceding equation reduces to

$$\frac{\text{Cos.}(S'+m')+\cos.d}{\cos.S'\cos.m'}=\frac{\cos.(S+m)+\cos.x}{\cos.S\cos.m}.$$

Whence

$$\text{os.}x=\left(\cos.(S'+m')+\cos.d\right)\frac{\cos.S\cos.m}{\cos.S'\cos.m'}-\cos.(S+m)\quad(A)$$

It is here important to notice that the moon's horizontal arallax given in the Nautical Almanac, is the equatorial orizontal parallax; that is, it corresponds to the greatest dius of the earth. The diameter of the earth through any ther latitude is less, and of course the corresponding parallax less.

We therefore give the following table for the reduction of e equatorial horizontal parallax, to the horizontal parallax f any other latitude; it is computed on the supposition that e equatorial diameter is to its polar as 230 to 229. For xample, if the horizontal parallax in the Nautical Almanac is 5', in the latitude 40° the reduction would be 6'', and the rallax reduced would be 54' 54''; and if the parallax from e Nautical Almanac were 60' the reduction would be 6.6', d the reduced parallax would be 59' 53.4''.

The semi-diameter of the moon given in the Nautical lmanac is her horizontal semi-diameter; but when she is in e zenith she is nearer to us by the whole radius of the earth, out one-sixtieth part of her whole distance. Consequently e must appear under a larger and larger angle as she rises m the horizon, and this is called the augmentation of the mi-diameter.

We give the reduction for the parallax; and the augmentan for the semi-diameter in the following tables:

RED. OF MOON'S EQ. HOR. PARALLAX.

Lat.	Eq. Par. 55′	Eq. Par. 60′
°	″	″
20	0.9	1
25	2.8	3
30	3.7	4
35	4.6	5
40	6.0	6.6
45	7.3	8
50	8.6	9.4
55	10.1	11
60	11	12
65	11.8	13
70	12.8	14
75	13.9	15
80	14.6	16

AUG. OF THE MOON'S SEMI-DIAM.

Ap. Alt.	Aug.
°	″
6	2
12	3
18	5
24	6
30	8
36	9
42	11
48	12
54	13
60	14
66	15
72	16
90	16

Example 1.

On the 25th of Jan. 1852, between three and four o'clock in the afternoon, local time, the observed distance between the nearest limbs of the sun and moon was 50° 3′ 20″; the altitude of the sun's lower limb was 20° 1′, and the altitude of the moon's lower limb was 48° 57′, height of the eye 16 feet. The latitude corrected for the sun from noon was 34° 12′ north, and the supposed longitude about 65° west. What was the longitude?

Preparation.

Supposed time at ship $= 3^h\ 15^m$ P. M.
Supposed longitude = 65° $= 4^h\ 20^m$
Supposed Greenwich time $= 7^h\ 35^m$ P. M.

N.	0	1	2	3	4	5	6	7	8	9
400	602060	2169	2277	2386	2494	2603	2711	2819	2928	3036
401	3144	3253	3361	3469	3573	3686	3794	3902	4010	4118
402	4226	4334	4442	4550	4658	4766	4874	4982	5089	5197
403	5305	5413	5521	5628	5736	5844	5951	6059	6166	6274
404	6381	6489	6596	6704	6811	6919	7026	7133	7241	7348
					108					
405	7455	7562	7669	7777	7884	7991	8098	8205	8312	8419
406	8526	8633	8740	8847	8954	9061	9167	9274	9381	9488
407	9594	9701	9808	9914	..21	.128	.234	.341	.447	.554
408	610660	0767	0873	0979	1086	1192	1298	1405	1511	1617
409	1723	1829	1936	2042	2148	2254	2360	2466	2572	2678
410	2784	2890	2996	3102	3207	3313	3419	3525	3630	3736
411	3842	3947	4053	4159	4264	4370	4475	4581	4686	4792
412	4897	5003	5108	5213	5319	5424	5529	5634	5740	5845
413	5950	6055	6160	6265	6370	6476	6581	6686	6790	6895
414	7000	7105	7210	7315	7420	7525	7629	7734	7839	7943
415	8048	8153	8257	8362	8466	8571	8676	8780	8884	8989
416	9293	9198	9302	9406	9511	9615	9719	9824	9928	..32
417	620136	0140	0344	0448	0552	0656	0760	0864	0968	1072
418	1176	1280	1384	1488	1592	1695	1799	1903	2007	2110
419	2214	2318	2421	2525	2628	2732	2835	2939	3042	3146
420	3249	3353	3456	3559	3663	3766	3869	3973	4076	4179
421	4282	4385	4488	4591	4695	4798	4901	5004	5107	5210
422	5312	5415	5518	5621	5724	5827	5929	6032	6135	6238
423	6340	6443	6546	6648	6751	6853	6956	7058	7161	7263
424	7366	7468	7571	7673	7775	7878	7980	8082	8185	8287
					103					
425	8389	8491	8593	8695	8797	8900	9002	9104	9206	9308
426	9410	9512	9613	9715	9817	9919	..21	.123	.224	.326
427	630428	0530	0631	0733	0835	0936	1038	1139	1241	1342
428	1444	1545	1647	1748	1849	1951	2052	2153	2255	2356
429	2457	2559	2660	2761	2862	2963	3064	3165	3266	3367
430	3468	3569	3670	3771	3872	3973	4074	4175	4276	4376
431	4477	4578	4679	4779	4880	4981	5081	5182	5283	5383
432	5484	5584	5685	5785	5886	5986	6087	6187	6287	6388
433	6488	6588	6688	6789	6889	6989	7089	7189	7290	7390
434	7490	7590	7690	7790	7890	7990	8090	8190	8290	8389
435	8489	8589	8689	8789	8888	8988	9088	9188	9287	9387
436	9486	9586	9686	9785	9885	9984	..84	.183	.283	.382
437	640481	0581	0680	0779	0879	0978	1077	1177	1276	1375
438	1474	1573	1672	1771	1871	1970	2069	2168	2267	2366
439	2465	2563	2662	2761	2860	2959	3058	3156	3255	3354
440	3453	3551	3650	3749	3847	3946	4044	4143	4242	4340
441	4439	4537	4636	4734	4832	4931	5029	5127	5226	5324
442	5422	5521	5619	5717	5815	5913	6011	6110	6208	6306
443	6404	6502	6600	6698	6796	6894	6992	7089	7187	7285
444	7383	7481	7579	7676	7774	7872	7969	8067	8165	8262
					98					
445	8360	8458	8555	8653	8750	8848	8945	9043	9140	9237
446	9335	9432	9530	9627	9724	9821	9919	..16	.113	.210
447	650308	0405	0502	0599	0696	0793	0890	0987	1084	1181
448	1278	1375	1472	1569	1666	1762	1859	1956	2053	2150
449	2246	2343	2440	2530	2633	2730	2826	2923	3019	3116

true distance. The equation requires the use of natural sines and cosines.

$$\text{Cos.}x = \left(\cos.(S'+m')+\cos.d\right)\frac{\cos.S\cos.m}{\cos.S'\cos.m'}-\cos.(S+m)$$

$$\begin{aligned}
(S'+m') &= 69^\circ\,21'\,22''; \text{ N. cos. } = .35256\\
d &= 50^\circ\,34'\,34''; \text{ N. cos.* } = \underline{.63505}\\
&\qquad\qquad .98761, \text{ log. } = \bar{1}.994585\\
S &= 20^\circ\,10'\,46'', \text{ log. cos. } = 9.972489\\
m &= 49^\circ\,42'\,38'', \text{ log. cos. } = 9.810669\\
S' &= 20^\circ\,13'\,20'', \text{ cos. com. } = 0.027631\\
m' &= 49^\circ\;\;8'\;\;2'', \text{ cos. com. } = \underline{0.184227}\\
&\qquad\qquad \text{Num. } .97616, \text{ log. } = \bar{1}.989521
\end{aligned}$$

N. cos.$(S+m)$, 69° 53′ 24″, —.34382
True distance, 50° 46′ 37″, cos.23463

In the Nautical Almanac, we find that at 6 P.M. mean Greenwich time, on said day, the true distance between the sun and moon was 49° 59′ 26″, and at 9 P.M. the distance was 51° 20′ 49″, showing a change of 1° 21′ 23″ in three hours of time. But the change from 49° 59′ 26″ to 50° 46′ 37″ is 47′ 11″; and on the supposition that the change is proportional to the time, we have the following

$$1^\circ\,21'\,23'' : 47'\,11'' :: 3h : t$$

Or $$4883 : 2831 :: 3h : 1^h\,48^m\,22^s$$

That is, the time that this observation was taken was $1^h\,44^m\,22^s$ after 6 at Greenwich, or $7^h\,44^m\,22^s$ Greenwich mean time.

With the true altitude of the sun 20° 10′ 46″, the latitude

---

* When d is greater than 90° its cosine becomes *minus*, and its numerical value is then the natural sine of the excess over 90°. Thus if d were 105°, its cosine would be numerically equal to the sine of 15°, and must then be subtracted from the cosine of the sum of apparent altitudes. The result (cos.x) would then be the sine of the excess over 90°.

† Less 20 because the table of natural sines is to radius unity, and we used cos.S and cos.m to the radius of 10, making two tens to take away.

N.	0	1	2	3	4	5	6	7	8	9
00	698970	9057	9144	9231	9317	9404	9491	9578	9664	9751
01	9838	9924	11	..98	.184	.271	.358	.444	.531	.617
02	700704	0790	0877	0963	1050	1136	1222	1309	1395	1482
03	1568	1654	1741	1827	1913	1999	2086	2172	2258	2344
04	2431	2517	2603	2689	2775	2861	2947	3033	3119	3205
					86					
05	3291	3377	3463	3549	3635	3721	3807	3895	3979	4065
06	4151	4236	4322	4408	4494	4579	4665	4751	4837	4922
07	5008	5094	5179	5265	5350	5436	5522	5607	5693	5778
08	5864	5949	6035	6120	6206	6291	6376	6462	6547	6632
09	6718	6803	6888	6974	7059	7144	7229	7315	7400	7485
10	7570	7655	7740	7826	7910	7996	8081	8166	8251	8336
11	8421	8506	8591	8676	8761	8846	8931	9015	9100	9185
12	9270	9355	9440	9524	9609	9694	9779	9863	9948	..33
13	710117	0202	0287	0371	0456	0540	0625	0710	0794	0879
14	0963	1048	1132	1217	1301	1385	1470	1554	1639	1723
15	1807	1892	1976	2060	2144	2229	2313	2397	2481	2566
16	2650	2734	2818	2902	2986	3070	3154	3238	3326	3407
17	3491	3575	3659	3742	3826	3910	3994	4078	4162	4246
18	4330	4414	4497	4581	4665	4749	4833	4916	5000	5084
19	5167	5251	5335	5418	5502	5586	5669	5753	5836	5920
20	6003	6087	6170	6254	6337	6421	6504	6588	6671	6754
21	6838	6921	7004	7088	7171	7254	7338	7421	7504	7587
22	7671	7754	7837	7920	8003	8086	8169	8253	8336	8419
23	8502	8585	8668	8751	8834	8917	9000	9083	9165	9248
24	9331	9414	9497	9580	9663	9745	9828	9911	9994	..77
					82					
25	720159	0242	0325	0407	0490	0573	0655	0738	0821	0903
26	0986	1068	1151	1233	1316	1398	1481	1563	1646	1728
27	1811	1893	.975	2058	2140	2222	2305	2387	2469	2552
28	2634	2716	2798	2881	2963	3045	3127	3209	3291	3374
29	3456	3538	3620	3702	3784	3866	3948	4030	4112	4194
30	4276	4358	4440	4522	4604	4685	4767	4849	4931	5013
31	5095	5176	5258	5340	5422	5503	5585	5667	5748	5830
32	5912	5993	6075	6156	6238	6320	6401	6483	6564	6646
33	6727	6809	6890	6972	7053	7134	7216	7297	7379	7460
34	7541	7623	7704	7785	7866	7948	8029	8110	8191	8273
35	8354	8435	8516	8597	8678	8759	8841	8922	9003	9084
36	9165	9246	9327	9404	9489	9570	9651	9732	9813	9893
37	9974	..55	.136	.217	.298	.378	.459	.840	.621	.702
38	730782	0863	0944	1024	1105	1186	1266	1347	1428	1508
39	1589	1669	1750	1830	1911	1991	2072	2152	2233	2313
40	2394	2474	2555	2635	2715	2796	2876	2956	3037	3117
41	3197	3278	3358	3438	3518	3598	3679	3759	3839	3919
42	3999	4079	4160	4240	4320	4400	4480	4560	4640	4720
43	4800	4880	4960	5040	5120	5200	5279	5359	5439	5519
44	5599	5679	5759	5838	5918	5998	6078	6157	6237	6317
					80					
45	6397	6476	6556	6636	6715	6795	6874	6954	7034	7113
46	7193	7272	7352	7431	7511	7590	7670	7749	7829	7908
47	7987	8067	8146	8225	8305	8384	8463	8543	8622	8701
48	8781	8860	8939	9018	9097	9177	9256	9335	9414	9493
49	9572	9651	9731	9810	9889	9968	..47	.126	.205	.284

$$\begin{array}{llll}
\text{Log. }.11984 & & = & \bar{1}.078602 \\
\text{Cos.}S & = \cos.\ 54^\circ\ 9'\ 20'' & = & 9.767591 \\
\text{Cos.}m & = \cos.\ 21^\circ\ 27'\ 58'' & = & 9.968779 \\
\text{Com. cos.}S' & = \text{com. cos. } 54^\circ\ 10' & = & 0.232525 \\
\text{Com. cos.}m' & = \text{com. cos. } 20^\circ\ 37' & = & 0.028744 \\
\hline
\text{Log. }.11919 & & = & \bar{1}.076241
\end{array}$$

$$\begin{array}{lll}
 & & +.11919 \\
-\text{Cos.}(S+m) & = -\cos.\ 75^\circ\ 37'\ 18'' & = -.24833 \\
\hline
\text{Cos.}x & = \cos.\ 97^\circ\ 25'\ 12'' & = -.12914
\end{array}$$

which is the true distance.

SECOND METHOD OF WORKING A LUNAR.

The foregoing method of clearing a lunar distance is very good, as an educational exercise; but for practical use, it is objectionable, as the equation requires the use of natural sines and cosines. To insure a complete understanding of this important subject, theoretically and practically, we will further transform the equation,

$$\text{Cos.}x = \Big(\cos.(S'+m')+\cos.d\Big)\frac{\cos.S\ \cos.m}{\cos.S'\ \cos.m'}-\cos.(S+m), \quad (1)$$

and adapt it to the use of logarithmic sines and cosines.

Conceiving $(S'+m')$ to be a single arc, and applying equation (17) (page 83), to the first factor in the second member of (1), we shall have,

$$\text{Cos.}x = \qquad (2)$$

$$\frac{2\cos.\tfrac{1}{2}(S'+m'+d)\ \cos.\tfrac{1}{2}(S'+m'-d)\ \cos.S\ \cos.m}{\cos.S'\ \cos.m'} - \cos.(S+m).$$

By equation (32) (p. 85), we find that $\cos.x = 1-2\ \sin.^2\tfrac{1}{2}x$.

By equation (31) (p. 85), $\cos.(S+m) = 2\ \cos.^2\tfrac{1}{2}(S+m)-1$.

These values of $\cos.x$ and $\cos.(S+m)$, placed in (2) will give

$$1-2\sin.^2\tfrac{1}{2}x = \frac{2\ \cos.\tfrac{1}{2}(S'+m'+d)\cos.\tfrac{1}{2}(S'+m'-d)\cos.S\ \cos.m}{\cos.S'\ \cos.m'}$$

$$+1-2\ \cos.^2\tfrac{1}{2}(S+m).$$

By dropping unity from each member, and dividing by —2, we have,

$$\text{Sin.}^2\tfrac{1}{2}x = \tag{3}$$
$$\text{Cos.}^2\tfrac{1}{2}(S+m) - \frac{\cos.\tfrac{1}{2}(S'+m'+d)\cos.\tfrac{1}{2}(S'+m'-d)\cos.S\cos.m.}{\cos.S'\cos.m'}$$

By division, we obtain.

$$\frac{\text{Sin.}^2\tfrac{1}{2}x}{\text{Cos.}^2\tfrac{1}{2}(S+m)} =$$
$$1 - \frac{\text{Cos.}\tfrac{1}{2}(S'+m'+d)\cos.\tfrac{1}{2}(S'+m'-d)\cos.S\cos.m}{\cos.^2\tfrac{1}{2}(S+m)\cos.S'\cos.m'} \tag{4}$$

Assume

$$\text{Sin.}^2P = \frac{\cos.\tfrac{1}{2}(S'+m'+d)\cos.\tfrac{1}{2}(S'+m'-d)\cos.S\cos.m}{\cos.^2\tfrac{1}{2}(S+m)\cos.S'\cos.m'} \tag{5}$$

Where P is an auxiliary arc; equation (4) now becomes

$$\frac{\sin.^2\tfrac{1}{2}x}{\cos.^2\tfrac{1}{2}(S+m)} = 1-\sin.^2P.$$

Since $\sin.^2P+\cos.^2P = 1$, we have $\cos.^2P = 1-\sin.^2P$.

Whence, $$\frac{\sin.^2\tfrac{1}{2}x}{\cos.^2\tfrac{1}{2}(S+m)} = \cos.^2P.$$

By extracting square root and clearing of fractions, we have

$$\text{Sin.}\tfrac{1}{2}x = \cos.P\cos.\tfrac{1}{2}(\text{S}+m). \tag{6}$$

Equations (5) and (6) are plain and practical; they can be easily remembered, and they are adapted to logarithms.

Equations (5) and (6) can be put in words, and called a rule, but in our opinion this is not necessary.

We will now re-compute the last example, in which

$$S' = 54^\circ\ 10',\quad S = 54^\circ\ 9'\ 20'',\ m' = 20^\circ\ 37',\ m = 21^\circ\ 27'\ 58'',$$
$$d = 98^\circ\ 12',\quad (S'+m') = 74^\circ\ 47'.$$

$\frac{1}{2}(d+S'+m') = 86° 29' 30''$, cos. (less 10) $= \overline{2}.786704$

$\frac{1}{2}(d-S'-m') = 11° 42' 30''$, cos. " $= \overline{1}.990867$

$S = 54° 9' 20''$, cos. " $= \overline{1}.767591$

$m = 21° 27' 58''$, cos. " $= \overline{1}.968779$

$\frac{1}{2}(S+m) = 37° 48' 39''$, cos. complement $= 0.102353$

*cos. complement $= 0.102353$

$S' = 54° 10'$, cos. complement $= 0.232525$

$m' = 20° 37'$, cos. complement $= 0.028744$

$2)\overline{2}.979916$

-1.490038

Add 10

Sin.P, 17° 59′ 56″, $= 9.489958$

Cos.$P = 9.978209$

Cos.$\frac{1}{2}(S+m) = 9.897648$

Sin.$\frac{1}{2}x = 9.875857 = 48° 42' 35''$

Whence, true distance $= 97° 23' 10''$, *Ans.*

The two methods do not give the same result precisely. But this one is the more reliable of the two.

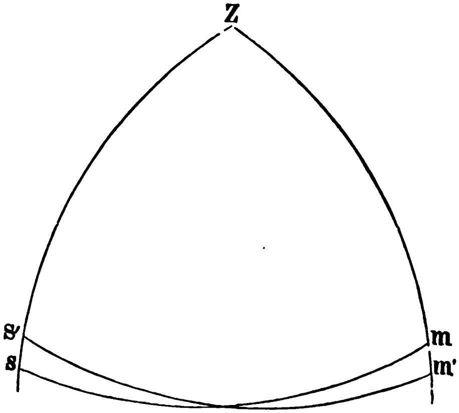
EXAMPLES.

NO.	APPARENT ALT. OF SUN OR A FIXED STAR.	MOON'S AP. ALTITUDE.	APPARENT CENTRAL DISTANCE.	MOON'S HOR. PAR.	TRUE DISTANCE.
	° ′	° ′	° ′ ″	′ ″	° ′ ″
1	⊙ 86 3	39 18	46 45 0	53 51	46 4 25
2	✳ 29 47	57 22	27 35 0	60 3	28 8 24
3	⊙ 31 14	28 7	14 21 30	54 29	14 9 24
4	⊙ 60 5	63 12	51 3 21	58 30	50 41 16
5	✳ 34 28	10 42	49 18 38	61 11	48 45 39
6	⊙ 8 26	19 24	120 18 46	57 14	120 1 46
7	✳ 43 27	40 9	18 21 35	60 20	18 8 12
8	✳ 53 13	57 32	60 13 49	60 52	59 48 12
9	⊙ 72 26	18 30	81 2 28	60 58	80 9 33
10	⊙ 60 33	9 26	70 36 16	59 57	69 49 12

---

* The preceding log. repeated to obtain the square of the last quantity.

THIRD METHOD OF WORKING A LUNAR.



Let Z be the observer's zenith, S' the apparent place of the sun or star, and S its true place; m' the apparent place of the moon, m its true place. Then Sm' will be the apparent distance of the moon from the sun or star, and Sm will be the true distance.

Now if we regard the differences between these apparent and true places as differentials, we shall obtain another formula for correcting Lunar Distances.

Let $S =$ the apparent altitude of the sun or star.
$m =$ the apparent altitude of the moon.
And $x =$ the apparent or observed distance, $S'm'$.

Now by Spherical Trigonometry, (see page 136 of this book), we have

$$\text{Cos.}Z = \frac{\cos.x - \sin.S \sin.m}{\cos.S \cos.m.} \qquad (1)$$

In this problem the angle Z is always a constant quantity, S and m are variable, and x varies in consequence of the variations of S and m. But we may take these effects separately, that is, by supposing m only to vary, and discover the corresponding variation for x. Then we may suppose S to vary, and obtain the corresponding variation of x; and lastly, these two effects put together will be the total variation for x, or the difference between the apparent and true distance between the sun and the moon, or a star and the moon as the case may be.

We will therefore differentiate (1) on the supposition that x and m are variables. Thus,

$$d.\ \cos.Z \cos.S \cos.m = d.\ \cos.x - d.\ \sin.S \sin.m.$$

Or $$-\cos.Z \cos.S \sin.m \cdot dm = -\sin.x \cdot dx - \sin.S \cos.m \cdot dm.$$

$$\text{Sin}.x \frac{dx}{dm} = \cos.Z \cos.S \sin.m - \sin.S \cos.m. \qquad (2)$$

But equation (1) gives

$$\text{Cos}.Z \cos.S = \frac{\cos.x - \sin.S \sin.m}{\cos.m}$$

Multiply by sin.m, then

$$\text{Cos}.Z \cos.S \sin.m = \frac{\cos.x \sin.m - \sin.S \sin.^2 m}{\cos.m}$$

This value placed in equation (2), that equation becomes

$$\text{Sin}.x \frac{dx}{dm} = \frac{\cos.x \sin.m - \sin.S \sin.^2 m}{\cos.m} - \sin.S \cos.m.$$

Or

$$\text{Cos}.m \sin.x \frac{dx}{dm} = \cos.x \sin.m - \sin.S \sin.^2 m - \sin.S \cos.^2 m.$$

$$= \cos.x \sin.m - \sin.S(\sin.^2 m + \cos.^2 m).$$

But $(\text{Sin}.^2 m + \cos.^2 m) = 1.$ Therefore

$$\text{Cos}.m \sin.x \frac{dx}{dm} = \cos.x \sin.m - \sin.S.$$

Or $$dx = \left(\frac{\cos.x \sin.m - \sin.S}{\cos.m \sin.x}\right) dm \qquad (3)$$

Now if we suppose that x and S are the variables, in place of x and m, the result will be the same as (3) if we change S to m and m to S.

Therefore $\left(\frac{\cos.x \sin.S - \sin.m}{\cos.S \sin.x}\right) dS$ is the value of dx corresponding to the variation of the sun's or star's latitude.

The apparent place of the moon is below its true place, and the apparent place of the sun or star is above its true place, therefore dm and dS must have contrary signs. Consequently, the whole variation of x, when both S and m vary, (as is always the case,) must be

$$dx = \left(\frac{\cos.x \sin.m - \sin.S}{\cos.m \sin.x}\right)dm - \left(\frac{\cos.x \sin.S - \sin.m}{\cos.S \sin.x}\right)dS \quad (4)$$

When the sun or star is at the zenith, dS is then nothing, and the value of dx is expressed by the first term of the second member. When the moon is in the zenith, then dm becomes nothing; but in practice, such cases would not be likely to occur, once in a life time.

We will work the fourth example by this formula:

Given the sun's apparent altitude 60° 5′. *The moon's apparent altitude* 63° 12′. *The apparent distance* 51° 3′ 21″, *and the moon's horizontal parallax* 58′ 30″, *to find the true distance from center to center, as seen from the center of the earth.** *Ans.* 50° 41′ 15″.

In this example $S = 60° 5'$; $m = 63° 12'$; $x = 51° 3' 21''$.

Moon's h. p. = 58′ 30″ = 3510″

Log. 3510 = 3.545307
Cos. 63° 12′ = 9.654059
Log. 1583 = 3.199366

Therefore parallax in altitude = 1583″
Refraction = −29
dm = 1554″
dS = −33″, sun's refraction.

For the coefficient of dm,

Sin. m = 9.950650 cos. m = 9.654059
Cos. x = 9.798348 sin. x = 9.890845
Log. .56105 = $\bar{1}.748998$ $\bar{1}.544904$
Sin. S = .86675

---

* Correction may be made for the figure of the earth by correcting the parallax for the latitude of the observer. See table preceding.

$$\begin{array}{llr}
\text{Therefore} \quad .56105 & & \\
\qquad\qquad\; -.86675 & & \bar{1}.544904 \\
\qquad\qquad\; -.30570 \quad \text{therefore log. } .30570 & = & \bar{1}.485295 \\
 & & \bar{1}.940391 \\
\text{And log. } dm = \text{log. } 1554 & = & 3.191451 \\
\qquad \text{whence, log. } 1355 & = & 3.131842
\end{array}$$

Therefore $\left(\dfrac{\cos.x \sin.m - \sin.S}{\cos.m \sin.x}\right) dm = -1355''$

For the coefficient dS,

$$\begin{array}{llll}
\text{Sin.}S = & 9.937895 & \cos.S & = 9.697874 \\
\text{Cos.}x = & 9.798348 & \sin.x & = 9.890845 \\
 & -1.736243 = .54481 & & \bar{1}.588719 \\
\multicolumn{2}{l}{\text{Subtract } \sin.m = .89259} & & \\
\multicolumn{3}{r}{.34778;\ \text{log. } .34778} & = \bar{1}.541305 \\
 & & & \bar{1}.952586 \\
\multicolumn{3}{l}{\qquad \text{Log. } dS = \text{log. } {-33}} & = 1.518514 \\
\multicolumn{3}{l}{\qquad \text{Log. } 29.6''} & = 1.471100
\end{array}$$

Therefore $\left(\dfrac{\cos.x \sin.S - \sin.m}{\cos.S \sin.x}\right) dS = 29.6''$

Whence, putting these parts together, we find

$$\begin{array}{ll}
dx = -1355'' + 29.6'' = & -22' \;\; 5'' \\
\text{Apparent distance} = & 51^\circ \;\; 3' \; 21'' \\
\text{True distance} = & 50^\circ \; 41' \; 16''
\end{array}$$

The equation

$$dx = \left(\frac{\cos.x \sin.m - \sin.S}{\cos.m \sin.x}\right) dm - \left(\frac{\cos.x \sin.S - \sin.m}{\cos.S \sin.x}\right) dS$$

can be put under another form.

Assume $\quad \text{Cos.}x \sin.m = \sin.A$

$\qquad\qquad\; \text{Cos.}x \sin.S = \sin.B$

Then we shall have,

$$dx = \left(\frac{\sin.A - \sin.S}{\cos.m \sin.x}\right) dm - \left(\frac{\sin.B - \sin.m}{\cos.S \sin.x}\right) dS$$

The first term of the second member will be positive or negative, according as A is greater or less than S. The co-efficient of dS is positive when B is greater than m; but dS is always negative; hence the product will be positive or negative, as m is greater or less than B.

From trigonometry, we get by substituting for the difference of the sines their values in factors,

$$\tfrac{1}{2}dx = \frac{\cos.\tfrac{1}{2}(A+S)\sin.\tfrac{1}{2}(A\sim S)dm}{\cos.m\sin.x} - \frac{\cos.\tfrac{1}{2}(B+m)\sin.\tfrac{1}{2}(B\sim m)dS}{\cos.S\sin.x}$$

Example.

Suppose that in latitude 46° north, the moon's apparent altitude was 36° 28′, and that of a planet 24° 43′, and their apparent distance asunder was 71° 46′ 24″. The moon's h. parallax at that time was 58′ 31″, and that of the planet 29″. What was the true distance of the moon from the planet?

Moon's parallax = 58′ 31″
Correction for lat. = 7.7″
58′ 23.3″ = 3503.3″.

Log. 3503.3 = 3.544477
Cos. alt. = cos. 36° 28′ = 9.905366
Log. 2817″ = 3.449843

Moon's parallax in alt. = 2817″
Refraction = 77″
dm = 2740″

Planet.
Log. 29″ = 1.462398
Cos. 24° 43′ = 9.958271
Parallax in alt. = + 26.3″ = 1.420669
Refraction = −124″
dS − 97.7″

Here $m = 36^\circ\ 28'$, $S = 24^\circ\ 43'$, and $x = 71^\circ\ 46'$.

For the auxiliary arcs A and B,

$$\begin{array}{llll}
\text{Cos.}x,\ 71^\circ\ 46', & 9.495388 & & 9.495388 \\
\text{Sin.}m,\ 36^\circ\ 28', & 9.774046 & \text{Sin.}S,\ 24^\circ\ 43', & 9.621313 \\
\hline
A = 10^\circ\ 43', & 9.269434 & B = 7^\circ\ 31' & 9.116701 \\
S = 24^\circ\ 43' & & m = 36^\circ\ 28' & \\
\hline
\tfrac{1}{2}(S+A) = 17^\circ\ 43' & & \tfrac{1}{2}(m+B) = 21^\circ\ 59' & \\
\tfrac{1}{2}(S-A) = 7^\circ\ \ 0' & & \tfrac{1}{2}(m-B) = 14^\circ\ 28' &
\end{array}$$

We now follow the formula.

1st Term.

$$\begin{array}{llll}
\text{Cos.}\tfrac{1}{2}(S+A) = & \cos.\ 17^\circ\ 43' & = & 9.978898 \\
\text{Sin.}\tfrac{1}{2}(S-A) = & \sin.\ \ 7^\circ\ \ 0' & = & 9.085894 \\
\text{Cos. com.}m & = \text{cos. com.}\ 36^\circ\ 28' & = & 0.094634 \\
\text{Sin. com.}x & = \text{sin. com.}\ 71^\circ\ 46' & = & 0.022372 \\
\text{Log.}\ dm & = \log.\ 2740'' & = & 3.437751 \\
\hline
 & -416.4'' & & 2.619549
\end{array}$$

2d Term.

$$\begin{array}{llll}
\text{Cos.}\tfrac{1}{2}(m+B) = & \cos.\ \ 21^\circ\ 59' & = & 9.967217 \\
\text{Sin.}\tfrac{1}{2}(m-B) = & \sin.\ \ 14^\circ\ 28' & = & 9.397631 \\
\text{Cos. com.}S & = \text{cos. com.}\ 24^\circ\ 43' & = & 0.041729 \\
\text{Sin. com.}x & = \text{sin. com.}\ 71^\circ\ 46' & = & 0.022372 \\
\text{Log.}\ dS & = \log.\ \ -97.7'' & = & 1.989895 \\
\hline
 & +26.2'' & & 1.418834
\end{array}$$

The first term is minus because A is less than S, and th second term is plus, because it contains the product of tw minus factors, $(\sin.B - \sin.m)$ and dS.

$$\begin{array}{lll}
\text{Whence,} & \tfrac{1}{2}dx = -416.4'' + 26.2'' = -390.2'' & \\
\text{Or,} & dx = -780'' & = \ \ -13' \\
\text{Apparent distance} & & = 71^\circ\ 46'\ 24'' \\
\hline
\text{True distance} & & = 71^\circ\ 33'\ 24''
\end{array}$$

N	0	1	2	3	4	5	6	7	8	9
600	778151	8224	8296	5368	8441	8513	8585	8658	8730	8802
601	8874	8947	9019	9091	9163	9236	9308	9380	9452	9524
602	9596	6669	9741	9813	9885	9957	..29	.101	.173	.245
603	780317	0389	0461	0533	0605	0677	0749	0821	0893	0965
604	1037	1109	1181	1253	1324	1396	1468	1540	1612	1684
					72					
605	1755	1827	1899	1971	2042	2114	2186	2258	2329	2401
606	2473	2544	2616	2688	2759	2831	2902	2974	3046	3117
607	3189	3260	3332	3403	3475	3546	3618	3689	3761	3832
608	3904	3975	4046	4118	4189	4261	4332	4403	4475	4546
609	4617	4689	4760	4831	4902	4974	5045	5116	5187	5259
610	5330	5401	5472	5543	5615	5686	5757	5828	5899	5970
611	6041	6112	6183	6254	6325	6396	6467	6538	6609	6680
612	6751	6822	6893	6964	7035	7106	7177	7248	7319	7390
613	7460	7531	7602	7673	7744	7815	7885	7956	8027	8098
614	8168	8239	8310	8381	8451	8522	8593	8663	8734	8804
615	8875	8946	9016	9087	9157	9228	9299	9369	9440	9510
616	9581	9651	9722	9792	9863	9933	...4	..74	.144	.215
617	790285	0356	0426	0496	0567	0637	0707	0778	0848	0918
618	0988	1059	1129	1199	1269	1340	1410	1480	1550	1620
619	1691	1761	1831	1901	1971	2041	2111	2181	2252	2322
620	2392	2462	2532	2602	2672	2742	2812	2882	2952	3022
621	3092	3162	3231	3301	3371	3441	3511	3581	3651	3721
622	3790	3860	3930	4000	4070	4139	4209	4279	4349	4418
623	4488	4558	4627	4697	4767	4836	4906	4976	5045	5115
624	5185	5254	5324	5393	5463	5532	5602	5672	5741	5811
					69					
625	5880	5949	6019	6088	6158	6227	6297	6366	6436	6505
626	6574	6644	6713	6782	6852	6921	6990	7060	7129	7198
627	7268	7337	7406	7475	7545	7614	7683	7752	7821	7890
628	7960	8029	8098	8167	8236	8305	8374	8443	8513	8582
629	8651	8720	8789	8858	8927	8996	9065	6134	9203	9272
630	9341	9409	9478	9547	9610	9685	9754	9823	9892	9961
631	800026	0098	0167	0236	0305	0373	0442	0511	0580	0648
632	0717	0786	0854	0923	0992	1061	1129	1198	1266	1335
633	1404	1472	1541	1609	1678	1747	1815	1884	1952	2021
634	2089	2158	2226	2295	2363	2432	2500	2568	2637	2705
635	2774	2842	2910	2979	3047	3116	3184	3252	3321	3389
636	3457	3525	3594	3662	3730	3798	3867	3935	4003	4071
637	4139	4208	4276	4354	4412	4480	4548	4616	4685	4753
638	4821	4889	4957	5025	5093	5161	5229	5297	5365	5433
639	5501	5569	5637	5705	5773	5841	5908	5976	6044	6112
640	6180	6248	6316	6384	6451	6519	6587	6655	6723	6790
641	6858	6926	6994	7061	7129	7157	7264	7332	7400	7467
642	7535	7603	7670	7738	7806	7873	7941	8008	8076	8143
643	8211	8279	8346	8414	8481	8549	8616	8684	8751	8818
644	8886	8953	9021	9088	9156	9223	9290	9358	9425	9492
645	9560	9627	9694	9762	9829	9896	9964	..31	..98	.165
646	810233	0300	0367	0434	0501	0596	0636	0703	0770	0837
647	0904	0971	1039	1106	1173	1240	1307	1374	1441	1508
648	1575	1642	1709	1776	1843	1910	1977	2044	2111	2178
649	2245	2312	2379	2445	2512	2579	2646	2713	2780	2847

W. & L. E. GURLEY'S PRICE LIST.

Troy, N. Y., April 1st, 1866.

In common with all other manufacturers, we have been compelled by the great advance in the cost of labor, the war tax, and the materials used, to increase our old established prices for Instruments, &c.

We believe, however, that in most cases they are still far below those of other makers of established reputation.

SURVEYORS' COMPASSES.

Plain, with Jacob's Staff Mountings, 4 inch Needle	$30 00
“ “ “ “ “ 5 “ “	38 00
“ “ “ “ “ 6 “ “	42 00
Vernier, with Jacob's Staff Mountings, 6 inch Needle	53 00
Railroad, “ “ “ “ 5½ “ “	83 00

EXTRAS.

Compass Tripod, with Cherry Legs	$8 00
“ “ “ Leveling Screws and Clamp and Tangent Movement	18 00
“ “ “ “ “ without “ “ “ “	16 00
“ “ “ Mountings, without Legs	7 00
Compound Tangent Ball	7 00
Brass Cover for Compass Glass	1 75
Outkeeper, for keeping Tally	1 75

TRANSIT INSTRUMENTS.

*Vernier, Plain Telescope, 6 inch Needle, with Compass Tripod	$90 00
*Surveyors' “ 4 “ “ “ Adjusting Tripod	160 00
“ “ “ 5 “ “ “ “ “	165 00
“ “ “ 5½ “ “ “ “ “	165 00
Engineers' “ “ 4 “ “ “ “ “	180 00
“ “ “ 5 “ “ “ “ “	185 00
“ “ “ 5 “ “ with Watch Telescope	225 00
“ “ “ 5 “ “ with Theodolite Axis	225 00
“ “ “ 5 “ “ with Two Telescopes	285 00

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* A “plain” telescope is one without any of the attachments or extras, as we term them, such as the clamp and tangent, vertical circle and level.

PRICE LIST.

EXTRAS.

Vertical Circle, 3½ inch diameter. Vernier Reading to five minutes......	$9 00
" " 4½ " " " " " single minutes.....	15 00
Clamp and Tangent Movement to Axis of Telescope....................	8 00
Level on Telescope, with Ground Bubble and Scale....................	15 00
Rack and Pinion Movement to Eye Glass.............................	5 00
Sights on Telescopes, with Folding Joints............................	8 00
Sights on Standards at right angles to Telescope......................	8 00

SOLAR COMPASSES.

Solar Compass, with Adjusting Sockets and Tripod..................	$215 00
Solar Telescope Compass, " " " "	240 00
Micrometer Telescope, 16 to 20 inches long, with Rack Movement to Object Glass, and with Movable Clips to attach the Sights to No. 1......	28 00

LEVELING RODS.

Yankee or Boston..	$18 00
New York, with Improved Mountings.............................	18 00

LEVELING INSTRUMENTS.

Sixteen inch Telescope, with Adjusting Tripod......................	$135 00
Eighteen " " " " "	135 00
Twenty " " " " "	135 00
Twenty-two inch " " " "	135 00
Builders' Level, with Adjusting Tripod.............................	50 00

POCKET COMPASSES.

With Folding Sights, 2½ inch Needle, very serviceable for tracing lines once surveyed..	$9 00
With Folding Sights, 2½ inch Needle, with Jacob Staff Mountings.......	11 50
" " " 3½ " " " " " "	13 50
" " " 3½ " " without Jacob Staff Mountings.....	11 00
Without Sights, 1 to 2 inch Needle...................from 25 cents to	5 00
Miners' Compass, or Dipping Needle, for tracing Iron Ore, a new and beautiful article, glass on both sides..................................	10 00

INFORMATION TO PURCHASERS.

Manual.—To those who may wish to purchase any of the instruments mentioned in the previous pages of this Advertisement, we will send our Manual—a book of 125 pages, containing a full description of the same, with the adjustments, etc., free of charge (postage included), on application to us at Troy, N. Y.

Instruments Wanted.—In regard to the best kind of instruments for particular purposes, we would here say, that where only common surveying, or the bearing of lines in the surveys for County Maps is required, a Plain Compass is all that is necessary. In cases where the variation of the needle is to be allowed, as in retracing the lines of an old survey, etc., the Vernier Compass, or the Vernier Transit, is required.

Where, in addition to the variation of the needle, horizontal angles are to be taken, and in cases of local attraction, the Railroad Compass is preferable; and for a mixed practice of Surveying and Engineering, we consider the Surveyor's Transit superior to any instrument made by us or any other manufacturers.

In the surveys of U. S. public lands, the county and township lines are required to be run by such instruments as the Solar Compass.

Where Engineering is the exclusive design, the Engineers' Transit and the Leveling Instruments are of course indispensable.

Warranty.—All our instruments are examined and tested by us in person, and are sent to the purchaser adjusted and ready for immediate use.

They are warranted correct in all their parts—we agreeing in the event of any defect appearing after reasonable use, to repair, or replace with a new and perfect instrument, promptly and at our own cost, express charges included, or we will refund the money, and the express charges paid by the purchaser.

Trial of Instruments.—It may often happen that this statement of the prices and quality of our instruments may come into the hands of those who are entirely unacquainted with us, or with the quality of our work, and who therefore feel unwilling to make a final purchase of an article, of the excellence of which they are not perfectly assured.

To such we make the following proposition: We will send the instrument to the express station nearest the person giving the order, and direct the Express Agent, on delivery of the same, to collect our bill, together with charges of transportation, and hold the money on deposit until the purchaser shall have had—say two weeks' actual trial of its quality.

If not found as represented, he may return the instrument before the expiration of that time, and receive the money paid, in full, including express charges, and direct the instrument to be returned to us.

Packing, etc.—Each instrument is packed in a well-finished mahogany case, furnished with lock and key and brass hooks, the larger ones having besides these a leather strap for convenience in carrying. Each case is provided with screw-drivers, adjusting-pin, and wrench for centre-pin, and, if accompanied by a tripod, with a brass plumb-bob; with all instruments for taking angles, without the needle, a reading microscope is also furnished.

Means of Transportation.—Instruments can be sent by express to almost every town in the United States and Canadas, regular agents being located at all the more important points, by whom they are forwarded to smaller places by stage. The charges of transportation from Troy to the purchaser are in all cases to be borne by him, we guaranteeing the safe arrival of our instruments to the extent of express transportation, and holding the Express Companies responsible to us for all losses or damages by the way.

Terms of Payment are uniformly cash, and we have but one price. Our prices for instruments are nearly one-third less than those of other makers of established reputation. They are as low as we think instruments of equal quality can be made, and will not be varied from the list given on the previous pages.

Remittances may be made by a draft, payable to our order at Troy, Albany, New York, Boston, or Philadelphia, which can be procured from Banks or Bankers in almost all of the larger villages.

These may be sent by mail with the order for the instrument, and if lost or stolen on the route, can be replaced by a duplicate draft, obtained as before, and without additional cost.

Or the customer may pay the bill on receipt of the instrument to the Express Agent, taking care to send funds bankable in New York or Boston. The cost of returning bills collected by express of amounts under $10 will be charged to the customer.

W. & L. E. GURLEY,
Mathematical Instrument Makers,
Fulton-st., opposite North End of Union R. R. Depot, Troy, N. Y.

LOGARITHMIC TABLES;

ALSO A TABLE OF THE

TRIGONOMETRICAL LINES;

AND OTHER NECESSARY TABLES.

LOGARITHMS OF NUMBERS

FROM

1 TO 10000.

N.	Log.	N.	Log.	N.	Log.	N.	Log.
1	0 000000	26	1 414973	51	1 707570	76	1 880814
2	0 301030	27	1 431364	52	1 716003	77	1 886491
3	0 477121	28	1 447158	53	1 724276	78	1 892095
4	0 602060	29	1 462398	54	1 732394	79	1 897627
5	0 698970	30	1 477121	55	1 740363	80	1 903090
6	0 778151	31	1 491362	56	1 748188	81	1 908485
7	0 845098	32	1 505150	57	1 755875	82	1 913814
8	0 903090	33	1 518514	58	1 763428	83	1 919078
9	0 954243	34	1 531479	59	1 770852	84	1 924279
10	1 000000	35	1 544068	60	1 778151	85	1 929419
11	1 041393	36	1 556303	61	1 785330	86	1 934498
12	1 079181	37	1 568202	62	1 792392	87	1 939519
13	1 113943	38	1 579784	63	1 799341	88	1 944483
14	1 146128	39	1 591065	64	1 806180	89	1 949390
15	1 176091	40	1 602060	65	1 812913	90	1 954243
16	1 204120	41	1 612784	66	1 819544	91	1 959041
17	1 230449	42	1 623249	67	1 826075	92	1 963788
18	1 255273	43	1 633468	68	1 832509	93	1 968483
19	1 278754	44	1 643453	69	1 838849	94	1 973128
20	1 301030	45	1 653213	70	1 845098	95	1 977724
21	1 322219	46	1 662758	71	1 851258	96	1 982271
22	1 342423	47	1 672098	72	1 857333	97	1 986772
23	1 361728	48	1 681241	73	1 863323	98	1 991226
24	1 380211	49	1 690196	74	1 869232	99	1 995635
25	1 397940	50	1 698970	75	1 875061	100	2 000000

NOTE. In the following table, in the last nine columns of each page, where the first or leading figures change from 9's to 0's, points or dots are now introduced instead of the 0's through the rest of the line, to catch the eye, and to indicate that from thence the corresponding natural number in the first column stands in the *next lower line*, and its annexed first two figures of the Logarithms in the second column.

N.	0	1	2	3	4	5	6	7	8	9
100	000000	0434	0868	1301	1734	2166	2598	3029	3461	3891
101	4321	4750	5181	5609	6038	6466	6894	7321	7748	8174
102	8600	9026	9451	9876	.300	.724	1147	1570	1993	2415
103	012837	3259	3680	4100	4521	4940	5360	5779	6197	6616
104	7033	7451	7868	8284	8700	9116	9532	9947	.361	.775
105	021189	1603	2016	2428	2841	3252	3664	4075	4486	4896
106	5306	5715	6125	6533	6942	7350	7757	8164	8571	8978
107	9384	9789	.195	.600	1004	1408	1812	2216	2619	3021
108	033424	3826	4227	4628	5029	5430	5830	6230	6629	7028
109	7426	7825	8223	8620	9017	9414	9811	.207	.602	.998
110	041393	1787	2182	2576	2969	3362	3755	4148	4540	4932
111	5323	5714	6105	6495	6885	7275	7664	8053	8442	8830
112	9218	9606	9993	.380	.766	1153	1538	1924	2309	2694
113	053078	3463	3846	4230	4613	4996	5378	5760	6142	6524
114	6905	7286	7666	8046	8426	8805	9185	9563	9942	.320
115	060698	1075	1452	1829	2206	2582	2958	3333	3709	4083
116	4458	4832	5206	5580	5953	6326	6699	7071	7443	7815
117	8186	8557	8928	9298	9668	..38	.407	.776	1145	1514
118	071882	2250	2617	2985	3352	3718	4085	4451	4816	5182
119	5547	5912	6276	6640	7004	7368	7731	8094	8457	8819
120	9181	9543	9904	.266	.626	.987	1347	1707	2067	2426
121	082785	3144	3503	3861	4219	4576	4934	5291	5647	6004
122	6360	6716	7071	7426	7781	8136	8490	8845	9198	9552
123	9905	.258	.611	.963	1315	1667	2018	2370	2721	3071
124	093422	3772	4122	4471	4820	5169	5518	5866	6215	6562
125	6910	7257	7604	7951	8298	8644	8990	9335	9681	..26
126	100371	0715	1059	1403	1747	2091	2434	2777	3119	3462
127	3804	4146	4487	4828	5169	5510	5851	6191	6531	6871
128	7210	7549	7888	8227	8565	8903	9241	9579	9916	.253
129	110590	0926	1263	1599	1934	2270	2605	2940	3275	3609
130	3943	4277	4611	4944	5278	5611	5943	6276	6608	6940
131	7271	7603	7934	8265	8595	8926	9256	9586	9915	0245
132	120574	0903	1231	1560	1888	2216	2544	2871	3198	3525
133	3852	4178	4504	4830	5156	5481	5806	6131	6456	6781
134	7105	7429	7753	8076	8399	8722	9045	9368	9690	..12
135	130334	0655	0977	1298	1619	1939	2260	2580	2900	3219
136	3539	3858	4177	4496	4814	5133	5451	5769	6086	6403
137	6721	7037	7354	7671	7987	8303	8618	8934	9249	9564
138	9879	.194	.508	.822	1136	1450	1763	2076	2389	2702
139	143015	3327	3630	3951	4263	4574	4885	5196	5507	5818
140	6128	6438	6748	7058	7367	7676	7985	8294	8603	8911
141	9219	9527	9835	.142	.449	.756	1063	1370	1676	1982
142	152288	2594	2900	3205	3510	3815	4120	4424	4728	5032
143	5336	5640	5943	6246	6549	6852	7154	7457	7759	8061
144	8362	8664	8965	9266	9567	9868	.168	.469	.769	1068
145	161368	1667	1967	2266	2564	2863	3161	3460	3758	4055
146	4353	4650	4947	5244	5541	5838	6134	6430	6726	7022
147	7317	7613	7908	8203	8497	8792	9086	9380	9674	9968
148	170262	0555	0848	1141	1434	1726	2019	2311	2603	2895
149	3186	3478	3769	4060	4351	4641	4932	5222	5512	5802

′	Sine.	D 10″	Cosine.	D. 10″	Tang.	D 10″	Cotang.	N. sine.	N. cos.	
0	8.241855	1196	9.999934	0.4	8.241921	1197	11.758079	01745	99985	60
1	249033	1177	999932	0.4	249102	1177	750898	01774	99984	59
2	256094	1158	999929	0.4	256165	1158	743835	01803	99984	58
3	263042	1140	999927	0.4	263115	1140	736885	01832	99983	57
4	269881	1122	999925	0.4	269956	1122	730044	01862	99983	56
5	276614	1105	999922	0.4	276691	1105	723309	01891	99982	55
6	283243	1088	999920	0.4	283323	1089	716677	01920	99982	54
7	289773	1072	999918	0.4	289856	1073	710144	01949	99981	53
8	296207	1056	999915	0.4	296292	1057	703708	01978	99980	52
9	302546	1041	999913	0.4	302634	1042	697366	02007	99980	51
10	308794	1027	999910	0.4	308884	1027	691116	02036	99979	50
11	8.314954	1012	9.999907	0.4	8.315046	1013	11.684954	02065	99979	49
12	321027	998	999905	0.4	321122	999	678878	02094	99978	48
13	327016	985	999902	0.4	327114	985	672886	02123	99977	47
14	332924	971	999899	0.5	333025	972	666975	02152	99977	46
15	338753	959	999897	0.5	338856	959	661144	02181	99976	45
16	344504	946	999894	0.5	344610	946	655390	02211	99976	44
17	350181	934	999891	0.5	350289	934	649711	02240	99975	43
18	355783	922	999888	0.5	355895	922	644105	02269	99974	42
19	361315	910	999885	0.5	361430	911	638570	02298	99974	41
20	366777	899	999882	0.5	366895	899	633105	02327	99973	40
21	8.372171	888	9.999879	0.5	8.372292	888	11.627708	02356	99972	39
22	377499	877	999876	0.5	377622	879	622378	02385	99972	38
23	382762	867	999873	0.5	382889	867	617111	02414	99971	37
24	387962	856	999870	0.5	388092	857	611908	02443	99970	36
25	393101	846	999867	0.5	393234	847	606766	02472	99969	35
26	398179	837	999864	0.5	398315	837	601685	02501	99969	34
27	403199	827	999861	0.5	403338	828	596662	02530	99968	33
28	408161	818	999858	0.5	408304	818	591696	02560	99967	32
29	413068	809	999854	0.5	413213	809	586787	02589	99966	31
30	417919	800	999851	0.6	418068	800	581932	02618	99966	30
31	8.422717	791	9.999848	0.6	8.422869	791	11.577131	02647	99965	29
32	427462	782	999844	0.6	427618	783	572382	02676	99964	28
33	432156	774	999841	0.6	432315	774	567685	02705	99963	27
34	436800	766	999838	0.6	436962	766	563038	02734	99963	26
35	441394	758	999834	0.6	441560	758	558440	02763	99962	25
36	445941	750	999831	0.6	446110	750	553890	02792	99961	24
37	450440	742	999827	0.6	450613	743	549387	02821	99960	23
38	454893	735	999823	0.6	455070	735	544930	02850	99959	22
39	459301	727	999820	0.6	459481	728	540519	02879	99959	21
40	463665	720	999816	0.6	463849	720	536151	02908	99958	20
41	8.467985	712	9.999812	0.6	8.468172	713	11.531828	02938	99957	19
42	472263	706	999809	0.6	472454	707	527546	02967	99956	18
43	476498	699	999805	0.6	476693	700	523307	02996	99955	17
44	480693	692	999801	0.6	480892	693	519108	03025	99954	16
45	484848	686	999797	0.7	485050	686	514950	03054	99953	15
46	488963	679	999793	0.7	489170	680	510830	03083	99952	14
47	493040	673	999790	0.7	493250	674	506750	03112	99952	13
48	497078	667	999786	0.7	497293	668	502707	03141	99951	12
49	501080	661	999782	0.7	501298	661	498702	03170	99950	11
50	505045	655	999778	0.7	505267	655	494733	03199	99949	10
51	8.508974	649	9.99977[illegible]	0.7	8.509200	650	11.490800	03228	99948	9
52	512867	643	999769	0.7	513098	644	486902	03257	99947	8
53	516726	637	999765	0.7	516961	638	483039	03286	99946	7
54	520551	632	999761	0.7	520790	633	479210	03316	99945	6
55	524343	626	999757	0.7	524586	627	475414	03345	99944	5
56	528102	621	999753	0.7	528349	622	471651	03374	99943	4
57	531828	616	999748	0.7	532080	616	467920	03403	99942	3
58	535523	611	999744	0.7	535779	611	464221	03432	99941	2
59	539186	605	999740	0.7	539447	606	460553	03461	99940	1
60	542819		999735		543084		456916	03490	99939	0
	Cosine.		Sine.		Cotang.		Tang.	N. cos.	N. sine.	′

88 Degrees.

Sine.	D. 10″	Cosine.	D. 10″	Tang.	D. 10″	Cotang.	N. sine.	N. cos.	
542819	600	9.999735	0.7	8.543084	602	11.456916	03490	99939	60
546422	595	999731	0.7	546691	596	453309	03519	99938	59
549995	591	999726	0.7	550268	591	449732	03548	99937	58
553539	586	999722	0.8	553817	587	446183	03577	99936	57
557054	581	999717	0.8	557336	582	442664	03606	99935	56
560540	576	999713	0.8	560828	577	439172	03635	99934	55
563999	572	999708	0.8	564291	573	435709	03664	99933	54
567431	567	999704	0.8	567727	568	432273	03693	99932	53
570836	563	999699	0.8	571137	564	428863	03723	99931	52
574214	559	999694	0.8	574520	559	425480	03752	99930	51
577566	554	999689	0.8	577877	555	422123	03781	99929	50
583892	550	9.999685	0.8	8.581208	551	11.418792	03810	99927	49
584193	546	999680	0.8	584514	547	415486	03839	99926	48
587469	542	999675	0.8	587795	543	412205	03868	99925	47
590721	538	999670	0.8	591051	539	408949	03897	99924	46
593948	534	999665	0.8	594283	535	405717	03926	99923	45
597152	530	999660	0.8	597492	531	402508	03955	99922	44
600332	526	999655	0.8	600677	527	399323	03984	99921	43
603489	522	999650	0.8	603839	523	396161	04013	99919	42
606623	519	999645	0.8	606978	519	393022	04042	99918	41
609734	515	999640	0.9	610094	516	389906	04071	99917	40
612823	511	9.999635	0.9	8.613189	512	11.386811	04100	99916	39
615891	508	999629	0.9	616262	508	383738	03129	99915	38
618937	504	999324	0.9	619313	505	380687	04159	99913	37
621962	501	999619	0.9	622343	501	377657	04188	99912	36
624965	497	999614	0.9	625352	498	374648	04217	99911	35
627948	494	999608	0.9	628340	495	371660	04246	99910	34
630911	490	999603	0.9	631308	491	368692	04275	99909	33
633854	487	999597	0.9	634256	488	365744	04304	99907	32
636776	484	999592	0.9	637184	485	362816	04333	99906	31
639680	481	999586	0.9	640093	482	359907	04362	99905	30
642563	477	9.999581	0.9	8.642982	478	11.357018	04391	99904	29
645428	474	999575	0.9	645853	475	354147	04420	99902	28
648274	471	999570	0.9	648704	472	351296	04449	99901	27
651102	468	999564	0.9	651537	469	348463	04478	99900	26
653911	465	999558	1.0	654352	466	345648	04507	99898	25
656702	462	999553	1.0	657149	463	342851	04536	99897	24
659475	459	999547	1.0	659928	460	340072	04565	99896	23
662230	456	999541	1.0	662689	457	337311	04594	99894	22
664968	453	999535	1.0	665433	454	334567	04623	99893	21
667689	451	999529	1.0	668160	453	331840	04653	99892	20
670393	448	9.999524	1.0	8.670870	449	11.329130	04682	99890	19
673080	445	999518	1.0	673563	446	326437	04711	99889	18
675751	442	999512	1.0	676239	443	323761	04740	99888	17
678405	440	999506	1.0	678900	442	321100	04769	99886	16
681043	437	999500	1.0	681544	438	318456	04798	99885	15
683665	434	999493	1.0	684172	435	315828	04827	99883	14
686272	432	999487	1.0	6 6784	433	313216	04856	99882	13
688863	429	999481	1.0	689381	430	310619	04885	99881	12
691438	427	999475	1.0	691963	428	308037	04914	99879	11
693998	424	999469	1.0	694529	425	305471	04943	99878	10
696543	422	9.999463	1.1	8.697081	423	11.302919	04972	99876	9
699073	419	999456	1.1	699617	420	300383	05001	99875	8
701589	417	999450	1.1	702139	418	297861	05030	99873	7
704090	414	999443	1.1	704246	415	295354	05059	99872	6
706577	412	999437	1.1	707140	413	292860	05088	99870	5
709049	410	999431	1.1	709618	411	290382	05117	99869	4
711507	407	999424	1.1	702083	408	287917	05146	99867	3
713952	405	999418	1.1	714534	406	285465	05175	99866	2
716383	403	999411	1.1	716972	404	283028	05205	99864	1
718800		999404		719396		280604	05234	99863	0
osine.		Sine.		Cotang.		Tang.	N. cos.	N.sine.	′

87 Degrees.

′	Sine.	D. 10″	Cosine.	D. 1″	Tang.	D. 10″	Cotang.	N. sine.	N. cos.	
0	8.718800	401	9.999404	1.1	8.719396	402	11.280604	05234	99863	60
1	721204	398	999398	1.1	721806	399	278194	05263	99861	59
2	723595	396	999391	1.1	724204	397	275796	05292	99860	58
3	725972	394	999384	1.1	726588	395	273412	05321	99858	57
4	728337	392	999378	1.1	728959	393	271041	05350	99857	56
5	730688	390	999371	1.1	731317	391	268683	05379	99855	55
6	733027	388	999364	1.2	733663	389	266337	05408	99854	54
7	735354	386	999357	1.2	735996	387	264004	05437	99852	53
8	737667	384	999350	1.2	738317	385	261683	05466	99851	52
9	739969	382	999343	1.2	740626	383	259374	05495	99849	51
10	742259	380	999336	1.2	742922	381	257078	05524	99847	50
11	8.744536	378	9.999329	1.2	8.745207	379	11.254793	05553	99846	49
12	746802	376	999322	1.2	747479	377	252521	05582	99844	48
13	749055	374	999315	1.2	749740	375	250260	05611	99842	47
14	751297	372	999308	1.2	751989	373	248011	05640	99841	46
15	753528	370	999301	1.2	754227	371	245773	05669	99839	45
16	755747	368	999294	1.2	756453	369	243547	05698	99838	44
17	757955	366	999286	1.2	758668	367	241332	05727	99836	43
18	760151	364	999279	1.2	760872	365	239128	05756	99834	42
19	762337	362	999272	1.2	763065	364	236935	05785	99833	41
20	764511	361	999265	1.2	765246	362	234754	05814	99831	40
21	8.766675	359	9.999257	1.2	8.767417	360	11.232583	05844	99829	39
22	768828	357	999250	1.3	769578	358	230422	05873	99827	38
23	770970	355	999242	1.3	771727	356	228273	05902	99826	37
24	773101	353	999235	1.3	773866	355	226134	05931	99824	36
25	775223	352	999227	1.3	775995	353	224005	05960	99822	35
26	777333	350	999220	1.3	778114	351	221886	05989	99821	34
27	779434	348	999212	1.3	780229	350	219778	06018	99819	33
28	781524	347	999205	1.3	7825[illegible]	348	217680	06047	99817	32
29	783605	345	999197	1.3	784408	346	215592	06076	99815	31
30	785675	343	999189	1.3	786486	345	213514	06105	99813	30
31	8.787736	342	9.999181	1.3	8.788554	343	11.211446	06134	99812	29
32	789787	340	999174	1.3	790613	341	209387	06163	99810	28
33	791828	339	999166	1.3	792662	340	207338	06192	99808	27
34	793859	337	999158	1.3	794701	338	205299	06221	99806	26
35	795881	335	999150	1.3	796731	337	203269	06250	99804	25
36	797894	334	999142	1.3	798752	335	201248	06279	99803	24
37	799897	332	999134	1.3	800763	334	199237	06308	99801	23
38	801892	331	999126	1.3	802765	332	197235	06337	99799	22
39	803876	329	999118	1.3	804858	331	195242	06366	99797	21
40	805852	328	999110	1.3	806742	329	193258	06395	99795	20
41	8.807819	326	9.999102	1.3	8.808717	328	11.191283	06424	99793	19
42	809777	325	999094	1.3	810683	326	189317	06453	99792	18
43	811726	323	999086	1.4	812641	325	187359	06482	99790	17
44	813667	322	999077	1.4	814589	323	185411	06511	99788	16
45	815599	320	999069	1.4	816529	322	183471	06540	99786	15
46	817522	319	999061	1.4	818461	320	181539	06569	99784	14
47	819436	318	999053	1.4	820384	319	179616	06598	99782	13
48	821343	316	999044	1.4	822298	318	177702	06627	99780	12
49	823240	315	999036	1.4	824205	316	175795	06656	99778	11
50	825130	313	999027	1.4	826103	315	173897	06685	99776	10
51	8.827011	312	9.999019	1.4	8.827992	314	11.172008	06714	99774	9
52	828884	311	999010	1.4	829874	312	170126	06743	99772	8
53	830749	309	999002	1.4	831748	311	168252	06773	99770	7
54	832607	308	998993	1.4	833613	310	166387	06802	99768	6
55	834456	307	998984	1.4	835471	308	164529	06831	99766	5
56	836297	306	998976	1.4	837321	307	162679	06860	99764	4
57	838130	304	998967	1.5	839163	306	160837	06889	99762	3
58	839956	303	998958	1.5	840998	304	159002	06918	99760	2
59	841774	302	998950	1.5	842825	303	157175	06947	99758	1
60	843585		998941		844644		155356	06976	99756	0
	Cosine.		Sine.		Cotang.		Tang.	N. cos.	N. sine.	′

86 Degrees.

′	Sine.	D. 10″	Cosine.	D. 10″	Tang.	D. 10″	Cotang.	N. sine.	N. cos.	
0	8.843585	300	9.998941	1.5	8.844644	302	11.155356	06976	99756	60
1	845387	299	998932	1.5	846455	301	153545	07005	99754	59
2	847183	298	998923	1.5	848260	299	151740	07034	99752	58
3	848971	297	998914	1.5	850057	298	149943	07063	99750	57
4	850751	295	998905	1.5	851846	297	148154	07092	99748	56
5	852525	294	998896	1.5	853628	296	146372	07121	99746	55
6	854291	293	998887	1.5	855403	295	144597	07150	99744	54
7	856049	292	998878	1.5	857171	293	142829	07179	99742	53
8	857801	291	998869	1.5	858932	292	141068	07208	99740	52
9	859546	290	998860	1.5	860686	291	139314	07237	99738	51
10	861283	288	998851	1.5	862433	290	137567	07266	99736	50
11	8.863014	287	9.998841	1.5	8.864173	289	11.135827	07295	99734	49
12	864738	286	998832	1.5	865906	288	134094	07324	99731	48
13	866455	285	998823	1.6	867632	287	132368	07353	99729	47
14	868165	284	998813	1.6	869351	285	130649	07382	99727	46
15	869868	283	998804	1.6	871064	284	128936	07411	99725	45
16	871565	282	998795	1.6	872770	283	127230	07440	99723	44
17	873255	281	998785	1.6	874469	282	125531	07469	99721	43
18	874938	279	998776	1.6	876162	281	123838	07498	99719	42
19	876615	279	998766	1.6	877849	280	122151	07527	99716	41
20	878285	277	998757	1.6	879529	279	120471	07556	99714	40
21	8.879949	276	9.998747	1.6	8.881202	278	11.118798	07585	99712	39
22	881607	275	998738	1.6	882869	277	117131	07614	99710	38
23	883258	274	998728	1.6	884530	276	115470	07643	99708	37
24	884903	273	998718	1.6	886185	275	113815	07672	99705	36
25	886542	272	998708	1.6	887833	274	112167	07701	99703	35
26	888174	271	998699	1.6	889476	273	110524	07730	99701	34
27	889801	270	998689	1.6	891112	272	108888	07759	99699	33
28	891421	269	998679	1.6	892742	271	107258	07788	99696	32
29	893035	268	998669	1.7	894366	270	105634	07817	99694	31
30	894643	267	998659	1.7	895984	269	104016	07846	99692	30
31	8.896246	266	9.998649	1.7	8.897596	268	11.102404	07875	99689	29
32	897842	265	998639	1.7	899203	267	100797	07904	99687	28
33	899432	264	998629	1.7	900803	266	099197	07933	99685	27
34	901017	263	998619	1.7	902398	265	097602	07962	99683	26
35	902596	262	998609	1.7	903987	264	096013	07991	99680	25
36	904169	261	998599	1.7	905570	263	094430	08020	99678	24
37	905736	260	998589	1.7	907147	262	092853	08049	99676	23
38	907297	259	998578	1.7	908719	261	091281	08078	99673	22
39	908853	258	998568	1.7	910285	260	089715	08107	99671	21
40	910404	257	998558	1.7	911846	259	088154	08136	99668	20
41	8.911949	257	9.998548	1.7	8.913401	258	11.086599	08165	99666	19
42	913488	256	998537	1.7	914951	257	085049	08194	99664	18
43	915022	255	998527	1.7	916495	256	083505	08223	99661	17
44	916550	254	998516	1.8	918034	256	081966	08252	99659	16
45	918073	253	998506	1.8	919568	255	080432	08281	99657	15
46	919591	252	998495	1.8	921096	254	078904	08310	99654	14
47	921103	251	998485	1.8	922619	253	077381	08339	99652	13
48	922610	250	998474	1.8	924136	252	075864	08368	99649	12
49	924112	249	998464	1.8	925649	251	074351	08397	99647	11
50	925609	249	998453	1.8	927156	250	072844	08426	99644	10
51	8.927100	248	9.998442	1.8	8.928658	249	11.071342	08455	99642	9
52	928587	247	998431	1.8	930155	249	069845	08484	99639	8
53	930068	246	998421	1.8	931647	248	068353	08513	99637	7
54	931544	245	998410	1.8	933134	247	066866	08542	99635	6
55	933015	244	998399	1.8	934616	246	065384	08571	99632	5
56	934481	243	998388	1.8	936093	245	063907	08600	99630	4
57	935942	243	998377	1.8	937565	244	062435	08629	99627	3
58	937398	242	998366	1.8	939032	244	060968	08658	99625	2
59	938850	241	998355	1.8	940494	243	059506	08687	99622	1
60	940296		998344		941952		058048	08716	99619	0
	Cosine.		Sine.		Cotang.		Tang.	N. cos.	N.sine.	′

'	Sine.	D. 10"	Cosine.	D. 10"	Tang.	D. 10"	Cotang.	N. sine.	N. cos.	
0	8.940296	240	9.998344	1.9	8.941952	242	11.058048	08716	99619	60
1	941738	239	998333	1.9	943404	241	056596	08745	99617	59
2	943174	239	998322	1.9	944852	240	055148	08774	99614	58
3	944606	238	998311	1.9	946295	240	053705	08803	99612	57
4	946034	237	998300	1.9	947734	239	052266	08831	99609	56
5	947456	236	998289	1.9	949168	238	050832	08860	99607	55
6	948874	235	998277	1.9	950597	237	049403	08889	99604	54
7	950287	235	998266	1.9	952021	237	047979	08918	99602	53
8	951693	234	998255	1.9	953441	236	046559	08947	99599	52
9	953100	233	998243	1.9	954856	235	045144	08976	99596	51
10	954499	232	998232	1.9	956267	234	043733	09005	99594	50
11	8.955894	232	9.998220	1.9	8.957674	234	11.042326	09034	99591	49
12	957284	231	998209	1.9	959075	233	040925	09063	99588	48
13	958670	230	998197	1.9	960473	232	039527	09092	99586	47
14	960052	229	998186	1.9	961866	231	038134	09121	99583	46
15	961429	229	998174	1.9	963255	231	036745	09150	99580	45
16	962801	228	998163	1.9	964639	230	035361	09179	99578	44
17	964170	227	998151	1.9	966019	229	033981	09208	99575	43
18	965534	227	998139	2.0	967394	229	032606	09237	99572	42
19	966893	226	998128	2.0	968766	228	031234	09266	99570	41
20	968249	225	998116	2.0	970133	227	029867	09295	99567	40
21	8.969600	224	9.998104	2.0	8.971496	226	11.028504	09324	99564	39
22	970947	224	998092	2.0	972855	226	027145	09353	99562	38
23	972289	223	998080	2.0	974209	225	025791	09382	99559	37
24	973628	222	998068	2.0	975560	224	024440	09411	99556	36
25	974962	222	998056	2.0	976906	224	023094	09440	99553	35
26	976293	221	998044	2.0	978248	223	021752	09469	99551	34
27	977619	220	998032	2.0	979586	222	020414	09498	99548	33
28	978941	220	998020	2.0	980921	222	019079	09527	99545	32
29	980259	219	998008	2.0	982251	221	017749	09556	99542	31
30	981573	218	997996	2.0	983577	220	016423	09585	99540	30
31	8.982883	218	9.997984	2.0	8.984899	220	11.015101	09614	99537	29
32	984189	217	997972	2.0	986217	219	013783	09642	99534	28
33	985491	216	997959	2.0	987532	218	012468	09671	99531	27
34	986789	216	997947	2.0	988842	218	011158	09700	99528	26
35	988083	215	997935	2.1	990149	217	009851	09729	99526	25
36	989374	214	997922	2.1	991451	216	008549	06758	99523	24
37	990660	214	997910	2.1	992750	216	007250	09787	99520	23
38	991943	213	997897	2.1	994045	215	005955	09816	99517	22
39	993222	212	997885	2.1	995337	215	004663	09845	99514	21
40	994497	212	997872	2.1	996624	214	003376	09874	99511	20
41	8.995768	211	9.997860	2.1	8.997908	213	11.002092	09903	99508	19
42	997036	211	997847	2.1	999188	213	000812	09932	99505	18
43	998299	210	997835	2.1	9.000465	212	10.999535	09961	99503	17
44	999560	209	997822	2.1	001738	211	998262	09990	99500	16
45	9.000816	209	997809	2.1	003007	211	996993	10019	99497	15
46	002059	208	997797	2.1	004272	210	995728	10048	99494	14
47	003318	208	997784	2.1	005534	210	994466	10077	99491	13
48	004563	207	997771	2.1	006792	209	993208	10106	99488	12
49	005805	206	997758	2.1	008047	208	991953	10135	99485	11
50	007044	206	997745	2.1	009298	208	990702	10164	99482	10
51	9.008278	205	9.997732	2.1	9.010546	207	10.989454	10192	99479	9
52	009510	205	997719	2.1	011790	207	988210	10221	99476	8
53	010737	204	997706	2.1	013031	206	686969	10250	99473	7
54	011962	203	997693	2.2	014268	206	985732	10279	99470	6
55	013182	203	997680	2.2	015502	205	984498	10308	99467	5
56	014400	202	997667	2.2	016732	204	983268	10337	99464	4
57	015613	202	997654	2.2	017959	204	983041	10366	99461	3
58	016824	201	997641	2.2	019183	203	980817	10395	99458	2
59	018031	201	997628	2.2	020403	203	979597	10424	99455	1
60	019235		997614		021620		978380	10453	99452	0
	Cosine.		Sine.		Cotang.		Tang.	N. cos.	N. sine.	'

84 Degrees.

′	Sine.	D. 10″	Cosine.	D. 10″	Tang.	D. 10″	Cotang.	N. sine.	N. cos.	
0	9.019235	200	9.997614	2.2	9.021620	202	10.978380	10453	99452	60
1	020435	199	997601	2.2	022834	202	977166	10482	99449	59
2	021632	199	997588	2.2	024044	201	975956	10511	99446	58
3	022825	198	997574	2.2	025251	201	974749	10540	99443	57
4	024016	198	997561	2.2	026455	200	973545	10569	99440	56
5	025203	197	997547	2.2	027655	199	972345	10597	99437	55
6	026386	197	997534	2.3	028852	199	971148	10626	99434	54
7	027567	196	997520	2.3	030046	198	969954	10655	99431	53
8	028744	196	997507	2·3	031237	198	968763	10684	99428	52
9	029918	195	997493	2·3	032425	197	967575	10713	99424	51
10	031089	195	997480	2·3	033609	197	966391	10742	99421	50
11	9.032257	194	9.997466	2·3	9.034791	196	10.965209	10771	99418	49
12	033421	194	997452	2·3	035969	196	964031	10800	99415	48
13	034582	193	997439	2·3	037144	195	962856	10829	99412	47
14	035741	192	997425	2·3	038316	195	961684	10858	99409	46
15	036896	192	997411	2·3	039485	194	960515	10887	99406	45
16	038048	191	997397	2·3	040651	194	959349	10916	99402	44
17	039197	191	997383	2·3	041813	193	958187	10945	99399	43
18	040342	190	997369	2·3	042973	193	957027	10973	99396	42
19	041485	190	997355	2·3	044130	192	955870	11002	99393	41
20	042625	189	997341	2·3	045284	192	954716	11031	99390	40
21	9.043762	189	9.997327	2·4	9.046434	191	10.953566	11060	99386	39
22	044895	180	997313	2·4	047582	191	952418	11089	99383	38
23	046026	188	997299	2·4	048727	190	951273	11118	99380	37
24	047154	187	997285	2·4	049869	190	950131	11147	99377	36
25	048279	187	997271	2·4	051008	189	948992	11176	99374	35
26	049400	186	997257	2.4	052144	189	947856	11205	99370	34
27	050519	186	997242	2·4	053277	188	946723	11234	99367	33
28	051635	185	997228	2·4	054407	188	945593	11263	99364	32
29	052749	185	997214	2·4	055535	187	944465	11291	99360	31
30	053859	184	997199	2·4	056659	187	943341	11320	99357	30
31	9.054966	184	9.997185	2·4	9.057781	186	10.942219	11349	99354	29
32	056071	184	997170	2·4	058900	186	941100	11378	99351	28
33	057172	183	997156	2·4	060016	185	939984	11407	99347	27
34	058271	183	997141	2·4	061130	185	938870	11436	99344	26
35	059367	182	997127	2.4	062240	185	937760	11465	99341	25
36	060460	182	997112	2.4	063348	184	936652	11494	99337	24
37	061551	181	997098	2.4	064453	184	935547	11523	99334	23
38	062639	181	997083	2·5	065556	183	934444	11552	99331	22
39	063724	180	997068	2.5	066655	183	933345	11580	99327	21
40	064806	180	997053	2·5	067752	182	932248	11609	99324	20
41	9.065885	179	9.997039	2·5	9.068846	182	10.931154	11638	99320	19
42	066962	179	997024	2·5	069038	181	930062	11667	99317	18
43	068036	179	997009	2.5	071027	181	928973	11696	99314	17
44	069107	178	996994	2.5	072113	181	927887	11725	99310	16
45	070176	178	996979	2·5	073197	180	926803	11754	99307	15
46	071242	177	996964	2·5	074278	180	925722	11783	99303	14
47	072306	177	996949	2.5	075356	179	924644	11812	99300	13
48	073366	176	996934	2.5	076432	179	923568	11840	99297	12
49	074424	176	996919	2.5	077505	178	922495	11869	99293	11
50	075480	175	996904	2.5	078576	178	921424	11898	99290	10
51	9.076533	175	9.996889	2.5	9.079644	178	10.920356	11927	99286	9
52	077583	175	996874	2.5	080710	177	919290	11956	99283	8
53	078631	174	996858	2.5	081773	177	918227	11985	99279	7
54	079676	174	996843	2.5	082833	176	917167	12014	99276	6
55	080719	173	996828	2.5	083891	176	916109	12043	99272	5
56	081759	173	996812	2.6	084947	175	915053	12071	99269	4
57	082797	172	996797	2.6	086000	175	914000	12100	99265	3
58	083832	172	996782	2.6	087050	175	912950	12129	99262	2
59	084864	172	996766	2.6	088098	174	911902	12158	99258	1
60	085894		996751		089144		910856	12187	9	
	Cosine.		Sine.		Cotang.		Tang.	N. co		

83 Degrees.

′	Sine.	D. 10″	Cosine.	D. 10″	Tang.	D. 10″	Cotang.	N. sine.	N. cos.	
0	9.085894	171	9.996751	2.6	9.089144	174	10.910856	12187	99255	60
1	086922	171	996735	2.6	090187	173	909813	12216	99251	59
2	087947	170	996720	2.6	091228	173	908772	12245	99248	58
3	088970	170	996704	2.6	092266	173	907734	12274	99244	57
4	089990	170	996688	2.6	093302	172	906698	12302	99240	56
5	091008	169	996673	2.6	094336	172	905664	12331	99237	55
6	092024	169	996657	2.6	095367	171	904633	12360	99233	54
7	093037	168	996641	2.6	096395	171	903605	12389	99230	53
8	094047	168	996625	2.6	097422	171	902578	12418	99226	52
9	095056	168	996610	2.6	098446	170	901554	12447	99222	51
10	096062	167	996594	2.6	099468	170	900532	12476	99219	50
11	9.097065	167	9.996578	2.7	9.100487	169	10.899513	12504	99215	49
12	098066	166	996562	2.7	101504	169	898496	12533	99211	48
13	099065	166	996546	2.7	102519	169	897481	12562	99208	47
14	100062	166	996530	2.7	103532	168	896468	12591	99204	46
15	101056	165	996514	2.7	104542	168	895458	12620	99200	45
16	102048	165	996498	2.7	105550	168	894450	12649	99197	44
17	103037	164	996482	2.7	106556	167	893444	12678	99193	43
18	104025	164	996465	2.7	107559	167	892441	12706	99189	42
19	105010	164	996449	2.7	108560	166	891440	12735	99186	41
20	105992	163	996433	2.7	109559	166	890441	12764	99182	40
21	9.106973	163	9.996417	2.7	9.110556	166	10.889444	12793	99178	39
22	107951	163	996400	2.7	111551	165	888449	12822	99175	38
23	108927	162	996384	2.7	112543	165	887457	12851	99171	37
24	109901	162	996368	2.7	113533	165	886467	12880	99167	36
25	110873	162	996351	2.7	114521	164	885479	12908	99163	35
26	111842	161	996335	2.7	115507	164	884493	12937	99160	34
27	112809	161	996318	2.7	116491	164	883509	12966	99156	33
28	113774	160	996302	2.8	117472	163	882528	12995	99152	32
29	114737	160	996285	2.8	118452	163	881548	13024	99148	31
30	115698	160	996269	2.8	119429	162	880571	13053	99144	30
31	9.116656	159	9.996252	2.8	9.120404	162	10.879596	13081	99141	29
32	117613	159	996235	2.8	121377	162	878623	13110	99137	28
33	118567	159	996219	2.8	122348	161	877652	13139	99133	27
34	119519	158	996202	2.8	123317	161	876683	13168	99129	26
35	120469	158	996185	2.8	124284	161	875716	13197	99125	25
36	121417	158	996168	2.8	125249	160	874751	13226	99122	24
37	122362	157	996151	2.8	126211	160	873789	13254	99118	23
38	123306	157	996134	2.8	127172	160	872828	13283	99114	22
39	124248	157	996117	2.8	128130	159	871870	13312	99110	21
40	125187	156	996100	2.8	129087	159	870913	13341	99106	20
41	9.126125	156	9.996083	2.9	9.130041	159	10.869959	13370	99102	19
42	127060	156	996066	2.9	130994	158	869006	13399	99098	18
43	127993	155	996049	2.9	131944	158	868056	13427	99094	17
44	128925	155	996032	2.9	132893	158	867107	13456	99091	16
45	129854	154	996015	2.9	133839	157	866161	13485	99087	15
46	130781	154	995998	2.9	134784	157	865216	13514	99083	14
47	131706	154	995980	2.9	135726	157	864274	13543	99079	13
48	132630	153	995963	2.9	136667	156	863333	13572	99075	12
49	133551	153	995946	2.9	137605	156	862395	13600	99071	11
50	134470	153	995928	2.9	138542	156	861458	13629	99067	10
51	9.135387	152	9.995911	2.9	9.139476	155	10.860524	13658	99063	9
52	136303	152	995894	2.9	140409	155	859591	13687	99059	8
53	137216	152	995876	2.9	141340	155	858660	13716	99055	7
54	138128	152	995859	2.9	142269	154	857731	13744	99051	6
55	139037	151	995841	2.9	143196	154	856804	13773	99047	5
56	139944	151	995823	2.9	144121	154	855879	13802	99043	4
57	140850	151	995806	2.9	145044	153	854956	13831	99039	3
58	141754	150	995788	2.9	145966	153	854034	13860	99035	2
59	142655	150	995771	2.9	146885	153	853115	13889	99031	1
60	143555		995753		147803		852197	13917	99027	0
	Cosine.		Sine.		Cotang.		Tang.	N. cos.	N. sine.	′

82 Degrees.

N.	0	1	2	3	4	5	6	7	8	9
500	698970	9057	9144	9231	9317	9404	9491	9578	9664	9751
501	9838	9924	..11	..98	.184	.271	.358	.444	.531	.617
502	709704	0790	0877	0963	1050	1136	1222	1309	1395	1482
503	1568	1654	1741	1827	1913	1999	2086	2172	2258	2344
504	2431	2517	2603	2689	2775	2861	2947	3033	3119	3205
					86					
505	3291	3377	3463	3549	3635	3721	3807	3895	3979	4065
506	4151	4236	4322	4408	4494	4579	4665	4751	4837	4922
507	5008	5094	5179	5265	5350	5436	5522	5607	5693	5778
508	5864	5949	6035	6120	6206	6291	6376	6462	6547	6632
509	6718	6803	6888	6974	7059	7144	7229	7315	7400	7485
510	7570	7655	7740	7826	7910	7996	8081	8166	8251	8336
511	8421	8506	8591	8676	8761	8846	8931	9015	9100	9185
512	9270	9355	9440	9524	9609	9694	9779	9863	9948	..33
513	710117	0202	0287	0371	0456	0540	0625	0710	0794	0879
514	0963	1048	1132	1217	1301	1385	1470	1554	1639	1723
515	1807	1892	1976	2060	2144	2229	2313	2397	2481	2566
516	2650	2734	2818	2902	2986	3070	3154	3238	3326	3407
517	3491	3575	3659	3742	3826	3910	3994	4078	4162	4246
518	4330	4414	4497	4581	4665	4749	4833	4916	5000	5084
519	5167	5251	5335	5418	5502	5586	5669	5753	5836	5920
520	6003	6087	6170	6254	6337	6421	6504	6588	6671	6754
521	6838	6921	7004	7088	7171	7254	7338	7421	7504	7587
522	7671	7754	7837	7920	8003	8086	8169	8253	8336	8419
523	8502	8585	8668	8751	8834	8917	9000	9083	9165	9248
524	9331	9414	9497	9580	9663	9745	9828	9911	9994	..77
					82					
525	720159	0242	0325	0407	0490	0573	0655	0738	0821	0903
526	0986	1068	1151	1233	1316	1398	1481	1563	1646	1728
527	1811	1893	.975	2058	2140	2222	2305	2387	2469	2552
528	2634	2716	2798	2881	2963	3045	3127	3209	3291	3374
529	3456	3538	3620	3702	3784	3866	3948	4030	4112	4194
530	4276	4358	4440	4522	4604	4685	4767	4849	4931	5013
531	5095	5176	5258	5340	5422	5503	5585	5667	5748	5830
532	5912	5993	6075	6156	6238	6320	6401	6483	6564	6646
533	6727	6809	6890	6972	7053	7134	7216	7297	7379	7460
534	7541	7623	7704	7785	7866	7948	8029	8110	8191	8273
535	8354	8435	8516	8597	8678	8759	8841	8922	9003	9084
536	9165	9246	9327	9404	9489	9570	9651	9732	9813	9893
537	9974	..55	.136	.217	.298	.378	.459	.840	.621	.702
538	730782	0863	0944	1024	1105	1186	1266	1347	1428	1508
539	1589	1669	1750	1830	1911	1991	2072	2152	2233	2313
540	2394	2474	2555	2635	2715	2796	2876	2956	3037	3117
541	3197	3278	3358	3438	3518	3598	3679	3759	3839	3919
542	3999	4079	4160	4240	4320	4400	4480	4560	4640	4720
543	4800	4880	4960	5040	5120	5200	5279	5359	5439	5519
544	5599	5679	5759	5838	5918	5998	6078	6157	6237	6317
					80					
545	6397	6476	6556	6636	6715	6795	6874	6954	7034	7113
546	7193	7272	7352	7431	7511	7590	7670	7749	7829	7908
547	7987	8067	8146	8225	8305	8384	8463	8543	8622	8701
548	8781	8860	8939	9018	9097	9177	9256	9335	9414	9493
549	9572	9651	9731	9810	9889	9968	..47	.126	.205	.284

′	Sine.	D. 10″	Cosine.	D. 10″	Tang.	D. 10′	Cotang.	N. sine.	N. cos.	
0	9.194332	133	9.994620	3.3	9.199713	136	10.800287	15643	98769	60
1	195129	133	994600	3.3	200529	136	799471	15672	98764	59
2	195925	132	994580	3.3	201345	136	798655	15701	98760	58
3	196719	132	994560	3.4	202159	135	797841	15730	98755	57
4	197511	132	994540	3.4	202971	135	797029	15758	98751	56
5	198302	132	994519	3.4	203782	135	796218	15787	98746	55
6	199091	131	994499	3.4	204592	135	795408	15816	98741	54
7	199879	131	994479	3.4	205400	134	794600	15845	98737	53
8	200666	131	994459	3.4	206207	134	793793	15873	98732	52
9	201451	131	994438	3.4	207013	134	792987	15902	98728	51
10	202234	130	994418	3.4	207817	134	792183	15931	98723	50
11	9.203017	130	9.994397	3.4	9.208619	133	10.791381	15959	98718	49
12	203797	130	994377	3.4	209420	133	790580	15988	98714	48
13	204577	130	994357	3.4	210220	133	789780	16017	98709	47
14	205354	129	994336	3.4	211018	133	788982	16046	98704	46
15	206131	129	994316	3.4	211815	133	788185	16074	98700	45
16	206906	129	994295	3.4	212611	132	787389	16103	98695	44
17	207679	129	994274	3.5	213405	132	786595	16132	98690	43
18	208452	128	994254	3.5	214198	132	785802	16160	98686	42
19	209222	128	994233	3.5	214989	132	735011	16189	98681	41
20	209992	128	994212	3.5	215780	131	784220	16218	98676	40
21	9.210760	128	9.994191	3.5	9.216568	131	10.783432	16246	98671	39
22	211526	127	994171	3.5	217356	131	782644	16275	98667	38
23	212291	127	994150	3.5	218142	131	781858	16304	98662	37
24	213055	127	994129	3.5	218926	130	781074	16333	98657	36
25	213818	127	994108	3.5	219710	130	780290	16361	98652	35
26	214579	127	994087	3.5	220492	130	779508	16390	98648	34
27	215338	126	994066	3.5	221272	130	778728	16419	98643	33
28	216097	126	994045	3.5	222052	130	777948	16447	98638	32
29	216854	126	994024	3.5	222830	129	777170	16476	98633	31
30	217609	126	994003	3.5	223606	129	776394	16505	98629	30
31	9.218363	125	9.993981	3.5	9.224382	129	10.775618	16533	98624	29
32	219116	125	993960	3.5	225156	129	774844	16562	98619	28
33	219868	125	993939	3.5	225929	129	774071	16591	98614	27
34	220618	125	993918	3.5	226700	128	773300	16620	98609	26
35	221367	125	993896	3.6	227471	128	772529	16648	98604	25
36	222115	124	993875	3.6	228239	128	771761	16677	98600	24
37	222861	124	993854	3.6	229007	128	770993	16706	98595	23
38	223606	124	993832	3.6	229773	127	770227	16734	98590	22
39	224349	124	993811	3.6	230539	127	769461	16763	98585	21
40	225092	123	993789	3.6	231302	127	768698	16792	98580	20
41	9.225833	123	9.993768	3.6	9.232065	127	10.767935	16820	98575	19
42	226573	123	993746	3.6	232826	127	767174	16849	98570	18
43	227311	123	993725	3.6	233586	126	766414	16878	98565	17
44	228048	123	993703	3.6	234345	126	765655	16906	98561	16
45	228784	122	993681	3.6	235103	126	764897	16935	98556	15
46	229518	122	993660	3.6	235859	126	764141	16964	98551	14
47	230252	122	993638	3.6	236614	126	763386	16992	98546	13
48	230984	122	993616	3.6	237368	125	762632	17021	98541	12
49	231714	122	993594	3.7	238120	125	761880	17050	98536	11
50	232444	121	993572	3.7	238872	125	761128	17078	98531	10
51	9.233172	121	9.993550	3.7	9.239622	125	10.760378	17107	98526	9
52	233899	121	994528	3.7	240371	125	759629	17136	98521	8
53	234625	121	993506	3.7	241118	124	758882	17164	98516	7
54	235349	120	993484	3.7	241865	124	758135	17193	98511	6
55	236073	120	993462	3.7	242610	124	757390	17222	98506	5
56	236795	120	993440	3.7	243354	124	756646	17250	98501	4
57	237515	120	993418	3.7	244097	124	755903	17279	98496	3
58	238235	120	993396	3.7	244839	123	755161	17308	98491	2
59	238953	119	993374	3.7	245579	123	754421	17336	98486	1
60	239670		993351		246319		753681	17365	98481	0
	Cosine.		Sine.		Cotang.		Tang.	N. cos.	N.sine.	′

80 Degrees.

Sine.	D. 10″	Cosine.	D. 10″	Tang.	D. 10″	Cotang.	N.sine.	N. cos.	
9.239670	119	9.993351	3.7	9.246319	123	10.753681	17365	98481	60
240386	119	993329	3.7	247057	123	752943	17393	98476	59
241101	119	993307	3.7	247794	123	752206	17422	98471	58
241814	119	993285	3.7	248530	122	751470	17451	98466	57
242526	118	993262	3.7	249264	122	750736	17479	98461	56
243237	118	993240	3.7	249998	122	750002	17508	98455	55
243947	118	993217	3.8	250730	122	749270	17537	98450	54
244656	118	993195	3.8	251461	122	748539	17565	98445	53
245363	118	993172	3.8	252191	121	747809	17594	98440	52
246069	117	993149	3.8	252920	121	747080	17623	98435	51
246775	117	993127	3.8	253648	121	746352	17651	98430	50
9.247478	117	9.993104	3.8	9.254374	121	10.745626	17680	98425	49
248181	117	993081	3.8	255100	121	744900	17708	98420	48
248883	117	993059	3.8	255824	120	744176	17737	98414	47
249585	116	993036	3.8	256547	120	743453	17766	98409	46
250282	116	993013	3.8	257269	120	742731	17794	98404	45
250980	116	992990	3.8	257990	120	742010	17823	98399	44
251677	116	992967	3.8	258710	120	741290	17852	98394	43
252378	116	992944	3.8	259429	120	740571	17880	98389	42
253067	116	992921	3.8	260146	119	739854	17909	98383	41
253761	115	992898	3.8	260863	119	739137	17937	98378	40
9.254453	115	9.992875	3.8	9.261578	119	10.738422	17966	98373	39
255144	115	992852	3.8	262292	119	737708	17995	98368	38
255834	115	992829	3.9	263005	119	736995	18023	98362	37
256523	115	992806	3.9	263717	118	736283	18052	98357	36
257211	114	992783	3.9	264428	118	735572	18081	98352	35
257898	114	992759	3.9	265138	118	734862	18109	98347	34
258583	114	992736	3.9	265847	118	734153	18138	98341	33
259268	114	992713	3.9	266555	118	733445	18166	98336	32
259951	114	992690	3.9	267261	118	732739	18195	98331	31
260633	113	992666	3.9	267967	117	732033	18224	98325	30
9.261314	113	9.992643	3.9	9.268671	117	10.731329	18252	98320	29
261994	113	992619	3.9	269375	117	730625	18281	98315	28
262673	113	992596	3.9	270077	117	729923	18309	98310	27
263351	113	992572	3.9	270779	117	729221	18338	98304	26
264027	113	992549	3.9	271479	116	728521	18367	98299	25
264703	112	992525	3.9	272178	116	727822	18395	98294	24
265377	112	992501	3.9	272876	116	727124	18424	98288	23
266051	112	992478	4.0	273573	116	726427	18452	98283	22
266723	112	992454	4.0	274269	116	725731	18481	98277	21
267395	112	992430	4.0	274964	116	725036	18509	98272	20
9.268065	111	9.992406	4.0	9.275658	115	10.724342	18538	98267	19
268734	111	992382	4.0	276351	115	723649	18567	98261	18
269402	111	992359	4.0	277043	115	722957	18595	98256	17
270069	111	992335	4.0	277734	115	722266	18624	98250	16
270735	111	992311	4.0	278424	115	721576	18652	98245	15
271400	111	992287	4.0	279113	115	720887	18681	98240	14
272064	110	992263	4.0	279801	114	720199	18710	98234	13
272726	110	992239	4.0	280488	114	719512	18738	98229	12
273388	110	992214	4.0	281174	114	718826	18767	98223	11
274049	110	992190	4.0	281858	114	718142	18795	98218	10
9.274708	110	9.992166	4.0	9.282542	114	10.717458	18824	98212	9
275367	110	992142	4.0	283225	114	716775	18852	98207	8
276024	109	992117	4.1	283907	113	716093	18881	98201	7
276681	109	992093	4.1	284588	113	715412	18910	98196	6
277337	109	992069	4.1	285268	113	714732	18938	98190	5
277991	109	992044	4.1	285947	113	714053	18967	98185	4
278644	109	992020	4.1	286624	113	713376	18995	98179	3
279297	109	991996	4.1	287301	113	712699	19024	98174	2
279948	108	991971	4.1	287977	112	712023	19052	98168	1
280599		991947		288652		711348	19081	98163	0
Cosine.		Sine.		Cotang.		Tang.	N. cos.	N.sine.	′

79 Degrees.

'	Sine.	D. 10″	Cosine.	D. 10″	Tang.	D. 10'	Cotang.	N. sine.	N. cos.	
0	9.280599	108	9.991947	4.1	9.288652	112	10.711348	19081	98163	60
1	281248	108	991922	4.1	289326	112	710674	19109	98157	59
2	281897	108	991897	4.1	289999	112	710001	19138	98152	58
3	282544	108	991873	4.1	290671	112	709329	19167	98146	57
4	283190	108	991848	4.1	291342	112	708658	19195	98140	56
5	283836	107	991823	4.1	292013	111	707987	19224	98135	55
6	284480	107	991799	4.1	292682	111	707318	19252	98129	54
7	285124	107	991774	4.2	293350	111	706650	19281	98124	53
8	285766	107	991749	4.2	294017	111	705983	19309	98118	52
9	286408	107	991724	4.2	294684	111	705316	19338	98112	51
10	287048	107	991699	4.2	295349	111	704651	19366	98107	50
11	9.287687	106	9.991674	4.2	9.296013	111	10.703987	19395	98101	49
12	288326	106	991649	4.2	296677	110	703323	19423	98096	48
13	288964	106	991624	4.2	297339	110	702661	19452	98090	47
14	289600	106	991599	4.2	298001	110	701999	19481	98084	46
15	290236	106	991574	4.2	298662	110	701338	19509	98079	45
16	290870	106	991549	4.2	299322	110	700678	19538	98073	44
17	291504	105	991524	4.2	299980	110	700020	19566	98067	43
18	292137	105	991498	4.2	300638	109	699362	19595	98061	42
19	292768	105	991473	4.2	301295	109	698705	19623	98056	41
20	293399	105	991448	4.2	301951	109	698049	19652	98050	40
21	9.294029	105	9.991422	4.2	9.302607	109	10.697393	19680	98044	39
22	294658	105	991397	4.2	303261	109	696739	19709	98039	38
23	295286	104	991372	4.3	303914	109	696086	19737	98033	37
24	295913	104	991346	4.3	304567	109	695433	19766	98027	36
25	296539	104	991321	4.3	305218	108	694782	19794	98021	35
26	297164	104	991295	4.3	305869	108	694131	19823	98016	34
27	297788	104	991270	4.3	306519	108	693481	19851	98010	33
28	298412	104	991244	4.3	307168	108	692832	19880	98004	32
29	299034	104	991218	4.3	307815	108	692185	19908	97998	31
30	299655	103	991193	4.3	308463	108	691537	19937	97992	30
31	9.300276	103	9.991167	4.3	9.309109	107	10.690891	19965	97987	29
32	300895	103	991141	4.3	309754	107	690246	19994	97981	28
33	301514	103	991115	4.3	310398	107	689602	20022	97975	27
34	302132	103	991090	4.3	311042	107	688958	20051	97969	26
35	302748	103	991064	4.3	311685	107	688315	20079	97963	25
36	303364	102	991038	4.3	312327	107	687673	20108	97958	24
37	303979	102	991012	4.3	312967	107	687033	20136	97952	23
38	304593	102	990986	4.3	313608	106	686392	20165	97946	22
39	305207	102	990960	4.3	314247	106	685753	20193	97940	21
40	305819	102	990934	4.4	314885	106	685115	20222	97934	20
41	9.306430	102	9.990908	4.4	9.315523	106	10.684477	20250	97928	19
42	307041	102	990882	4.4	316159	106	683841	20279	97922	18
43	307650	101	990855	4.4	316795	106	683205	20307	97916	17
44	308259	101	990829	4.4	317430	106	682570	20336	97910	16
45	308867	101	990803	4.4	318064	105	681936	20364	97905	15
46	309474	101	990777	4.4	318697	105	681303	20393	97899	14
47	310080	101	990750	4.4	319329	105	680671	20421	97893	13
48	310685	101	990724	4.4	319961	105	680039	20450	97887	12
49	311289	100	990697	4.4	320592	105	679408	20478	97881	11
50	311893	100	990671	4.4	321222	105	678778	20507	97875	10
51	9.312495	100	9.990644	4.4	9.321851	105	10.678149	20535	97869	9
52	313097	100	990618	4.4	322479	104	677521	20563	97863	8
53	313698	100	990591	4.4	323106	104	676894	20592	97857	7
54	314297	100	990565	4.4	323733	104	676267	20620	97851	6
55	314897	100	990538	4.4	324358	104	675642	20649	97845	5
56	315495	100	990511	4.5	324983	104	675017	20677	97839	4
57	316092	99	990485	4.5	325607	104	674393	20706	97833	3
58	316689	99	990458	4.5	326231	104	673769	20734	97827	2
59	317284	99	990431	4.5	326853	104	673147	20763	97821	1
60	317879		990404		327475		672525	20791	97815	0
	Cosine.		Sine.		Cotang.		Tang.	N. cos.	N. sine.	'

78 Degrees.

N.	0	1	2	3	4	5	6	7	8	9
700	845098	5160	5222	5284	5346	5408	5470	5532	5594	5656
701	5718	5780	5842	5904	5966	6028	6090	6151	6213	6275
702	6337	6399	6461	6523	6585	6646	6708	6770	6832	6894
703	6955	7017	7079	7141	7202	7264	7326	7388	7449	7511
704	7573	7634	7676	7758	7819	7881	7943	8004	8066	8128
					62					
705	8189	8251	8312	8374	8435	8497	8559	8620	8682	8743
706	8805	8866	8928	8989	9051	9112	9174	9235	9297	9358
707	9419	9481	9542	9604	9665	9726	9788	9849	9911	9972
708	850033	0095	0156	0217	0279	0340	0401	0462	0524	0585
709	0646	0707	0769	0830	0891	0952	1014	1075	1136	1197
710	1258	1320	1381	1442	1503	1564	1625	1686	1747	1809
711	1870	1931	1992	2053	2114	2175	2236	2297	2358	2419
712	2480	2541	2602	2663	2724	2785	2846	2907	2968	3029
713	3090	3150	3211	3272	3333	3394	3455	3516	3577	3637
714	3698	3759	3820	3881	3941	4002	4063	4124	4185	4245
715	4306	4367	4428	4488	4549	4610	4670	4731	4792	4852
716	4913	4974	5034	5095	5156	5216	5277	5337	5398	5459
717	5519	5580	5640	5701	5761	5822	5882	5943	6003	6064
718	6124	6185	6245	6306	6366	6427	6487	6548	6608	6668
719	6729	6789	6850	6910	6970	7031	7091	7152	7212	7272
720	7332	7393	7453	7513	7574	7634	7694	7755	7815	7875
721	7935	7995	8056	8116	8176	8236	8297	8357	8417	8477
722	8537	8597	8657	8718	8778	8838	8898	8958	9018	9078
723	9138	9198	9258	9318	9379	9439	9499	95 .9	9619	9679
724	9739	9799	9859	9918	9978	..38	..98	.158	.218	.278
					60					
725	860338	0398	0458	0518	0578	0637	0697	0757	0817	0877
726	0937	0996	1056	1116	1176	1236	1295	1355	1415	1475
727	1534	1594	1654	1714	1773	1833	1893	1952	2012	2072
728	2131	2191	2251	2310	2370	2430	2489	2549	2608	2668
729	2728	2787	2847	2906	2966	3025	3085	3144	3204	3263
730	3323	3382	3442	3501	3561	3620	3680	3739	3799	3858
731	3917	3977	4036	4096	4155	4214	4274	4333	4392	4452
732	4511	4570	4630	4689	4148	4808	4867	4926	4985	5045
733	5104	5163	5222	5282	5341	5400	5459	5519	5578	5637
734	5696	5755	5814	5874	5933	5992	6051	6110	6169	6228
735	6287	6346	6405	6465	6524	6583	6642	6701	6760	6819
736	6878	6937	6996	7055	7114	7173	7232	7291	7350	7409
737	7467	7526	7585	7644	7703	7762	7821	7880	7939	7998
738	8056	8115	8174	8233	8292	8350	8409	8468	8527	8586
739	8644	8703	8762	8821	8879	8938	8997	9056	9114	9173
740	9232	9290	9349	9408	9466	9525	9584	9642	9701	9760
741	9818	9877	9935	9994	..53	.111	.170	.228	.287	.345
742	870404	0462	0521	0579	0638	0696	0755	0813	0872	0930
743	0989	1047	1106	1164	1223	1281	1339	1398	1456	1515
744	1573	1631	1690	1748	1806	1865	1923	1981	2040	2098
					59					
745	2156	2215	2273	2331	2389	2448	2506	2564	2622	2681
746	2739	2797	2855	2913	2972	3030	3088	3146	3204	3262
747	3321	3379	3437	3495	3553	3611	3669	3727	3785	3844
748	3902	3960	4018	4076	4134	4192	4250	4308	4360	4424
749	4482	4540	4598	4656	4714	4772	4830	4888	4945	5003

′	Sine.	D. 10″	Cosine.	D. 10″	Tang.	D. 10″	Cotang.	N.sine	N. cos.	
0	9.352088	91.1	9.988724	4.9	9.363364	96.0	10.636636	22495	97437	60
1	352635	91.0	988695	4.9	363940	95.9	636060	22523	97430	59
2	353181	90.9	988666	4.9	364515	95.8	635485	22552	97424	58
3	353726	90.8	988636	4.9	365090	95.7	634910	22580	97417	57
4	354271	90.7	988607	4.9	365664	95.5	634336	22608	97411	56
5	354815	90.5	988578	4.9	366237	95.4	633763	22637	97404	55
6	355358	90.4	988548	4.9	366810	95.3	633190	22665	97398	54
7	355901	90.3	988519	4.9	367382	95.2	632618	22693	97391	53
8	356443	90.2	988489	4.9	367953	95.1	632047	22722	97384	52
9	356984	90.1	988460	4.9	368524	95.0	631476	22750	97378	51
10	357524	89.9	988430	4.9	369094	94.9	630906	22778	97371	50
11	9.358064	89.8	9.988401	4.9	9.369663	94.8	10.630337	22807	97365	49
12	358603	89.7	988371	4.9	370232	94.6	629768	22835	97358	48
13	359141	89.6	988342	4.9	370799	94.5	629201	22863	97351	47
14	359678	89.5	988312	5.0	371367	94.4	628633	22892	97345	46
15	360215	89.3	988282	5.0	371933	94.3	628067	22920	97338	45
16	360752	89.2	988252	5.0	372499	94.2	627501	22948	97331	44
17	361287	89.1	988223	5.0	373064	94.1	626936	22977	97325	43
18	361822	89.0	988193	5.0	373629	94.0	626371	23005	97318	42
19	362356	88.9	988163	5.0	374193	93.9	625807	23033	97311	41
20	362889	88.8	988133	5.0	374756	93.8	625244	23062	97304	40
21	9.363422	88.7	9.988103	5.0	9.375319	93.7	10.624681	23090	97298	39
22	363954	88.5	988073	5.0	375881	93.5	624119	23118	97291	38
23	364485	88.4	988043	5.0	376442	93.4	623558	23146	97284	37
24	365016	88.3	988013	5.0	377003	93.3	622997	23175	97278	36
25	365546	88.2	987983	5.0	377563	93.2	622437	23203	97271	35
26	366075	88.1	987953	5.0	378122	93.1	621878	23231	97264	34
27	366604	88.0	987922	5.0	378681	93.0	621319	23260	97257	33
28	367131	87.9	987892	5.0	379239	92.9	620761	23288	97251	32
29	367659	87.7	987862	5.0	379797	92.8	620203	23316	97244	31
30	368185	87.6	987832	5.1	380354	92.7	619646	23345	97237	30
31	9.368711	87.5	9.987801	5.1	9.380910	92.6	10.619090	23373	97230	29
32	369236	87.4	987771	5.1	381466	92.5	618534	23401	97223	28
33	369761	87.3	987740	5.1	382020	92.4	617980	23429	97217	27
34	370285	87.2	987710	5.1	382575	92.3	617425	23458	97210	26
35	370808	87.1	987679	5.1	383129	92.2	616871	23486	97203	25
36	371330	87.0	987649	5.1	383682	93.1	616318	23514	97196	24
37	371852	86.9	987618	5.1	384234	92.0	615766	23542	97189	23
38	372373	86.7	987588	5.1	384786	91.9	615214	23571	97182	22
39	372894	86.6	987557	5.1	385337	91.8	614663	23599	97176	21
40	373414	86.5	987526	5.1	385888	91.7	614112	23627	97169	20
41	9.373933	86.4	9.987496	5.1	9.386438	91.5	10.613562	23656	97162	19
42	374452	86.3	987465	5.1	386987	91.4	613013	23684	97155	18
43	374970	86.2	987434	5.1	387536	91.3	612464	23712	97148	17
44	375487	86.1	987403	5.2	388084	91.2	611916	23740	97141	16
45	376003	86.0	987372	5.2	388631	91.1	611369	23769	97134	15
46	376519	85.9	987341	5.2	389178	91.0	610822	23797	97127	14
47	377035	85.8	987310	5.2	389724	90.9	610276	23825	97120	13
48	377549	85.7	987279	5.2	390270	90.8	609730	23853	97113	12
49	378063	85.6	987248	5.2	390815	90.7	609185	23882	97106	11
50	378577	85.4	987217	5.2	391360	90.6	608640	23910	97100	10
51	9.379089	85.3	9.987186	5.2	9.391903	90.5	10.608097	23938	97093	9
52	379601	85.2	987155	5.2	392447	90.4	607553	23966	97086	8
53	380113	85.1	987124	5.2	392989	90.3	607011	23995	97079	7
54	380624	85.0	987092	5.2	393531	90.2	606469	24023	97072	6
55	381134	84.9	987061	5.2	394073	90.1	605927	24051	97065	5
56	381643	84.8	987030	5.2	394614	90.0	605386	24079	97058	4
57	382152	84.7	986998	5.2	395154	89.9	604846	24108	97051	3
58	382661	84.6	986967	5.2	395694	89.8	604306	24136	97044	2
59	383168	84.5	986936	5.2	396233	89.7	603767	24164	97037	1
60	383675		986904		396771		603229	24192	97030	0
	Cosine.		Sine.		Cotang.		Tang.	N. cos.	N.sine.	′

76 Degrees.

′	Sine.	D. 10″	Cosine.	D. 10″	Tang.	D. 10″	Cotang.	N. sine.	N. cos.	
0	9.383675	84.4	9.986904	5.2	9.396771	89.6	10.603229	24192	97030	60
1	384182	84.3	986873	5.3	397309	89.6	602691	24220	97023	59
2	384687	84.2	986841	5.3	397846	89.5	602154	24249	97015	58
3	385192	84.1	986809	5.3	398383	89.4	601617	24277	97008	57
4	385697	84.0	986778	5.3	398919	89.3	601081	24305	97001	56
5	386201	83.9	986746	5.3	399455	89.2	600545	24333	96994	55
6	386701	83.8	986714	5.3	399990	89.1	600010	24362	96987	54
7	387207	83.7	986683	5.3	400524	89.0	599476	24390	96980	53
8	387709	83.6	986651	5.3	401058	88.9	598942	24418	96973	52
9	388210	83.5	986619	5.3	401591	88.8	598409	24446	96966	51
10	388711	83.4	986587	5.3	402124	88.7	597876	24474	96959	50
11	9.389211	83.3	9.986555	5.3	9.402656	88.6	10.597344	24503	96952	49
12	389711	83.2	986523	5.3	403187	88.5	596813	24531	96945	48
13	390210	83.1	986491	5.3	403718	88.4	596282	24559	96937	47
14	390708	83.0	986459	5.3	404249	88.3	595751	24587	96930	46
15	391206	82.8	986427	5.3	404778	88.2	595222	24615	96923	45
16	391703	82.7	986395	5.3	405308	88.1	594692	24644	96916	44
17	392199	82.6	986363	5.4	405836	88.0	594164	24672	96909	43
18	392695	82.5	986331	5.4	406364	87.9	593636	24700	96902	42
19	393191	82.4	986299	5.4	406892	87.8	593108	24728	96894	41
20	393685	82.3	986266	5.4	407419	87.7	592581	24756	96887	40
21	9.394179	82.2	9.986234	5.4	9.407945	87.6	10.592055	24784	96880	39
22	394673	82.1	986202	5.4	408471	87.5	591529	24813	96873	38
23	395166	82.0	986169	5.4	408997	87.4	591003	24841	96866	37
24	395658	81.9	986137	5.4	409521	87.4	590479	24869	96858	36
25	396150	81.8	986104	5.4	410045	87.3	589955	24897	96851	35
26	396641	81.7	986072	5.4	410569	87.2	589431	24925	96844	34
27	397132	81.7	986039	5.4	411092	87.1	588908	24954	96837	33
28	397621	81.6	986007	5.4	411615	87.0	588385	24982	96829	32
29	398111	81.5	985974	5.4	412137	86.9	587863	25010	96822	31
30	398600	81.4	985942	5.4	412658	86.8	587342	25038	96815	30
31	9.399088	81.3	9.985909	5.5	9.413179	86.7	10.586821	25066	96807	29
32	399575	81.2	985876	5.5	413699	86.6	586301	25094	96800	28
33	400062	81.1	985843	5.5	414219	86.5	585781	25122	96793	27
34	400549	81.0	985811	5.5	414738	86.4	585262	25151	96786	26
35	401035	80.9	985778	5.5	415257	86.4	584743	25179	96778	25
36	401520	80.8	985745	5.5	415775	86.3	584225	25207	96771	24
37	402005	80.7	985712	5.5	416293	86.2	583707	25235	96764	23
38	402489	80.6	985679	5.5	416810	86.1	583190	25263	96756	22
39	402972	80.5	985646	5.5	417326	86.0	582674	25291	96749	21
40	403455	80.4	985613	5.5	417842	85.9	582158	25320	96742	20
41	9.403938	80.3	9.985580	5.5	9.418358	85.8	10.581642	25348	96734	19
42	404420	80.2	985547	5.5	418873	85.7	581127	25376	96727	18
43	404901	80.1	985514	5.5	419387	85.6	580613	25404	96719	17
44	405382	80.0	985480	5.5	419901	85.5	580099	25432	96712	16
45	405862	79.9	985447	5.5	420415	85.5	579585	25460	96705	15
46	406341	79.8	985414	5.6	420927	85.4	579073	25488	96697	14
47	406820	79.7	985380	5.6	421440	85.3	578560	25516	96690	13
48	407299	79.6	985347	5.6	421952	85.2	578048	25545	96682	12
49	407777	79.5	985314	5.6	422463	85.1	577537	25573	96675	11
50	408254	79.4	985280	5.6	422974	85.0	577026	25601	96667	10
51	9.408731	79.4	9.985247	5.6	9.423484	84.9	10.576516	25629	96660	9
52	409207	79.3	985213	5.6	423993	84.8	576007	25657	96653	8
53	409682	79.2	985180	5.6	424503	84.8	575497	25685	96645	7
54	410157	79.1	985146	5.6	425011	84.7	574989	25713	96638	6
55	410632	79.0	985113	5.6	425519	84.6	574481	25741	96630	5
56	411105	78.9	985079	5.6	426027	84.5	573973	25769	96623	4
57	411579	78.8	985045	5.6	426534	84.4	573466	25798	96615	3
58	412052	78.7	985011	5.6	427041	84.3	572959	25826	96608	2
59	412524	78.6	984978	5.6	427547	84.3	572453	25854	96600	1
60	412996		984944		428052		571948	25882	96593	0
	Cosine.		Sine.		Cotang.		Tang.	N. cos.	N. sine.	′

Log. Sines and Tangents. (15°) Natural Sines. TABLE II.

′	Sine.	D. 10″	Cosine.	D. 10″	Tang.	D. 10″	Cotang.	N. sine	N. cos.	
0	9.412996	78.5	9.984944	5.7	9.428052	84.2	10.571948	25882	96593	60
1	413467	78.4	984910	5.7	428557	84.1	571443	25910	96585	59
2	413938	78.3	984876	5.7	429062	84.0	570938	25938	96578	58
3	414408	78.3	984842	5.7	429566	83.9	570434	25966	96570	57
4	414878	78.2	984808	5.7	430070	83.8	569930	25994	96562	56
5	415347	78.1	984774	5.7	430573	83.8	569427	26022	96555	55
6	415815	78.0	984740	5.7	431075	83.7	568925	26050	96547	54
7	416283	77.9	984706	5.7	431577	83.6	568423	26079	96540	53
8	416751	77.8	984672	5.7	432079	83.5	567921	26107	96532	52
9	417217	77.7	984637	5.7	432580	83.4	567420	26135	96524	51
10	417684	77.6	984603	5.7	433080	83.3	566920	26163	96517	50
11	9.418150	77.5	9.984569	5.7	9.433580	83.2	10.566420	26191	96509	49
12	418615	77.4	984535	5.7	434080	83.2	565920	26219	96502	48
13	419079	77.3	984500	5.7	434579	83.1	565421	26247	96494	47
14	419544	77.3	984466	5.7	435078	83.0	564922	26275	96486	46
15	420007	77.2	984432	5.8	435576	82.9	564424	26303	96479	45
16	420470	77.1	984397	5.8	436073	82.8	563927	26331	96471	44
17	420933	77.0	984363	5.8	436570	82.8	563430	26359	96463	43
18	421395	76.9	984328	5.8	437067	82.7	562933	26387	96456	42
19	421857	76.8	984294	5.8	437563	82.6	562437	26415	96448	41
20	422318	76.7	984259	5.8	438059	82.5	561941	26443	96440	40
21	9.422778	76.7	9.984224	5.8	9.438554	82.4	10.561446	26471	96433	39
22	423238	76.6	984190	5.8	439048	82.3	560952	26500	96425	38
23	423697	76.5	984155	5.8	439543	82.3	560457	26528	96417	37
24	424156	76.4	984120	5.8	440036	82.2	559964	26556	96410	36
25	424615	76.3	984085	5.8	440529	82.1	559471	26584	96402	35
26	425073	76.2	984050	5.8	441022	82.0	558978	26612	96394	34
27	425530	76.1	984015	5.8	441514	81.9	558486	26640	96386	33
28	425987	76.0	983981	5.8	442006	81.9	557994	26668	96379	32
29	426443	76.0	983946	5.8	442497	81.8	557503	26696	96371	31
30	426899	75.9	983911	5.8	442988	81.7	557012	26724	96363	30
31	9.427354	75.8	9.983875	5.8	9.443479	81.6	10.556521	26752	96355	29
32	427809	75.7	983840	5.9	443968	81.6	556032	26780	96347	28
33	428263	75.6	983805	5.9	444458	81.5	555542	26808	96340	27
34	428717	75.5	983770	5.9	444947	81.4	555053	26836	96332	26
35	429170	75.4	983735	5.9	445435	81.3	554565	26864	96324	25
36	429623	75.3	983700	5.9	445923	81.2	554077	26892	96316	24
37	430075	75.2	983664	5.9	446411	81.2	553589	26920	96308	23
38	430527	75.2	983629	5.9	446898	81.1	553102	26948	96301	22
39	430978	75.1	983594	5.9	447384	81.0	552616	26976	96293	21
40	431429	75.0	983558	5.9	447870	80.9	552130	27004	96285	20
41	9.431879	74.9	9.983523	5.9	9.448356	80.9	10.551644	27032	96277	19
42	432329	74.9	983487	5.9	448841	80.8	551159	27060	96269	18
43	432778	74.8	983452	5.9	449326	80.7	550674	27088	96261	17
44	433226	74.7	983416	5.9	449810	80.6	550190	27116	96253	16
45	433675	74.6	983381	5.9	450294	80.6	549706	27144	96246	15
46	434122	74.5	983345	5.9	450777	80.5	549223	27172	96238	14
47	434569	74.4	983309	5.9	451260	80.4	548740	27200	96230	13
48	435016	74.4	983273	6.0	451743	80.3	548257	27228	96222	12
49	435462	74.3	983238	6.0	452225	80.2	547775	27256	96214	11
50	435908	74.2	983202	6.0	452706	80.2	547294	27284	96206	10
51	9.436353	74.1	9.983166	6.0	9.453187	80.1	10.546813	27312	96198	9
52	436798	74.0	983130	6.0	453668	80.0	546332	27340	96190	8
53	437242	74.0	983094	6.0	454148	79.9	545852	27368	96182	7
54	437686	73.9	983058	6.0	454628	79.9	545372	27396	96174	6
55	438129	73.8	983022	6.0	455107	79.8	544893	27424	96166	5
56	438572	73.7	982986	6.0	455586	79.7	544414	27452	96158	4
57	439014	73.6	982950	6.0	456064	79.6	543936	27480	96150	3
58	439456	73.6	982914	6.0	456542	79.6	543458	27508	96142	2
59	439897	73.5	982878	6.0	457019	79.5	542981	27536	96134	1
60	440338		982842		457496		542504	27564	96126	0
	Cosine.		Sine.		Cotang.		Tang.	N. cos.	N.sine.	′

74 Degrees.

N.	0	1	2	3	4	5	6	7	8	9
900	954243	4291	4839	4387	4435	4484	4532	4580	4628	4677
901	4725	4773	4821	4869	4918	4966	5014	5062	5110	5158
902	5207	5255	5303	5351	5399	5447	5495	5543	5592	5640
903	5688	5736	5784	5832	5880	5928	5976	6024	6072	6120
904	6168	6216	6265	6313	6351 48	6409	6457	6505	6553	6601
905	6649	6697	6745	6793	6840	6888	6936	6984	7032	7080
906	7128	7176	7224	7272	7320	7368	7416	7464	7512	7559
907	7607	7655	7703	7751	7799	7847	7894	7942	7990	8038
908	8086	8134	8181	8229	8277	8325	8373	8421	8468	8516
909	8564	8612	8659	8707	8755	8803	8850	8898	8946	8994
910	9041	9089	9137	9185	9232	9280	9328	9375	9423	9471
911	9518	9566	9614	9661	9709	9757	9804	9852	9900	9947
912	9995	..42	..90	.138	.185	.233	.280	.328	.376	.423
913	960471	0518	0566	0613	0661	0709	0756	0804	0851	0899
914	0946	0994	1041	1089	1136	1184	1231	1279	1326	1374
915	1421	1469	1516	1563	1611	1658	1706	1753	1801	1848
916	1895	1943	1990	2038	2085	2132	2180	2227	2275	2322
917	2369	2417	2464	2511	2559	2606	2653	2701	2748	2795
918	2843	2890	2937	2985	3032	3079	3126	3174	3221	3268
919	3316	3363	3410	3457	3504	3552	3599	3646	3693	3741
920	3788	3835	3882	3929	3977	4024	4071	4118	4165	4212
921	4260	4307	4354	4401	4448	4495	4542	4590	4637	4684
922	4731	4778	4825	4872	4919	4966	5013	5061	5108	5155
923	5202	5249	5296	5343	5390	5437	5484	5531	5578	5625
924	5672	5719	5766	5813	5860	5907	5954	6001	6048	6095
925	6142	6189	6236	6283	6329	6376	6423	6470	6517	6564
926	6611	6658	6705	6752	6799	6845	6892	6939	6986	7033
927	7080	7127	7173	7220	7267	7314	7361	7408	7454	7501
928	7548	7595	7642	7688	7735	7782	7829	7875	7922	7969
929	8016	8062	8109	8156	8203	8249	8296	8343	8390	8436
930	8483	8530	8576	8623	8670	8716	8763	8810	8856	8903
931	8950	8996	9043	9090	9136	9183	9229	9276	9323	9369
932	9416	9463	9509	9556	9602	9649	9695	9742	9789	9835
933	9882	9928	9975	..21	..68	.114	.161	.207	.254	.300
934	970347	0393	0440	0486	0533	0579	0626	0672	0719	0765
935	0812	0858	0904	0951	0997	1044	1090	1137	1183	1229
936	1276	1322	1369	1415	1461	1508	1554	1601	1647	1693
937	1740	1786	1832	1879	1925	1971	2018	2064	2110	2157
938	2203	2249	2295	2342	2388	2434	2481	2527	2573	2619
939	2666	2712	2758	2804	2851	2897	2943	2989	3035	3082
940	3128	3174	3220	3266	3313	3359	3405	3451	3497	3543
941	3590	3636	3682	3728	3774	3820	3866	3913	3959	4005
942	4051	4097	4143	4189	4235	4281	4327	4374	4420	4466
943	4512	4558	4604	4650	4696	4742	4788	4834	4880	4926
944	4972	5018	5064	5110	5156 46	5202	5248	5294	5340	5386
945	5432	5478	5524	5570	5616	5662	5707	5753	5799	5845
946	5891	5937	5983	6029	6075	6121	6167	6212	6258	6304
947	6350	6396	6442	6488	6533	6579	6625	6671	6717	6763
948	6803	6854	6900	6946	6992	7037	7083	7129	7175	7220
949	7266	7312	7358	7403	7449	7495	7541	7586	7632	7678

'	Sine.	D. 10"	Cosine.	D. 10"	Tang.	D. 10"	Cotang.	N. sine.	N. cos.	
0	9.465935	68.8	9.980596	6.4	9.485339	75.3	10.514661	29237	95630	60
1	466348	68.8	980558	6.4	485791	75.2	514209	29265	95622	59
2	466761	68.7	980519	6.5	486242	75.1	513758	29293	95613	58
3	467173	68.6	980480	6.5	486693	75.1	513307	29321	95605	57
4	467585	68.5	980442	6.5	487143	75.0	512857	29348	95596	56
5	467996	68.5	980403	6.5	487593	74.9	512407	29376	95588	55
6	468407	68.4	980364	6.5	488043	74.9	511957	29404	95579	54
7	468817	68.3	980325	6.5	488492	74.8	511508	29432	95571	53
8	469227	68.3	980286	6.5	488941	74.7	511059	29460	95562	52
9	469637	68.2	980247	6.5	489390	74.7	510610	29487	95554	51
10	470046	68.1	980208	6.5	489838	74.6	510162	29515	95545	50
11	9.470455	68.0	9.980169	6.5	9.490286	74.6	10.509714	29543	95536	49
12	470863	68.0	980130	6.5	490733	74.5	509267	29571	95528	48
13	471271	67.9	980091	6.5	491180	74.4	508820	29599	95519	47
14	471679	67.8	980052	6.5	491627	74.4	508373	29626	95511	46
15	472086	67.8	980012	6.5	492073	74.3	507927	29654	95502	45
16	472492	67.7	979973	6.5	492519	74.3	507481	29682	95493	44
17	472898	67.6	979934	6.6	492965	74.2	507035	29710	95485	43
18	473304	67.6	979895	6.6	493410	74.1	506590	29737	95476	42
19	473710	67.5	979855	6.6	493854	74.0	506146	29765	95467	41
20	474115	67.4	979816	6.6	494299	74.0	505701	29793	95459	40
21	9.474519	67.4	9.979776	6.6	9.494743	74.0	10.505257	29821	95450	39
22	474923	67.3	979737	6.6	495186	73.9	504814	29849	95441	38
23	475327	67.2	979697	6.6	495630	73.8	504370	29876	95433	37
24	475730	67.2	979658	6.6	496073	73.7	503927	29904	95424	36
25	476133	67.1	979618	6.6	496515	73.7	503485	29932	95415	35
26	476536	67.0	979579	6.6	496957	73.6	503043	29960	95407	34
27	476938	66.9	979539	6.6	497399	73.6	502601	29987	95398	33
28	477340	66.9	979499	6.6	497841	73.5	502159	30015	95389	32
29	477741	66.8	979459	6.6	468282	73.4	501718	30043	95380	31
30	478142	66.7	979420	6.6	498722	73.4	501278	30071	95372	30
31	9.478542	66.7	9.979380	6.6	9.499163	73.3	10.500837	30098	95363	29
32	478942	66.6	979340	6.6	499603	73.3	500397	30126	95354	28
33	479342	66.5	979300	6.7	500042	73.2	499958	30154	95345	27
34	479741	66.5	979260	6.7	500481	73.1	499519	30182	95337	26
35	480140	66.4	979220	6.7	500920	73.1	499080	30209	95328	25
36	480539	66.3	979180	6.7	501359	73.0	498641	30237	95319	24
37	480937	66.3	979140	6.7	501797	73.0	498203	30265	95310	23
38	481334	66.2	979100	6.7	502235	72.9	497765	30292	95301	22
39	481731	66.1	979059	6.7	502672	72.8	497328	30320	95293	21
40	482128	66.1	979019	6.7	503109	72.8	496891	30348	95284	20
41	9.482525	66.0	9.978979	6.7	9.503546	72.7	10.496454	30376	95275	19
42	482921	65.9	978939	6.7	503982	72.7	496018	30403	95266	18
43	483316	65.9	978898	6.7	504418	72.6	495582	30431	95257	17
44	483712	65.8	978858	6.7	504854	72.5	495146	30459	95248	16
45	484107	65.7	978817	6.7	505289	72.5	494711	30486	95240	15
46	484501	65.7	978777	6.7	505724	72.4	494276	30514	95231	14
47	484895	65.6	978736	6.7	506159	72.4	493841	30542	95222	13
48	485289	65.5	978696	6.8	506593	72.3	493407	30570	95213	12
49	485682	65.5	978655	6.8	507027	72.2	492973	30597	95204	11
50	486075	65.4	978615	6.8	507460	72.2	492540	30625	95195	10
51	9.486467	66.3	9.978574	6.8	9.507893	72.1	10.492107	30653	95186	9
52	486860	65.3	978533	6.8	508326	72.1	491674	30680	95177	8
53	487251	65.2	978493	6.8	508759	72.0	491241	30708	95168	7
54	487643	65.1	978452	6.8	509191	71.9	490809	30736	95159	6
55	488034	65.1	978411	6.8	509622	71.9	490378	30763	95150	5
56	488424	65.0	978370	6.8	510054	71.8	489946	30791	95142	4
57	488814	65.0	978329	6.8	510485	71.8	489515	30819	95133	3
58	489204	64.9	978288	6.8	510916	71.7	489084	30846	95124	2
59	489593	64.8	978247	6.8	511346	71.6	488654	30874	95115	1
60	489982		978206		511776		488224	3090[illegible]	95106	0
	Cosine.		Sine.		Cotang.		Tang.	N. cos.	N. sine.	'

72 Degrees.

'	Sine.	D. 10"	Cosine.	D. 10"	Tang.	D. 10"	Cotang.	N. sine.	N. cos.	
0	9.489982	64.8	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	60
1	490371	64.8	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	59
2	490759	64.7	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	58
3	491147	64.6	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	57
4	491535	64.6	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	56
5	491922	64.5	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	55
6	492308	64.4	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	54
7	492695	64.4	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	53
8	493081	64.3	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	52
9	493466	64.2	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	51
10	493851	64.2	[illegible]	6.9	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	50
11	9.494236	64.1	9.977752	6.9	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	49
12	494621	64.1	977711	6.9	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	48
13	495005	64.0	977669	6.9	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	47
14	495388	63.9	977628	6.9	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	46
15	495772	63.9	977586	6.9	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	45
16	496154	63.8	977544	7.0	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	44
17	496537	63.7	977503	7.0	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	43
18	496919	63.7	977461	7.0	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	42
19	497301	63.6	977419	7.0	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	41
20	497682	63.6	977377	7.0	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	40
21	9.498064	63.5	9.977335	7.0	[illegible]	70.4	[illegible]	[illegible]	[illegible]	39
22	498444	63.4	977293	7.0	[illegible]	70.3	[illegible]	[illegible]	[illegible]	38
23	498825	63.4	977251	7.0	[illegible]	70.3	[illegible]	[illegible]	[illegible]	37
24	499204	63.3	977209	7.0	[illegible]	70.3	[illegible]	[illegible]	[illegible]	36
25	499584	63.2	977167	7.0	[illegible]	70.2	[illegible]	[illegible]	[illegible]	35
26	499963	63.2	977125	7.0	[illegible]	70.2	[illegible]	[illegible]	[illegible]	34
27	500342	63.1	977083	7.0	[illegible]	70.1	[illegible]	[illegible]	[illegible]	33
28	500721	63.1	977041	7.0	[illegible]	70.1	[illegible]	[illegible]	[illegible]	32
29	501099	63.0	976999	7.0	[illegible]	70.0	[illegible]	[illegible]	[illegible]	31
30	501476	62.9	976957	7.0	[illegible]	69.9	[illegible]	31730	94832	30
31	9.501854	62.9	9.976914	7.0	[illegible]	69.9	[illegible]	31758	94823	29
32	502231	62.8	976872	7.1	525359	69.8	474641	31786	94814	28
33	502607	62.8	976830	7.1	525778	69.8	474222	31813	94805	27
34	502984	62.7	976787	7.1	526197	69.7	473803	31841	94795	26
35	503360	62.6	976745	7.1	526615	69.7	473385	31868	94786	25
36	503735	62.6	976702	7.1	527033	69.6	472967	31896	94777	24
37	504110	62.5	976660	7.1	527451	69.6	472549	31923	94768	23
38	504485	62.5	976617	7.1	527868	69.5	472132	31951	94758	22
39	504860	62.4	976574	7.1	528285	69.5	471715	31979	94749	21
40	505234	62.3	976532	7.1	528702	69.4	471298	32006	94740	20
41	9.505608	62.3	9.976489	7.1	9.529119	69.3	10.470881	32034	94730	19
42	505981	62.2	976446	7.1	529535	69.3	470465	32061	94721	18
43	506354	62.2	976404	7.1	529950	69.3	470050	32089	94712	17
44	506727	62.1	976361	7.1	530366	69.2	469634	32116	94702	16
45	507099	62.0	976318	7.1	530781	69.1	469219	32144	94693	15
46	507471	62.0	976275	7.1	531196	69.1	468804	32171	94684	14
47	507843	61.9	976232	7.2	531611	69.0	468389	32199	94674	13
48	508214	61.9	976189	7.2	532025	69.0	4679.5	32227	94665	12
49	508585	61.8	976146	7.2	532439	68.9	467561	32254	94656	11
50	508956	61.8	976103	7.2	532853	68.9	467147	32282	94646	10
51	9.509326	61.7	9.976060	7.2	9.533266	68.8	10.466734	32309	94637	9
52	509696	61.6	976017	7.2	533679	68.8	466321	32337	94627	8
53	510065	61.6	975974	7.2	534092	68.7	465908	32364	94618	7
54	510434	61.5	975930	7.2	534504	68.7	465496	32392	94609	6
55	510803	61.5	975887	7.2	534916	68.6	465084	32419	94599	5
56	511172	61.4	975844	7.2	535328	68.6	464672	32447	94590	4
57	511540	61.3	975800	7.2	535739	68.5	464261	32474	94580	3
58	511907	61.3	975757	7.2	536150	68.5	463850	32502	94571	2
59	512275	61.2	975714	7.2	536561	68.4	463439	32529	94561	1
60	512642		975670		536972		463028	32557	94552	0
	Cosine.		Sine.		Cotang.		Tang.	N. cos.	N. sine.	'

71 Degrees.

′	Sine.	D. 10″	Cosine.	D. 10″	Tang.	D. 10″	Cotang.	N. sine.	N. cos.	
0	9.512642	61.2	9.975670	7.3	9.536972	68.4	10.463028	32557	94552	60
1	513009	61.1	975627	7.3	537382	68.3	462618	32584	94542	59
2	513375	61.1	975583	7.3	537792	68.3	462208	32612	94533	58
3	513741	61.0	975539	7.3	538202	68.2	461798	32639	94523	57
4	514107	60.9	975496	7.3	538611	68.2	461389	32667	94514	56
5	514472	60.9	975452	7.3	539020	68.1	460980	32694	94504	55
6	514837	60.8	975408	7.3	539429	68.1	460571	32722	94495	54
7	515202	60.8	975365	7.3	539837	68.0	460163	32749	94485	53
8	515566	60.7	975321	7.3	540245	68.0	459755	32777	94476	52
9	515930	60.7	975277	7.3	540653	67.9	459347	32804	94466	51
10	516294	60.6	975233	7.3	541061	67.9	458939	32832	94457	50
11	9.516657	60.5	9.975189	7.3	9.541468	67.8	10.458532	32859	94447	49
12	517020	60.5	975145	7.3	541875	67.8	458125	32887	94438	48
13	517382	60.4	975101	7.3	542281	67.7	457719	32914	94428	47
14	517745	60.4	975057	7.3	542688	67.7	457312	32942	94418	46
15	518107	60.3	975013	7.3	543094	67.6	456906	32969	94409	45
16	518468	60.3	974969	7.4	543499	67.6	456501	32997	94399	44
17	518829	60.2	974925	7.4	543905	67.5	456095	33024	94390	43
18	519190	60.1	974880	7.4	544310	67.5	455690	33051	94380	42
19	519551	60.1	974836	7.4	544715	67.4	455285	33079	94370	41
20	519911	60.0	974792	7.4	545119	67.4	454881	33106	94361	40
21	9.520271	60.0	9.974748	7.4	9.545524	67.3	10.454476	33134	94351	39
22	520631	59.9	974703	7.4	545928	67.3	454072	33161	94342	38
23	520990	59.9	974659	7.4	546331	67.2	453669	33189	94332	37
24	521349	59.8	974614	7.4	546735	67.2	453265	33216	94322	36
25	521707	59.8	974570	7.4	547138	67.1	452862	33244	94313	35
26	522066	59.7	974525	7.4	547540	67.1	452460	33271	94303	34
27	522424	59.6	974481	7.4	547943	67.0	452057	33298	94293	33
28	522781	59.6	974436	7.4	548345	67.0	451655	33326	94284	32
29	523138	59.5	974391	7.4	548747	66.9	451253	33353	94274	31
30	523495	59.5	974347	7.5	549149	66.9	450851	33381	94264	30
31	9.523852	59.4	9.974302	7.5	9.549550	66.8	10.450450	33408	94254	29
32	524208	59.4	974257	7.5	549951	66.8	450049	33436	94245	28
33	524564	59.3	974212	7.5	550352	66.7	449648	33463	94235	27
34	524920	59.3	974167	7.5	550752	66.7	449248	33490	94225	26
35	525275	59.2	974122	7.5	551152	66.6	448848	33518	94215	25
36	525630	59.1	974077	7.5	551552	66.6	448448	33545	94206	24
37	525984	59.1	974032	7.5	551952	66.5	448048	33573	94196	23
38	526339	59.0	973987	7.5	552351	66.5	447649	33600	94186	22
39	526693	59.0	973942	7.5	552750	66.5	447250	33627	94176	21
40	527046	58.9	973897	7.5	553149	66.4	446851	33655	94167	20
41	9.527400	58.9	9.973852	7.5	9.553548	66.4	10.446452	33682	94157	19
42	527753	58.8	973807	7.5	553946	66.3	446054	33710	94147	18
43	528105	58.8	973761	7.5	554344	66.3	445656	33737	94137	17
44	528458	58.7	973716	7.6	554741	66.2	445259	33764	94127	16
45	528810	58 7	973671	7.6	555139	66.2	444861	33792	94118	15
46	529161	58.6	973625	7.6	555536	66.1	444464	33819	94108	14
47	529513	58.6	973580	7.6	555933	66.1	444067	33846	94098	13
48	529864	58.5	973535	7.6	556329	66.0	443671	33874	94088	12
49	530215	58.5	973489	7.6	556725	66.0	443275	33901	94078	11
50	530565	58.4	973444	7.6	557121	65.9	442879	33929	94068	10
51	9.530915	58.4	9.973398	7.6	9.557517	65.9	10.442483	33956	94058	9
52	531265	58.3	973352	7.6	557913	65.9	442087	33983	94049	8
53	531614	58.2	973307	7.6	558308	65.8	441692	34011	94039	7
54	531963	58.2	973261	7.6	558702	65.8	441298	34038	94029	6
55	532312	58.1	973215	7.6	559097	65.7	440903	34065	94019	5
56	532661	58.1	973169	7.6	559491	65.7	440509	34093	94009	4
57	533009	58.0	973124	7.6	559885	65.6	440115	34120	93999	3
58	533357	58.0	973078	7.6	560279	65.6	439721	34147	93989	2
59	533704	57.9	973032	7.7	560673	65.5	439327	34175	93979	1
60	534052		972986		561066		438934	34202	93969	0
	Cosine.		Sine.		Cotang.		Tang.	N. cos.	N. sine.	′

70 Degrees.

	D. 10″	Cosine.	D. 10″	Tang.	D. 10″	Cotang.	N. sine.	N. cos.	
	57.8	9.972986	7.7	9.561066	65.5	10.438934	34202	93969	60
	57.7	972940	7.7	561459	65.4	438541	34229	93959	59
	57.7	972894	7.7	561851	65.4	438149	34257	93949	58
	57·7	972848	7.7	562244	65 3	437756	34284	93939	57
3	57.6	972802	7.7	562636	65.3	437364	34311	93929	56
3	57.6	972755	7.7	563028	65.3	436972	34339	93919	55
9	57.5	972709	7.7	563419	65.2	436581	34366	93909	54
74	57.4	972663	7.7	563811	65.2	436189	34393	93899	53
18	57.4	972617	7.7	564202	65.1	435798	34421	93889	52
63	57.3	972570	7.7	564592	65.1	435408	34448	93879	51
07	57.3	972524	7.7	564983	65.0	435017	34475	93869	50
51	57.2	9.972478	7.7	9.565373	65.0	10.434627	34503	93859	49
194	57.2	972431	7.8	565763	64.9	434237	34530	93849	48
538	57.1	972385	7.8	566153	64.9	433847	34557	93839	47
880	57.1	972338	7.8	566542	64.9	433458	34584	93829	46
223	57.0	972291	7.8	566932	64.8	433068	34612	93819	45
9565	57.0	972245	7.8	567320	64.8	432680	34639	93809	44
9907	56.9	972198	7.8	567709	64.7	432291	34666	93799	43
0249	56.9	972151	7.8	568098	64.7	431902	34694	93789	42
10590	56.8	972105	7.8	568486	64.6	431514	34721	93779	41
40931	56.8	972058	7.8	568873	64.6	431127	34748	93769	40
41272	56.7	9.972011	7.8	9.569261	64.5	10.430739	34776	93759	39
41613	56.7	971964	7.8	569648	64.5	430352	34803	93748	38
41953	56.6	971917	7.8	570035	64.5	429965	34830	93738	37
542293	56.6	971870	7.8	570422	64.4	429578	34857	93728	36
542632	56.5	971823	7.8	570809	64.4	429191	34884	93718	35
542971	56.5	971776	7.8	571195	64.3	428805	34912	93708	34
543310	56.4	971729	7.9	571581	64.3	428419	34939	93698	33
543649	56.4	971682	7.9	571967	64.2	428033	34966	93688	32
543987	56.3	971635	7.9	572352	64.2	427648	34993	93677	31
544325	56.3	971588	7.9	572738	64.2	427262	35021	93667	30
.544663	56.2	9.971540	7.9	9.573123	64.1	10.426877	35048	93657	29
545000	56.2	971493	7.9	573507	64.1	426493	35075	93647	28
545338	56.1	971446	7.9	573892	64.0	426108	35102	93637	27
545674	56.1	971398	7.9	574276	64.0	425724	35130	93626	26
546011	56.0	971351	7.9	574660	63.9	425340	35157	93616	25
546347	56.0	971303	7.9	575044	63.9	424956	35184	93606	24
546683	55.9	971256	7.9	575427	63.9	424573	35211	93596	23
547019	55.9	971208	7.9	575810	63.8	424190	35239	93585	22
547354	55.8	971161	7.9	576193	63.8	423807	35266	93575	21
547689	55.8	971113	7.9	576576	63.7	423424	35293	93565	20
9.548024	55.7	9.971066	8.0	9.576958	63.7	10.423041	35320	93555	19
548359	55.7	971018	8.0	577341	63.6	422659	35347	93544	18
548693	55.6	970970	8.0	577723	63.6	422277	35375	93534	17
549027	55.6	970922	8.0	578104	63.6	421896	35402	93524	16
549360	55.5	970874	8.0	578486	63.5	421514	35429	93514	15
549693	55.5	970827	8.0	578867	63.5	421133	35456	93503	14
550026	55.4	970779	8.0	579248	63.4	420752	35484	93493	13
550359	55.4	970731	8.0	579629	63.4	420371	35511	93483	12
550692	55.3	970683	8.0	580009	63.4	419991	35538	93472	11
551024	55.3	970635	8.0	580389	63.3	419611	35565	93462	10
9.551356	55.2	9.970586	8.0	9.580769	63.3	10.419231	35592	93452	9
551687	55.2	970538	8.0	581149	63.2	418851	35619	93441	8
552018	55.2	970490	8.0	581528	63.2	418472	35647	93431	7
552349	55.1	970442	8.0	581907	63.2	418093	35674	93420	6
552680	55.1	970394	8.0	582286	63.1	417714	35701	93410	5
553010	55.0	970345	8.1	582665	63.1	417335	35728	93400	4
553341	55.0	970297	8.1	583043	63.0	416957	35755	93389	3
553670	54.9	970249	8.1	583422	63.0	416578	35782	93379	2
554000	54.9	970200	8.1	583800	62.9	416200	35810	93368	1
554329		970152		584177		415823	35837	93358	0
Cosine.		Sine.		Cotang.		Tang.	N. cos.	N.sine.	′

69 Degrees.

′	Sine.	D. 10″	Cosine.	D. 10″	Tang.	D. 10″	Cotang.	N. sine.	N. cos.	
0	9.554329	54.8	9.970152	8.1	9.584177	62.9	10.415823	35837	93358	60
1	554658	54.8	970103	8.1	584555	62.9	415445	35864	93348	59
2	554987	54.7	970055	8.1	584932	62.8	415068	35891	93337	58
3	555315	54.7	970006	8.1	585309	62.8	414691	35918	93327	57
4	555643	54.6	969957	8.1	585686	62.7	414314	35945	93316	56
5	555971	54.6	969909	8.1	586062	62.7	413938	35973	93306	55
6	556299	54.5	969860	8.1	586439	62.7	413561	36000	93295	54
7	556626	54.5	969811	8.1	586815	62.6	413185	36027	93285	53
8	556953	54.4	969762	8.1	587190	62.6	412810	36054	93274	52
9	557280	54.4	969714	8.1	587566	62.5	412434	36081	93264	51
10	557606	54.3	969665	8.1	587941	62.5	412059	36108	93253	50
11	9.557932	54.3	9.969616	8.2	9.588316	62.5	10.411684	36135	93243	49
12	558258	54.3	969567	8.2	588691	62.4	411309	36162	93232	48
13	558583	54.2	969518	8.2	589066	62.4	410934	36190	93222	47
14	558909	54.2	969469	8.2	589440	62.3	410560	36217	93211	46
15	559234	54.1	969420	8.2	589814	62.3	410186	36244	93201	45
16	559558	54.1	969370	8.2	590188	62.3	409812	36271	93190	44
17	559883	54.0	969321	8.2	590562	62.2	409438	36298	93180	43
18	560207	54.0	969272	8.2	590935	62.2	409065	36325	93169	42
19	560531	53.9	969223	8.2	591308	62.2	408692	36352	93159	41
20	560855	53.9	969173	8.2	591681	62.1	408319	36379	93148	40
21	9.561178	53.8	9.969124	8.2	9.592054	62.1	10.407946	36406	93137	39
22	561501	53.8	969075	8.2	592426	62.0	407574	36434	93127	38
23	561824	53.7	969025	8.2	592798	62.0	407202	36461	93116	37
24	562146	53.7	968976	8.2	593170	61.9	406829	36488	93106	36
25	562468	53.6	968926	8.3	593542	61.9	406458	36515	93095	35
26	562790	53.6	968877	8.3	593914	61.8	406086	36542	93084	34
27	563112	53.6	968827	8.3	594285	61.8	405715	36569	93074	33
28	563433	53.5	968777	8.3	594656	61.8	405344	36596	93063	32
29	563755	53.5	968728	8.3	595027	61.7	404973	36623	93052	31
30	564075	53.4	968678	8.3	595398	61.7	404602	36650	93042	30
31	9.564396	53.4	9.968628	8.3	9.595768	61.7	10.404232	36677	93031	29
32	564716	53.3	968578	8.3	596138	61.6	403862	36704	93020	28
33	565036	53.3	968528	8.3	596508	61.6	403492	36731	93010	27
34	565356	53.2	968479	8.3	596878	61.6	403122	36758	92999	26
35	565676	53.2	968429	8.3	597247	61.5	402753	36785	92988	25
36	565995	53.1	968379	8.3	597616	61.5	402384	36812	92978	24
37	566314	53.1	968329	8.3	597985	61.5	402015	36839	92967	23
38	566632	53.1	968278	8.3	598354	61.4	401646	36867	92956	22
39	566951	53.0	968228	8.4	598722	61.4	401278	36894	92945	21
40	567269	53.0	968178	8.4	599091	61.3	400909	36921	92935	20
41	9.567587	52.9	9.968128	8.4	9.599459	61.3	10.400541	36948	92926	19
42	567904	52.9	968078	8.4	599827	61.3	400173	36975	92913	18
43	568222	52.8	968027	8.4	600194	61.2	399806	37002	92902	17
44	568539	52.8	967977	8.4	600562	61.2	399438	37029	92892	16
45	568856	52.8	967927	8.4	600929	61.1	399071	37056	92881	15
46	569172	52.7	967876	8.4	601296	61.1	398704	37083	92870	14
47	569488	52.7	967826	8.4	601662	61.1	398338	37110	92859	13
48	569804	52.6	967775	8.4	602029	61.0	397971	37137	92849	12
49	570120	52.6	967725	8.4	602395	61.0	397605	37164	92838	11
50	570435	52.5	967674	8.4	602761	61.0	397239	37191	92827	10
51	9.570751	52.5	9.967624	8.4	9.603127	60.9	10.396873	37218	92816	9
52	571066	52.4	967573	8.4	603493	60.9	396507	37245	92805	8
53	571380	52.4	967522	8.5	603858	60.9	396142	37272	92794	7
54	571695	52.3	967471	8.5	604223	60.8	395777	37299	92784	6
55	572009	52.3	967421	8.5	604588	60.8	395412	37326	92773	5
56	572323	52.3	967370	8.5	604953	60.7	395047	37353	92762	4
57	572636	52.2	967319	8.5	605317	60.7	394683	37380	92751	3
58	572950	52.2	967268	8.5	605682	60.7	394318	37407	92740	2
59	573263	52.1	967217	8.5	606046	60.6	393954	37434	92729	1
50	573575		967166		606410		393590	37461	92718	0
	Cosine.		Sine.		Cotang.		Tang.	N. cos.	N. Sine.	′

68 Degrees.

'	Sine.	D. 10"	Cosine.	D. 10"	Tang.	D. 10"	Cotang.	N. sine.	N. cos.	
0	8.843585	300	9.998941	1.5	8.844644	302	11.155356	06976	99756	60
1	845387	299	998932	1.5	846455	301	153545	07005	99754	59
2	847183	298	998923	1.5	848260	299	151740	07034	99752	58
3	848971	297	998914	1.5	850057	298	149943	07063	99750	57
4	850751	295	998905	1.5	851846	297	148154	07092	99748	56
5	852525	294	998896	1.5	853628	296	146372	07121	99746	55
6	854291	293	998887	1.5	855403	295	144597	07150	99744	54
7	856049	292	998878	1.5	857171	293	142829	07179	99742	53
8	857801	291	998869	1.5	858932	292	141068	07208	99740	52
9	859546	290	998860	1.5	860686	291	139314	07237	99738	51
10	861283	288	998851	1.5	862433	290	137567	07266	99736	50
11	8.863014	287	9.998841	1.5	8.864173	289	11.135827	07295	99734	49
12	864738	286	998832	1.5	865906	288	134094	07324	99731	48
13	866455	285	998823	1.6	867632	287	132368	07353	99729	47
14	868165	284	998813	1.6	869351	285	130649	07382	99727	46
15	869868	283	998804	1.6	871064	284	128936	07411	99725	45
16	871565	282	998795	1.6	872770	283	127230	07440	99723	44
17	873255	281	998785	1.6	874469	282	125531	07469	99721	43
18	874938	279	998776	1.6	876162	281	123838	07498	99719	42
19	876615	279	998766	1.6	877849	280	122151	07527	99716	41
20	878285	277	998757	1.6	879529	279	120471	07556	99714	40
21	8.879949	276	9.998747	1.6	8.881202	278	11.118798	07585	99712	39
22	881607	275	998738	1.6	882869	277	117131	07614	99710	38
23	883258	274	998728	1.6	884530	276	115470	07643	99708	37
24	884903	273	998718	1.6	886185	275	113815	07672	99705	36
25	886542	272	998708	1.6	887833	274	112167	07701	99703	35
26	888174	271	998699	1.6	889476	273	110524	07730	99701	34
27	889801	270	998689	1.6	891112	272	108888	07759	99699	33
28	891421	269	998679	1.6	892742	271	107258	07788	99696	32
29	893035	268	998669	1.7	894366	270	105634	07817	99694	31
30	894643	267	998659	1.7	895984	269	104016	07846	99692	30
31	8.896246	266	9.998649	1.7	8.897596	268	11.102404	07875	99689	29
32	897842	265	998639	1.7	899203	267	100797	07904	99687	28
33	899432	264	998629	1.7	900803	266	099197	07933	99685	27
34	901017	263	998619	1.7	902398	265	097602	07962	99683	26
35	902596	262	998609	1.7	903987	264	096013	07991	99680	25
36	904169	261	998599	1.7	905570	263	094430	08020	99678	24
37	905736	260	998589	1.7	907147	262	092853	08049	99676	23
38	907297	259	998578	1.7	908719	261	091281	08078	99673	22
39	908853	258	998568	1.7	910285	260	089715	08107	99671	21
40	910404	257	998558	1.7	911846	259	088154	08136	99668	20
41	8.911949	257	9.998548	1.7	8.913401	258	11.086599	08165	99666	19
42	913488	256	998537	1.7	914951	257	085049	08194	99664	18
43	915022	255	998527	1.7	916495	256	083505	08223	99661	17
44	916550	254	998516	1.8	918034	256	081966	08252	99659	16
45	918073	253	998506	1.8	919568	255	080432	08281	99657	15
46	919591	252	998495	1.8	921096	254	078904	08310	99654	14
47	921103	251	998485	1.8	922619	253	077381	08339	99652	13
48	922610	250	998474	1.8	924136	252	075864	08368	99649	12
49	924112	249	998464	1.8	925649	251	074351	08397	99647	11
50	925609	249	998453	1.8	927156	250	072844	08426	99644	10
51	8.927100	248	9.998442	1.8	8.928658	249	11.071342	08455	99642	9
52	928587	247	998431	1.8	930155	249	069845	08484	99639	8
53	930068	246	998421	1.8	931647	248	068353	08513	99637	7
54	931544	245	998410	1.8	933134	247	066866	08542	99635	6
55	933015	244	998399	1.8	934616	246	065384	08571	99632	5
56	934481	243	998388	1.8	936093	245	063907	08600	99630	4
57	935942	243	998377	1.8	937565	244	062435	08629	99627	3
58	937398	242	998366	1.8	939032	244	060968	08658	99625	2
59	938850	241	998355	1.8	940494	243	059506	08687	99622	1
60	940296		998344		941952		058048	08716	99619	0
	Cosine.		Sine.		Cotang.		Tang.	N. cos.	N.sine.	'

85 Degrees.

'	Sine.	D. 10"	Cosine.	D. 10"	Tang.	D. 10"	Cotang.	N.sine	N. cos.	
0	9.352088	91.1	9.988724	4.9	9.363364	96.0	10.636636	22495	97437	60
1	352635	91.0	988695	4.9	363940	95.9	636060	22523	97430	59
2	353181	90.9	988666	4.9	364515	95.8	635485	22552	97424	58
3	353726	90.8	988636	4.9	365090	95.7	634910	22580	97417	57
4	354271	90.7	988607	4.9	365664	95.5	634336	22608	97411	56
5	354815	90.5	988578	4.9	366237	95.4	633763	22637	97404	55
6	355358	90.4	988548	4.9	366810	95.3	633190	22665	97398	54
7	355901	90.3	988519	4.9	367382	95.2	632618	22693	97391	53
8	356443	90.2	988489	4.9	367953	95.1	632047	22722	97384	52
9	356984	90.1	988460	4.9	368524	95.0	631476	22750	97378	51
10	357524	89.9	988430	4.9	369094	94.9	630906	22778	97371	50
11	9.358064	89.8	9.988401	4.9	9.369663	94.8	10.630337	22807	97365	49
12	358603	89.7	988371	4.9	370232	94.6	629768	22835	97358	48
13	359141	89.6	988342	4.9	370799	94.5	629201	22863	97351	47
14	359678	89.5	988312	5.0	371367	94.4	628633	22892	97345	46
15	360215	89.3	988282	5.0	371933	94.3	628067	22920	97338	45
16	360752	89.2	988252	5.0	372499	94.2	627501	22948	97331	44
17	361287	89.1	988223	5.0	373064	94.1	626936	22977	97325	43
18	361822	89.0	988193	5.0	373629	94.0	626371	23005	97318	42
19	362356	88.9	988163	5.0	374193	93.9	625807	23033	97311	41
20	362889	88.8	988133	5.0	374756	93.8	625244	23062	97304	40
21	9.363422	88.7	9.988103	5.0	9.375319	93.7	10.624681	23090	97298	39
22	363954	88.5	988073	5.0	375881	93.5	624119	23118	97291	38
23	364485	88.4	988043	5.0	376442	93.4	623558	23146	97284	37
24	365016	88.3	988013	5.0	377003	93.3	622997	23175	97278	36
25	365546	88.2	987983	5.0	377563	93.2	622437	23203	97271	35
26	366075	88.1	987953	5.0	378122	93.1	621878	23231	97264	34
27	366604	88.0	987922	5.0	378681	93.0	621319	23260	97257	33
28	367131	87.9	987892	5.0	379239	92.9	620761	23288	97251	32
29	367659	87.7	987862	5.0	379797	92.8	620203	23316	97244	31
30	368185	87.6	987832	5.1	380354	92.7	619646	23345	97237	30
31	9.368711	87.5	9.987801	5.1	9.380910	92.6	10.619090	23373	97230	29
32	369236	87.4	987771	5.1	381466	92.5	618534	23401	97223	28
33	369761	87.3	987740	5.1	382020	92.4	617980	23429	97217	27
34	370285	87.2	987710	5.1	382575	92.3	617425	23458	97210	26
35	370808	87.1	987679	5.1	383129	92.2	616871	23486	97203	25
36	371330	87.0	987649	5.1	383682	93.1	616318	23514	97196	24
37	371852	86.9	987618	5.1	384234	92.0	615766	23542	97189	23
38	372373	86.7	987588	5.1	384786	91.9	615214	23571	97182	22
39	372894	86.6	987557	5.1	385337	91.8	614663	23599	97176	21
40	373414	86.5	987526	5.1	385888	91.7	614112	23627	97169	20
41	9.373933	86.4	9.987496	5.1	9.386438	91.5	10.613562	23656	97162	19
42	374452	86.3	987465	5.1	386987	91.4	613013	23684	97155	18
43	374970	86.2	987434	5.1	387536	91.3	612464	23712	97148	17
44	375487	86.1	987403	5.2	388084	91.2	611916	23740	97141	16
45	376003	86.0	987372	5.2	388631	91.1	611369	23769	97134	15
46	376519	85.9	987341	5.2	389178	91.0	610822	23797	97127	14
47	377035	85.8	987310	5.2	389724	90.9	610276	23825	97120	13
48	377549	85.7	987279	5.2	390270	90.8	609730	23853	97113	12
49	378063	85.6	987248	5.2	390815	90.7	609185	23882	97106	11
50	378577	85.4	987217	5.2	391360	90.6	608640	23910	97100	10
51	9.379089	85.3	9.987186	5.2	9.391903	90.5	10.608097	23938	97093	9
52	379601	85.2	987155	5.2	392447	90.4	607553	23966	97086	8
53	380113	85.1	987124	5.2	392989	90.3	607011	23995	97079	7
54	380624	85.0	987092	5.2	393531	90.2	606469	24023	97072	6
55	381134	84.9	987061	5.2	394073	90.1	605927	24051	97065	5
56	381643	84.8	987030	5.2	394614	90.0	605386	24079	97058	4
57	382152	84.7	986998	5.2	395154	89.9	604846	24108	97051	3
58	382661	84.6	986967	5.2	395694	89.8	604306	24136	97044	2
59	383168	84.5	986936	5.2	396233	89.7	603767	24164	97037	1
60	383675		986904		396771		603229	24192	97030	0
	Cosine.		Sine.		Cotang.		Tang.	N. cos.	N.sine.	'

76 Degrees.

Sine.	D. 10″	Cosine.	D. 10″	Tang.	D. 10″	Cotang.	N. sine.	N. cos.	
9.383675	84.4	9.986904	5.2	9.396771	89.6	10.603229	24192	97030	60
384182	84.3	986873	5.3	397309	89.6	602691	24220	97023	59
384687	84.2	986841	5.3	397846	89.5	602154	24249	97015	58
385192	84.1	986809	5.3	398383	89.4	601617	24277	97008	57
385697	84.0	986778	5.3	398919	89.3	601081	24305	97001	56
386201	83.9	986746	5.3	399455	89.2	600545	24333	96994	55
386704	83.8	986714	5.3	399990	89.1	600010	24362	96987	54
387207	83.7	986683	5.3	400524	89.0	599476	24390	96980	53
387709	83.6	986651	5.3	401058	88.9	598942	24418	96973	52
388210	83.5	986619	5.3	401591	88.8	598409	24446	96966	51
388711	83.4	986587	5.3	402124	88.7	597876	24474	96959	50
9.389211	83.3	9.986555	5.3	9.402656	88.6	10.597344	24503	96952	49
389711	83.2	986523	5.3	403187	88.5	596813	24531	96945	48
390210	83.1	986491	5.3	403718	88.4	596282	24559	96937	47
390708	83.0	986459	5.3	404249	88.3	595751	24587	96930	46
391206	82.8	986427	5.3	404778	88.2	595222	24615	96923	45
391703	82.7	986395	5.3	405308	88.1	594692	24644	96916	44
392199	82.6	986363	5.4	405836	88.0	594164	24672	96909	43
392695	82.5	986331	5.4	406364	87.9	593636	24700	96902	42
393191	82.4	986299	5.4	406892	87.8	593108	24728	96894	41
393685	82.3	986266	5.4	407419	87.7	592581	24756	96887	40
.394179	82.2	9 986234	5.4	9 407945	87.6	10.592055	24784	96880	39
394673	82.1	986202	5.4	408471	87.5	591529	24813	96873	38
395166	82.0	986169	5.4	408997	87.4	591003	24841	96866	37
395658	81.9	986137	5.4	409521	87.4	590479	24869	96858	36
396150	81.8	986104	5.4	410045	87.3	589955	24897	96851	35
396641	81.7	986072	5.4	410569	87.2	589431	24925	96844	34
397132	81.7	986039	5.4	411092	87.1	588908	24954	96837	33
397621	81.6	986007	5.4	411615	87.0	588385	24982	96829	32
398111	81.5	985974	5.4	412137	86.9	587863	25010	96822	31
398600	81.4	985942	5.4	412658	86.8	587342	25038	96815	30
399088	81.3	9 985909	5.5	9.413179	86.7	10.386821	25066	96807	29
399575	81.2	985876	5.5	413699	86.6	586301	25094	96800	28
400062	81.1	985843	5.5	414219	86.5	585781	25122	96793	27
400549	81.0	985811	5.5	414738	86.4	585262	25151	96786	26
401035	80.9	985778	5.5	415257	86.4	584743	25179	96778	25
401520	80.8	985745	5.5	415775	86.3	584225	25207	96771	24
402005	80.7	985712	5.5	416293	86.2	583707	25235	96764	23
402489	80.6	985679	5.5	416810	86.1	583190	25263	96756	22
402972	80.5	985646	5.5	417326	86.0	582674	25291	96749	21
403455	80.4	985613	5.5	417842	85.9	582158	25320	96742	20
.403938	80.3	9.985580	5.5	9 418358	85.8	10.581642	25348	96734	19
404420	80.2	985547	5.5	418873	85.7	581127	25376	96727	18
404901	80.1	985514	5.5	419387	85.6	580613	25404	96719	17
405382	80.0	985480	5.5	419901	85.5	580099	25432	96712	16
405862	79.9	985447	5.5	420415	85.5	579585	25460	96705	15
406341	79.8	985414	5.6	420927	85.4	579073	25488	96697	14
406820	79.7	985380	5.6	421440	85.3	578560	25516	96690	13
407299	79.6	985347	5.6	421952	85.2	578048	25545	96682	12
407777	79.5	985314	5.6	422463	85.1	577537	25573	96675	11
408254	79.4	985280	5.6	422974	85.0	577026	25601	96667	10
.408731	79.4	9 985247	5.6	9 423484	84.9	10.576516	25629	96660	9
409207	79.3	985213	5.6	423993	84.8	576007	25657	96653	8
409682	79.2	985180	5.6	424503	84.8	575497	25685	96645	7
410157	79.1	985146	5.6	425011	84.7	574989	25713	96638	6
410632	79.0	985113	5.6	425519	84.6	574481	25741	96630	5
411106	78.9	985079	5.6	426027	84.5	573973	25766	96623	4
411579	78.8	985045	5.6	426534	84.4	573466	25738	96615	3
412052	78.7	985011	5.6	427041	84.3	572959	25826	96608	2
412524	78.6	984978	5.6	427547	84.3	572453	25854	96600	1
412996		984944		428052		571948	25882	96593	0
Cosine.		Sine.		Cotang.		Tang.	N. cos.	N.sine.	′

75 Degrees.

′	Sine.	D. 10″	Cosine.	D. 10″	Tang.	D. 10″	Cotang.	N. sine	N. cos.	
0	9.412996	78.5	9.984944	5.7	9.428052	84.2	10.571948	25882	96593	60
1	413467	78.4	984910	5.7	428557	84.1	571443	25910	96585	59
2	413938	78.3	984876	5.7	429062	84.0	570938	25938	96578	58
3	414408	78.3	984842	5.7	429566	83.9	570434	25966	96570	57
4	414878	78.2	984808	5.7	430070	83.8	569930	25994	96562	56
5	415347	78.1	984774	5.7	430573	83.8	569427	26022	96555	55
6	415815	78.0	984740	5.7	431075	83.7	568925	26050	96547	54
7	416283	77.9	984706	5.7	431577	83.6	568423	26079	96540	53
8	416751	77.8	984672	5.7	432079	83.5	567921	26107	96532	52
9	417217	77.7	984637	5.7	432580	83.4	567420	26135	96524	51
10	417684	77.6	984603	5.7	433080	83.3	566920	26163	96517	50
11	9.418150	77.5	9.984569	5.7	9.433580	83.2	10.566420	26191	96509	49
12	418615	77.4	984535	5.7	434080	83.2	565920	26219	96502	48
13	419079	77.3	984500	5.7	434579	83.1	565421	26247	96494	47
14	419544	77.3	984466	5.7	435078	83.0	564922	26275	96486	46
15	420007	77.2	984432	5.8	435576	82.9	564424	26303	96479	45
16	420470	77.1	984397	5.8	436073	82.8	563927	26331	96471	44
17	420933	77.0	984363	5.8	436570	82.8	563430	26359	96463	43
18	421395	76.9	984328	5.8	437067	82.7	562933	26387	96456	42
19	421857	76.8	984294	5.8	437563	82.6	562437	26415	96448	41
20	422318	76.7	984259	5.8	438059	82.5	561941	26443	96440	40
21	9.422778	76.7	9.984224	5.8	9.438554	82.4	10.561446	26471	96433	39
22	423238	76.6	984190	5.8	439048	82.3	560952	26500	96425	38
23	423697	76.5	984155	5.8	439543	82.3	560457	26528	96417	37
24	424156	76.4	984120	5.8	440036	82.2	559964	26556	96410	36
25	424615	76.3	984085	5.8	440529	82.1	559471	26584	96402	35
26	425073	76.2	984050	5.8	441022	82.0	558978	26612	96394	34
27	425530	76.1	984015	5.8	441514	81.9	558486	26640	96386	33
28	425987	76.0	983981	5.8	442006	81.9	557994	26668	96379	32
29	426443	76.0	983946	5.8	442497	81.8	557503	26696	96371	31
30	426899	75.9	983911	5.8	442988	81.7	557012	26724	96363	30
31	9.427354	75.8	9.983875	5.8	9.443479	81.6	10.556521	26752	96355	29
32	427809	75.7	983840	5.9	443968	81.6	556032	26780	96347	28
33	428263	75.6	983805	5.9	444458	81.5	555542	26808	96340	27
34	428717	75.5	983770	5.9	444947	81.4	555053	26836	96332	26
35	429170	75.4	983735	5.9	445435	81.3	554565	26864	96324	25
36	429623	75.3	983700	5.9	445923	81.2	554077	26892	96316	24
37	430075	75.2	983664	5.9	446411	81.2	553589	26920	96308	23
38	430527	75.2	983629	5.9	446898	81.1	553102	26948	96301	22
39	430978	75.1	983594	5.9	447384	81.0	552616	26976	96293	21
40	431429	75.0	983558	5.9	447870	80.9	552130	27004	96285	20
41	9.431879	74.9	9.983523	5.9	9.448356	80.9	10.551644	27032	96277	19
42	432329	74.9	983487	5.9	448841	80.8	551159	27060	96269	18
43	432778	74.8	983452	5.9	449326	80.7	550674	27088	96261	17
44	433226	74.7	983416	5.9	449810	80.6	550190	27116	96253	16
45	433675	74 6	983381	5.9	450294	80.6	549706	27144	96246	15
46	434122	74.5	983345	5.9	450777	80.5	549223	27172	96238	14
47	434569	74.4	983309	5.9	451260	80.4	548740	27200	96230	13
48	435016	74.4	983273	6.0	451743	80.3	548257	27228	96222	12
49	435462	74.3	983238	6.0	452225	80.2	547775	27256	96214	11
50	435908	74.2	983202	6.0	452706	80.2	547294	27284	96206	10
51	9.436353	74.1	9.983166	6.0	9.453187	80.1	10.546813	27312	96198	9
52	436798	74.0	983130	6.0	453668	80.0	546332	27340	96190	8
53	437242	74.0	983094	6.0	454148	79.9	545852	27368	96182	7
54	437686	73.9	983058	6.0	454628	79.9	545372	27396	96174	6
55	438129	73.8	983022	6.0	455107	79.8	544893	27424	96166	5
56	438572	73.7	982986	6.0	455586	79.7	544414	27452	96158	4
57	439014	73.6	982950	6.0	456064	79.6	543936	27480	96150	3
58	439456	73.6	982914	6.0	456542	79.6	543458	27508	96142	2
59	439897	73.5	982878	6.0	457019	79.5	542981	27536	96134	1
60	440338		982842		457496		542504	27564	96126	0
	Cosine.		Sine.		Cotang.		Tang.	N. cos.	N.sine.	′

74 Degrees.

Sine.	D. 10″	Cosine.	D. 10″	Tang.	D. 10″	Cotang.	N. sine.	N. cos.	
9.440338	73.4	9.982842	6.0	9.457496	79.4	10.542504	27564	96126	60
440778	73.3	982805	6.0	457973	79.3	542027	27592	96118	59
441218	73.2	982769	6.1	458449	79.3	541551	27620	96110	58
441658	73·1	982733	6.1	458925	79 2	541075	27648	96102	57
442096	73.1	982696	6.1	459400	79.1	540600	27676	96094	56
442535	73.0	982660	6.1	459875	79.0	540125	27704	96086	55
442973	72.9	982624	6.1	460349	79.0	539651	27731	96078	54
443410	72.8	982587	6.1	460823	78.9	539177	27759	96070	53
443847	72.7	982551	6.1	461297	78.8	538703	27787	96062	52
444284	72.7	982514	6.1	461770	78.9	538230	27815	96054	51
444720	72.6	982477	6.1	462242	78.7	537758	27843	96046	50
9.445155	72.5	9.982441	6.1	9.462714	78.6	10.537286	27871	96037	49
445590	72.4	982404	6.1	463186	78.5	536814	27899	96029	48
446025	72.3	982367	6.1	463658	78.5	536342	27927	96021	47
446459	72.3	982331	6.1	464129	78.4	535871	27955	96013	46
446893	72.2	982294	6.1	464599	78.3	535401	27983	96005	45
447326	72.1	982257	6.1	465069	78.3	534931	28011	95997	44
447759	72.0	982220	6.2	465539	78.2	534461	28039	95989	43
448191	72.0	982183	6.2	466008	78.1	533992	28067	95981	42
448623	71.9	982146	6.2	466476	78.0	533524	28095	95972	41
449054	71.8	982109	6.2	466945	78.0	533055	28123	95964	40
9.449485	71.7	9.982072	6.2	9.467413	77.9	10.532587	28150	95956	39
449915	71.6	982035	6.2	467880	77.8	532120	28178	95948	38
450345	71.6	981998	6.2	468347	77.8	531653	28206	95940	37
450775	71.5	981961	6.2	468814	77.7	531186	28234	95931	36
451204	71.4	981924	6.2	469280	77.6	530720	28262	95923	35
451632	71.3	981886	6.2	469746	77.5	530254	28290	95915	34
452060	71.3	981849	6.2	470211	77.5	529789	28318	95907	33
452488	71.2	981812	6.2	470676	77.4	529324	28346	95898	32
452915	71.1	981774	6.2	471141	77.3	528859	28374	95890	31
453342	71.0	981737	6.2	471605	77.3	528395	28402	95882	30
9.453768	71.0	9.981699	6.3	9.472068	77.2	10.527932	28429	95874	29
454194	70.9	981662	6.3	472532	77.1	527468	28457	95865	28
454619	70.8	981625	6.3	472995	77.1	527005	28485	95857	27
455044	70.7	981587	6.3	473457	77.0	526543	28513	95849	26
455469	70.7	981549	6.3	473919	76.9	526081	28541	95841	25
455893	70.6	981512	6.3	474381	76.9	525619	28569	95832	24
456316	70.5	981474	6.3	474842	76.8	525158	28597	95824	23
456739	70.4	981436	6.3	475303	76.7	524697	28625	95816	22
457162	70.4	981399	6.3	475763	76.7	524237	28652	95807	21
457584	70.3	981361	6.3	476223	76.6	523777	28680	95799	20
9.458006	70.2	9.981323	6.3	9.476683	76.5	10.523317	28708	95791	19
458427	70.1	981285	6.3	477142	76.5	522858	28736	95782	18
458848	70.1	981247	6.3	477601	76.4	522399	28764	95774	17
459268	70.0	981209	6.3	478059	76.3	521941	28792	95766	16
459688	69.9	981171	6.3	478517	76.3	521483	28820	95757	15
460108	69.8	981133	6.4	478975	76.2	521025	28847	95749	14
460527	69.8	981095	6.4	479432	76.1	520568	28875	95740	13
460946	69.7	981057	6.4	479889	76.1	520111	28903	95732	12
461364	69.6	981019	6.4	480345	76.0	519655	28931	95724	11
461782	69.5	980981	6.4	480801	75.9	519199	28959	95715	10
9.462199	69.5	9.980942	6.4	9.481257	75.9	10.518743	28987	95707	9
462616	69.4	980904	6.4	481712	75.8	518288	29015	95698	8
463032	69.3	980866	6.4	482167	75.7	517833	29042	95690	7
463448	69.3	980827	6.4	482621	75.7	517379	29070	95681	6
463864	69.2	980789	6.4	483075	75.6	516925	29098	95673	5
464279	69.1	980750	6.4	483529	75.5	516471	29126	95664	4
464694	69.0	980712	6.4	483982	75.5	516018	29154	95656	3
465108	69.0	980673	6.4	484435	75.4	515565	29182	95647	2
465522	68.9	980635	6.4	484887	75.3	515113	2920[illegible]	95639	1
465935		980596		485339		514661	29247	95630	0
Cosine.		Sine.		Cotang.		Tang.	N. cos.	N.sine.	′

73 Degrees.

′	Sine.	D. 10″	Cosine.	D. 10″	Tang.	D. 10″	Cotang.	N. sine.	N. cos.	
0	9.465935	68.8	9.980596	6.4	9.485339	75.3	10.514661	29237	95630	60
1	466348	68.8	980558	6.4	485791	75.2	514209	29265	95622	59
2	466761	68.7	980519	6.5	486242	75.1	513758	29293	95613	58
3	467173	68.6	980480	6.5	486693	75.1	513307	29321	95605	57
4	467585	68.5	980442	6.5	487143	75.0	512857	29348	95596	56
5	467996	68.5	980403	6.5	487593	74.9	512407	29376	95588	55
6	468407	68.4	980364	6.5	488043	74.9	511957	29404	95579	54
7	468817	68.3	980325	6.5	488492	74.8	511508	29432	95571	53
8	469227	68.3	980286	6.5	488941	74.7	511059	29460	95562	52
9	469637	68.2	980247	6.5	489390	74.7	510610	29487	95554	51
10	470046	68.1	980208	6.5	489838	74.6	510162	29515	95545	50
11	9.470455	68.0	9.980169	6.5	9.490286	74.6	10.509714	29543	95536	49
12	470863	68.0	980130	6.5	490733	74.5	509267	29571	95528	48
13	471271	67.9	980091	6.5	491180	74.4	508820	29599	95519	47
14	471679	67.8	980052	6.5	491627	74.4	508373	29626	95511	46
15	472086	67.8	980012	6.5	492073	74.3	507927	29654	95502	45
16	472492	67.7	979973	6.5	492519	74.3	507481	29682	95493	44
17	472898	67.6	979934	6.6	492965	74.2	507035	29710	95485	43
18	473304	67.6	979895	6.6	493410	74.1	506590	29737	95476	42
19	473710	67.5	979855	6.6	493854	74.0	506146	29765	95467	41
20	474115	67.4	979816	6.6	494299	74.0	505701	29793	95459	40
21	9.474519	67.4	9.979776	6.6	9.494743	74.0	10.505257	29821	95450	39
22	474923	67.3	979737	6.6	495186	73.9	504814	29849	95441	38
23	475327	67.2	979697	6.6	495630	73.8	504370	29876	95433	37
24	475730	67.2	979658	6.6	496073	73.7	503927	29904	95424	36
25	476133	67.1	979618	6.6	496515	73.7	503485	29932	95415	35
26	476536	67.0	979579	6.6	496957	73.6	503043	29960	95407	34
27	476938	66.9	979539	6.6	497399	73.6	502601	29987	95398	33
28	477340	66.9	979499	6.6	497841	73.5	502159	30015	95389	32
29	477741	66.8	979459	6.6	468282	73.4	501718	30043	95380	31
30	478142	66.7	979420	6.6	498722	73.4	501278	30071	95372	30
31	9.478542	66.7	9.979380	6.6	9.499163	73.3	10.500837	30098	95363	29
32	478942	66.6	979340	6.6	499603	73.3	500397	30126	95354	28
33	479342	66.5	979300	6.7	500042	73.2	499958	30154	95345	27
34	479741	66.5	979260	6.7	500481	73.1	499519	30182	95337	26
35	480140	66.4	979220	6.7	500920	73.1	499080	30209	95328	25
36	480539	66.3	979180	6.7	501359	73.0	498641	30237	95319	24
37	480937	66.3	979140	6.7	501797	73.0	498203	30265	95310	23
38	481334	66.2	979100	6.7	502235	72.9	497765	30292	95301	22
39	481731	66.1	979059	6.7	502672	72.8	497328	30320	95293	21
40	482128	66.1	979019	6.7	503109	72.8	496891	30348	95284	20
41	9.482525	66.0	9.978979	6.7	9.503546	72.7	10.496454	30376	95275	19
42	482921	65.9	978939	6.7	503982	72.7	496018	30403	95266	18
43	483316	65.9	978898	6.7	504418	72.6	495582	30431	95257	17
44	483712	65.8	978858	6.7	504854	72.5	495146	30459	95248	16
45	484107	65.7	978817	6.7	505289	72.5	494711	30486	95240	15
46	484501	65.7	978777	6.7	505724	72.4	494276	30514	95231	14
47	484895	65.6	978736	6.7	506159	72.4	493841	30542	95222	13
48	485289	65.5	978696	6.8	506593	72.3	493407	30570	95213	12
49	485682	65.5	978655	6.8	507027	72.2	492973	30597	95204	11
50	486075	65.4	978615	6.8	507460	72.2	492540	30625	95195	10
51	9.486467	66.3	9.978574	6.8	9.507893	72.1	10.492107	30653	95186	9
52	486860	65.3	978533	6.8	508326	72.1	491674	30680	95177	8
53	487251	65.2	978493	6.8	508759	72.0	491241	30708	95168	7
54	487643	65.1	978452	6.8	509191	71.9	490809	30736	95159	6
55	488034	65.1	978411	6.8	509622	71.9	490378	30763	95150	5
56	488424	65.0	978370	6.8	510054	71.8	489946	30791	95142	4
57	488814	65.0	978329	6.8	510485	71.8	489515	30819	95133	3
58	489204	64.9	978288	6.8	510916	71.7	489084	30846	95124	2
59	489593	64.8	978247	6.8	511346	71.6	488654	30874	95115	1
60	489982		978206		511776		488224	30902	95106	0
	Cosine.		Sine.		Cotang.		Tang.	N. cos.	N.sine.	′

72 Degrees.

′	Sine.	D. 10″	Cosine.	D. 10″	Tang.	D. 10″	Cotang.	N. sine.	N. cos.	
0	9.489982	64.8	9.978206	6.8	9.511776	71.6	10.488224	30902	95106	60
1	490371	64.8	978165	6.8	512206	71.6	487794	30929	95097	59
2	490759	64.7	978124	6.8	512635	71.5	487365	30957	95088	58
3	491147	64.6	978083	6.9	513064	71.4	486936	30985	95079	57
4	491535	64.6	978042	6.9	513493	71.4	486507	31012	95070	56
5	491922	64.5	978001	6.9	513921	71.3	486079	31040	95061	55
6	492308	64.4	977959	6.9	514349	71.3	485651	31068	95052	54
7	492695	64.4	977918	6.9	514777	71.2	485223	31095	95043	53
8	493081	64.3	977877	6.9	515204	71.2	484796	31123	95033	52
9	493466	64.2	977835	6.9	515631	71.1	484369	31151	95024	51
10	493851	64.2	977794	6.9	516057	71.0	483943	31178	95015	50
11	9.494236	64.1	9.977752	6.9	9.516484	71.0	10.483516	31206	95006	49
12	494621	64.1	977711	6.9	516910	70.9	483090	31233	94997	48
13	495005	64.0	977669	6.9	517335	70.9	482665	31261	94988	47
14	495388	63.9	977628	6.9	517761	70.8	482239	31289	94979	46
15	495772	63.9	977586	6.9	518185	70.8	481815	31316	94970	45
16	496154	63.8	977544	7.0	518610	70.7	481390	31344	94961	44
17	496537	63.7	977503	7.0	519034	70.6	480966	31372	94952	43
18	496919	63.7	977461	7.0	519458	70.6	480542	31399	94943	42
19	497301	63.6	977419	7.0	519882	70.5	480118	31427	94933	41
20	497682	63.6	977377	7.0	520305	70.5	479695	31454	94924	40
21	9.498064	63.5	9.977335	7.0	9.520728	70.4	10.479272	31482	94915	39
22	498444	63.4	977293	7.0	521151	70.3	478849	31510	94906	38
23	498825	63.4	977251	7.0	521573	70.3	478427	31537	94897	37
24	499204	63.3	977209	7.0	521995	70.3	478005	31565	94888	36
25	499584	63.2	977167	7.0	522417	70.2	477583	31593	94878	35
26	499963	63.2	977125	7.0	522838	70.2	477162	31620	94869	34
27	500342	63.1	977083	7.0	523259	70.1	476741	31648	94860	33
28	500721	63.1	977041	7.0	523680	70.1	476320	31675	94851	32
29	501099	63.0	976999	7.0	524100	70.0	475900	31703	94842	31
30	501476	62.9	976957	7.0	524520	69.9	475480	31730	94832	30
31	9.501854	62.9	9.976914	7.0	9.524939	69.9	10.475061	31758	94823	29
32	502231	62.8	976872	7.1	525359	69.8	474641	31786	94814	28
33	502607	62.8	976830	7.1	525778	69.8	474222	31813	94805	27
34	502984	62.7	976787	7.1	526197	69.7	473803	31841	94795	26
35	503360	62.6	976745	7.1	526615	69.7	473385	31868	94786	25
36	503735	62.6	976702	7.1	527033	69.6	472967	31896	94777	24
37	504110	62.5	976660	7.1	527451	69.6	472549	31923	94768	23
38	504485	62.5	976617	7.1	527868	69.5	472132	31951	94758	22
39	504860	62.4	976574	7.1	528285	69.5	471715	31979	94749	21
40	505234	62.3	976532	7.1	528702	69.4	471298	32006	94740	20
41	9.505608	62.3	9.976489	7.1	9.529119	69.3	10.470881	32034	94730	19
42	505981	62.2	976446	7.1	529535	69.3	470465	32061	94721	18
43	506354	62.2	976404	7.1	529950	69.3	470050	32089	94712	17
44	506727	62.1	976361	7.1	530366	69.2	469634	32116	94702	16
45	507099	62.0	976318	7.1	530781	69.1	469219	32144	94693	15
46	507471	62.0	976275	7.1	531196	69.1	468804	32171	94684	14
47	507843	61.9	976232	7.2	531611	69.0	468389	32199	94674	13
48	508214	61.9	976189	7.2	532025	69.0	467975	32227	94665	12
49	508585	61.8	976146	7.2	532439	68.9	467561	32254	94656	11
50	508956	61.8	976103	7.2	532853	68.9	467147	32282	94646	10
51	9.509326	61.7	9.976060	7.2	9.533266	68.8	10.466734	32309	94637	9
52	509696	61.6	976017	7.2	533679	68.8	466321	32337	94627	8
53	510065	61.6	975974	7.2	534092	68.7	465908	32364	94618	7
54	510434	61.5	975930	7.2	534504	68.7	465496	32392	94609	6
55	510803	61.5	975887	7.2	534916	68.6	465084	32419	94599	5
56	511172	61.4	975844	7.2	535328	68.6	464672	32447	94590	4
57	511540	61.3	975800	7.2	535739	68.5	464261	32474	94580	3
58	511907	61.3	975757	7.2	536150	68.5	463850	32502	94571	2
59	512275	61.2	975714	7.2	536561	68.4	463439	32529	94561	1
60	512642		975670		536972		463028	32557	94552	0
	Cosine.		Sine.		Cotang.		Tang.	N. cos.	N.sine.	′

71 Degrees.

′	Sine.	D. 10″	Cosine.	D. 10″	Tang.	D. 10″	Cotang.	N. sine.	N. cos.	
0	9.512642	61.2	9.975670	7.3	9.536972	68.4	10.463028	32557	94552	60
1	513009	61.1	975627	7.3	537382	68.3	462618	32584	94542	59
2	513375	61.1	975583	7.3	537792	68.3	462208	32612	94533	58
3	513741	61.0	975539	7.3	538202	68.2	461798	32639	94523	57
4	514107	60.9	975496	7.3	538611	68.2	461389	32667	94514	56
5	514472	60.9	975452	7.3	539020	68.1	460980	32694	94504	55
6	514837	60.8	975408	7.3	539429	68.1	460571	32722	94495	54
7	515202	60.8	975365	7.3	539837	68.0	460163	32749	94485	53
8	515566	60.7	975321	7.3	540245	68.0	459755	32777	94476	52
9	515930	60.7	975277	7.3	540653	67.9	459347	32804	94466	51
10	516294	60.6	975233	7.3	541061	67.9	458939	32832	94457	50
11	9.516657	60.5	9.975189	7.3	9.541468	67.8	10.458532	32859	94447	49
12	517020	60.5	975145	7.3	541875	67.8	458125	32887	94438	48
13	517382	60.4	975101	7.3	542281	67.7	457719	32914	94428	47
14	517745	60.4	975057	7.3	542688	67.7	457312	32942	94418	46
15	518107	60.3	975013	7.3	543094	67.6	456906	32969	94409	45
16	518468	60.3	974969	7.4	543499	67.6	456501	32997	94399	44
17	518829	60.2	974925	7.4	543905	67.5	456095	33024	94390	43
18	519190	60.1	974880	7.4	544310	67.5	455690	33051	94380	42
19	519551	60.1	974836	7.4	544715	67.4	455285	33079	94370	41
20	519911	60.0	974792	7.4	545119	67.4	454881	33106	94361	40
21	9.520271	60.0	9.974748	7.4	9.545524	67.3	10.454476	33134	94351	39
22	520631	59.9	974703	7.4	545928	67.3	454072	33161	94342	38
23	520990	59.9	974659	7.4	546331	67.2	453669	33189	94332	37
24	521349	59.8	974614	7.4	546735	67.2	453265	33216	94322	36
25	521707	59.8	974570	7.4	547138	67.1	452862	33244	94313	35
26	522066	59.7	974525	7.4	547540	67.1	452460	33271	94303	34
27	522424	59.6	974481	7.4	547943	67.0	452057	33298	94293	33
28	522781	59.6	974436	7.4	548345	67.0	451655	33326	94284	32
29	523138	59.5	974391	7.4	548747	66.9	451253	33353	94274	31
30	523495	59.5	974347	7.5	549149	66.9	450851	33381	94264	30
31	9.523852	59.4	9.974302	7.5	9.549550	66.8	10.450450	33408	94254	29
32	524208	59.4	974257	7.5	549951	66.8	450049	33436	94245	28
33	524564	59.3	974212	7.5	550352	66.7	449648	33463	94235	27
34	524920	59.3	974167	7.5	550752	66.7	449248	33490	94225	26
35	525275	59.2	974122	7.5	551152	66.6	448848	33518	94215	25
36	525630	59.1	974077	7.5	551552	66.6	448448	33545	94206	24
37	525984	59.1	974032	7.5	551952	66.5	448048	33573	94196	23
38	526339	59.0	973987	7.5	552351	66.5	447649	33600	94186	22
39	526693	59.0	973942	7.5	552750	66.5	447250	33627	94176	21
40	527046	58.9	973897	7.5	553149	66.4	446851	33655	94167	20
41	9.527400	58.9	9.973852	7.5	9.553548	66.4	10.446452	33682	94157	19
42	527753	58.8	973807	7.5	553946	66.3	446054	33710	94147	18
43	528105	58.8	973761	7.5	554344	66.3	445656	33737	94137	17
44	528458	58.7	973716	7.6	554741	66.2	445259	33764	94127	16
45	528810	58 7	973671	7.6	555139	66.2	444861	33792	94118	15
46	529161	58.6	973625	7.6	555536	66.1	444464	33819	94108	14
47	529513	58.6	973580	7.6	555933	66.1	444067	33846	94098	13
48	529864	58.5	973535	7.6	556329	66.0	443671	33874	94088	12
49	530215	58.5	973489	7.6	556725	66.0	443275	33901	94078	11
50	530565	58.4	973444	7.6	557121	65.9	442879	33929	94068	10
51	9.530915	58.4	9.973398	7.6	9.557517	65.9	10.442483	33956	94058	9
52	531265	58.3	973352	7.6	557913	65.9	442087	33983	94049	8
53	531614	58.2	973307	7.6	558308	65.8	441692	34011	94039	7
54	531963	58.2	973261	7.6	558702	65.8	441298	34038	94029	6
55	532312	58.1	973215	7.6	559097	65.7	440903	34065	94019	5
56	532661	58.1	973169	7.6	559491	65.7	440509	34093	94009	4
57	533009	58.0	973124	7.6	559885	65.6	440115	34120	93999	3
58	533357	58.0	973078	7.6	560279	65.6	439721	34147	93989	2
59	533704	57.9	973032	7.7	560673	65.5	439327	34175	93979	1
60	534052		972986		561066		438934	34202	93969	0
	Cosine.		Sine.		Cotang.		Tang.	N. cos.	N. sine.	′

70 Degrees.

′	Sine.	D. 10″	Cosine.	D. 10″	Tang.	D. 10″	Cotang.	N. sine.	N. cos.	
0	9.317879	99.0	9.990104	4.5	9.327474	103	10.672526	20791	97815	60
1	318473	98.8	990378	4.5	328095	103	671905	20820	97809	59
2	319066	98.7	990351	4.5	328715	103	671285	20848	97803	58
3	319658	98.6	990324	4.5	329334	103	670666	20877	97797	57
4	320249	98.4	990297	4.5	329953	103	670047	20905	97791	56
5	320840	98.3	990270	4.5	330570	103	669430	20933	97784	55
6	321430	98.2	990243	4.5	331187	103	668813	20962	97778	54
7	322019	98.0	990215	4.5	331803	103	668197	20990	97772	53
8	322607	97.9	990188	4.5	332418	102	667582	21019	97766	52
9	323194	97.7	990161	4.5	333033	102	666967	21047	97760	51
10	323780	97.6	990134	4.5	333646	102	666354	21076	97754	50
11	9.324366	97.5	9.990107	4.6	9.334259	102	10.665741	21104	97748	49
12	324950	97.3	990079	4.6	334871	102	665129	21132	97742	48
13	325534	97.2	990052	4.6	335482	102	664518	21161	97735	47
14	326117	97.0	990025	4.6	336093	102	663907	21189	97729	46
15	326700	96.9	989997	4.6	336702	101	663298	21218	97723	45
16	327281	96.8	989970	4.6	337311	101	662689	21246	97717	44
17	327862	96.6	989942	4.6	337919	101	662081	21275	97711	43
18	328442	96.5	989915	4.6	338527	101	661473	21303	97705	42
19	329021	96.4	989887	4.6	339133	101	660867	21331	97698	41
20	329599	96.2	989860	4.6	339739	101	660261	21360	97692	40
21	9.330176	96.1	9.989832	4.6	9.340344	101	10.659656	21388	97686	39
22	330753	96.0	989804	4.6	340948	101	659052	21417	97680	38
23	331329	95.8	989777	4.6	341552	100	658448	21445	97673	37
24	331903	95.7	989749	4.7	342155	100	657845	21474	97667	36
25	332478	95.6	989721	4.7	342757	100	657243	21502	97661	35
26	333051	95.4	989693	4.7	343358	100	656642	21530	97655	34
27	333624	95.3	989665	4.7	343958	100	656042	21559	97648	33
28	334195	95.2	989637	4.7	344558	100	655442	21587	97642	32
29	334766	95.0	989609	4.7	345157	100	654843	21616	97636	31
30	335337	94.9	989582	4.7	345755	100	654245	21644	97630	30
31	9.335906	94.8	9.989553	4.7	9.346353	99.4	10.653647	21672	97623	29
32	336475	94.6	989525	4.7	346949	99.3	653051	21701	97617	28
33	337043	94.5	989497	4.7	347545	99.2	652455	21729	97611	27
34	337610	94.4	989469	4.7	348141	99.1	651859	21758	97604	26
35	338176	94.3	989441	4.7	348735	99.0	651265	21786	97598	25
36	338742	94.1	989413	4.7	349329	98.8	650671	21814	97592	24
37	339306	94.0	989384	4.7	349922	98.7	650078	21843	97585	23
38	339871	93.9	989356	4.7	350514	98.6	649486	21871	97579	22
39	340434	93.7	989328	4.7	351106	98.5	648894	21899	97573	21
40	340996	93.6	989300	4.7	351697	98.3	648303	21928	97566	20
41	9.341558	93.5	9.989271	4.7	9.352287	98.2	10.647713	21956	97560	19
42	342119	93.4	989243	4.7	352876	98.1	647124	21985	97553	18
43	342679	93.2	989214	4.7	353465	98.0	646535	22013	97547	17
44	343239	93.1	989186	4.7	354053	97.9	645947	22041	97541	16
45	343797	93.0	989157	4.7	354640	97.7	645360	22070	97534	15
46	344355	92.9	989128	4.8	355227	97.6	644773	22098	97528	14
47	344912	92.7	989100	4.8	355813	97.5	644187	22126	97521	13
48	345469	92.6	989071	4.8	356398	97.4	643602	22155	97515	12
49	346024	92.5	989042	4.8	356982	97.3	643018	22183	97508	11
50	346579	92.4	989014	4.8	357566	97.1	642434	22212	97502	10
51	9.347134	92.2	9.988985	4.8	9.358149	97.0	10.641851	22240	97496	9
52	347687	92.1	988956	4.8	358731	96.9	641269	22268	97489	8
53	348240	92.0	988927	4.8	359313	96.8	640687	22297	97483	7
54	348792	91.9	988898	4.8	359893	96.7	640107	22325	97476	6
55	349343	91.7	988869	4.8	360474	96.6	639526	22353	97470	5
56	349893	91.6	988840	4.8	361053	96.5	638947	22382	97463	4
57	350443	91.5	988811	4.9	361632	96.3	638368	22410	97457	3
58	350992	91.4	988782	4.9	362210	96.2	637790	22438	97450	2
59	351540	91.3	988753	4.9	362787	96.1	637213	22467	97444	1
60	352088		988724		363364		636636	22495	97437	0
	Cosine.		Sine.		Cotang.		Tang.	N. cos.	N.sine.	′

′	Sine.	D. 10″	Cosine.	D. 10″	Tang.	D. 10″	Cotang.	N. sine.	N. cos.	
0	9.554329	54.8	9.970152	8.1	9.584177	62.9	10.415823	35837	93358	60
1	554658	54.8	970103	8.1	584555	62.9	415445	35864	93348	59
2	554987	54.7	970055	8.1	584932	62.8	415068	35891	93337	58
3	555315	54.7	970006	8.1	585309	62.8	414691	35918	93327	57
4	555643	54.6	969957	8.1	585686	62.7	414314	35945	93316	56
5	555971	54.6	969909	8.1	586062	62.7	413938	35973	93306	55
6	556299	54.5	969860	8.1	586439	62.7	413561	36000	93295	54
7	556626	54.5	969811	8.1	586815	62.6	413185	36027	93285	53
8	556953	54.4	969762	8.1	587190	62.6	412810	36054	93274	52
9	557280	54.4	969714	8.1	587566	62.5	412434	36081	93264	51
10	557606	54.3	969665	8.1	587941	62.5	412059	36108	93253	50
11	9.557932	54.3	9.969616	8.2	9.588316	62.5	10.411684	36135	93243	49
12	558258	54.3	969567	8.2	588691	62.4	411309	36162	93232	48
13	558583	54.2	969518	8.2	589066	62.4	410934	36190	93222	47
14	558909	54.2	969469	8.2	589440	62.3	410560	36217	93211	46
15	559234	54.1	969420	8.2	589814	62.3	410186	36244	93201	45
16	559558	54.1	969370	8.2	590188	62.3	409812	36271	93190	44
17	559883	54.0	969321	8.2	590562	62.2	409438	36298	93180	43
18	560207	54.0	969272	8.2	590935	62.2	409065	36325	93169	42
19	560531	53.9	969223	8.2	591308	62.2	408692	36352	93159	41
20	560855	53.9	969173	8.2	591681	62.1	408319	36379	93148	40
21	9.561178	53.8	9.969124	8.2	9.592054	62.1	10.407946	36406	93137	39
22	561501	53.8	969075	8.2	592426	62.0	407574	36434	93127	38
23	561824	53.7	969025	8.2	592798	62.0	407202	36461	93116	37
24	562146	53.7	968976	8.2	593170	61.9	406829	36488	93106	36
25	562468	53.6	968926	8.3	593542	61.9	406458	36515	93095	35
26	562790	53.6	968877	8.3	593914	61.8	406086	36542	93084	34
27	563112	53.6	968827	8.3	594285	61.8	405715	36569	93074	33
28	563433	53.5	968777	8.3	594656	61.8	405344	36596	93063	32
29	563755	53.5	968728	8.3	595027	61.7	404973	36623	93052	31
30	564075	53.4	968678	8.3	595398	61.7	404602	36650	93042	30
31	9.564396	53.4	9.968628	8.3	9.595768	61.7	10.404232	36677	93031	29
32	564716	53.3	968578	8.3	596138	61.6	403862	36704	93020	28
33	565036	53.3	968528	8.3	596508	61.6	403492	36731	93010	27
34	565356	53.2	968479	8.3	596878	61.6	403122	36758	92999	26
35	565676	53.2	968429	8.3	597247	61.5	402753	36785	92988	25
36	565995	53.1	968379	8.3	597616	61.5	402384	36812	92978	24
37	566314	53.1	968329	8.3	597985	61.5	402015	36839	92967	23
38	566632	53.1	968278	8.3	598354	61.4	401646	36867	92956	22
39	566951	53.0	968228	8.4	598722	61.4	401278	36894	92945	21
40	567269	53.0	968178	8.4	599091	61.3	400909	36921	92935	20
41	9.567587	52.9	9.968128	8.4	9.599459	61.3	10.400541	36948	92926	19
42	567904	52.9	968078	8.4	599827	61.3	400173	36975	92913	18
43	568222	52.8	968027	8.4	600194	61.2	399806	37002	92902	17
44	568539	52.8	967977	8.4	600562	61.2	399438	37029	92892	16
45	568856	52.8	967927	8.4	600929	61.1	399071	37056	92881	15
46	569172	52.7	967876	8.4	601296	61.1	398704	37083	92870	14
47	569488	52.7	967826	8.4	601662	61.1	398338	37110	92859	13
48	569804	52.6	967775	8.4	602029	61.0	397971	37137	92849	12
49	570120	52.6	967725	8.4	602395	61.0	397605	37164	92838	11
50	570435	52.5	967674	8.4	602761	61.0	397239	37191	92827	10
51	9.570751	52.5	9.967624	8.4	9.603127	60.9	10.396873	37218	92816	9
52	571066	52.4	967573	8.4	603493	60.9	396507	37245	92805	8
53	571380	52.4	967522	8.5	603858	60.9	396142	37272	92794	7
54	571695	52.3	967471	8.5	604223	60.8	395777	37299	92784	6
55	572009	52.3	967421	8.5	604588	60.8	395412	37326	92773	5
56	572323	52.3	967370	8.5	604953	60.7	395047	37353	92762	4
57	572636	52.2	967319	8.5	605317	60.7	394683	37380	92751	3
58	572950	52.2	967268	8.5	605682	60.7	394318	37407	92740	2
59	573263	52.1	967217	8.5	606046	60.6	393954	37434	92729	1
60	573575		967166		606410		393590	37461	92718	0
	Cosine.		Sine.		Cotang.		Tang.	N. cos.	N. Sine.	′

68 Degrees.

′	Sine.	D. 10″	Cosine.	D. 10″	Tang.	D. 10″	Cotang.	N. sine.	N. cos.	
0	9.573575	52.1	9.967166	8.5	9.606410	60.6	10.393590	37461	92718	60
1	573888	52.0	967115	8.5	606773	60.6	393227	37488	92707	59
2	574200	52.0	967064	8.5	607137	60.5	392863	37515	92697	58
3	574512	51.9	967013	8.5	607500	60.5	392500	37542	92686	57
4	574824	51.9	966961	8.5	607863	60.4	392137	37569	92675	56
5	575136	51.9	966910	8.5	608225	60.4	391775	37595	92664	55
6	575447	51.8	966859	8.5	608588	60.4	391412	37622	92653	54
7	575758	51.8	966808	8.5	608950	60.3	391050	37649	92642	53
8	576069	51.7	966756	8.6	609312	60.3	390688	37676	92631	52
9	576379	51.7	966705	8.6	609674	60.3	390326	37703	92620	51
10	576689	51.6	966653	8.6	610036	60.2	389964	37730	92609	50
11	9.576999	51.6	9.966602	8.6	9.610397	60.2	10.389603	37757	92598	49
12	577309	51.6	966550	8.6	610759	60.2	389241	37784	92587	48
13	577618	51.5	966499	8.6	611120	60.1	388880	37811	92576	47
14	577927	51.5	966447	8.6	611480	60.1	388520	37838	92565	46
15	578236	51.4	966395	8.6	611841	60.1	388159	37865	92554	45
16	578545	51.4	966344	8.6	612201	60.0	387799	37892	92543	44
17	578853	51.3	966292	8.6	612561	60.0	387439	37919	92532	43
18	579162	51.3	966240	8.6	612921	60.0	387079	37946	92521	42
19	579470	51.3	966188	8.6	613281	59.9	386719	37973	92510	41
20	579777	51.2	966136	8.6	613641	59.9	386359	37999	92499	40
21	9.580085	51.2	9.966085	8.7	9.614000	59.8	10.386000	38026	92488	39
22	580392	51.1	966033	8.7	614359	59.8	385641	38053	92477	38
23	580699	51.1	965981	8.7	614718	59.8	385282	38080	92466	37
24	581005	51.1	965928	8.7	615077	59.7	384923	38107	92455	36
25	581312	51.0	965876	8.7	615435	59.7	384565	38134	92444	35
26	581618	51.0	965824	8.7	615793	59.7	384207	38161	92432	34
27	581924	50.9	965772	8.7	616151	59.6	383849	38188	92421	33
28	582229	50.9	965720	8.7	616509	59.6	383491	38215	92410	32
29	582535	50.9	965668	8.7	616867	59.6	383133	38241	92399	31
30	582840	50.8	965615	8.7	617224	59.5	382776	38268	92388	30
31	9.583145	50.8	9.965563	8.7	9.617582	59.5	10.382418	38295	92377	29
32	583449	50.7	965511	8.7	617939	59.5	382061	38322	92366	28
33	583754	50.7	965458	8.7	618295	59.4	381705	38349	92355	27
34	584058	50.6	965406	8.7	618652	59.4	381348	38376	92343	26
35	584361	50.6	965353	8.8	619008	59.4	380992	38403	92332	25
36	584665	50.6	965301	8.8	619364	59.3	380636	38430	92321	24
37	584968	50.5	965248	8.8	619721	59.3	380279	38456	92310	23
38	585272	50.5	965195	8.8	620076	59.3	379924	38483	92299	22
39	585574	50.4	965143	8.8	620432	59.2	379568	38510	92287	21
40	585877	50.4	965090	8.8	620787	59.2	379213	38537	92276	20
41	9.586179	50.3	9.965037	8.8	9.621142	59.2	10.378858	38564	92265	19
42	586482	50.3	964984	8.8	621497	59.1	378503	38591	92254	18
43	586783	50.3	964931	8.8	621852	59.1	378148	38617	92243	17
44	587085	50.2	964879	8.8	622207	59.0	377793	38644	92231	16
45	587386	50.2	964826	8.8	622561	59.0	377439	38671	92220	15
46	587688	50.1	964773	8.8	622915	59.0	377085	38698	92209	14
47	587989	50.1	964719	8.8	623269	58.9	376731	38725	92198	13
48	588289	50.1	964666	8.9	623623	58.9	376377	38752	92186	12
49	588590	50.0	964613	8.9	623976	58.9	376024	38778	92175	11
50	588890	50.0	964560	8.9	624330	58.8	375670	38805	92164	10
51	9.589190	49.9	9.964507	8.9	9.624683	58.8	10.375317	38832	92152	9
52	589489	49.9	964454	8.9	625036	58.8	374964	38859	92141	8
53	589789	49.9	964400	8.9	625388	58.7	374612	38886	92130	7
54	590088	49.8	964347	8.9	625741	58.7	374259	38912	92119	6
55	590387	49.8	964294	8.9	626093	58.7	373907	38939	92107	5
56	590686	49.7	964240	8.9	626445	58.6	373555	38966	92096	4
57	590984	49.7	964187	8.9	626797	58.6	373203	38993	92085	3
58	591282	49.7	964133	8.9	627149	58.6	372851	39020	92073	2
59	591580	49.6	964080	8.9	627501	58.5	372499	39046	92062	1
60	591878		964026		627852		372148	39073	92050	0
	Cosine.		Sine.		Cotang.		Tang.	N. cos.	N. sine.	′

67 Degrees.

′	Sine.	D 10″	Cosine.	D. 10″	Tang.	D. 10″	Cotang.	N. sine.	N. cos.	
0	9.591878	49.6	9.964026	8.9	9.627852	58.5	10.372148	39073	92050	60
1	592176	49.5	963972	8.9	628203	58.5	371797	39100	92039	59
2	592473	49.5	963919	8.9	628554	58.5	371446	39127	92028	58
3	592770	49.5	963865	9.0	628905	58.4	371095	39153	92016	57
4	593067	49.4	963811	9.0	629256	58.4	370745	39180	92005	56
5	593363	49.4	963757	9.0	629606	58.3	370394	39207	91994	55
6	593659	49.3	963704	9.0	629956	58.3	370044	39234	91982	54
7	593955	49.3	963650	9.0	630306	58.3	369694	39260	91971	53
8	594251	49.3	963596	9.0	630656	58.3	369344	39287	91959	52
9	594547	49.2	963542	9.0	631005	58.2	368995	39314	91948	51
10	594842	49.2	963488	9.0	631355	58.2	368645	39341	91936	50
11	9.595137	49.1	9.963434	9.0	9.631704	58.2	10.368296	39367	91925	49
12	595432	49.1	963379	9.0	632053	58.1	367947	39394	91914	48
13	595727	49.1	963325	9.0	632401	58.1	367599	39421	91902	47
14	596021	49.0	963271	9.0	632750	58.1	367250	39448	91891	46
15	596315	49.0	963217	9.0	633098	58.0	366902	39474	91879	45
16	596609	48.9	963163	9.0	633447	58.0	366553	39501	91868	44
17	596903	48.9	963108	9.1	633795	58.0	366205	39528	91856	43
18	597196	48.9	963054	9.1	634143	57.9	365857	39555	91845	42
19	597490	48.8	962999	9.1	634490	57.9	365510	39581	91833	41
20	597783	48.8	962945	9.1	634838	57.9	365162	39608	91822	40
21	9.598075	48.7	9.962890	9.1	9.635185	57.8	10.364815	39635	91810	39
22	598368	48.7	962836	9.1	635532	57.8	364468	39661	91799	38
23	598660	48.7	962781	9.1	635879	57.8	364121	39688	91787	37
24	598952	48.6	962727	9.1	636226	57.7	363774	39715	91775	36
25	599244	48.6	962672	9.1	636572	57.7	363428	39741	91764	35
26	599536	48.5	962617	9.1	636919	57.7	363081	39768	91752	34
27	599827	48.5	962562	9.1	637265	57.7	362735	39795	91741	33
28	600118	48.5	962508	9.1	637611	57.6	362389	39822	91729	32
29	600409	48.4	962453	9.1	637956	57.6	362044	39848	91718	31
30	600700	48.4	962398	9 2	638302	57.6	361698	39875	91706	30
31	9.600990	48.4	9.962343	9.2	9.638647	57.5	10.361353	39902	91694	29
32	601280	48.3	962288	9.2	638992	57.5	361008	39928	91683	28
33	601570	48.3	962233	9.2	639337	57.5	360663	39955	91671	27
34	601860	48.2	962178	9.2	639682	57.4	360318	39982	91660	26
35	602150	48.2	962123	9.2	640027	57.4	359973	40008	91648	25
36	602439	48.2	962067	9.2	640371	57.4	359629	40035	91636	24
37	602728	48.1	962012	9.2	640716	57.3	359284	40062	91625	23
38	603017	48.1	961957	9.2	641060	57.3	358940	40088	91613	22
39	603305	48.1	961902	9.2	641404	57.3	358596	40115	91601	21
40	603594	48.0	961846	9.2	641747	57.2	358253	40141	91590	20
41	9.603882	48.0	9.961791	9.2	9.642091	57.2	10.357909	40168	91578	19
42	604170	47.9	961735	9.2	642434	57.2	357566	40195	91566	18
43	604457	47.9	961680	9.2	642777	57.2	357223	40221	91555	17
44	604745	47.9	961624	9.3	643120	57.1	356880	40248	91543	16
45	605032	47 8	961569	9.3	643463	57.1	356537	40275	91531	15
46	605319	47.8	961513	9.3	643806	57.1	356194	40301	91519	14
47	605606	47.8	961458	9.3	644148	57.0	355852	40328	91508	13
48	605892	47.7	961402	9.3	644490	57.0	355510	40355	91496	12
49	606179	47.7	961346	9.3	644832	57.0	355168	40381	91484	11
50	606465	47.6	961290	9.3	645174	56.9	354826	40408	91472	10
51	9.606751	47.6	9.961235	9.3	9.645516	56.9	10.354484	40434	91461	9
52	607036	47.6	961179	9.3	645857	56.9	354143	40461	91449	8
53	607322	47.5	961123	9.3	646199	56.9	353801	40488	91437	7
54	607607	47.5	961067	9.3	646540	56.8	353460	40514	91425	6
55	607892	47.4	961011	9.3	646881	56.8	353119	40541	91414	5
56	608177	47.4	960955	9.3	647222	56.8	352778	40567	91402	4
57	608461	47.4	960899	9.3	647562	56.7	352438	40594	91390	3
58	608745	47.3	960843	9.4	647903	56.7	352097	40621	91378	2
59	609029	47.3	960786	9.4	648243	56.7	351757	40647	91366	1
60	609313		960730		648583		351417	40674	91355	0
	Cosine.		Sine.		Cotang.		Tang.	N. cos.	N.sine.	′

66 Degrees.

′	Sine.	D. 10″	Cosine.	D. 10″	Tang.	D. 10″	Cotang.	N. sine	N. cos.	
0	9.609313	47.3	9.960730	9.4	9.648583	56.6	10.351417	40674	91355	60
1	609597	47.2	960674	9.4	648923	56.6	351077	40700	91343	59
2	609880	47.2	960618	9.4	649263	56.6	350737	40727	91331	58
3	610164	47.2	960561	9.4	649602	56 6	350398	40753	91319	57
4	610447	47.1	960505	9.4	649942	56.5	350058	40780	91307	56
5	610729	47.1	960448	9.4	650281	56.5	349719	40806	91295	55
6	611012	47.0	960392	9.4	650620	59.5	349380	40833	91283	54
7	611294	47.0	960335	9.4	650959	56.4	349041	40860	91272	53
8	611576	47.0	960279	9.4	651297	56.4	348703	40886	91260	52
9	611858	46.9	960222	9.4	651636	56.4	348364	40913	91248	51
10	612140	46.9	960165	9.4	651974	56.3	348026	40939	91236	50
11	9.612421	46.9	9.960109	9.5	9.652312	56.3	10.347688	40966	91224	49
12	612702	46.8	960052	9.5	652650	56.3	347350	40992	91212	48
13	612983	46.8	959995	9.5	652988	56.3	347012	41019	91200	47
14	613264	46.7	959938	9.5	653326	56.2	346674	41045	91188	46
15	613545	46.7	959882	9.5	653663	56.2	346337	41072	91176	45
16	613825	46.7	959825	9.5	654000	56.2	346000	41098	91164	44
17	614105	46.6	959768	9.5	654337	56.1	345663	41125	91152	43
18	614385	46.6	959711	9.5	654174	56.1	345326	41151	91140	42
19	614665	46.6	959654	9.5	655011	56.1	344989	41178	91128	41
20	614944	46.5	959596	9.5	655348	56.1	344652	41204	91116	40
21	9.615223	46.5	9.959539	9.5	9.655684	56.0	10.344316	41231	91104	39
22	615502	46.5	959482	9.5	656020	56.0	343980	41257	91092	38
23	615781	46.4	959425	9.5	656356	56.0	343644	41284	91080	37
24	616060	46.4	959368	9.5	656692	55.9	343308	41310	91068	36
25	616338	46.4	959310	9.6	657028	55.9	342972	41337	91056	35
26	616616	46.3	959253	9.6	657364	55.9	342636	41363	91044	34
27	616894	46.3	959195	9.6	657699	55.9	342301	41390	91032	33
28	617172	46.2	959138	9.6	658034	55.8	341966	41416	91020	32
29	617450	46.2	959081	9.6	658369	55.8	341631	41443	91008	31
30	617727	46.2	959023	9.6	658704	55.8	341296	41469	90996	30
31	9.618004	46.1	9.958965	9.6	9.659039	55.8	10.340961	41496	90984	29
32	618281	46.1	958908	9.6	659373	55.7	340627	41522	90972	28
33	618558	46.1	958850	9.6	659708	55.7	340292	41549	90960	27
34	618834	46.0	958792	9.6	660042	55.7	339958	41575	90948	26
35	619110	46.0	958734	9.6	660376	55.7	339624	41602	90936	25
36	619386	46.0	958677	9.6	660710	55.6	339290	41628	90924	24
37	619662	45.9	958619	9.6	661043	55.6	338957	41655	90911	23
38	619938	45.9	958561	9.6	661377	55.6	338623	41681	90899	22
39	620213	45.9	958503	9.7	661710	55.5	338290	41707	90887	21
40	620488	45.8	958445	9.7	662043	55.5	337957	41734	90875	20
41	9.620763	45.8	9.958387	9.7	9.662376	55.5	10.337624	41760	90863	19
42	621038	45.7	958329	9.7	662709	55.4	337291	41787	90851	18
43	621313	45.7	958271	9.7	663042	55.4	336958	41813	90839	17
44	621587	45.7	958213	9.7	663375	55.4	336625	41840	90826	16
45	621861	45.6	958154	9.7	663707	55.4	336293	41866	90814	15
46	622135	45.6	958096	9.7	664039	55.3	335961	41892	90802	14
47	622409	45.6	958038	9.7	664371	55.3	335629	41919	90790	13
48	622682	45.5	957979	9.7	664703	55.3	335297	41945	90778	12
49	622956	45.5	957921	9.7	665035	55.3	334965	41972	90766	11
50	623229	45.5	957863	9.7	665366	55.2	334634	41998	90753	10
51	9.623512	45.4	9.957804	9.7	9.665697	55.2	10.334303	42024	90741	9
52	623774	45.4	957746	9.8	666029	55.2	333971	42051	90729	8
53	624047	45.4	957687	9.8	666360	55.1	333640	42077	90717	7
54	624319	45.3	957628	9.8	666691	55.1	333309	42104	90704	6
55	624591	45.3	957570	9.8	667021	55.1	332979	42130	90692	5
56	624863	46.3	957511	9.8	667352	55.1	332648	42156	90680	4
57	625135	45.2	957452	9.8	667682	55.0	332318	42183	90668	3
58	625406	45.2	957393	9.8	668013	55.0	331987	42209	90655	2
59	625677	45.2	957335	9.8	668343	55.0	331657	42235	90643	1
60	625948		957276		668672		331328	42262	90631	0
	Cosine.		Sine.		Cotang.		Tang.	N. cos.	N. sine.	

65 Degrees.

′	Sine.	D. 10″	Cosine.	D. 10″	Tang.	D. 10″	Cotang.	N. sine.	N. cos.	
0	9.625948	45.1	9.957276	9.8	9.668673	55.0	10.331327	42262	90631	60
1	626219	45.1	957217	9.8	669002	54.9	330998	42288	90613	59
2	626490	45.1	957158	9.8	669332	54.9	330668	42315	90606	58
3	626760	45.0	957099	9.8	669661	54.9	330339	42341	90594	57
4	627030	45.0	957040	9.8	669991	54.8	330009	42367	90582	56
5	627300	45.0	956981	9.8	670320	54.8	329680	42394	90569	55
6	627570	44.9	956921	9.9	670649	54.8	329351	42420	90557	54
7	627840	44.9	956862	9.9	670977	54.8	329023	42446	90545	53
8	628109	44.9	956803	9.9	671306	54.7	328694	42473	90532	52
9	628378	44.8	956744	9.9	671634	54.7	328366	42499	90520	51
10	628647	44.8	956684	9.9	671963	54.7	328037	42525	90507	50
11	9.628916	44.7	9.956625	9.9	9.672291	54.7	10.327709	42552	90495	49
12	629185	44.7	956566	9.9	672619	54.6	327381	42578	90483	48
13	629453	44.7	956506	9.9	672947	54.6	327053	42604	90470	47
14	629721	44.6	956447	9.9	673274	54.6	326726	42631	90458	46
15	629989	44.6	956387	9.9	673602	54.6	326398	42657	90446	45
16	630257	44.6	956327	9.9	673929	54.5	326071	42683	90433	44
17	630524	44.6	956268	9.9	674257	54.5	325743	42709	90421	43
18	630792	44.5	956208	10.0	674584	54.5	325416	42736	90408	42
19	631059	44.5	956148	10.0	674910	54.4	325090	42762	90396	41
20	631326	44.5	956089	10.0	675237	54.4	324763	42788	90383	40
21	9.631593	44.4	9.956029	10.0	9.675564	54.4	10.324436	42815	90371	39
22	631859	44.4	955969	10.0	675890	54.4	324110	42841	90358	38
23	632125	44.4	955909	10.0	676216	54.3	323784	42867	90346	37
24	632392	44.3	955849	10.0	676543	54.3	323457	42894	90334	36
25	632658	44.3	955789	10.0	676869	54.3	323131	42920	90321	35
26	632923	44.3	955729	10.0	677194	54.3	322806	42946	90309	34
27	633189	44.2	955669	10.0	677520	54.2	322480	42972	90296	33
28	633454	44.2	955609	10.0	677846	54.2	322154	42999	90284	32
29	633719	44.2	955548	10.0	678171	54.2	321829	43025	90271	31
30	633984	44.1	955488	10.0	678496	54.2	321504	43051	90259	30
31	9.634249	44.1	9.955428	10.1	9.678821	54.1	10.321179	43077	90246	29
32	634514	44.0	955368	10.1	679146	54.1	320854	43104	90233	28
33	634778	44.0	955307	10.1	679471	54.1	320529	43130	90221	27
34	635042	44.0	955247	10.1	679795	54.1	320205	43156	90208	26
35	635303	43.9	955186	10.1	680120	54.0	319880	43182	90196	25
36	635570	43.9	955126	10.1	680444	54.0	319556	43209	90183	24
37	635834	43.9	955065	10.1	680768	54.0	319232	43235	90171	23
38	636097	43.8	955005	10.1	681092	54.0	318908	43261	90158	22
39	636360	43.8	954944	10.1	681416	53.9	318584	43287	90146	21
40	636623	43.8	954883	10.1	681740	53.9	318260	43313	90133	20
41	9.636886	43.7	9.954823	10.1	9.682063	53.9	10.317937	43340	90120	19
42	637148	43.7	954762	10.1	682387	53.9	317613	43366	90108	18
43	637411	43.7	954701	10.1	682710	53.8	317290	43392	90095	17
44	637673	43.7	954640	10.1	683033	53.8	316967	43418	90082	16
45	637935	43.6	954579	10.1	683356	53.8	316644	43445	90070	15
46	638197	43.6	954518	10.2	683679	53.8	316321	43471	90057	14
47	638458	43.6	954457	10.2	684001	53.7	315999	43497	90045	13
48	638720	43.5	954396	10.2	684324	53.7	315676	43523	90032	12
49	638981	43.5	954335	10.2	684646	53.7	315354	43549	90019	11
50	639242	43.5	954274	10.2	684968	53.7	315032	43575	90007	10
51	9.639503	43.4	9.954213	10.2	9.685290	53.6	10.314710	43602	89994	9
52	639764	43.4	954152	10.2	685612	53.6	314388	43628	89981	8
53	640024	43.4	954090	10.2	685934	53.6	314066	43654	89968	7
54	640284	43.3	954029	10.2	686255	53.6	313745	43680	89956	6
55	640544	43.3	953968	10.2	686577	53.5	313423	43706	89943	5
56	640804	43.3	953906	10.2	686898	53.5	313102	43733	89930	4
57	641064	43.2	953845	10.2	687219	53.5	312781	43759	89918	3
58	641324	43.2	953783	10.2	687540	53.5	312460	43785	89905	2
59	641584	43.2	953722	10.3	687861	53.4	312139	43811	89892	1
60	641842		953660		688182		311818	43837	89879	0
	Cosine.		Sine.		Cotang.		Tang.	N. cos.	N. sine.	′

64 Degrees.

'	Sine.	D. 10"	Cosine.	D. 10"	Tang.	D. 10"	Cotang.	N. sine.	N. cos.	
0	9.641842	43.1	9.953660	10.3	9.688182	53.4	10.311818	43837	89879	60
1	642101	43.1	953599	10.3	688502	53.4	311498	43863	89867	59
2	642360	43.1	953537	10.3	688823	53.4	311177	43889	89854	58
3	642618	43.0	953475	10.3	689143	53.3	310857	43916	89841	57
4	642877	43.0	953413	10.3	689463	53.3	310537	43942	89828	56
5	643135	43.0	953352	10.3	689783	53.3	310217	43968	89816	55
6	643393	43.0	953290	10.3	690103	53.3	309897	43994	89803	54
7	643650	42.9	953228	10.3	690423	53.3	309577	44020	89790	53
8	643908	42.9	953166	10.3	690742	53.2	309258	44046	89777	52
9	644165	42.9	953104	10.3	691062	53.2	308938	44072	89764	51
10	644423	42.8	953042	10.3	691381	53.2	308619	44098	89752	50
11	9.644680	42.8	9.952980	10.4	9.691700	53.1	10.308300	44124	89739	49
12	644936	42.8	952918	10.4	692019	53.1	307981	44151	89726	48
13	645193	42.7	952855	10.4	692338	53.1	307662	44177	89713	47
14	645450	42.7	952793	10.4	692656	53.1	307344	44203	89700	46
15	645706	42.7	952731	10.4	692975	53.1	307025	44229	89687	45
16	645962	42.6	952669	10.4	693293	53.0	306707	44255	89674	44
17	646218	42.6	952606	10.4	693612	53.0	306388	44281	89662	43
18	646474	42.6	952544	10.4	693930	53.0	306070	44307	89649	42
19	646729	42.5	952481	10.4	694248	53.0	305752	44333	89636	41
20	646984	42.5	952419	10.4	694566	52.9	305434	44359	89623	40
21	9.647240	42.5	9.952356	10.4	9.694883	52.9	10.305117	44385	89610	39
22	647494	42.4	952294	10.4	695201	52.9	304799	44411	89597	38
23	647749	42.4	952231	10.4	695518	52.9	304482	44437	89584	37
24	648004	42.4	952168	10.5	695836	52.9	304164	44464	89571	36
25	648258	42.4	952106	10.5	696153	52.8	303847	44490	89558	35
26	648512	42.3	952043	10.5	696470	52.8	303530	44516	89545	34
27	648766	42.3	951980	10.5	696787	52.8	303213	44542	89532	33
28	649020	42.3	951917	10.5	697103	52.8	302897	44568	89519	32
29	649274	42.2	951854	10.5	697420	52.7	302580	44594	89506	31
30	649527	42.2	951791	10.5	697736	52.7	302264	44620	89493	30
31	9.649781	42.2	9.951728	10.5	9.698053	52.7	10.301947	44646	89480	29
32	650034	42.2	951665	10.5	698369	52.7	301631	44672	89467	28
33	650287	42.1	951602	10.5	698685	52.6	301315	44698	89454	27
34	650539	42.1	951539	10.5	699001	52.6	300999	44724	89441	26
35	650792	42.1	951476	10.5	699316	52.6	300684	44750	89428	25
36	651044	42.0	951412	10.5	699632	52.6	300368	44776	89415	24
37	651297	42.0	951349	10.6	699947	52.6	300053	44802	89402	23
38	651549	42.0	951286	10.6	700263	52.5	299737	44828	89389	22
39	651800	41.9	951222	10.6	700578	52.5	299422	44854	89376	21
40	652052	41.9	951159	10.6	700893	52.5	299107	44880	89363	20
41	9.652304	41.9	9 951096	10.6	9.701208	52.4	10.298792	44906	89350	19
42	652555	41.8	951032	10.6	701523	52.4	298477	44932	89337	18
43	652806	41.8	950968	10.6	701837	52.4	298163	44958	89324	17
44	653057	41.8	950905	10.6	702152	52.4	297848	44984	89311	16
45	653308	41.8	950841	10.6	702466	52.4	297534	45010	89298	15
46	653558	41.7	950778	10.6	702780	52.3	297220	45036	89285	14
47	653808	41.7	950714	10.6	703095	52.3	296905	45062	89272	13
48	654059	41.7	950650	10.6	703409	52.3	296591	45088	89259	12
49	654309	41.6	950586	10.6	703723	52.3	296277	45114	89245	11
50	654558	41.6	950522	10.7	704036	52.2	295964	45140	89232	10
51	9.654808	41.6	9 950458	10.7	9 704350	52.2	10.295650	45166	89219	9
52	655058	41.6	950394	10.7	704663	52.2	295337	45192	89206	8
53	655307	41.5	950330	10.7	704977	52.2	295023	45218	89193	7
54	655556	41.5	950266	10.7	705290	52.2	294710	45243	89180	6
55	655805	41.5	950202	10.7	705603	52.1	294397	45269	89167	5
56	656054	41.4	950138	10.7	705916	52.1	294084	45295	89153	4
57	656302	41.4	950074	10.7	706228	52.1	293772	45321	89140	3
58	656551	41.4	950010	10.7	706541	52.1	293459	45347	89127	2
59	656799	41.3	949945	10.7	706854	52.1	293146	45373	89114	1
60	657047		949881		707166		292834	45399	89101	0
	Cosine.		Sine.		Cotang		Tang	N. cos.	N.sine.	'

63 Degrees.

′	Sine.	D. 10″	Cosine.	D. 10″	Tang.	D. 10″	Cotang.	N. sine.	N. cos.	
0	9.657047	41.3	9.949881	10.7	9.707166	52.0	10.292834	45399	89101	60
1	657295	41.3	949816	10.7	707478	52.0	292522	45425	89087	59
2	657542	41.2	949752	10.7	707790	52.0	292210	45451	89074	58
3	657790	41.2	949688	10.8	708102	52.0	291898	45477	89061	57
4	658037	41.2	949623	10.8	708414	51.9	291586	45503	89048	56
5	658284	41.2	949558	10.8	708726	51.9	291274	45529	89035	55
6	658531	41.1	949494	10.8	709037	51.9	290963	45554	89021	54
7	658778	41.1	949429	10.8	709349	51.9	290651	45580	89008	53
8	659025	41.1	949364	10.8	709660	51.9	290340	45606	88995	52
9	659271	41.0	949300	10.8	709971	51.8	290029	45632	88981	51
10	659517	41.0	949235	10.8	710282	51.8	289718	45658	88968	50
11	9.659763	41.0	9.949170	10.8	9.710593	51.8	10.289407	45684	88955	49
12	660009	40.9	949105	10.8	710904	51.8	289096	45710	88942	48
13	660255	40.9	949040	10.8	711215	51.8	288785	45736	88928	47
14	660501	40.9	948975	10.8	711525	51.7	288475	45762	88915	46
15	660746	40.9	948910	10.8	711836	51.7	288164	45787	88902	45
16	660991	40.8	948845	10.8	712146	51.7	287854	45813	88888	44
17	661236	40.8	948780	10.9	712456	51.7	287544	45839	88875	43
18	661481	40.8	948715	10.9	712766	51.6	287234	45865	88862	42
19	661726	40.7	948650	10.9	713076	51.6	286924	45891	88848	41
20	661970	40.7	948584	10.9	713386	51.6	286614	45917	88835	40
21	9.662214	40.7	9.948519	10.9	9.713696	51.6	10.286304	45942	88822	39
22	662459	40.7	948454	10.9	714005	51.6	285995	45968	88808	38
23	662703	40.6	948388	10.9	714314	51.5	285686	45994	88795	37
24	662946	40.6	948323	10.9	714624	51.5	285376	46020	88782	36
25	663190	40.6	948257	10.9	714933	51.5	285067	46046	88768	35
26	663433	40.5	948192	10.9	715242	51.5	284758	46072	88755	34
27	663677	40.5	948126	10.9	715551	51.4	284449	46097	88741	33
28	663920	40.5	948060	10.9	715860	51.4	284140	46123	88728	32
29	664163	40.5	947995	11.0	716168	51.4	283832	46149	88715	31
30	664406	40.4	947929	11.0	716477	51.4	283523	46175	88701	30
31	9.664648	40.4	9.947863	11.0	9.716785	51.4	10.283215	46201	88688	29
32	664891	40.4	947797	11.0	717093	51.3	282907	46226	88674	28
33	665133	40.3	947731	11.0	717401	51.3	282599	46252	88661	27
34	665375	40.3	947665	11.0	717709	51.3	282291	46278	88647	26
35	665617	40.3	947600	11.0	718017	51.3	281983	46304	88634	25
36	665859	40.2	947533	11.0	718325	51.3	281675	46330	88620	24
37	666100	40.2	947467	11.0	718633	51.2	281367	46355	88607	23
38	666342	40.2	947401	11.0	718940	51.2	281060	46381	38593	22
39	666583	40.2	947335	11.0	719248	51.2	280752	46407	88580	21
40	666824	40.1	947269	11.0	719555	51.2	280445	46433	88566	20
41	9.667065	40.1	9.947203	11.0	9.719862	51.2	10.280138	46458	88553	19
42	667305	40.1	947136	11.1	720169	51.1	279831	46484	88539	18
43	667546	40.1	947070	11.1	720476	51.1	279524	46510	88526	17
44	667786	40.0	947004	11.1	720783	51.1	279217	46536	88512	16
45	668027	40 0	946937	11.1	721089	51.1	278911	46561	88499	15
46	668267	40.0	946871	11.1	721396	51.1	278604	46587	88485	14
47	668506	39.9	946804	11.1	721702	51.0	278298	46613	88472	13
48	668746	39.9	946738	11.1	722009	51.0	277991	46639	88458	12
49	668986	39.9	946671	11.1	722315	51.0	277685	46664	88445	11
50	669225	39.9	946604	11.1	722621	51.0	277379	46690	88431	10
51	9.669464	39.8	9.946538	11.1	9.722927	51.0	10.277073	46716	88417	9
52	669703	39.8	946471	11.1	723232	50.9	276768	46742	88404	8
53	669942	39.8	946404	11.1	723538	50.9	276462	46767	88390	7
54	670181	39.7	946337	11.1	723844	50.9	276156	46793	88377	6
55	670419	39.7	946270	11.2	724149	50.9	275851	46819	88363	5
56	670658	39.7	946203	11.2	724454	50.9	275546	46844	88349	4
57	670896	39.7	946136	11.2	724759	50.8	275241	46870	88336	3
58	671134	39.6	946069	11.2	725065	50.8	274935	46896	88322	2
59	671372	39.6	946002	11.2	725369	50.8	274631	46921	88308	1
60	671609		945935		725674		274326	46947	88295	0
	Cosine.		Sine.		Cotang.		Tang.	N. cos.	N. sine.	′

62 Degrees.

′	Sine.	D. 10″	Cosine.	D. 10″	Tang.	D. 10″	Cotang.	N. sine.	N. cos.	
0	9.671609	39.6	9.945935	11.2	9.725674	50.8	10.274326	46947	88295	60
1	671847	39.5	945868	11.2	725979	50.8	274021	46973	88281	59
2	672084	39.5	945800	11.2	726284	50.7	273716	46999	88267	58
3	672321	39.5	945733	11.2	726588	50.7	273412	47024	88254	57
4	672558	39.5	945666	11.2	726892	50.7	273108	47050	88240	56
5	672795	39.4	945598	11.2	727197	50.7	272803	47076	88226	55
6	673032	39.4	945531	11.2	727501	50.7	272499	47101	88213	54
7	673268	39.4	945464	11.3	727805	50.6	272195	47127	88199	53
8	673505	39.4	945396	11.3	728109	50.6	271891	47153	88185	52
9	673741	39.3	945328	11.3	728412	50.6	271588	47178	88172	51
10	673977	39.3	945261	11.3	728716	50.6	271284	47204	88158	50
11	9.674213	39.3	9.945193	11.3	9.729020	50.6	10.270980	47229	88144	49
12	674448	39.2	945125	11.3	729323	50.5	270677	47255	88130	48
13	674684	39.2	945058	11.3	729626	50.5	270374	47281	88117	47
14	674919	39.2	944990	11.3	729929	50.5	270071	47306	88103	46
15	675155	39.2	944922	11.3	730233	50.5	269767	47332	88089	45
16	675390	39.1	944854	11.3	730535	50.5	269465	47358	88075	44
17	675624	39.1	944786	11.3	730838	50.4	269162	47383	88062	43
18	675859	39.1	944718	11.3	731141	50.4	268859	47409	88048	42
19	676094	39.1	944650	11.3	731444	50.4	268556	47434	88034	41
20	676328	39.0	944582	11.4	731746	50.4	268254	47460	88020	40
21	9.676562	39.0	9.944514	11.4	9.732048	50.4	10.267952	47486	88006	39
22	676796	39.0	944446	11.4	732351	50.3	267649	47511	87993	38
23	677030	39.0	944377	11.4	732653	50.3	267347	47537	87979	37
24	677264	38.9	944309	11.4	732955	50.3	267045	47562	87965	36
25	677498	38.9	944241	11.4	733257	50.3	266743	47588	87951	35
26	677731	38.9	944172	11.4	733558	50.3	266442	47614	87937	34
27	677964	38.8	944104	11.4	733860	50.2	266140	47639	87923	33
28	678197	38.8	944036	11.4	734162	50.2	265838	47665	87909	32
29	678430	38.8	943967	11.4	734463	50.2	265537	47690	87896	31
30	678663	38.8	943899	11.4	734764	50.2	265236	47716	87882	30
31	9.678895	38.7	9.943830	11.4	9.735066	50.2	10.264934	47741	87868	29
32	679128	38.7	943761	11.4	735367	50.2	264633	47767	87854	28
33	679360	38.7	943693	11.5	735668	50.1	264332	47793	87840	27
34	679592	38.7	943624	11.5	735969	50.1	264031	47818	87826	26
35	679824	38.6	943555	11.5	736269	50.1	263731	47844	87812	25
36	680056	38.6	943486	11.5	736570	50.1	263430	47869	87798	24
37	680288	38.6	943417	11.5	736871	50.1	263129	47895	87784	23
38	680519	38.5	943348	11.5	737171	50.0	262829	47920	87770	22
39	680750	38.5	943279	11.5	737471	50.0	262529	47946	87756	21
40	680982	38.5	943210	11.5	737771	50.0	262229	47971	87743	20
41	9.681213	38.5	9.943141	11.5	9.738071	50.0	10.261929	47997	87729	19
42	681443	38.4	943072	11.5	738371	50.0	261629	48022	87715	18
43	681674	38.4	943003	11.5	738671	49.9	261329	48048	87701	17
44	681905	38.4	942934	11.5	738971	49.9	261029	48073	87687	16
45	682135	38.4	942864	11.5	739271	49.9	260729	48099	87673	15
46	682365	38.3	942795	11.6	739570	49.9	260430	48124	87659	14
47	682595	38.3	942726	11.6	739870	49.9	260130	48150	87645	13
48	682825	38.3	942656	11.6	740169	49.9	259831	48175	87631	12
49	683055	38.3	942587	11.6	740468	49.8	259532	48201	87617	11
50	683284	38.2	942517	11.6	740767	49.8	259233	48226	87603	10
51	9.683514	38.2	9.942448	11.6	9.741066	49.8	10.258934	48252	87589	9
52	683743	38.2	942378	11.6	741365	49.8	258635	48277	87575	8
53	683972	38.2	942308	11.6	741664	49.8	258336	48303	87561	7
54	684201	38.1	942239	11.6	741962	49.7	258038	48328	87546	6
55	684430	38.1	942169	11.6	742261	49.7	257739	48354	87532	5
56	684658	38.1	942099	11.6	742559	49.7	257441	48379	87518	4
57	684887	38.0	942029	11.6	742858	49.7	257142	48405	87504	3
58	685115	38.0	941959	11.6	743156	49.7	256844	48430	87490	2
59	685343	38.0	941889	11.7	743454	49.7	256546	48456	87476	1
60	685571		941819		743752		256248	48481	87462	0
	Cosine.		Sine.		Cotang.		Tang.	N. cos.	N. sine.	′

'	Sine.	D. 10"	Cosine.	D. 10"	Tang.	D. 10"	Cotang.	N. sine.	N. cos.	
0	9.685571	38.0	9.941819	11.7	9.743752	49.6	10.256248	48481	87462	60
1	685799	37.9	941749	11.7	744050	49.6	255950	48506	87448	59
2	686027	37.9	941679	11.7	744348	49.6	255652	48532	87434	58
3	686254	37.9	941609	11.7	744645	49.6	255355	48557	87420	57
4	686482	37.9	941539	11.7	744943	49.6	255057	48583	87406	56
5	686709	37.8	941469	11.7	745240	49.6	254760	48608	87391	55
6	686936	37.8	941398	11.7	745538	49.5	254462	48634	87377	54
7	687163	37.8	941328	11.7	745835	49.5	254165	48659	87363	53
8	687389	37.8	941258	11.7	746132	49.5	253868	48684	87349	52
9	687616	37.7	941187	11.7	746429	49.5	253571	48710	87335	51
10	687843	37.7	941117	11.7	746726	49.5	253274	48735	87321	50
11	9.688069	37.7	9.941046	11.8	9.747023	49.4	10.252977	48761	87306	49
12	688295	37.7	940975	11.8	747319	49.4	252681	48786	87292	48
13	688521	37.6	940905	11.8	747616	49.4	252384	48811	87278	47
14	688747	37.6	940834	11.8	747913	49.4	252087	48837	87264	46
15	688972	37.6	940763	11.8	748209	49.4	251791	48862	87250	45
16	689198	37.6	940693	11.8	748505	49.3	251495	48888	87235	44
17	689423	37.5	940622	11.8	748801	49.3	251199	48913	87221	43
18	689648	37.5	940551	11.8	749097	49.3	250903	48938	87207	42
19	689873	37.5	940480	11.8	749393	49.3	250607	48964	87193	41
20	690098	37.5	940409	11.8	749689	49.3	250311	48989	87178	40
21	9.690323	37.4	9.940338	11.8	9.749985	49.3	10.250015	49014	87164	39
22	690548	37.4	940267	11.8	750281	49.2	249719	49040	87150	38
23	690772	37.4	940196	11.8	750576	49.2	249424	49065	87136	37
24	690996	37.4	940125	11.9	750872	49.2	249128	49090	87121	36
25	691220	37.3	940054	11.9	751167	49.2	248833	49116	87107	35
26	691444	37.3	939982	11.9	751462	49.2	248538	49141	87093	34
27	691668	37.3	939911	11.9	751757	49.2	248243	49166	87079	33
28	691892	37.3	939840	11.9	752052	49.1	247948	49192	87064	32
29	692115	37.2	939768	11.9	752347	49.1	247653	49217	87050	31
30	692339	37.2	939697	11.9	752642	49.1	247358	49242	87036	30
31	9.692562	37.2	9.939625	11.9	9.752937	49.1	10.247063	49268	87021	29
32	692785	37.1	939554	11.9	753231	49.1	246769	49293	87007	28
33	693008	37.1	939482	11.9	753526	49.1	246474	49318	86993	27
34	693231	37.1	939410	11.9	753820	49.0	246180	49344	86978	26
35	693453	37.1	939339	11.9	754115	49.0	245885	49369	86964	25
36	693676	37.0	939267	12.0	754409	49.0	245591	49394	86949	24
37	693898	37.0	939195	12.0	754703	49.0	245297	49419	86935	23
38	694120	37.0	939123	12.0	754997	49.0	245003	49445	86921	22
39	694342	37.0	939052	12.0	755291	49.0	244709	49470	86906	21
40	694564	36.9	938980	12.0	755585	48.9	244415	49495	86892	20
41	9.694786	36.9	9.938908	12.0	9.755878	48.9	10.244122	49521	86878	19
42	695007	36.9	938836	12.0	756172	48.9	243828	49546	86863	18
43	695229	36.9	938763	12.0	756465	48.9	243535	49571	86849	17
44	695450	36.8	938691	12.0	756759	48.9	243241	49596	86834	16
45	695671	36.8	938619	12.0	757052	48.9	242948	49622	86820	15
46	695892	36.8	938547	12.0	757345	48.8	242655	49647	86805	14
47	696113	36.8	938475	12.0	757638	48.8	242352	49672	86791	13
48	696334	36.7	938402	12.1	757931	48.8	242069	49697	86777	12
49	696554	36.7	938330	12.1	758224	48.8	241776	49723	86762	11
50	696775	36.7	938258	12.1	758517	48.8	241483	49748	86748	10
51	9.696995	36.7	9.938185	12.1	9.758810	48.8	10.241190	49773	86733	9
52	697215	36.6	938113	12.1	759102	48.7	240898	49798	86719	8
53	697435	36.6	938040	12.1	759395	48.7	240605	49824	86704	7
54	697654	36.6	937967	12.1	759687	48.7	240313	49849	86690	6
55	697874	36.6	937895	12.1	759979	48.7	240021	49874	86675	5
56	698094	36.5	937822	12.1	760272	48.7	239728	49899	86661	4
57	698313	36.5	937749	12.1	760564	48.7	239436	49924	86646	3
58	698532	36.5	937676	12.1	760856	48.6	239144	49950	86632	2
59	698751	36.5	937604	12.1	761148	48.6	238852	49975	86617	1
60	698970		937531		761439		238561	50000	86603	0
	Cosine.		Sine.		Cotang.		Tang.	N. cos.	N. sine.	'

60 Degrees.

'	Sine.	D. 10"	Cosine.	D. 10"	Tang.	D. 10"	Cotang.	N. sine.	N. cos.	
0	9 573575	52.1	9.967166	8.5	9.606410	60.6	10.393590	37461	92718	60
1	573888	52.0	967115	8.5	606773	60.6	393227	37488	92707	59
2	574200	52.0	967064	8.5	607137	60.5	392863	37515	92697	58
3	574512	51.9	967013	8.5	607500	60.5	392500	37542	92686	57
4	574824	51.9	966961	8.5	607863	60.4	392137	37569	92675	56
5	575136	51.9	966910	8.5	608225	60.4	391775	37595	92664	55
6	575447	51.8	966859	8.5	608588	60.4	391412	37622	92653	54
7	575758	51.8	966808	8.5	608950	60.3	391050	37649	92642	53
8	576069	51.7	966756	8.6	609312	60.3	390688	37676	92631	52
9	576379	51.7	966705	8.6	609674	60.3	390326	37703	92620	51
10	576689	51.6	966653	8.6	610036	60.2	389964	37730	92609	50
11	9.576999	51.6	9.966602	8.6	9.610397	60.2	10.389603	37757	92598	49
12	577309	51.6	966550	8.6	610759	60.2	389241	37784	92587	48
13	577618	51.5	966499	8.6	611120	60.1	388880	37811	92576	47
14	577927	51.5	966447	8.6	611480	60.1	388520	37838	92565	46
15	578236	51.4	966395	8.6	611841	60.1	388159	37865	92554	45
16	578545	51.4	966344	8.6	612201	60.0	387799	37892	92543	44
17	578853	51.3	966292	8.6	612561	60.0	387439	37919	92532	43
18	579162	51.3	966240	8.6	612921	60.0	387079	37946	92521	42
19	579470	51.3	966188	8.6	613281	59.9	386719	37973	92510	41
20	579777	51.2	966136	8.6	613641	59.9	386359	37999	92499	40
21	9.580085	51.2	9.966085	8.7	9.614000	59.8	10.386000	38026	92488	39
22	580392	51.1	966033	8.7	614359	59.8	385641	38053	92477	38
23	580699	51.1	965981	8.7	614718	59.8	385282	38080	92466	37
24	581005	51.1	965928	8.7	615077	59.7	384923	38107	92455	36
25	581312	51.0	965876	8.7	615435	59.7	384565	38134	92444	35
26	581618	51.0	965824	8.7	615793	59.7	384207	38161	92432	34
27	581924	50.9	965772	8.7	616151	59.6	383849	38188	92421	33
28	582229	50.9	965720	8.7	616509	59.6	383491	38215	92410	32
29	582535	50.9	965668	8.7	616867	59.6	383133	38241	92399	31
30	582840	50.8	965615	8.7	617224	59.5	382776	38268	92388	30
31	9.583145	50.8	9.965563	8.7	9.617582	59.5	10.382418	38295	92377	29
32	583449	50.7	965511	8.7	617939	59.5	382061	38322	92366	28
33	583754	50.7	965458	8.7	618295	59.4	381705	38349	92355	27
34	584058	50.6	965406	8.7	618652	59.4	381348	38376	92343	26
35	584361	50.6	965353	8.8	619008	59.4	380992	38403	92332	25
36	584665	50.6	965301	8.8	619364	59.3	380636	38430	92321	24
37	584968	50.5	965248	8.8	619721	59.3	380279	38456	92310	23
38	585272	50.5	965195	8.8	620076	59.3	379924	38483	92299	22
39	585574	50.4	965143	8.8	620432	59.2	379568	38510	92287	21
40	585877	50.4	965090	8.8	620787	59.2	379213	38537	92276	20
41	9.586179	50.3	9.965037	8.8	9.621142	59.2	10.378858	38564	92265	19
42	586482	50.3	964984	8.8	621497	59.1	378503	38591	92254	18
43	586783	50.3	964931	8.8	621852	59.1	378148	38617	92243	17
44	587085	50.2	964879	8.8	622207	59.0	377793	38644	92231	16
45	587386	50.2	964826	8.8	622561	59.0	377439	38671	92220	15
46	587688	50.1	964773	8.8	622915	59.0	377085	38698	92209	14
47	587989	50.1	964719	8.8	623269	58.9	376731	38725	92198	13
48	588289	50.1	964666	8.9	623623	58.9	376377	38752	92186	12
49	588590	50.0	964613	8.9	623976	58.9	376024	38778	92175	11
50	588890	50.0	964560	8.9	624330	58.8	375670	38805	92164	10
51	9.589190	49.9	9.964507	8.9	9.624683	58.8	10.375317	38832	92152	9
52	589489	49.9	964454	8.9	625036	58.8	374964	38859	92141	8
53	589789	49.9	964400	8.9	625388	58.7	374612	38886	92130	7
54	590088	49.8	964347	8.9	625741	58.7	374259	38912	92119	6
55	590387	49.8	964294	8.9	626093	58.7	373907	38939	92107	5
56	590686	49.7	964240	8.9	626445	58.6	373555	38966	92096	4
57	590984	49.7	964187	8.9	626797	58.6	373203	38993	92085	3
58	591282	49.7	964133	8.9	627149	58.6	372851	39020	92073	2
59	591580	49.6	964080	8.9	627501	58.5	372499	39046	92062	1
60	591878		934026		627852		372148	39073	92050	0
	Cosine.		Sine.		Cotang.		Tang.	N. cos.	N.sine.	'

67 Degrees.

'	Sine.	D. 10"	Cosine.	D. 10"	Tang.	D. 10"	Cotang.	N.sine.	N. cos.	
0	9.711839	35.0	9.933036	12.6	9.778774	47.7	10.221226	51504	85717	60
1	712050	35.0	932990	12.7	779060	47.7	220940	51529	85702	59
2	712260	35.0	932914	12.7	779346	47.6	220654	51554	85687	58
3	712469	34.9	932838	12.7	779632	47.6	220368	51579	85672	57
4	712679	34.9	932762	12.7	779918	47.6	220082	51604	85657	56
5	712889	34.9	932685	12.7	780203	47.6	219797	51628	85642	55
6	713098	34.9	932609	12.7	780489	47.6	219511	51653	85627	54
7	713308	34.9	932533	12.7	780775	47.6	219225	51678	85612	53
8	713517	34.8	932457	12.7	781060	47.6	218940	51703	85597	52
9	713726	34.8	932380	12.7	781346	47.5	218654	51728	85582	51
10	713935	34.8	932304	12.7	781631	47.5	218369	51753	85567	50
11	9.714144	34.8	9.932228	12.7	9.781916	47.5	10.218084	51778	85551	49
12	714352	34.7	932151	12.7	782201	47.5	217799	51803	85536	48
13	714561	34.7	932075	12.8	782486	47.5	217514	51828	85521	47
14	714769	34.7	931998	12.8	782771	47.5	217229	51852	85506	46
15	714978	34.7	931921	12.8	783056	47.5	216944	51877	85491	45
16	715186	34.7	931845	12.8	783341	47.5	216659	51902	85476	44
17	715394	34.6	931768	12.8	783626	47.4	216374	51927	85461	43
18	715602	34.6	931691	12.8	783910	47.4	216090	51952	85446	42
19	715809	34.6	931614	12.8	784195	47.4	215805	51977	85431	41
20	716017	34.6	931537	12.8	784479	47.4	215521	52002	85416	40
21	9.716224	34.5	9.931460	12.8	9.784764	47.4	10.215236	52026	85401	39
22	716432	34.5	931383	12.8	785048	47.4	214952	52051	85385	38
23	716639	34.5	931306	12.8	785332	47.3	214668	52076	85370	37
24	716846	34.5	931229	12.9	785616	47.3	214384	52101	85355	36
25	717053	34.5	931152	12.9	785900	47.3	214100	52126	85340	35
26	717259	34.4	931075	12.9	786184	47.3	213816	52151	85325	34
27	717466	34.4	930998	12.9	786468	47.3	213532	52175	85310	33
28	717673	34.4	930921	12.9	786752	47.3	213248	52200	85294	32
29	717879	34.4	930843	12.9	787036	47.3	212964	52225	85279	31
30	718085	34.3	930766	12.9	787319	47.2	212681	52250	85264	30
31	9.718291	34.3	9.930688	12.9	9.787603	47.2	10.212397	52275	85249	29
32	718497	34.3	930611	12.9	787886	47.2	212114	52299	85234	28
33	718703	34.3	930533	12.9	788170	47.2	211830	52324	85218	27
34	718909	34.3	930456	12.9	788453	47.2	211547	52349	85203	26
35	719114	34.2	930378	12.9	788736	47.2	211264	52374	85188	25
36	719320	34.2	930300	13.0	789019	47.2	210981	52399	85173	24
37	719525	34.2	930223	13.0	789302	47.1	210698	52423	85157	23
38	719730	34.2	930145	13.0	789585	47.1	210415	52448	85142	22
39	719935	34.1	930067	13.0	789868	47.1	210132	52473	85127	21
40	720140	34.1	929989	13.0	790151	47.1	209849	52498	85112	20
41	9.720345	34.1	9.929911	13.0	9.790433	47.1	10.209567	52522	85096	19
42	720549	34.1	929833	13.0	790716	47.1	209284	52547	85081	18
43	720754	34.0	929755	13.0	790999	47.1	209001	52572	85066	17
44	720958	34.0	929677	13.0	791281	47.1	208719	52597	85051	16
45	721162	34 0	929599	13.0	791563	47.0	208437	52621	85035	15
46	721366	34.0	929521	13.0	791846	47.0	208154	52646	85020	14
47	721570	34.0	929442	13.0	792128	47.0	207872	52671	85005	13
48	721774	33.9	929364	13.1	792410	47.0	207590	52696	84989	12
49	721978	33.9	929286	13.1	792692	47.0	207308	52720	84974	11
50	722181	33.9	929207	13.1	792974	47.0	207026	52745	84959	10
51	9.722385	33.9	9.929129	13.1	9.793256	47.0	10.206744	52770	84943	9
52	722588	33.9	929050	13.1	793538	46.9	206462	52794	84928	8
53	722791	33.8	928972	13.1	793819	46.9	206181	52819	84913	7
54	722994	33.8	928893	13.1	794101	46.9	205899	52844	84897	6
55	723197	33.8	928815	13.1	794383	46.9	205617	52869	84882	5
56	723400	33.8	928736	13.1	794664	46.9	205336	52893	84866	4
57	723603	33.7	928657	13.1	794945	46.9	205055	52918	84851	3
58	723805	33.7	928578	13.1	795227	46.9	204773	52943	84836	2
59	724007	33.7	928499	13.1	795508	46.8	204492	52967	84820	1
60	724210		928420		795789		204211	52992	84805	0
	Cosine.		Sine.		Cotang.		Tang.	N. cos.	N.sine.	'

58 Degrees.

′	Sine.	D. 10″	Cosine.	D. 10′	Tang.	D. 10′	Cotang.	N. sine.	N. cos.	
0	9.609313	47.3	9.960730	9.4	9.648583	56.6	10.351417	40674	91355	60
1	609597	47.2	960674	9.4	648923	56.6	351077	40700	91343	59
2	609880	47.2	960618	9.4	649263	56.6	350737	40727	91331	58
3	610164	47.2	960561	9.4	649602	56 6	350398	40753	91319	57
4	610447	47.1	960505	9.4	649942	56.5	350058	40780	91307	56
5	610729	47.1	960448	9.4	650281	56.5	349719	40806	91295	55
6	611012	47.0	960392	9.4	650620	59.5	349380	40833	91283	54
7	611294	47.0	960335	9.4	650959	56.4	349041	40860	91272	53
8	611576	47.0	960279	9.4	651297	56.4	348703	40886	91260	52
9	611858	46.9	960222	9.4	651636	56.4	348364	40913	91248	51
10	612140	46.9	960165	9.4	651974	56.3	348026	40939	91236	50
11	9.612421	46.9	9.960109	9.5	9.652312	56.3	10.347688	40966	91224	49
12	612702	46.8	960052	9.5	652650	56.3	347350	40992	91212	48
13	612983	46.8	959995	9.5	652988	56.3	347012	41019	91200	47
14	613264	46.7	959938	9.5	653326	56.2	346674	41045	91188	46
15	613545	46.7	959882	9.5	653663	56.2	346337	41072	91176	45
16	613825	46.7	959825	9.5	654000	56.2	346000	41098	91164	44
17	614105	46.6	959768	9.5	654337	56.1	345663	41125	91152	43
18	614385	46.6	959711	9.5	654174	56.1	345326	41151	91140	42
19	614665	46.6	959654	9.5	655011	56.1	344989	41178	91128	41
20	614944	46.5	959596	9.5	655348	56.1	344652	41204	91116	40
21	9.615223	46.5	9.959539	9.5	9.655684	56.0	10.344316	41231	91104	39
22	615502	46.5	959482	9.5	656020	56.0	343980	41257	91092	38
23	615781	46.4	959425	9.5	656356	56.0	343644	41284	91080	37
24	616060	46.4	959368	9.5	656692	55.9	343308	41310	91068	36
25	616338	46.4	959310	9.6	657028	55.9	342972	41337	91056	35
26	616616	46.3	959253	9.6	657364	55.9	342636	41363	91044	34
27	616894	46.3	959195	9.6	657699	55.9	342301	41390	91032	33
28	617172	46.2	959138	9.6	658034	55.8	341966	41416	91020	32
29	617450	46.2	959081	9.6	658369	55.8	341631	41443	91008	31
30	617727	46.2	959023	9.6	658704	55.8	341296	41469	90996	30
31	9.618004	46.1	9.958965	9.6	9.659039	55.8	10.340961	41496	90984	29
32	618281	46.1	958908	9.6	659373	55.7	340627	41522	90972	28
33	618558	46.1	958850	9.6	659708	55.7	340292	41549	90960	27
34	618834	46.0	958792	9.6	660042	55.7	339958	41575	90948	26
35	619110	46.0	958734	9.6	660376	55.7	339624	41602	90936	25
36	619386	46.0	958677	9.6	660710	55.6	339290	41628	90924	24
37	619662	45.9	958619	9.6	661043	55.6	338957	41655	90911	23
38	619938	45.9	958561	9.6	661377	55.6	338623	41681	90899	22
39	620213	45.9	958503	9.7	661710	55.5	338290	41707	90887	21
40	620488	45.8	958445	9.7	662043	55.5	337957	41734	90875	20
41	9.620763	45.8	9.958387	9.7	9.662376	55.5	10.337624	41760	90863	19
42	621038	45.7	958329	9.7	662709	55.4	337291	41787	90851	18
43	621313	45.7	958271	9.7	663042	55.4	336958	41813	90839	17
44	621587	45.7	958213	9.7	663375	55.4	336625	41840	90826	16
45	621861	45.6	958154	9.7	663707	55.4	336293	41866	90814	15
46	622135	45.6	958096	9.7	664039	55.3	335961	41892	90802	14
47	622409	45.6	958038	9.7	664371	55.3	335629	41919	90790	13
48	622682	45.5	957979	9.7	664703	55.3	335297	41945	90778	12
49	622956	45.5	957921	9.7	665035	55.3	334965	41972	90766	11
50	623229	45.5	957863	9.7	665366	55.2	334634	41998	90753	10
51	9.623512	45.4	9.957804	9.7	9.665697	55.2	10.334303	42024	90741	9
52	623774	45.4	957746	9.8	666029	55.2	333971	42051	90729	8
53	624047	45.4	957687	9.8	666360	55.1	333620	42077	90717	7
54	624319	45.3	957628	9.8	666691	55.1	333309	42104	90704	6
55	624591	45.3	957570	9.8	667021	55.1	332979	42130	90692	5
56	624863	46.3	957511	9.8	667352	55.1	332648	42156	90680	4
57	625135	45.2	957452	9.8	667682	55.0	332318	42183	90668	3
58	625406	45.2	957393	9.8	668013	55.0	331987	42209	90655	2
59	625677	45.2	957335	9.8	668343	55.0	331657	42235	90643	1
60	625948		957276		668672		331328	42262	90631	0
	Cosine.		Sine.		Cotang.		Tang.	N. cos.	N. sine.	′

65 Degrees.

′	Sine.	D. 10″	Cosine.	D. 10″	Tang.	D. 10″	Cotang.	N. sine.	N. cos.	
0	9.736109	32.4	9.923591	13.7	9.812517	46.1	10.187482	54464	83867	60
1	736303	32.4	923509	13.7	812794	46.1	187206	54488	83851	59
2	736498	32.4	923427	13.7	813070	46.1	186930	54513	83835	58
3	736692	32.3	923345	13.7	813347	46.0	186653	54537	83819	57
4	736886	32.3	923263	13.7	813623	46.0	186377	54561	83804	56
5	737080	32.3	923181	13.7	813899	46.0	186101	54586	83788	55
6	737274	32.3	923098	13.7	814175	46.0	185825	54610	83772	54
7	737467	32.3	923016	13.7	814452	46.0	185548	54635	83756	53
8	737661	32.2	922933	13.7	814728	46.0	185272	54659	83740	52
9	737855	32.2	922851	13.7	815004	46.0	184996	54683	83724	51
10	738048	32.2	922768	13.8	815279	46.0	184721	54708	83708	50
11	9.738241	32.2	9.922686	13.8	9.815555	45.9	10.184445	54732	83692	49
12	738434	32.2	922603	13.8	815831	45.9	184169	54756	83676	48
13	738627	32.1	922520	13.8	816107	45.9	183893	54781	83660	47
14	738820	32.1	922438	13.8	816382	45.9	183618	54805	83645	46
15	739013	32.1	922355	13.8	816658	45.9	183342	54829	83629	45
16	739206	32.1	922272	13.8	816933	45.9	183067	54854	83613	44
17	739398	32.1	922189	13.8	817209	45.9	182791	54878	83597	43
18	739590	32.0	922106	13.8	817484	45.9	182516	54902	83581	42
19	739783	32.0	922023	13.8	817759	45.9	182241	54927	83565	41
20	739975	32.0	921940	13.8	818035	45.8	181965	54951	83549	40
21	9.740167	32.0	9.921857	13.9	9.818310	45.8	10.181690	54975	83533	39
22	740359	32.0	921774	13.9	818585	45.8	181415	54999	83517	38
23	740550	31.9	921691	13.9	818860	45.8	181140	55024	83501	37
24	740742	31.9	921607	13.9	819135	45.8	180865	55048	83485	36
25	740934	31.9	921524	13.9	819410	45.8	180590	55072	83469	35
26	741125	31.9	921441	13.9	819684	45.8	180316	55097	83453	34
27	741316	31.9	921357	13.9	819959	45.8	180041	55121	83437	33
28	741508	31.8	921274	13.9	820234	45.8	179766	55145	83421	32
29	741699	31.8	921190	13.9	820508	45.7	179492	55169	83405	31
30	741889	31.8	921107	13.9	820783	45.7	179217	55194	83389	30
31	9.742080	31.8	9.921023	13.9	9.821057	45.7	10.178943	55218	83373	29
32	742271	31.8	920939	14.0	821332	45.7	178668	55242	83356	28
33	742462	31.7	920856	14.0	821606	45.7	178394	55266	83340	27
34	742652	31.7	920772	14.0	821880	45.7	178120	55291	83324	26
35	742842	31.7	920688	14.0	822154	45.7	177846	55315	83308	25
36	743033	31.7	920604	14.0	822429	45.7	177571	55339	83292	24
37	743223	31.7	920520	14.0	822703	45.7	177297	55363	83276	23
38	743413	31.6	920436	14.0	822977	45.6	177023	55388	83260	22
39	743602	31.6	920352	14.0	823250	45.6	176750	55412	83244	21
40	743792	31.6	920268	14.0	823524	45.6	176476	55436	83228	20
41	9.743982	31.6	9.920184	14.0	9.823798	45.6	10.176202	55460	83212	19
42	744171	31.6	920099	14.0	824072	45.6	175928	55484	83195	18
43	744361	31.5	920015	14.0	824345	45.6	175655	55509	83179	17
44	744550	31.5	919931	14.1	824619	45.6	175381	55533	83163	16
45	744739	31.5	919846	14.1	824893	45.6	175107	55557	83147	15
46	744928	31.5	919762	14.1	825166	45.6	174834	55581	83131	14
47	745117	31.5	919677	14.1	825439	45.5	174561	55605	83115	13
48	745306	31.4	919593	14.1	825713	45.5	174287	55630	83098	12
49	745494	31.4	919508	14.1	825986	45.5	174014	55654	83082	11
50	745683	31.4	919424	14.1	826259	45.5	173741	55678	83066	10
51	9.745871	31.4	9.919339	14.1	9.826532	45.5	10.173468	55702	83050	9
52	746059	31.4	919254	14.1	826805	45.5	173195	55726	83034	8
53	746248	31.3	919169	14.1	827078	45.5	172922	55750	83017	7
54	746436	31.3	919085	14.1	827351	45.5	172649	55775	83001	6
55	746624	31.3	919000	14.1	827624	45.5	172376	55799	82985	5
56	746812	31.3	918915	14.2	827897	45.4	172103	55823	82969	4
57	746999	31.3	918830	14.2	828170	45.4	171830	55847	82953	3
58	747187	31.2	918745	14.2	828442	45.4	171558	55871	82936	2
59	747374	31.2	918659	14.2	828716	45.4	171285	55895	82920	1
60	747562		918574		828987		171013	55919	82904	0
	Cosine.		Sine.		Cotang.		Tang.	N. cos.	N.sine.	′

56 Degrees.

′	Sine.	D. 10″	Cosine.	D. 10″	Tang.	D. 10″	Cotang.	N. sine.	N. cos.	
0	9.641842	43.1	9.953660	10.3	9.688182	53.4	10.311818	43837	89879	60
1	642101	43.1	953599	10.3	688502	53.4	311498	43863	89867	59
2	642360	43.1	953537	10.3	688823	53.4	311177	43889	89854	58
3	642618	43.0	953475	10.3	689143	53.3	310857	43916	89841	57
4	642877	43.0	953413	10.3	689463	53.3	310537	43942	89828	56
5	643135	43.0	953352	10.3	689783	53.3	310217	43968	89816	55
6	643393	43.0	953290	10.3	690103	53.3	309897	43994	89803	54
7	643650	42.9	953228	10.3	690423	53.3	309577	44020	89790	53
8	643908	42.9	953166	10.3	690742	53.2	309258	44046	89777	52
9	644165	42.9	953104	10.3	691062	53.2	308938	44072	89764	51
10	644423	42.8	953042	10.3	691381	53.2	308619	44098	89752	50
11	9.644680	42.8	9.952980	10.4	9.691700	53.1	10.308300	44124	89739	49
12	644938	42.8	952918	10.4	692019	53.1	307981	44151	89726	48
13	645193	42.7	952855	10.4	692338	53.1	307662	44177	89713	47
14	645450	42.7	952793	10.4	692656	53.1	307344	44203	89700	46
15	645706	42.7	952731	10.4	692975	53.1	307025	44229	89687	45
16	645962	42.6	952669	10.4	693293	53.0	306707	44255	89674	44
17	646218	42.6	952606	10.4	693612	53.0	306388	44281	89662	43
18	646474	42.6	952544	10.4	693930	53.0	306070	44307	89649	42
19	646729	42.5	952481	10.4	694248	53.0	305752	44333	89636	41
20	646984	42.5	952419	10.4	694566	52.9	305434	44359	89623	40
21	9.647240	42.5	9.952356	10.4	9.694883	52.9	10.305117	44385	89610	39
22	647494	42.4	952294	10.4	695201	52.9	304799	44411	89597	38
23	647749	42.4	952231	10.4	695518	52.9	304482	44437	89584	37
24	648004	42.4	952168	10.5	695836	52.9	304164	44464	89571	36
25	648258	42.4	952106	10.5	696153	52.8	303847	44490	89558	35
26	648512	42.3	952043	10.5	696470	52.8	303530	44516	89545	34
27	648766	42.3	951980	10.5	696787	52.8	303213	44542	89532	33
28	649020	42.3	951917	10.5	697103	52.8	302897	44568	89519	32
29	649274	42.2	951854	10.5	697420	52.7	302580	44594	89506	31
30	649527	42.2	951791	10.5	697736	52.7	302264	44620	89493	30
31	9.649781	42.2	9.951728	10.5	9.698053	52.7	10.301947	44646	89480	29
32	650034	42.2	951665	10.5	698369	52.7	301631	44672	89467	28
33	650287	42.1	951602	10.5	698685	52.6	301315	44698	89454	27
34	650539	42.1	951539	10.5	699001	52.6	300999	44724	89441	26
35	650792	42.1	951476	10.5	699316	52.6	300684	44750	89428	25
36	651044	42.0	951412	10.5	699632	52.6	300368	44776	89415	24
37	651297	42.0	951349	10.6	699947	52.6	300053	44802	89402	23
38	651549	42.0	951286	10.6	700263	52.5	299737	44828	89389	22
39	651800	41.9	951222	10.6	700578	52.5	299422	44854	89376	21
40	652052	41.9	951159	10.6	700893	52.5	299107	44880	89363	20
41	9.652304	41.9	9.951096	10.6	9.701208	52.4	10.298792	44906	89350	19
42	652555	41.8	951032	10.6	701523	52.4	298477	44932	89337	18
43	652806	41.8	950968	10.6	701837	52.4	298163	44958	89324	17
44	653057	41.8	950905	10.6	702152	52.4	297848	44984	89311	16
45	653308	41.8	950841	10.6	702466	52.4	297534	45010	89298	15
46	653558	41.7	950778	10.6	702780	52.3	297220	45036	89285	14
47	653808	41.7	950714	10.6	703095	52.3	296905	45062	89272	13
48	654059	41.7	950650	10.6	703409	52.3	296591	45088	89259	12
49	654309	41.6	950586	10.6	703723	52.3	296277	45114	89245	11
50	654558	41.6	950522	10.7	704036	52.2	295964	45140	89232	10
51	9.654808	41.6	9.950458	10.7	9.704350	52.2	10.295650	45166	89219	9
52	655058	41.6	950394	10.7	704663	52.2	295337	45192	89206	8
53	655307	41.5	950330	10.7	704977	52.2	295023	45218	89193	7
54	655556	41.5	950366	10.7	705290	52.2	294710	45243	89180	6
55	655805	41.5	950202	10.7	705603	52.1	294397	45269	89167	5
56	656054	41.4	950138	10.7	705916	52.1	294084	45295	89153	4
57	656302	41.4	950074	10.7	706228	52.1	293772	45321	89140	3
58	656551	41.4	950010	10.7	706541	52.1	293459	45347	89127	2
59	656799	41.3	949945	10.7	706854	52.1	293146	45373	89114	1
60	657047		949881		707166		292834	45399	89101	0
	Cosine.		Sine.		Cotang.		Tang.	N. cos.	N. sine.	′

Log. Sines and Tangents. (35°) Natural Sines. TABLE II.

'	Sine.	D. 10"	Cosine.	D. 10"	Tang.	D. 10"	Cotang.	N. sine.	N. cos.	
0	9.758591	30.1	9.913365	14.7	9.845227	44.8	10.154773	57358	81915	60
1	758772	30.0	913276	14.7	845496	44.8	154504	57381	81899	59
2	758952	30.0	913187	14.8	845764	44.8	154236	57405	81882	58
3	759132	30.0	913099	14.8	846033	44.8	153967	57429	81865	57
4	759312	30.0	913010	14.8	846302	44.8	153698	57453	81848	56
5	759492	30.0	912922	14.8	846570	44.7	153430	57477	81832	55
6	759672	29.9	912833	14.8	846839	44.7	153161	57501	81815	54
7	759852	29.9	912744	14.8	847107	44.7	152893	57524	81798	53
8	760031	29.9	912655	14.8	847376	44.7	152624	57548	81782	52
9	760211	29.9	912566	14.8	847644	44.7	152356	57572	81765	51
10	760390	29.9	912477	14.8	847913	44.7	152087	57596	81748	50
11	9.760569	29.8	9.912388	14.8	9.848181	44.7	10.151819	57619	81731	49
12	760748	29.8	912299	14.9	848449	44.7	151551	57643	81714	48
13	760927	29.8	912210	14.9	848717	44.7	151283	57667	81698	47
14	761106	29.8	912121	14.9	848986	44.7	151014	57691	81681	46
15	761285	29.8	912031	14.9	849254	44.7	150746	57715	81664	45
16	761464	29.8	911942	14.9	849522	44.7	150478	57738	81647	44
17	761642	29.7	911853	14.9	849790	44.6	150210	57762	81631	43
18	761821	29.7	911763	14.9	850058	44.6	149942	57786	81614	42
19	761999	29.7	911674	14.9	850325	44.6	149675	57810	81597	41
20	762177	29.7	911584	14.9	850593	44.6	149407	57833	81580	40
21	9.762356	29.7	9.911495	14.9	9.850861	44.6	10.149139	57857	81563	39
22	762534	29.6	911405	14.9	851129	44.6	148871	57881	81546	38
23	762712	29.6	911315	15.0	851396	44.6	148604	57904	81530	37
24	762889	29.6	911226	15.0	851664	44.6	148336	57928	81513	36
25	763067	29.6	911136	15.0	851931	44.6	148069	57952	81496	35
26	763245	29.6	911046	15.0	852199	44.6	147801	57976	81479	34
27	763422	29.6	910956	15.0	852466	44.6	147534	57999	81462	33
28	763600	29.5	910866	15.0	852733	44.5	147267	58023	81445	32
29	763777	29.5	910776	15.0	853001	44.5	146999	58047	81428	31
30	763954	29.5	910686	15.0	853268	44.5	146732	58070	81412	30
31	9.764131	29.5	9.910596	15.0	9.853535	44.5	10.146465	58094	81395	29
32	764308	29.5	910506	15.0	853802	44.5	146198	58118	81378	28
33	764485	29.4	910415	15.0	854069	44.5	145931	58141	81361	27
34	764662	29.4	910325	15.1	854336	44.5	145664	58165	81344	26
35	764838	29.4	910235	15.1	854603	44.5	145397	58189	81327	25
36	765015	29.4	910144	15.1	854870	44.5	145130	58212	81310	24
37	765191	29.4	910054	15.1	855137	44.5	144863	58236	81293	23
38	765367	29.4	909963	15.1	855404	44.5	144596	58260	81276	22
39	765544	29.3	909873	15.1	855671	44.4	144329	58283	81259	21
40	765720	29.3	909782	15.1	855938	44.4	144062	58307	81242	20
41	9.765896	29.3	9.909691	15.1	9.856204	44.4	10.143796	58330	81225	19
42	766072	29.3	909601	15.1	856471	44.4	143529	58354	81208	18
43	766247	29.3	909510	15.1	856737	44.4	143263	58378	81191	17
44	766423	29.3	909419	15.1	857004	44.4	142996	58401	81174	16
45	766598	29.2	909328	15.2	857270	44.4	142730	58425	81157	15
46	766774	29.2	909237	15.2	857537	44.4	142463	58449	81140	14
47	766949	29.2	909146	15.2	857803	44.4	142197	58472	81123	13
48	767124	29.2	909055	15.2	858069	44.4	141931	58496	81106	12
49	767300	29.2	908964	15.2	858336	44.4	141664	58519	81089	11
50	767475	29.1	908873	15.2	858602	44.3	141398	58543	81072	10
51	9.767649	29.1	9.908781	15.2	9.858868	44.3	10.141132	58567	81055	9
52	767824	29.1	908690	15.2	859134	44.3	140866	58590	81038	8
53	767999	29.1	908599	15.2	859400	44.3	140600	58614	81021	7
54	768173	29.1	908507	15.2	859666	44.3	140334	58637	81004	6
55	768348	29.0	908416	15.3	859932	44.3	140068	58661	80987	5
56	768522	29.0	908324	15.3	860198	44.3	139802	58684	80970	4
57	768697	29.0	908233	15.3	860464	44.3	139536	58708	80953	3
58	768871	29.0	908141	15.3	860730	44.3	139270	58731	80936	2
59	769045	29.0	908049	15.3	860995	44.3	139005	58755	80919	1
60	769219		907958		861261		138739	58779	80902	0
	Cosine.		Sine.		Cotang.		Tang.	N. cos.	N.sine.	'

54 Degrees.

′	Sine.	D. 10″	Cosine.	D. 10″	Tang.	D. 10″	Cotang.	N. sine	N. cos.	
0	9.769219	29.0	9.907958	15.3	9.861261	44.3	10.138739	58779	80902	60
1	769393	28.9	907866	15.3	861527	44.3	138473	58802	80885	59
2	769566	28.9	907774	15.3	861792	44.2	138208	58826	80867	58
3	769740	28.9	907682	15.3	862058	44.2	137942	58849	80850	57
4	769913	28.9	907590	15.3	862323	44.2	137677	58873	80833	56
5	770087	28.9	907498	15.3	862589	44.2	137411	58896	80816	55
6	770260	28.8	907406	15.3	862854	44.2	137146	58920	80799	54
7	770433	28.8	907314	15.4	863119	44.2	136881	58943	80782	53
8	770606	28.8	907222	15.4	863385	44.2	136615	58967	80765	52
9	770779	28.8	907129	15.4	863650	44.2	136350	58990	80748	51
10	770952	28.8	907037	15.4	863915	44.2	136085	59014	80730	50
11	9.771125	28.8	9.906945	15.4	9.864180	44.2	10.135820	59037	80713	49
12	771298	28.7	906852	15.4	864445	44.2	135555	59061	80696	48
13	771470	28.7	906760	15.4	864710	44.2	135290	59084	80679	47
14	771643	28.7	906667	15.4	864975	44.1	135025	59108	80662	46
15	771815	28.7	906575	15.4	865240	44.1	134760	59131	80644	45
16	771987	28.7	906482	15.4	865505	44.1	134495	59154	80627	44
17	772159	28.7	906389	15.5	865770	44.1	134230	59178	80610	43
18	772331	28.6	906296	15.5	866035	44.1	133965	59201	80593	42
19	772503	28.6	906204	15.5	866300	44.1	133700	59225	80576	41
20	772675	28.6	906111	15.5	866564	44.1	133436	59248	80558	40
21	9.772847	28.6	9.906018	15.5	9.866829	44.1	10.133171	59272	80541	39
22	773018	28.6	905925	15.5	867094	44.1	132906	59295	80524	38
23	773190	28.6	905832	15.5	867358	44.1	132642	59318	80507	37
24	773361	28.5	905739	15.5	867623	44.1	132377	59342	80489	36
25	773533	28.5	905645	15.5	867887	44.1	132113	59365	80472	35
26	773704	28.5	905552	15.5	868152	44.0	131848	59389	80455	34
27	773875	28.5	905459	15.5	868416	44.0	131584	59412	80438	33
28	774046	28.5	905366	15.6	868680	44.0	131320	59436	80422	32
29	774217	28.5	905272	15.6	868945	44.0	131055	59459	80403	31
30	774388	28.4	905179	15.6	869209	44.0	130791	59482	80386	30
31	9.774558	28.4	9.905085	15.6	9.869473	44.0	10.130527	59506	80368	29
32	774729	28.4	904992	15.6	869737	44.0	130263	59529	80351	28
33	774899	28.4	904898	15.6	870001	44.0	129999	59552	80334	27
34	775070	28.4	904804	15.6	870265	44.0	129735	59576	80316	26
35	775240	28.4	904711	15.6	870529	44.0	129471	59599	80299	25
36	775410	28.3	904617	15.6	870793	44.0	129207	59622	80282	24
37	775580	28.3	904523	15.6	871057	44.0	128943	59646	80264	23
38	775750	28.3	904429	15.7	871321	44.0	128679	59669	80247	22
39	775920	28.3	904335	15.7	871585	44.0	128415	59693	80230	21
40	776090	28.3	904241	15.7	871849	43.9	128151	59716	80212	20
41	9.776259	28.3	9.904147	15.7	9.872112	43.9	10.127888	59739	80195	19
42	776429	28.2	904053	15.7	872376	43.9	127624	59763	80178	18
43	776598	28.2	903959	15.7	872640	43.9	127360	59786	80160	17
44	776768	28.2	903864	15.7	872903	43.9	127097	59809	80143	16
45	776937	28.2	903770	15.7	873167	43.9	126833	59832	80125	15
46	777106	28.2	903676	15.7	873430	43.9	126570	59856	80108	14
47	777275	28.1	903581	15.7	873694	43.9	126306	59879	80091	13
48	777444	28.1	903487	15.7	873957	43.9	126043	59902	80073	12
49	777613	28.1	903392	15.8	874220	43.9	125780	59926	80056	11
50	777781	28.1	903298	15.8	874484	43.9	125516	59949	80038	10
51	9.777950	28.1	9.903202	15.8	9.874747	43.9	10.125253	59972	80021	9
52	778119	28.1	903108	15.8	875010	43.9	124990	59995	80003	8
53	778287	28.0	903014	15.8	875273	43.8	124727	60019	79986	7
54	778455	28.0	902919	15.8	875536	43.8	124464	60042	79968	6
55	778624	28.0	902824	15.8	875800	43.8	124200	60065	79951	5
56	778792	28.0	902729	15.8	876063	43.8	123937	60089	79934	4
57	778960	28.0	902634	15.8	876326	43.8	123674	60112	79916	3
58	779128	28.0	902539	15.9	876589	43.8	123411	60135	79899	2
59	779295	27.9	902444	15.9	876851	43.8	123149	60158	79881	1
60	779463		902349		877114		122886	60182	79864	0
	Cosine.		Sine.		Cotang.		Tang.	N. cos.	N. sine.	′

53 Degrees.

′	Sine.	D. 10″	Cosine.	D. 10″	Tang.	D. 10″	Cotang.	N.sine.	N. cos.	
0	9.779463	27.9	9.902349	15.9	9.877114	43.8	10.122886	60182	79864	60
1	779631	27.9	902253	15.9	877377	43.8	122623	60205	79846	59
2	779798	27.9	902158	15.9	877640	43.8	122360	60228	79829	58
3	779966	27.9	902063	15.9	877903	43.8	122097	60251	79811	57
4	780133	27.9	901967	15.9	878165	43.8	121835	60274	79793	56
5	780300	27.8	901872	15.9	878428	43.8	121572	60298	79776	55
6	780467	27.8	901776	15.9	878691	43.8	121309	60321	79758	54
7	780634	27.8	901681	15.9	878953	43.7	121047	60344	79741	53
8	780801	27.8	901585	15.9	879216	43.7	120784	60367	79723	52
9	780968	27.8	901490	15.9	879478	43.7	120522	60390	79706	51
10	781134	27.8	901394	16.0	879741	43.7	120259	60414	79688	50
11	9.781301	27.7	9.901298	16.0	9.880003	43.7	10.119997	60437	79671	49
12	781468	27.7	901202	16.0	880265	43.7	119735	60460	79658	48
13	781634	27.7	901106	16.0	880528	43.7	119472	60483	79635	47
14	781800	27.7	901010	16.0	880790	43.7	119210	60506	79618	46
15	781966	27.7	900914	16.0	881052	43.7	118948	60529	79600	45
16	782132	27.7	900818	16.0	881314	43.7	118686	60553	79583	44
17	782298	27.6	900722	16.0	881576	43.7	118424	60576	79565	43
18	782464	27.6	906626	16.0	881839	43.7	118161	60599	79547	42
19	782630	27.6	900529	16.0	882101	43.7	117899	60622	79530	41
20	782796	27.6	900433	16.1	882363	43.6	117637	60645	79512	40
21	9.782961	27.6	9.900337	16.1	9.882625	43.6	10.117375	60668	79494	39
22	783127	27.6	900242	16.1	882887	43.6	117113	60691	79477	38
23	783282	27.5	900144	16.1	883148	43.6	116852	60714	79459	37
24	783458	27.5	900047	16.1	883410	43.6	116590	60738	79441	36
25	783623	27.5	899951	16.1	883672	43.6	116328	60761	79424	35
26	783788	27.5	899854	16.1	883934	43.6	116066	60784	79406	34
27	783953	27.5	899757	16.1	884196	43.6	115804	60807	79388	33
28	784118	27.5	899660	16.1	884457	43.6	115543	60830	79371	32
29	784282	27.4	899564	16.1	884719	43.6	115281	60853	79353	31
30	784447	27.4	899467	16.2	884980	43.6	115020	60876	79335	30
31	9.784612	27.4	9.899370	16.2	9.885242	43.6	10.114758	60899	79318	29
32	784776	27.4	899273	16.2	885503	43.6	114497	60922	79300	28
33	784941	27.4	899176	16.2	885765	43.6	114235	60945	79282	27
34	785105	27.4	899078	16.2	886026	43.6	113974	60968	79264	26
35	785269	27.3	898981	16.2	886288	43.6	113712	60991	79247	25
36	785433	27.3	898884	16.2	886549	43.5	113451	61015	79229	24
37	785597	27.3	898787	16.2	886810	43.5	113190	61038	79211	23
38	785761	27.3	898689	16.2	887072	43.5	112928	61061	79193	22
39	785925	27.3	898592	16.2	887333	43.5	112667	61084	79176	21
40	786089	27.3	898494	16.3	887594	43.5	112406	61107	79158	20
41	9.786252	27.2	9.898397	16.3	9.887855	43.5	10.112145	61130	79140	19
42	786416	27.2	898299	16.3	888116	43.5	111884	61153	79122	18
43	786579	27.2	898202	16.3	888377	43.5	111623	61176	79105	17
44	786742	27.2	898104	16.3	888639	43.5	111361	61199	79087	16
45	786905	27.2	898006	16.3	888900	43.5	111100	61222	79069	15
46	787069	27.2	897908	16.3	889160	43.5	110840	61245	79051	14
47	787232	27.1	897810	16.3	889421	43.5	110579	61268	79033	13
48	787395	27.1	897712	16.3	889682	43.5	110318	61291	79016	12
49	787557	27.1	897614	16.3	889943	43.5	110057	61314	78998	11
50	787720	27.1	897516	16.3	890204	43.4	109796	61337	78980	10
51	9.787883	27.1	9.897418	16.4	9.890465	43.4	10.109535	61360	78962	9
52	788045	27.1	897320	16.4	890725	43.4	109275	61383	78944	8
53	788208	27.1	897222	16.4	890986	43.4	109014	61406	78926	7
54	788370	27.0	897123	16.4	891247	43.4	108753	61429	78908	6
55	788532	27.0	897025	16.4	891507	43.4	108493	61451	78891	5
56	788694	27.0	896926	16.4	891768	43.4	108232	61474	78873	4
57	788856	27.0	896828	16.4	892028	43.4	107972	61497	78855	3
58	789018	27.0	896729	16.4	892289	43.4	107711	61520	78837	2
59	789180	27.0	896631	16.4	892549	43.4	107451	61543	78819	1
60	789342		896532		892810		107190	61566	78801	0
	Cosine.		Sine.		Cotang.		Tang.	N. cos.	N.sine.	′

52 Degrees.

'	Sine.	D. 10"	Cosine.	D. 10"	Tang.	D. 10"	Cotang.	N. sine.	N. cos.	'
0	9.789342	26.9	9.896532	16.4	[illegible]	43.4	10.[illegible]	[illegible]	[illegible]	[illegible]
1	789504	26.9	896433	16.5	[illegible]	43.4	[illegible]	[illegible]	[illegible]	[illegible]
2	789665	26.9	896335	16.5	[illegible]	43.4	[illegible]	[illegible]	[illegible]	[illegible]
3	789827	26.9	896236	16.5	[illegible]	43.4	[illegible]	[illegible]	[illegible]	[illegible]
4	789988	26.9	896137	16.5	[illegible]	43.4	[illegible]	[illegible]	[illegible]	[illegible]
5	790149	26.9	896038	16.5	[illegible]	43.4	[illegible]	[illegible]	[illegible]	[illegible]
6	790310	26.8	895939	16.5	[illegible]	43.4	[illegible]	[illegible]	[illegible]	[illegible]
7	790471	26.8	895840	16.5	[illegible]	43.3	[illegible]	[illegible]	[illegible]	[illegible]
8	790632	26.8	895741	16.5	[illegible]	43.3	[illegible]	[illegible]	[illegible]	[illegible]
9	790793	26.8	895641	16.5	[illegible]	43.3	[illegible]	[illegible]	[illegible]	[illegible]
10	790954	26.8	895542	16.5	[illegible]	43.3	[illegible]	[illegible]	[illegible]	[illegible]
11	9.791115	26.8	9.895443	16.6	9.[illegible]	43.3	10.[illegible]	[illegible]	[illegible]	[illegible]
12	791275	26.7	895343	16.6	[illegible]	43.3	[illegible]	[illegible]	[illegible]	[illegible]
13	791436	26.7	895244	16.6	[illegible]	43.3	[illegible]	[illegible]	[illegible]	47
14	791596	26.7	895145	16.6	[illegible]	43.3	[illegible]	[illegible]	[illegible]	[illegible]
15	791757	26.7	895045	16.6	896712	43.3	[illegible]	[illegible]	[illegible]	[illegible]
16	791917	26.7	894945	16.6	[illegible]	43.3	[illegible]	[illegible]	[illegible]	44
17	792077	26.7	894846	16.6	[illegible]	43.3	[illegible]	[illegible]	[illegible]	43
18	792237	26.6	894746	16.6	[illegible]	43.3	[illegible]	[illegible]	[illegible]	[illegible]
19	792397	26.6	894646	16.6	[illegible]	43.3	[illegible]	[illegible]	[illegible]	[illegible]
20	792557	26.6	894546	16.5	[illegible]	43.3	[illegible]	[illegible]	[illegible]	[illegible]
21	9.792716	26.6	9.894446	16.7	9.[illegible]	43.3	10.[illegible]	[illegible]	[illegible]	[illegible]
22	792876	26.6	894346	16.7	[illegible]	43.3	[illegible]	[illegible]	[illegible]	[illegible]
23	793035	26.6	894246	16.7	[illegible]	43.3	[illegible]	[illegible]	[illegible]	[illegible]
24	793195	26.5	894146	16.7	[illegible]	43.2	[illegible]	[illegible]	[illegible]	[illegible]
25	793354	26.5	894046	16.7	[illegible]	43.2	[illegible]	[illegible]	[illegible]	[illegible]
26	793514	26.5	893946	16.7	[illegible]	43.2	[illegible]	[illegible]	[illegible]	[illegible]
27	793673	26.5	893846	16.7	[illegible]	43.2	[illegible]	[illegible]	[illegible]	[illegible]
28	793832	26.5	893745	16.7	[illegible]	43.2	[illegible]	[illegible]	[illegible]	[illegible]
29	793991	26.5	893645	16.7	[illegible]	43.2	[illegible]	[illegible]	[illegible]	[illegible]
30	794150	26.4	893544	16.7	[illegible]	43.2	[illegible]	[illegible]	[illegible]	[illegible]
31	9.794308	26.4	9.893444	16.8	9.[illegible]	43.2	10.[illegible]	[illegible]	[illegible]	[illegible]
32	794467	26.4	893343	16.8	901124	43.2	[illegible]	[illegible]	[illegible]	[illegible]
33	794626	26.4	893243	16.8	[illegible]	43.2	[illegible]	[illegible]	[illegible]	27
34	794784	26.4	893142	16.8	[illegible]	43.2	[illegible]	[illegible]	[illegible]	[illegible]
35	794942	26.4	893041	16.8	[illegible]	43.2	[illegible]	[illegible]	[illegible]	[illegible]
36	795101	26.4	892940	16.8	[illegible]	43.2	[illegible]	[illegible]	[illegible]	24
37	795259	26.3	892839	16.8	[illegible]	43.2	[illegible]	[illegible]	[illegible]	[illegible]
38	795417	26.3	892739	16.8	[illegible]	43.2	[illegible]	[illegible]	[illegible]	22
39	795575	26.3	892638	16.8	[illegible]	43.2	[illegible]	[illegible]	[illegible]	21
40	795733	26.3	892536	16.8	[illegible]	43.1	[illegible]	[illegible]	[illegible]	20
41	9.795891	26.3	9.892435	16.9	9.903455	43.1	10.[illegible]	[illegible]	[illegible]	19
42	796049	26.3	892334	16.9	903714	43.1	[illegible]	[illegible]	[illegible]	18
43	796206	26.3	892233	16.9	[illegible]	43.1	[illegible]	[illegible]	[illegible]	17
44	796364	26.2	892132	16.9	[illegible]	43.1	[illegible]	[illegible]	[illegible]	16
45	796521	26.2	892030	16.9	[illegible]	43.1	[illegible]	[illegible]	[illegible]	15
46	796679	26.2	891929	16.9	904750	43.1	[illegible]	[illegible]	[illegible]	14
47	796836	26.2	891827	16.9	[illegible]	43.1	[illegible]	[illegible]	[illegible]	13
48	796993	26.2	891726	16.9	[illegible]	43.1	[illegible]	[illegible]	[illegible]	12
49	797150	26.1	891624	16.9	[illegible]	43.1	[illegible]	[illegible]	[illegible]	11
50	797307	26.1	891523	17.0	[illegible]	43.1	[illegible]	[illegible]	[illegible]	10
51	9.797464	26.1	9.891421	17.0	9.906043	43.1	10.093957	[illegible]	[illegible]	9
52	797621	26.1	891319	17.0	[illegible]	43.1	[illegible]	[illegible]	[illegible]	8
53	797777	26.1	891217	17.0	[illegible]	43.1	093440	[illegible]	[illegible]	7
54	797934	26.1	891115	17.0	[illegible]	43.1	093181	[illegible]	[illegible]	6
55	798091	26.1	891013	17.0	907077	43.1	092923	62819	77806	5
56	798247	26.1	890911	17.0	[illegible]	43.1	[illegible]	[illegible]	[illegible]	4
57	798403	26.0	890809	17.0	[illegible]	43.1	[illegible]	[illegible]	[illegible]	3
58	798560	26.0	890707	17.0	[illegible]	43.1	[illegible]	[illegible]	77751	2
59	798716	26.0	890605	17.0	908111	43.0	[illegible]	[illegible]	77733	1
60	798872		890503		[illegible]		[illegible]	[illegible]	77715	0
	Cosine.		Sine.		Cotang.		Tang.	N. cos.	N. sine.	'

51 Degrees.

'	Sine.	D. 10"	Cosine.	D. 10"	Tang.	D. 10"	Cotang.	N. sine.	N. cos.	
0	9.798772	26.0	9.890503	17.0	9.908369	43.0	10.091631	62932	77715	60
1	799028	26.0	890400	17.1	908628	43.0	091372	62955	77696	59
2	799184	26.0	890298	17.1	908886	43.0	091114	62977	77678	58
3	799339	25.9	890195	17.1	909144	43.0	090856	63000	77660	57
4	799495	25.9	890093	17.1	909402	43.0	090598	63022	77641	56
5	799651	25.9	889990	17.1	909660	43.0	090340	63045	77623	55
6	799806	25.9	889888	17.1	909918	43.0	090082	63068	77605	54
7	799962	25.9	889785	17.1	910177	43.0	089823	63090	77586	53
8	800117	25.9	889682	17.1	910435	43.0	089565	63113	77568	52
9	800272	25.8	889579	17.1	910693	43.0	089307	63135	77550	51
10	800427	25.8	889477	17.1	910951	43.0	089049	63158	77531	50
11	9.800582	25.8	9.889374	17.2	9.911209	43.0	10.088791	93180	77513	49
12	800737	25.8	889271	17.2	911467	43.0	088533	63203	77494	48
13	800892	25.8	889168	17.2	911724	43.0	088276	63225	77476	47
14	801047	25.8	889064	17.2	911982	43.0	088018	63248	77458	46
15	801201	25.8	888961	17.2	912240	43.0	087760	63271	77439	45
16	801356	25.7	888858	17.2	912498	43.0	087502	63293	77421	44
17	801511	25.7	888755	17.2	912756	43.0	087244	63316	77402	43
18	801665	25.7	888651	17.2	913014	42.9	086986	63338	77384	42
19	801819	25.7	888548	17.2	913271	42.9	086729	63361	77366	41
20	801973	25.7	888444	17.3	913529	42.9	086471	63383	77347	40
21	9.802128	25.7	9.888341	17.3	9.913787	42.9	10.086213	63406	77329	39
22	802282	25.6	888237	17.3	914044	42.9	085956	63428	77310	38
23	802436	25.6	888134	17.3	914302	42.9	085698	63451	77292	37
24	802589	25.6	888030	17.3	914560	42.9	085440	63473	77273	36
25	802743	25.6	887926	17.3	914817	42.9	085183	63496	77255	35
26	802897	25.6	887822	17.3	915075	42.9	084925	63518	77236	34
27	803050	25.6	887718	17.3	915332	42.9	084668	63540	77218	33
28	803204	25.6	887614	17.3	915590	42.9	084410	63563	77199	32
29	803357	25.5	887510	17.3	915847	42.9	084153	63585	77181	31
30	803511	25.5	887406	17.4	916104	42.9	083896	63608	77162	30
31	9.803664	25.5	9.887302	17.4	9.916362	42.9	10.083638	63630	77144	29
32	803817	25.5	887198	17.4	916619	42.9	083381	63653	77125	28
33	803970	25.5	887093	17.4	916877	42.9	083123	63675	77107	27
34	804123	25.5	886989	17.4	917134	42.9	082866	63698	77088	26
35	804276	25.4	886885	17.4	917391	42.9	082609	63720	77070	25
36	804428	25.4	886780	17.4	917648	42.9	082352	63742	77051	24
37	804581	25.4	886676	17.4	917905	42.9	082095	63765	77033	23
38	804734	25.4	886571	17.4	918163	42.8	081837	63787	77014	22
39	804886	25.4	886466	17.4	918420	42.8	081580	63810	76996	21
40	805039	25.4	886362	17.5	918677	42.8	081323	63832	76977	20
41	9.805191	25.4	9.886257	17.5	9.918934	42.8	10.081066	63854	76959	19
42	805343	25.3	886152	17.5	919191	42.8	080809	63877	76940	18
43	805495	25.3	886047	17.5	919448	42.8	080552	63899	76921	17
44	805647	25.3	885942	17.5	919705	42.8	080295	63922	76903	16
45	805799	25.3	885837	17.5	919962	42.8	080038	63944	76884	15
46	805951	25.3	885732	17.5	920219	42.8	079781	63966	76866	14
47	806103	25.3	885627	17.5	920476	42.8	079524	63989	76847	13
48	806254	25.3	885522	17.5	920733	42.8	079267	64011	76828	12
49	806406	25.2	885416	17.5	920990	42.8	079010	64033	76810	11
50	806557	25.2	885311	17.6	921247	42.8	078753	64056	76791	10
51	9.806709	25.2	9.885205	17.6	9.921503	42.8	10.078497	64078	76772	9
52	806860	25.2	885100	17.6	921760	42.8	078240	64100	76754	8
53	807011	25.2	884994	17.6	922017	42.8	077983	64123	76735	7
54	807163	25.2	884889	17.6	922274	42.8	077726	64145	76717	6
55	807314	25.2	884783	17.6	922530	42.8	077470	64167	76698	5
56	807465	25.1	884677	17.6	922787	42.8	077213	64190	76679	4
57	807615	25.1	884572	17.6	923044	42.8	076956	64212	76661	3
58	807766	25.1	884466	17.6	923300	42.8	076700	64234	76642	2
59	807917	25.1	884360	17.6	923557	42.7	076443	64256	76623	1
60	808067		884254		923813		076187	64279	76604	0
	Cosine.		Sine.		Cotang.		Tang.	N. cos.	N.sine.	'

50 Degrees.

TABLE II. Log. Sines and [illegible]

	Sine.	D. 10"	Cosine.	D. 10"	Tang.	D. 10"	Cotang.	N. sine.	N. cos.	
0	9.808067	25.1	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]
1	808218	25.1	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]
2	808368	25.1	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]
3	808519	25.0	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]
4	808669	25.0	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]
5	808819	25.0	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]
6	808969	25.0	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]
7	809119	25.0	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]
8	809269	25.0	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]
9	809419	24.9	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]
10	809569	24.9	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]
11	9.809718	24.9	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]
12	809868	24.9	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]
13	810017	24.9	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]
14	810167	24.9	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]
15	810316	24.8	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]
16	810465	24.8	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]
17	810614	24.8	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]
18	810763	24.8	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]
19	810912	24.8	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]
20	811061	24.8	882121	17.9	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]
21	9.811210	24.8	9.882014	17.9	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]
22	811358	24.7	881907	17.9	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]
23	811507	24.7	881799	17.9	[illegible]	[illegible]	[illegible]	64790	76173	37
24	811655	24.7	881692	17.9	[illegible]	42.6	[illegible]	64812	76154	36
25	811804	24.7	881584	17.9	930220	42.6	[illegible]	64834	76135	35
26	811952	24.7	881477	17.9	930475	42.6	[illegible]	64856	76116	34
27	812100	24.7	881369	17.9	930731	42.6	[illegible]	64879	76097	33
28	812248	24.7	881261	18.0	930987	42.6	[illegible]	64901	76078	32
29	812396	24.6	881153	18.0	931243	42.6	[illegible]	64923	76059	31
30	812544	24.6	881046	18.0	931499	42.6	[illegible]	64945	76041	30
31	9.812692	24.6	9.880935	18.0	9.931755	42.6	10.068245	64967	76022	29
32	812840	24.6	880828	18.0	932010	42.6	067990	64989	76003	28
33	812988	24.6	880722	18.0	932266	42.6	067734	65011	75984	27
34	813135	24.6	880613	18.0	932522	42.6	067478	65033	75965	26
35	813283	24.6	880505	18.0	932778	42.6	067222	65055	75946	25
36	813430	24.5	880397	18.0	933033	42.6	066967	65077	75927	24
37	813578	24.5	880289	18.1	933289	42.6	066711	65100	75908	23
38	813725	24.5	880180	18.1	933545	42.6	066455	65122	75889	22
39	813872	24.5	880072	18.1	933800	42.6	066200	65144	75870	21
40	814019	24.5	879963	18.1	934056	42.6	065944	65166	75851	20
41	9.814166	24.5	9.879855	18.1	9.934311	42.6	10.065689	65188	75832	19
42	814313	24.5	879746	18.1	934567	42.6	065433	65210	75813	18
43	814460	24.4	879637	18.1	934823	42.6	065177	65232	75794	17
44	814607	24.4	879529	18.1	935078	42.6	064922	65254	75775	16
45	814753	24.4	879420	18.1	935333	42.6	064667	65276	75756	15
46	814900	24.4	879311	18.1	935589	42.6	064411	65298	75738	14
47	815046	24.4	879202	18.2	935844	42.6	064156	65320	75719	13
48	815193	24.4	879093	18.2	936100	42.6	063900	65342	75700	12
49	815339	24.4	878984	18.2	936355	42.6	063645	65364	75680	11
50	815485	24.3	878875	18.2	936610	42.6	063390	65386	75661	10
51	9.815631	24.8	9.878766	18.2	9.936866	42.5	10.063134	65408	75642	9
52	815778	24.3	878656	18.2	937121	42.5	062879	65430	75623	8
53	815924	24.3	878547	18.2	937376	42.5	062624	65452	75604	7
54	816069	24.3	878438	18.2	937632	42.5	062368	65474	75585	6
55	816215	24.3	878328	18.2	937887	42.5	062113	65496	75566	5
56	816361	24.3	878219	18.3	938142	42.5	061858	65518	75547	4
57	816507	24.2	878109	18.3	938398	42.5	061602	65540	75528	3
58	816652	24.2	877999	18.3	938653	42.5	061347	65562	75509	2
59	816798	24.2	877890	18.3	938908	42.5	061092	65584	75490	1
60	816943		877780		939163		060837	65606	75471	0
	Cosine.		Sine.		Cotang.		Tang.	N. cos.	N. sine.	'

49 Degrees.

′	Sine.	D. 10″	Cosine.	D. 10″	Tang.	D. 10″	Cotang.	N. sine.	N. cos.	
0	9.816943	24.2	9.877780	18.3	9.939163	42.5	10.060837	65606	75471	60
1	817088	24.2	877670	18.3	939418	42.5	060582	65628	75452	59
2	817233	24.2	877560	18.3	939673	42.5	060327	65650	75433	58
3	817379	24.2	877450	18.3	939928	42.5	060072	65672	75414	57
4	817524	24.1	877340	18.3	940183	42.5	059817	65694	75395	56
5	817668	24.1	877230	18.4	940438	42.5	059562	65716	75375	55
6	817813	24.1	877120	18.4	940694	42.5	059306	65738	75356	54
7	817958	24.1	877010	18.4	940949	42.5	059051	65759	75337	53
8	818103	24.1	876899	18.4	941204	42.5	058796	65781	75318	52
9	818247	24.1	876789	18.4	941458	42.5	058542	65803	75299	51
10	818392	24.1	876678	18.4	941714	42.5	058286	65825	75280	50
11	9.818536	24.0	9.876568	18.4	9.941968	42.5	10.058032	65847	75261	49
12	818681	24.0	876457	18.4	942223	42.5	057777	65869	75241	48
13	818825	24.0	876347	18.4	942478	42.5	057522	65891	75222	47
14	818969	24.0	876236	18.5	942733	42.5	057267	65913	75203	46
15	819113	24.0	876125	18.5	942988	42.5	057012	65935	75184	45
16	819257	24.0	876014	18.5	943243	42.5	056757	65956	75165	44
17	819401	24.0	875904	18.5	943498	42.5	056502	65978	75146	43
18	819545	23.9	875793	18.5	943752	42.5	056248	66000	75126	42
19	819689	23.9	875682	18.5	944007	42.5	055993	66022	75107	41
20	819832	23.9	875571	18.5	944262	42.5	055738	66044	75088	40
21	9.819976	23.9	9.875459	18.5	9.944517	42.5	10.055483	66066	75069	39
22	820120	23.9	875348	18.5	944771	42.4	055229	66088	75050	38
23	820263	23.9	875237	18.5	945026	42.4	054974	66109	75030	37
24	820406	23.9	875126	18.6	945281	42.4	054719	66131	75011	36
25	820550	23.8	875014	18.6	945535	42.4	054465	66153	74992	35
26	820693	23.8	874903	18.6	945790	42.4	054210	66175	74973	34
27	820836	23.8	874791	18.6	946045	42.4	053955	66197	74953	33
28	820979	23.8	874680	18.6	946299	42.4	053701	66218	74934	32
29	821122	23.8	874568	18.6	946554	42.4	053446	66240	74915	31
30	821265	23.8	874456	18.6	946808	42.4	053192	66262	74896	30
31	9.821407	23.8	9.874344	18.6	9.947063	42.4	10.052937	66284	74876	29
32	821550	23.8	874232	18.7	947318	42.4	052682	66306	74857	28
33	821693	23.7	874121	18.7	947572	42.4	052428	66327	74838	27
34	821835	23.7	874009	18.7	947826	42.4	052174	66349	74818	26
35	821977	23.7	873896	18.7	948081	42.4	051919	66371	74799	25
36	822120	23.7	873784	18.7	948336	42.4	051664	66393	74780	24
37	822262	23.7	873672	18.7	948590	42.4	051410	66414	74760	23
38	822404	23.7	873560	18.7	948844	42.4	051156	66436	74741	22
39	822546	23.7	873448	18.7	949099	42.4	050901	66458	74722	21
40	822688	23.6	873335	18.7	949353	42.4	050647	66480	74703	20
41	9.822830	23.6	9.873223	18.7	9.949607	42.4	10.050393	66501	74683	19
42	822972	23.6	873110	18.8	949862	42.4	050138	66523	74663	18
43	823114	23.6	872998	18.8	950116	42.4	049884	66545	74644	17
44	823255	23.6	872885	18.8	950370	42.4	049630	66566	74625	16
45	823397	23.6	872772	18.8	950625	42.4	049375	66588	74606	15
46	823539	23.6	872659	18.8	950879	42.4	049121	66610	74586	14
47	823680	23.5	872547	18.8	951133	42.4	048867	66632	74567	13
48	823821	23.5	872434	18.8	951388	42.4	048612	66653	74548	12
49	823963	23.5	872321	18.8	951642	42.4	048358	66675	74522	11
50	824104	23.5	872208	18.8	951896	42.4	048104	66697	74509	10
51	9.824245	23.5	9.872095	18.9	9.952150	42.4	10.047850	66718	74489	9
52	824386	23.5	871981	18.9	952405	42.4	047595	66740	74470	8
53	824527	23.5	871868	18.9	952659	42.4	047341	66762	74451	7
54	824668	23.4	871755	18.9	952913	42.4	047087	66783	74431	6
55	824808	23.4	871641	18.9	953167	42.3	046833	66805	74412	5
56	824949	23.4	871528	18.9	953421	42.3	046579	66827	74392	4
57	825090	23.4	871414	18.9	953675	42.3	046325	66848	74373	3
58	825230	23.4	871301	18.9	953929	42.3	046071	66870	74353	2
59	825371	23.4	871187	18.9	954183	42.3	045817	66891	74334	1
60	825511		871073		954437		045563	66913	74314	0
	Cosine.		Sine.		Cotang.		Tang.	N. cos.	N.sine.	′

48 Degrees.

′	Sine.	D. 10″	Cosine.	D. 10″	Tang.	D. 10″	Cotang.	N.sine	N. cos.	
0	9.747562	31.2	9.918574	14.2	9.828987	45.4	10.171013	55919	82904	60
1	747749	31.2	918489	14.2	829260	45.4	170740	55943	82887	59
2	747936	31.2	918404	14.2	829532	45.4	170468	55968	82871	58
3	748123	31.1	918318	14.2	829805	45.4	170195	55992	82855	57
4	748310	31.1	918233	14.2	830077	45.4	169923	56016	82839	56
5	748497	31.1	918147	14.2	830349	45.3	169651	56040	82822	55
6	748683	31.1	918062	14.2	830621	45.3	169379	56064	82806	54
7	748870	31.1	917976	14.3	830893	45.3	169107	56088	82790	53
8	749056	31.0	917891	14.3	831165	45.3	168835	56112	82773	52
9	749243	31.0	917805	14.3	831437	45.3	168563	56136	82757	51
10	749426	31.0	917719	14.3	831709	45.3	168291	56160	82741	50
11	9.749615	31.0	9.917634	14.3	9.831981	45.3	10.168019	56184	82724	49
12	749801	31.0	917548	14.3	832253	45.3	167747	56208	82708	48
13	749987	30.9	917462	14.3	832525	45.3	167475	56232	82692	47
14	750172	30.9	917376	14.3	832796	45.3	167204	56256	82675	46
15	750358	30.9	917290	14.3	833068	45.2	166932	56280	82659	45
16	750543	30.9	917204	14.3	833339	45.2	166661	56305	82643	44
17	750729	30.9	917118	14.4	833611	45.2	166389	56329	82626	43
18	750914	30.8	917032	14.4	833882	45.2	166118	56353	82610	42
19	751099	30.8	916946	14.4	834154	45.2	165846	56377	82593	41
20	751284	30.8	916859	14.4	834425	45.2	165575	56401	82577	40
21	9.751469	30.8	9.916773	14.4	9.834696	45.2	10.165304	56425	82561	39
22	751654	30.8	916687	14.4	834967	45.2	165033	56449	82544	38
23	751839	30.8	916600	14.4	835238	45.2	164762	56473	82528	37
24	752023	30.7	916514	14.4	835509	45.2	164491	56497	82511	36
25	752208	30.7	916427	14.4	835780	45.1	164220	56521	82495	35
26	752392	30.7	916341	14.4	836051	45.1	163949	56545	82478	34
27	752576	30.7	916254	14.4	836322	45.1	163678	56569	82462	33
28	752760	30.7	916167	14.5	836593	45.1	163407	56593	82446	32
29	752944	30.6	916081	14.5	836864	45.1	163136	56617	82429	31
30	753128	30.6	915994	14.5	837134	45.1	162866	56641	82413	30
31	9.753312	30.6	9.915907	14.5	9.837405	45.1	10.162595	56665	82396	29
32	753495	30.6	915820	14.5	837675	45.1	162325	56689	82380	28
33	753679	30.6	915733	14.5	837946	45.1	162054	56713	82363	27
34	753862	30.5	915646	14.5	838216	45.1	161784	56736	82347	26
35	754046	30.5	915559	14.5	838487	45.0	161513	56760	82330	25
36	754229	30.5	915472	14.5	838757	45.0	161243	56784	82314	24
37	754412	30.5	915385	14.5	839027	45.0	160973	56808	82297	23
38	754595	30.5	915297	14.5	839297	45.0	160703	56832	82281	22
39	754778	30.4	915210	14.5	839568	45.0	160432	56856	82264	21
40	754960	30.4	915123	14.6	839838	45.0	160162	56880	82248	20
41	9.755143	30.4	9.915035	14.6	9.840108	45.0	10.159892	56904	82231	19
42	755326	30.4	914948	14.6	840378	45.0	159622	56928	82214	18
43	755508	30.4	914860	14.6	840647	45.0	159353	56952	82198	17
44	755690	30.4	914773	14.6	840917	44.9	159083	56976	82181	16
45	755872	30.3	914685	14.6	841187	44.9	158813	57000	82165	15
46	756054	30.3	914598	14.6	841457	44.9	158543	57024	82148	14
47	756236	30.3	914510	14.6	841726	44.9	158274	57047	82132	13
48	756418	30.3	914422	14.6	841996	44.9	158004	57071	82115	12
49	756600	30.3	914334	14.6	842266	44.9	157734	57095	82098	11
50	756782	30.2	914246	14.7	842535	44.9	157465	57119	82082	10
51	9.756963	30.2	9.914158	14.7	9.842805	44.9	10.157195	57143	82065	9
52	757144	30.2	914070	14.7	843074	44.9	156926	57167	82048	8
53	757326	30.2	913982	14.7	843343	44.9	156657	57191	82032	7
54	757507	30.2	913894	14.7	843612	44.9	156388	57215	82015	6
55	757688	30.1	913806	14.7	843882	44.8	156118	57238	81999	5
56	757869	30.1	913718	14.7	844151	44.8	155849	57262	81982	4
57	758050	30.1	913630	14.7	844420	44.8	155580	57286	81965	3
58	758230	30.1	913541	14.7	844689	44.8	155311	57310	81949	2
59	758411	30.1	913453	14.7	844958	44.8	155042	57334	81932	1
60	758591		913365		845227		154773	57358	81915	0
	Cosine.		Sine.		Cotang.		Tang.	N. cos.	N.sine.	′

55 Degrees.

′	Sine.	D. 10″	Cosine.	D. 10″	Tang.	D. 10″	Cotang.	N. sine.	N. cos.	
0	9.758591	30.1	9.913365	14.7	9.845227	44.8	10.154773	57358	81915	60
1	758772	30.0	913276	14.7	845496	44.8	154504	57381	81899	59
2	758952	30.0	913187	14.8	845764	44.8	154236	57405	81882	58
3	759132	30.0	913099	14.8	846033	44.8	153967	57429	81865	57
4	759312	30.0	913010	14.8	846302	44.8	153698	57453	81848	56
5	759492	30.0	912922	14.8	846570	44.7	153430	57477	81832	55
6	759672	29.9	912833	14.8	846839	44.7	153161	57501	81815	54
7	759852	29.9	912744	14.8	847107	44.7	152893	57524	81798	53
8	760031	29.9	912655	14.8	847376	44.7	152624	57548	81782	52
9	760211	29.9	912566	14.8	847644	44.7	152356	57572	81765	51
10	760390	29.9	912477	14.8	847913	44.7	152087	57596	81748	50
11	9.760569	29.8	9.912388	14.8	9.848181	44.7	10.151819	57619	81731	49
12	760748	29.8	912299	14.9	848449	44.7	151551	57643	81714	48
13	760927	29.8	912210	14.9	848717	44.7	151283	57667	81698	47
14	761106	29.8	912121	14.9	848986	44.7	151014	57691	81681	46
15	761285	29.8	912031	14.9	849254	44.7	150746	57715	81664	45
16	761464	29.8	911942	14.9	849522	44.7	150478	57738	81647	44
17	761642	29.7	911853	14.9	849790	44.6	150210	57762	81631	43
18	761821	29.7	911763	14.9	850058	44.6	149942	57786	81614	42
19	761999	29.7	911674	14.9	850325	44.6	149675	57810	81597	41
20	762177	29.7	911584	14.9	850593	44.6	149407	57833	81580	40
21	9.762356	29.7	9.911495	14.9	9.850861	44.6	10.149139	57857	81563	39
22	762534	29.6	911405	14.9	851129	44.6	148871	57881	81546	38
23	762712	29.6	911315	15.0	851396	44.6	148604	57904	81530	37
24	762889	29.6	911226	15.0	851664	44.6	148336	57928	81513	36
25	763067	29.6	911136	15.0	851931	44.6	148069	57952	81496	35
26	763245	29.6	911046	15.0	852199	44.6	147801	57976	81479	34
27	763422	29.6	910956	15.0	852466	44.6	147534	57999	81462	33
28	763600	29.5	910866	15.0	852733	44.5	147267	58023	81445	32
29	763777	29.5	910776	15.0	853001	44.5	146999	58047	81428	31
30	763954	29.5	910686	15.0	853268	44.5	146732	58070	81412	30
31	9.764131	29.5	9.910596	15.0	9.853535	44.5	10.146465	58094	81395	29
32	764308	29.5	910506	15.0	853802	44.5	146198	58118	81378	28
33	764485	29.4	910415	15.0	854069	44.5	145931	58141	81361	27
34	764662	29.4	910325	15.1	854336	44.5	145664	58165	81344	26
35	764838	29.4	910235	15.1	854603	44.5	145397	58189	81327	25
36	765015	29.4	910144	15.1	854870	44.5	145130	58212	81310	24
37	765191	29.4	910054	15.1	855137	44.5	144863	58236	81293	23
38	765367	29.4	909963	15.1	855404	44.5	144596	58260	81276	22
39	765544	29.3	909873	15.1	855671	44.4	144329	58283	81259	21
40	765720	29.3	909782	15.1	855938	44.4	144062	58307	81242	20
41	9.765896	29.3	9.909691	15.1	9.856204	44.4	10.143796	58330	81225	19
42	766072	29.3	909601	15.1	856471	44.4	143529	58354	81208	18
43	766247	29.3	909510	15.1	856737	44.4	143263	58378	81191	17
44	766423	29.3	909419	15.1	857004	44.4	142996	58401	81174	16
45	766598	29.2	909328	15.2	857270	44.4	142730	58425	81157	15
46	766774	29.2	909237	15.2	857537	44.4	142463	58449	81140	14
47	766949	29.2	909146	15.2	857803	44.4	142197	58472	81123	13
48	767124	29.2	909055	15.2	858069	44.4	141931	58496	81106	12
49	767300	29.2	908964	15.2	858336	44.4	141664	58519	81089	11
50	767475	29.1	908873	15.2	858602	44.3	141398	58543	81072	10
51	9.767649	29.1	9.908781	15.2	9.858868	44.3	10.141132	58567	81055	9
52	767824	29.1	908690	15.2	859134	44.3	140866	58590	81038	8
53	767999	29.1	908599	15.2	859400	44.3	140600	58614	81021	7
54	768173	29.1	908507	15.2	859666	44.3	140334	58637	81004	6
55	768348	29.0	908416	15.3	859932	44.3	140068	58661	80987	5
56	768522	29.0	908324	15.3	860198	44.3	139802	58684	80970	4
57	768697	29.0	908233	15.3	860464	44.3	139536	58708	80953	3
58	768871	29.0	908141	15.3	860730	44.3	139270	58731	80936	2
59	769045	29.0	908049	15.3	860995	44.3	139005	58755	80919	1
60	769219		907958		861261		138739	58779	80902	0
	Cosine.		Sine.		Cotang.		Tang.	N. cos.	N. sine.	′

54 Degrees.

′	Sine.	D. 10″	Cosine.	D. 10″	Tang.	D. 10″	Cotang.	N. sine.	N. cos.	
0	9.769219	29.0	9.907958	15.3	9.861261	44.3	10.138739	58779	80902	60
1	769393	28.9	907866	15.3	861527	44.3	138473	58802	80885	59
2	769566	28.9	907774	15.3	861792	44.2	138208	58826	80867	58
3	769740	28.9	907682	15.3	862058	44.2	137942	58849	80850	57
4	769913	28.9	907590	15.3	862323	44.2	137677	58873	80833	56
5	770087	28.9	907498	15.3	862589	44.2	137411	58896	80816	55
6	770260	28.8	907406	15.3	862854	44.2	137146	58920	80799	54
7	770433	28.8	907314	15.4	863119	44.2	136881	58943	80782	53
8	770606	28.8	907222	15.4	863385	44.2	136615	58967	80765	52
9	770779	28.8	907129	15.4	863650	44.2	136350	58990	80748	51
10	770952	28.8	907037	15.4	863915	44.2	136085	59014	80730	50
11	9.771125	28.8	9.906945	15.4	9.864180	44.2	10.135820	59037	80713	49
12	771298	28.7	906852	15.4	864445	44.2	135555	59061	80696	48
13	771470	28.7	906760	15.4	864710	44.2	135290	59084	80679	47
14	771643	28.7	906667	15.4	864975	44.1	135025	59108	80662	46
15	771815	28.7	906575	15.4	865240	44.1	134760	59131	80644	45
16	771987	28.7	906482	15.4	865505	44.1	134495	59154	80627	44
17	772159	28.7	906389	15.5	865770	44.1	134230	59178	80610	43
18	772331	28.6	906296	15.5	866035	44.1	133965	59201	80593	42
19	772503	28.6	906204	15.5	866300	44.1	133700	59225	80576	41
20	772675	28.6	906111	15.5	866564	44.1	133436	59248	80558	40
21	9.772847	28.6	9.906018	15.5	9.866829	44.1	10.133171	59272	80541	39
22	773018	28.6	905925	15.5	867094	44.1	132906	59295	80524	38
23	773190	28.6	905832	15.5	867358	44.1	132642	59318	80507	37
24	773361	28.5	905739	15.5	867623	44.1	132377	59342	80489	36
25	773533	28.5	905645	15.5	867887	44.1	132113	59365	80472	35
26	773704	28.5	905552	15.5	868152	44.0	131848	59389	80455	34
27	773875	28.5	905459	15.5	868416	44.0	131584	59412	80438	33
28	774046	28.5	905366	15.6	868680	44.0	131320	59436	80422	32
29	774217	28.5	905272	15.6	868945	44.0	131055	59459	80403	31
30	774388	28.4	905179	15.6	869209	44.0	130791	59482	80386	30
31	9.774558	28.4	9.905085	15.6	9.869473	44.0	10.130527	59506	80368	29
32	774729	28.4	904992	15.6	869737	44.0	130263	59529	80351	28
33	774899	28.4	904898	15.6	870001	44.0	129999	59552	80334	27
34	775070	28.4	904804	15.6	870265	44.0	129735	59576	80316	26
35	775240	28.4	904711	15.6	870529	44.0	129471	59599	80299	25
36	775410	28.3	904617	15.6	870793	44.0	129207	59622	80282	24
37	775580	28.3	904523	15.6	871057	44.0	128943	59646	80264	23
38	775750	28.3	904429	15.7	871321	44.0	128679	59669	80247	22
39	775920	28.3	904335	15.7	871585	44.0	128415	59693	80230	21
40	776090	28.3	904241	15.7	871849	43.9	128151	59716	80212	20
41	9.776259	28.3	9.904147	15.7	9.872112	43.9	10.127888	59739	80195	19
42	776429	28.2	904053	15.7	872376	43.9	127624	59763	80178	18
43	776598	28.2	903959	15.7	872640	43.9	127360	59786	80160	17
44	776768	28.2	903864	15.7	872903	43.9	127097	59809	80143	16
45	776937	28.2	903770	15.7	873167	43.9	126833	59832	80125	15
46	777106	28.2	903676	15.7	873430	43.9	126570	59856	80108	14
47	777275	28.1	903581	15.7	873694	43.9	126306	59879	80091	13
48	777444	28.1	903487	15.7	873957	43.9	126043	59902	80073	12
49	777613	28.1	903392	15.8	874220	43.9	125780	59926	80056	11
50	777781	28.1	903298	15.8	874484	43.9	125516	59949	80038	10
51	9.777950	28.1	9.903202	15.8	9.874747	43.9	10.125253	59972	80021	9
52	778119	28.1	903108	15.8	875010	43.9	124990	59995	80003	8
53	778287	28.0	903014	15.8	875273	43.8	124727	60019	79986	7
54	778455	28.0	902919	15.8	875536	43.8	124464	60042	79968	6
55	778624	28.0	902824	15.8	875800	43.8	124200	60065	79951	5
56	778792	28.0	902729	15.8	876063	43.8	123937	60089	79934	4
57	778960	28.0	902634	15.8	876326	43.8	123674	60112	79916	3
58	779128	28.0	902539	15.9	876589	43.8	123411	60135	79899	2
59	779295	27.9	902444	15.9	876851	43.8	123149	60158	79881	1
60	779463		902349		877114		122886	60182	79864	0
	Cosine.		Sine.		Co tang.		Tang.	N. cos.	N. sine.	′

'	Sine.	D. 10"	Cosine.	D. 10"	Tang.	D. 10"	Cotang.	N.sine.	N. cos.	
0	9.779463	27.9	9.902349	15.9	9.877114	43.8	10.122886	60182	79864	60
1	779631	27.9	902253	15.9	877377	43.8	122623	60205	79846	59
2	779798	27.9	902158	15.9	877640	43.8	122360	60228	79829	58
3	779966	27.9	902063	15.9	877903	43.8	122097	60251	79811	57
4	780133	27.9	901967	15.9	878165	43.8	121835	60274	79793	56
5	780300	27.8	901872	15.9	878428	43.8	121572	60298	79776	55
6	780467	27.8	901776	15.9	878691	43.8	121309	60321	79758	54
7	780634	27.8	901681	15.9	878953	43.7	121047	60344	79741	53
8	780801	27.8	901585	15.9	879216	43.7	120784	60367	79723	52
9	780968	27.8	901490	15.9	879478	43.7	120522	60390	79706	51
10	781134	27.8	901394	16.0	879741	43.7	120259	60414	79688	50
11	9.781301	27.7	9.901298	16.0	9.880003	43.7	10.119997	60437	79671	49
12	781468	27.7	901202	16.0	880265	43.7	119735	60460	79658	48
13	781634	27.7	901106	16.0	880528	43.7	119472	60483	79635	47
14	781800	27.7	901010	16.0	880790	43.7	119210	60506	79618	46
15	781966	27.7	900914	16.0	881052	43.7	118948	60529	79600	45
16	782132	27.7	900818	16.0	881314	43.7	118686	60553	79583	44
17	782298	27.6	900722	16.0	881576	43.7	118424	60576	79565	43
18	782464	27.6	900626	16.0	881839	43.7	118161	60599	79547	42
19	782630	27.6	900529	16.0	882101	43.7	117899	60622	79530	41
20	782796	27.6	900433	16.1	882363	43.6	117637	60645	79512	40
21	9.782961	27.6	9.900337	16.1	9.882625	43.6	10.117375	60668	79494	39
22	783127	27.6	900242	16.1	882887	43.6	117113	60691	79477	38
23	783282	27.5	900144	16.1	883148	43.6	116852	60714	79459	37
24	783458	27.5	900047	16.1	883410	43.6	116590	60738	79441	36
25	783623	27.5	899951	16.1	883672	43.6	116328	60761	79424	35
26	783788	27.5	899854	16.1	883934	43.6	116066	60784	79406	34
27	783953	27.5	899757	16.1	884196	43.6	115804	60807	79388	33
28	784118	27.5	899660	16.1	884457	43.6	115543	60830	79371	32
29	784282	27.4	899564	16.1	884719	43.6	115281	60853	79353	31
30	784447	27.4	899467	16.2	884980	43.6	115020	60876	79335	30
31	9.784612	27.4	9.899370	16.2	9.885242	43.6	10.114758	60899	79318	29
32	784776	27.4	899273	16.2	885503	43.6	114497	60922	79300	28
33	784941	27.4	899176	16.2	885765	43.6	114235	60945	79282	27
34	785105	27.4	899078	16.2	886026	43.6	113974	60968	79264	26
35	785269	27.3	898981	16.2	886288	43.6	113712	60991	79247	25
36	785433	27.3	898884	16.2	886549	43.5	113451	61015	79229	24
37	785597	27.3	898787	16.2	886810	43.5	113190	61038	79211	23
38	785761	27.3	898689	16.2	887072	43.5	112928	61061	79193	22
39	785925	27.3	898592	16.2	887333	43.5	112667	61084	79176	21
40	786089	27.3	898494	16.3	887594	43.5	112406	61107	79158	20
41	9.786252	27.2	9.898397	16.3	9.887855	43.5	10.112145	61130	79140	19
42	786416	27.2	898299	16.3	888116	43.5	111884	61153	79122	18
43	786579	27.2	898202	16.3	888377	43.5	111623	61176	79105	17
44	786742	27.2	898104	16.3	888639	43.5	111361	61199	79087	16
45	786906	27.2	898006	16.3	888900	43.5	111100	61222	79069	15
46	787069	27.2	897908	16.3	889160	43.5	110840	61245	79051	14
47	787232	27.1	897810	16.3	889421	43.5	110579	61268	79033	13
48	787395	27.1	897712	16.3	889682	43.5	110318	61291	79016	12
49	787557	27.1	897614	16.3	889943	43.5	110057	61314	78998	11
50	787720	27.1	897516	16.3	890204	43.4	109796	61337	78980	10
51	9.787883	27.1	9.897418	16.4	9.890465	43.4	10.109535	61360	78962	9
52	788045	27.1	897320	16.4	890725	43.4	109275	61383	78944	8
53	788208	27.1	897222	16.4	890986	43.4	109014	61406	78926	7
54	788370	27.0	897123	16.4	891247	43.4	108753	61429	78908	6
55	788532	27.0	897025	16.4	891507	43.4	108493	61451	78891	5
56	788694	27.0	896926	16.4	891768	43.4	108232	61474	78873	4
57	788856	27.0	896828	16.4	892028	43.4	107972	61497	78855	3
58	789018	27.0	896729	16.4	892289	43.4	107711	61520	78837	2
59	789180	27.0	896631	16.4	892549	43.4	107451	61543	78819	1
60	789342		896532		892810		107190	61566	78801	0
	Cosine.		Sine.		Cotang.		Tang.	N. cos.	N.sine.	'

52 Degrees.

′	Sine.	D. 10″	Cosine.	D. 10″	Tang.	D. 10″	Cotang.	N. sine.	N. cos.	
0	9.789342	26.9	9.896532	16.4	9.892810	43.4	10.107190	61566	78801	60
1	789504	26.9	896433	16.5	893070	43.4	106930	61589	78783	59
2	789665	26.9	896335	16.5	893331	43.4	106669	61612	78765	58
3	789827	26.9	896236	16.5	893591	43.4	106409	61635	78747	57
4	789988	26.9	896137	16.5	893851	43.4	106149	61658	78729	56
5	790149	26.9	896038	16.5	894111	43.4	105889	61681	78711	55
6	790310	26.8	895939	16.5	894371	43.4	105629	61704	78694	54
7	790471	26.8	895840	16.5	894632	43.3	105368	61726	78676	53
8	790632	26.8	895741	16.5	894892	43.3	105108	61749	78658	52
9	790793	26.8	895641	16.5	895152	43.3	104848	61772	78640	51
10	790954	26.8	895542	16.5	895412	43.3	104588	61795	78622	50
11	9.791115	26.8	9.895443	16.6	9.895672	43.3	10.104328	61818	78604	49
12	791275	26.7	895343	16.6	895932	43.3	104068	61841	78586	48
13	791436	26.7	895244	16.6	896192	43.3	103808	61864	78568	47
14	791596	26.7	895145	16.6	896452	43.3	103548	61887	78550	46
15	791757	26.7	895045	16.6	896712	43.3	103288	61909	78532	45
16	791917	26.7	894945	16.6	896971	43.3	103029	61932	78514	44
17	792077	26.7	894846	16.6	897231	43.3	102769	61955	78496	43
18	792237	26.6	894746	16.6	897491	43.3	102509	61978	78478	42
19	792397	26.6	894646	16.6	897751	43.3	102249	62001	78460	41
20	792557	26.6	894546	16.6	898010	43.3	101990	62024	78442	40
21	9.792716	26.6	9.894446	16.7	9.898270	43.3	10.101730	62046	78424	39
22	792876	26.6	894346	16.7	898530	43.3	101470	62069	78405	38
23	793035	26.6	894246	16.7	898789	43.3	101211	62092	78387	37
24	793195	26.5	894146	16.7	899049	43.2	100951	62115	78369	36
25	793354	26.5	894046	16.7	899308	43.2	100692	62138	78351	35
26	793514	26.5	893946	16.7	899568	43.2	100432	62160	78333	34
27	793673	26.5	893846	16.7	899827	43.2	100173	62183	78315	33
28	793832	26.5	893745	16.7	900086	43.2	099914	62206	78297	32
29	793991	26.5	893645	16.7	900346	43.2	099654	62229	78279	31
30	794150	26.4	893544	16.7	900605	43.2	099395	62251	78261	30
31	9.794308	26.4	9.893444	16.8	9.900864	43.2	10.099136	62274	78243	29
32	794467	26.4	893343	16.8	901124	43.2	098876	62297	78225	28
33	794626	26.4	893243	16.8	901383	43.2	098617	62320	78206	27
34	794784	26.4	893142	16.8	901642	43.2	098358	62342	78188	26
35	794942	26.4	893041	16.8	901901	43.2	098099	62365	78170	25
36	795101	26.4	892940	16.8	902160	43.2	097840	62388	78152	24
37	795259	26.3	892839	16.8	902419	43.2	097581	62411	78134	23
38	795417	26.3	892739	16.8	902679	43.2	097321	62433	78116	22
39	795575	26.3	892638	16.8	902938	43.2	097062	62456	78098	21
40	795733	26.3	892536	16.8	903197	43.1	096803	62479	78079	20
41	9.795891	26.3	9.892435	16.9	9.903455	43.1	10.096545	62502	78061	19
42	796049	26.3	892334	16.9	903714	43.1	096286	62524	78043	18
43	796206	26.3	892233	16.9	903973	43.1	096027	62547	78025	17
44	796364	26.2	892132	16.9	904232	43.1	095768	62570	78007	16
45	796521	26.2	892030	16.9	904491	43.1	095509	62592	77988	15
46	796679	26.2	891929	16.9	904750	43.1	095250	62615	77970	14
47	796836	26.2	891827	16.9	905008	43.1	094992	62638	77952	13
48	796993	26.2	891726	16.9	905267	43.1	094733	62660	77934	12
49	797150	26.1	891624	16.9	905526	43.1	094474	62683	77916	11
50	797307	26.1	891523	17.0	905784	43.1	094216	62706	77897	10
51	9.797464	26.1	9.891421	17.0	9.906043	43.1	10.093957	62728	77879	9
52	797621	26.1	891319	17.0	906302	43.1	093698	62751	77861	8
53	797777	26.1	891217	17.0	906560	43.1	093440	62774	77843	7
54	797934	26.1	891115	17.0	906819	43.1	093181	62796	77824	6
55	798091	26.1	891013	17.0	907077	43.1	092923	62819	77806	5
56	798247	26.1	890911	17.0	907336	43.1	092664	62842	77788	4
57	798403	26.0	890809	17.0	907594	43.1	092406	62864	77769	3
58	798560	26.0	890707	17.0	907852	43.1	092148	62887	77751	2
59	798716	26.0	890605	17.0	908111	43.0	091889	62909	77733	1
60	798872		890503		908369		091631	62932	77715	0
	Cosine.		Sine.		Cotang.		Tang.	N. cos.	N.sine.	′

51 Degrees.

Log. Sines and Tangents. (39°) Natural Sines. TABLE II.

′	Sine.	D. 10″	Cosine.	D. 10″	Tang.	D. 10″	Cotang.	N. sine.	N. cos.	
0	9.798772	26.0	9.890503	17.0	9.908369	43.0	10.091631	62932	77715	60
1	799028	26.0	890400	17.1	908628	43.0	091372	62955	77696	59
2	799184	26.0	890298	17.1	908886	43.0	091114	62977	77678	58
3	799339	25.9	890195	17.1	909144	43.0	090856	63000	77660	57
4	799495	25.9	890093	17.1	909402	43.0	090598	63022	77641	56
5	799651	25.9	889990	17.1	909660	43.0	090340	63045	77623	55
6	799806	25.9	889888	17.1	909918	43.0	090082	63068	77605	54
7	799962	25.9	889785	17.1	910177	43.0	089823	63090	77586	53
8	800117	25.9	889682	17.1	910435	43.0	089565	63113	77568	52
9	800272	25.8	889579	17.1	910693	43.0	089307	63135	77550	51
10	800427	25.8	889477	17.1	910951	43.0	089049	63158	77531	50
11	9.800582	25.8	9.889374	17.2	9.911209	43.0	10.088791	93180	77513	49
12	800737	25.8	889271	17.2	911467	43.0	088533	63203	77494	48
13	800892	25.8	889168	17.2	911724	43.0	088276	63225	77476	47
14	801047	25.8	889064	17.2	911982	43.0	088018	63248	77458	46
15	801201	25.8	888961	17.2	912240	43.0	087760	63271	77439	45
16	801356	25.7	888858	17.2	912498	43.0	087502	63293	77421	44
17	801511	25.7	888755	17.2	912756	43.0	087244	63316	77402	43
18	801665	25.7	888651	17.2	913014	42.9	086986	63338	77384	42
19	801819	25.7	888548	17.2	913271	42.9	086729	63361	77366	41
20	801973	25.7	888444	17.3	913529	42.9	086471	63383	77347	40
21	9.802128	25.7	9.888341	17.3	9.913787	42.9	10.086213	63406	77329	39
22	802282	25.6	888237	17.3	914044	42.9	085956	63428	77310	38
23	802436	25.6	888134	17.3	914302	42.9	085698	63451	77292	37
24	802589	25.6	888030	17.3	914560	42.9	085440	63473	77273	36
25	802743	25.6	887926	17.3	914817	42.9	085183	63496	77255	35
26	802897	25.6	887822	17.3	915075	42.9	084925	63518	77236	34
27	803050	25.6	887718	17.3	915332	42.9	084668	63540	77218	33
28	803204	25.6	887614	17.3	915590	42.9	084410	63563	77199	32
29	803357	25.5	887510	17.3	915847	42.9	084153	63585	77181	31
30	803511	25.5	887406	17.4	916104	42.9	083896	63608	77162	30
31	9.803664	25.5	9.887302	17.4	9.916362	42.9	10.083638	63630	77144	29
32	803817	25.5	887198	17.4	916619	42.9	083381	63653	77125	28
33	803970	25.5	887093	17.4	916877	42.9	083123	63675	77107	27
34	804123	25.5	886989	17.4	917134	42.9	082866	63698	77088	26
35	804276	25.4	886885	17.4	917391	42.9	082609	63720	77070	25
36	804428	25.4	886780	17.4	917648	42.9	082352	63742	77051	24
37	804581	25.4	886676	17.4	917905	42.9	082095	63765	77033	23
38	804734	25.4	886571	17.4	918163	42.8	081837	63787	77014	22
39	804886	25.4	886466	17.4	918420	42.8	081580	63810	76996	21
40	805039	25.4	886362	17.5	918677	42.8	081323	63832	76977	20
41	9.805191	25.4	9.886257	17.5	9.918934	42.8	10.081066	63854	76959	19
42	805343	25.3	886152	17.5	919191	42.8	080809	63877	76940	18
43	805495	25.3	886047	17.5	919448	42.8	080552	63899	76921	17
44	805647	25.3	885942	17.5	919705	42.8	080295	63922	76903	16
45	805799	25.3	885837	17.5	919962	42.8	080038	63944	76884	15
46	805951	25.3	885732	17.5	920219	42.8	079781	63966	76866	14
47	806103	25.3	885627	17.5	920476	42.8	079524	63989	76847	13
48	806254	25.3	885522	17.5	920733	42.8	079267	64011	76828	12
49	806406	25.2	885416	17.5	920990	42.8	079010	64033	76810	11
50	806557	25.2	885311	17.6	921247	42.8	078753	64056	76791	10
51	9.806709	25.2	9.885205	17.6	9.921503	42.8	10.078497	64078	76772	9
52	806860	25.2	885100	17.6	921760	42.8	078240	64100	76754	8
53	807011	25.2	884994	17.6	922017	42.8	077983	64123	76735	7
54	807163	25.2	884889	17.6	922274	42.8	077726	64145	76717	6
55	807314	25.2	884783	17.6	922530	42.8	077470	64167	76698	5
56	807465	25.1	884677	17.6	922787	42.8	077213	64190	76679	4
57	807615	25.1	884572	17.6	923044	42.8	076956	64212	76661	3
58	807766	25.1	884466	17.6	923300	42.8	076700	64234	76642	2
59	807917	25.1	884360	17.6	923557	42.7	076443	64256	76623	1
60	808067		884254		923813		076187	64279	76604	0
	Cosine.		Sine.		Cotang.		Tang.	N. cos.	N. sine.	′

50 Degrees.

′	Sine.	D. 10″	Cosine.	D. 10″	Tang.	D. 10″	Cotang.	N.sine.	N. cos.	
0	9.808067	25.1	9.884254	17.7	9.923813	42.7	10.076187	64279	76604	60
1	808218	25.1	884148	17.7	924070	42.7	075930	64301	76586	59
2	808368	25.1	884042	17.7	924327	42.7	075673	64323	76567	58
3	808519	25.0	883936	17.7	924583	42.7	075417	64346	76548	57
4	808669	25.0	883829	17.7	924840	42.7	075160	64368	76530	56
5	808819	25.0	883723	17.7	925096	42.7	074904	64390	76511	55
6	808969	25.0	883617	17.7	925352	42.7	074648	64412	76492	54
7	809119	25.0	883510	17.7	925609	42.7	074391	64435	76473	53
8	809269	25.0	883404	17.7	925865	42.7	074135	64457	76455	52
9	809419	24.9	883297	17.8	926122	42.7	073878	64479	76436	51
10	809569	24.9	883191	17.8	926378	42.7	073622	64501	76417	50
11	9.809718	24.9	9.883084	17.8	9.926634	42.7	10.073366	64524	76398	49
12	809868	24.9	882977	17.8	926890	42.7	073110	64546	76380	48
13	810017	24.9	882871	17.8	927147	42.7	072853	64568	76361	47
14	810167	24.9	882764	17.8	927403	42.7	072597	64590	76342	46
15	810316	24.8	882657	17.8	927659	42.7	072341	64612	76323	45
16	810465	24.8	882550	17.8	927915	42.7	072085	64635	76304	44
17	810614	24.8	882443	17.8	928171	42.7	071829	64657	76286	43
18	810763	24.8	882336	17.9	928427	42.7	071573	64679	76267	42
19	810912	24.8	882229	17.9	928683	42.7	071317	64701	76248	41
20	811061	24.8	882121	17.9	928940	42.7	071060	64723	76229	40
21	9.811210	24.8	9.882014	17.9	9.929196	42.7	10.070804	64746	76210	39
22	811358	24.7	881907	17.9	929452	42.7	070548	64768	76192	38
23	811507	24.7	881799	17.9	929708	42.7	070292	64790	76173	37
24	811655	24.7	881692	17.9	929964	42.6	070036	64812	76154	36
25	811804	24.7	881584	17.9	930220	42.6	069780	64834	76135	35
26	811952	24.7	881477	17.9	930475	42.6	069525	64856	76116	34
27	812100	24.7	881369	17.9	930731	42.6	069269	64878	76097	33
28	812248	24.7	881261	18.0	930987	42.6	069013	64901	76078	32
29	812396	24.6	881153	18.0	931243	42.6	068757	64923	76059	31
30	812544	24.6	881046	18.0	931499	42.6	068501	64945	76041	30
31	9.812692	24.6	9.880938	18.0	9.931755	42.6	10.068245	64967	76022	29
32	812840	24.6	880830	18.0	932010	42.6	067990	64989	76003	28
33	812988	24.6	880722	18.0	932266	42.6	067734	65011	75984	27
34	813135	24.6	880613	18.0	932522	42.6	067478	65033	75965	26
35	813283	24.6	880505	18.0	932778	42.6	067222	65055	75946	25
36	813430	24.5	880397	18.0	933033	42.6	066967	65077	75927	24
37	813578	24.5	880289	18.1	933289	42.6	066711	65100	75908	23
38	813725	24.5	880180	18.1	933545	42.6	066455	65122	75889	22
39	813872	24.5	880072	18.1	933800	42.6	066200	65144	75870	21
40	814019	24.5	879963	18.1	934056	42.6	065944	65166	75851	20
41	9.814166	24.5	9.879855	18.1	9.934311	42.6	10.065689	65188	75832	19
42	814313	24.5	879746	18.1	934567	42.6	065433	65210	75813	18
43	814460	24.4	879637	18.1	934823	42.6	065177	65232	75794	17
44	814607	24.4	879529	18.1	935078	42.6	064922	65254	75775	16
45	814753	24.4	879420	18.1	935333	42.6	064667	65276	75756	15
46	814900	24.4	879311	18.1	935589	42.6	064411	65298	75738	14
47	815046	24.4	879202	18.2	935844	42.6	064156	65320	75719	13
48	815193	24.4	879093	18.2	936100	42.6	063900	65342	75700	12
49	815339	24.4	878984	18.2	936355	42.6	063645	65364	75680	11
50	815485	24.3	878875	18.2	936610	42.6	063390	65386	75661	10
51	9.815631	24.3	9.878766	18.2	9.936866	42.5	10.063134	65408	75642	9
52	815778	24.3	878656	18.2	937121	42.5	062879	65430	75623	8
53	815924	24.3	878547	18.2	937376	42.5	062624	65452	75604	7
54	816069	24.3	878438	18.2	937632	42.5	062368	65474	75585	6
55	816215	24.3	878328	18.2	937887	42.5	062113	65496	75566	5
56	816361	24.3	878219	18.3	938142	42.5	061858	65518	75547	4
57	816507	24.2	878109	18.3	938398	42.5	061602	65540	75528	3
58	816652	24.2	877999	18.3	938653	42.5	061347	65562	75509	2
59	816798	24.2	877890	18.3	938908	42.5	061092	65584	75490	1
60	816943		877780		939163		060837	65606	75471	0
	Cosine.		Sine.		Cotang.		Tang.	N. cos.	N.sine.	′

49 Degrees.

'	Sine.	D. 10"	Cosine.	D. 10"	Tang.	D. 10"	Cotang.	N. sine.	N. cos.	
0	9.816943	24.2	9.877780	18.3	9.939163	42.5	10.060837	65606	75471	60
1	817088	24.2	877670	18.3	939418	42.5	060582	65628	75452	59
2	817233	24.2	877560	18.3	939673	42.5	060327	65650	75433	58
3	817379	24.2	877450	18.3	939928	42.5	060072	65672	75414	57
4	817524	24.1	877340	18.3	940183	42.5	059817	65694	75395	56
5	817668	24.1	877230	18.4	940438	42.5	059562	65716	75375	55
6	817813	24.1	877120	18.4	940694	42.5	059306	65738	75356	54
7	817958	24.1	877010	18.4	940949	42.5	059051	65759	75337	53
8	818103	24.1	876899	18.4	941204	42.5	058796	65781	75318	52
9	818247	24.1	876789	18.4	941458	42.5	058542	65803	75299	51
10	818392	24.1	876678	18.4	941714	42.5	058286	65825	75280	50
11	9.818536	24.0	9.876568	18.4	9.941968	42.5	10.058032	65847	75261	49
12	818681	24.0	876457	18.4	942223	42.5	057777	65869	75241	48
13	818825	24.0	876347	18.4	942478	42.5	057522	65891	75222	47
14	818969	24.0	876236	18.5	942733	42 5	057267	65913	75203	46
15	819113	24.0	876125	18.5	942988	42.5	057012	65935	75184	45
16	819257	24.0	876014	18.5	943243	42.5	056757	65956	75165	44
17	819401	24.0	875904	18.5	943498	42.5	056502	65978	75146	43
18	819545	23.9	875793	18.5	943752	42.5	056248	66000	75126	42
19	819689	23.9	875682	18.5	944007	42.5	055993	66022	75107	41
20	819832	23.9	875571	18.5	944262	42.5	055738	66044	75088	40
21	9.819976	23.9	9.875459	18.5	9.944517	42.5	10.055483	66066	75069	39
22	820120	23.9	875348	18.5	944771	42.4	055229	66088	75050	38
23	820263	23.9	875237	18.5	945026	42.4	054974	66109	75030	37
24	820406	23.9	875126	18.6	945281	42.4	054719	66131	75011	36
25	820550	23.8	875014	18.6	945535	42.4	054465	66153	74992	35
26	820693	23.8	874903	18.6	945790	42.4	054210	66175	74973	34
27	820836	23.8	874791	18.6	946045	42.4	053955	66197	74953	33
28	820979	23.8	874680	18.6	946299	42.4	053701	66218	74934	32
29	821122	23.8	874568	18.6	946554	42.4	053446	66240	74915	31
30	821265	23.8	874456	18.6	946808	42.4	053192	66262	74896	30
31	9.821407	23.8	9.874344	18.6	9.947063	42.4	10.052937	66284	74876	29
32	821550	23.8	874232	18.7	947318	42.4	052682	66306	74857	28
33	821693	23.7	874121	18.7	947572	42.4	052428	66327	74838	27
34	821835	23.7	874009	18.7	947826	42.4	052174	66349	74818	26
35	821977	23.7	873896	18.7	948081	42.4	051919	66371	74799	25
36	822120	23.7	873784	18.7	948336	42.4	051664	66393	74780	24
37	822262	23.7	873672	18.7	948590	42.4	051410	66414	74760	23
38	822404	23.7	873560	18.7	948844	42.4	051156	66436	74741	22
39	822546	23.7	873448	18.7	949099	42.4	050901	66458	74722	21
40	822688	23.6	873335	18.7	949353	42.4	050647	66480	74703	20
41	9.822830	23.6	9.873223	18.7	9.949607	42.4	10.050393	66501	74683	19
42	822972	23.6	873110	18.8	949862	42.4	050138	66523	74663	18
43	823114	23.6	872998	18.8	950116	42.4	049884	66545	74644	17
44	823255	23.6	872885	18.8	950370	42.4	049630	66566	74625	16
45	823397	23.6	872772	18.8	950625	42.4	049375	66588	74606	15
46	823539	23.6	872659	18.8	950879	42.4	049121	66610	74586	14
47	823680	23.5	872547	18.8	951133	42.4	048867	66632	74567	13
48	823821	23.5	872434	18.8	951388	42.4	048612	66653	74548	12
49	823963	23.5	872321	18.8	951642	42.4	048358	66675	74522	11
50	824104	23.5	872208	18.8	951896	42.4	048104	66697	74509	10
51	9.824245	23.5	9.872095	18.9	9.952150	42.4	10.047850	66718	74489	9
52	824386	23.5	871981	18.9	952405	42.4	047595	66740	74470	8
53	824527	23.5	871868	18.9	952659	42.4	047341	66762	74451	7
54	824668	23.4	871755	18.9	952913	42.4	047087	66783	74431	6
55	824808	23.4	871641	18.9	953167	42.3	046833	66805	74412	5
56	824949	23.4	871528	18.9	953421	42.3	046579	66827	74392	4
57	825090	23.4	871414	18.9	953675	42.3	046325	66848	74373	3
58	825230	23.4	871301	18.9	953929	42.3	046071	66870	74353	2
59	825371	23.4	871187	18.9	954183	42.3	045817	66891	74334	1
60	825511		871073		954437		045563	66913	74314	0
	Cosine.		Sine.		Cotang.		Tang.	N. cos.	N. sine.	'

48 Degrees.

Sine.	D. 10″	Cosine.	D. 10″	Tang.	D. 10″	Cotang.	N. sine.	N. cos.	
825511	23.4	9.871073	19.0	9.954437	42.3	10.045563	66913	74314	60
825651	23.3	870960	19.0	954691	42.3	045309	66935	74295	59
825791	23.3	870846	19.0	954945	42.3	045055	66956	74276	58
825931	23.3	870732	19.0	955200	42.3	044800	66978	74256	57
826071	23.3	870618	19.0	955454	42.3	044546	66999	74237	56
826211	23.3	870504	19.0	955707	42.3	044293	67021	74217	55
826351	23.3	870390	19.0	955961	42.3	044039	67043	74198	54
826491	23.3	870276	19.0	956215	42.3	043785	67064	74178	53
826631	23.3	870161	19.0	956469	42.3	043531	67086	74159	52
826770	23.2	870047	19.1	956723	42.3	043277	67107	74139	51
826910	23.2	869933	19.1	956977	42.3	043023	67129	74120	50
827049	23.2	9.869818	19.1	9.957231	42.3	10.042769	67151	74100	49
827189	23.2	869704	19.1	957485	42.3	042515	67172	74080	48
827328	23.2	869589	19.1	957739	42.3	042261	67194	74061	47
827467	23.2	869474	19.1	957993	42.3	042007	67215	74041	46
827606	23.2	869360	19.1	958246	42.3	041754	67237	74022	45
827745	23.2	869245	19.1	958500	42.3	041500	67258	74002	44
827884	23.1	869130	19.1	958754	42.3	041246	67280	73983	43
828023	23.1	869015	19.2	959008	42.3	040992	67301	73963	42
828162	23.1	868900	19.2	959262	42.3	040738	67323	73944	41
828301	23.1	868785	19.2	959516	42.3	040484	67344	73924	40
828439	23.1	9.868670	19.2	9.959769	42.3	10.040231	67366	73904	39
828578	23.1	868555	19.2	960023	42.3	039977	67387	73885	38
828716	23.1	868440	19.2	960277	42.3	039723	67409	73865	37
828555	23.0	868324	19.2	960531	42.3	039469	67430	73846	36
828993	23.0	868209	19.2	960784	42.3	039216	67452	73826	35
829131	23.0	868093	19.2	961038	42.3	038962	67473	73806	34
829269	23.0	867978	19.3	961291	42.3	038709	67495	73787	33
829407	23.0	867862	19.3	961545	42.3	038455	67516	73767	32
829545	23.0	867747	19.3	961799	42.3	038201	67538	73747	31
829683	23.0	867631	19.3	962052	42.3	037948	67559	73728	30
829821	22.9	9.867515	19.3	9.962306	42.3	10.037694	67580	73708	29
829959	22.9	867399	19.3	962560	42.3	037440	67602	73688	28
830097	22.9	867283	19.3	962813	42.3	037187	67623	73669	27
830234	22.9	867167	19.3	963067	42.3	036933	67645	73649	26
830372	22.9	867051	19.3	963320	42.3	036680	67666	73629	25
830509	22.9	866935	19.4	963574	42.3	036426	67688	73610	24
830646	22.9	866819	19.4	963827	42.3	036173	67709	73590	23
830784	22.9	866703	19.4	964081	42.3	035919	67730	73570	22
830921	22.8	866586	19.4	964335	42.3	035665	67752	73551	21
831058	22.8	866470	19.4	964588	42.2	035412	67773	73531	20
831195	22.8	9.866353	19.4	9.964842	42.2	10.035158	67795	73511	19
831332	22.8	866237	19.4	965095	42.2	034905	67816	73491	18
831469	22.8	866120	19.4	965349	42.2	034651	67837	73472	17
831606	22.8	866004	19.5	965602	42.2	034398	67859	73452	16
831742	22.8	865887	19.5	965855	42.2	034145	67880	73432	15
831879	22.8	865770	19.5	966109	42.2	033891	67901	73413	14
832015	22.7	865653	19.5	966362	42.2	033638	67923	73393	13
832152	22.7	865536	19.5	966616	42.2	033384	67944	73373	12
832288	22.7	865419	19.5	966869	42.2	033131	67965	73353	11
832425	22.7	865302	19.5	967123	42.2	032877	67987	73333	10
832561	22.7	9.865185	19.5	9.967376	42.2	10.032624	68008	73314	9
832697	22.7	865068	19.5	967629	42.2	032371	68029	73294	8
832833	22.7	864950	19.5	967883	42.2	032117	68051	73274	7
832969	22.6	864833	19.6	968136	42.2	031864	68072	73254	6
833105	22.6	864716	19.6	968389	42.2	031611	68093	73234	5
833241	22.6	864598	19.6	968643	42.2	031357	68115	73215	4
833377	22.6	864481	19.6	968896	42.2	031104	68136	73195	3
833512	22.6	864363	19.6	969149	42.2	030851	68157	73175	2
833648	22.6	864245	19.6	969403	42.2	030597	68179	73155	1
833783		864127		969656		030344	68200	73135	0
Cosine.		Sine.		Cotang.		Tang.	N. cos.	N. sine.	′

47 Degrees.

′	Sine.	D. 10″	Cosine.	D. 10″	Tang.	D. 10″	Cotang.	N .sine.	N. cos.	
0	9.833783	22.6	9.864127	19.6	9.969656	42.2	10.030344	68200	73135	60
1	833919	22.5	864010	19.6	969909	42.2	030091	68221	73116	59
2	834054	22.5	863892	19.7	970162	42.2	029838	68242	73096	58
3	834189	22.5	863774	19.7	970416	42.2	029584	68264	73076	57
4	834325	22.5	863656	19.7	970669	42.2	029331	68285	73056	56
5	834460	22.5	863538	19.7	970922	42.2	029078	68306	73036	55
6	834595	22.5	863419	19.7	971175	42.2	028825	68327	73016	54
7	834730	22.5	863301	19.7	971429	42.2	028571	68349	72996	53
8	834865	22.5	863183	19.7	971682	42.2	028318	68370	72976	52
9	834999	22.4	863064	19.7	971935	42.2	028065	68391	72957	51
10	835134	22.4	862946	19.8	972188	42.2	027812	68412	72937	50
11	9.835269	22.4	9.862827	19.8	9.972441	42.2	10.027559	68434	72917	49
12	835403	22.4	862709	19.8	972694	42.2	027306	68455	72897	48
13	835538	22.4	862590	19.8	972948	42.2	027052	68476	72877	47
14	835672	22.4	862471	19.8	973201	42.2	026799	68497	72857	46
15	835807	22.4	862353	19.8	973454	42.2	026546	68518	72837	45
16	835941	22.4	862234	19.8	973707	42.2	026293	68539	72817	44
17	836075	22.3	862115	19.8	973960	42.2	026040	68561	72797	43
18	836209	22.3	861996	19.8	974213	42.2	025787	68582	72777	42
19	836343	22.3	861877	19.8	974466	42.2	025534	68603	72757	41
20	836477	22.3	861758	19.9	974719	42.2	025281	68624	72737	40
21	9.836611	22.3	9.861638	19.9	9.974973	42.2	10.025027	68645	72717	39
22	836745	22.3	861519	19.9	975226	42.2	024774	68666	72697	38
23	836878	22.3	861400	19.9	975479	42.2	024521	68688	72677	37
24	837012	22.2	861280	19.9	975732	42.2	024268	68709	72657	36
25	837146	22.2	861161	19.9	975985	42.2	024015	68730	72637	35
26	837279	22.2	861041	19.9	976238	42.2	023762	68751	72617	34
27	837412	22.2	860922	19.9	976491	42.2	023509	68772	72597	33
28	837546	22.2	860802	19.9	976744	42.2	023256	68793	72577	32
29	837679	22.2	860682	20.0	976997	42.2	023003	68814	72557	31
30	837812	22.2	860562	20.0	977250	42.2	022750	68835	72537	30
31	9.837945	22.2	9.860442	20.0	9.977503	42.2	10.022497	68857	72517	29
32	838078	22.1	860322	20.0	977756	42.2	022244	68878	72497	28
33	838211	22.1	860202	20.0	978009	42.2	021991	68899	72477	27
34	838344	22.1	860082	20.0	978262	42.2	021738	68920	72457	26
35	838477	22.1	859962	20.0	978515	42.2	021485	68941	72437	25
36	838610	22.1	859842	20.0	978768	42.2	021232	68962	72417	24
37	838742	22.1	859721	20.1	979021	42.2	020979	68983	72397	23
38	838875	22.1	859601	20.1	979274	42.2	020726	69004	72377	22
39	839007	22.1	859480	20.1	979527	42.2	020473	69025	72357	21
40	839140	22.0	859360	20.1	979780	42.2	020220	69046	72337	20
41	9.839272	22.0	9.859239	20.1	9.980033	42.2	10.019967	69067	72317	19
42	839404	22.0	859119	20.1	980286	42.2	019714	69088	72297	18
43	839536	22.0	858998	20.1	980538	42.2	019462	69109	72277	17
44	839668	22.0	858877	20.1	980791	42.1	019209	69130	72257	16
45	839800	22.0	858756	20.2	981044	42.1	018956	69151	72236	15
46	839932	22.0	858635	20.2	981297	42.1	018703	69172	72216	14
47	840064	21.9	858514	20.2	981550	42.1	018450	69193	72196	13
48	840196	21.9	858393	20.2	981803	42.1	018197	69214	72176	12
49	840328	21.9	858272	20.2	982056	42.1	017944	69235	72156	11
50	840459	21.9	858151	20.2	982309	42.1	017691	69256	72136	10
51	9.840591	21.9	9.858029	20.2	9.982562	42.1	10.017438	69277	72116	9
52	840722	21.9	857908	20.2	982814	42.1	017186	69298	72095	8
53	840854	21.9	857786	20.2	983067	42.1	016933	69319	72075	7
54	840985	21.9	857665	20.3	983320	42.1	016680	69340	72055	6
55	841116	21.8	857543	20.3	983573	42.1	016427	69361	72035	5
56	841247	21.8	857422	20.3	983826	42.1	016174	69382	72015	4
57	841378	21.8	857300	20.3	984079	42.1	015921	69403	71995	3
58	841509	21.8	857178	20.3	984331	42.1	015669	69424	71974	2
59	841640	21.8	857056	20.3	984584	42.1	015416	69445	71954	1
60	841771		856934		984837		015163	69466	71934	0
	Cosine.		Sine.		Cotang.		Tang.	N. cos.	N.sine.	′

46 Degrees.

′	Sine.	D. 10″	Cosine.	D. 10″	Tang.	D. 10″	Cotang.	N. sine.	N. cos.	
0	9.841771	21.8	9.856934	20.3	9.984837	42.1	10.015163	69466	71934	60
1	841902	21.8	856812	20.3	985090	42.1	014910	69487	71914	59
2	842033	21.8	856690	20.4	985343	42.1	014657	69508	71894	58
3	842163	21.7	856568	20.4	985596	42.1	014404	69529	71873	57
4	842294	21.7	856446	20.4	985848	42.1	014152	69549	71853	56
5	842424	21.7	856323	20.4	986101	42.1	013899	69570	71833	55
6	842555	21.7	856201	20.4	986354	42.1	013646	69591	71813	54
7	842685	21.7	856078	20.4	986607	42.1	013393	69612	71792	53
8	842815	21.7	855956	20.4	986860	42.1	013140	69633	71772	52
9	842946	21.7	855833	20.4	987112	42.1	012888	69654	71752	51
10	843076	21.7	855711	20.5	987365	42.1	012635	69675	71732	50
11	9.843206	21.6	9.855588	20.5	9.987618	42.1	10.012382	69696	71711	49
12	843336	21.6	855465	20.5	987871	42.1	012129	69717	71691	48
13	843466	21.6	855342	20.5	988123	42.1	011877	69737	71671	47
14	843595	21.6	855219	20.5	988376	42.1	011624	69758	71650	46
15	843725	21.6	855096	20.5	988629	42.1	011371	69779	71630	45
16	843855	21.6	854973	20.5	988882	42.1	011118	69800	71610	44
17	843984	21.6	854850	20.5	989134	42.1	010866	69821	71590	43
18	844114	21.5	854727	20.6	989387	42.1	010613	69842	71569	42
19	844243	21.5	854603	20.6	989640	42.1	010360	69862	71549	41
20	844372	21.5	854480	20.6	989893	42.1	010107	69883	71529	40
21	9.844502	21.5	9.854356	20.6	9.990145	42.1	10.009855	69904	71508	39
22	844631	21.5	854233	20.6	990398	42.1	009602	69925	71488	38
23	844760	21.5	854109	20.6	990651	42.1	009349	69946	71468	37
24	844889	21.5	853986	20.6	990903	42.1	009097	69966	71447	36
25	845018	21.5	853862	20.6	991156	42.1	008844	69987	71427	35
26	845147	21.5	853738	20.6	991409	42.1	008591	70008	71407	34
27	845276	21.4	853614	20.7	991662	42.1	008338	70029	71386	33
28	845405	21.4	853490	20.7	991914	42.1	008086	70049	71366	32
29	845533	21.4	853366	20.7	992167	42.1	007833	70070	71345	31
30	845662	21.4	853242	20.7	992420	42.1	007580	70091	71325	30
31	9.845790	21.4	9.853118	20.7	9.992672	42.1	10.007328	70112	71305	29
32	845919	21.4	852994	20.7	992925	42.1	007075	70132	71284	28
33	846047	21.4	852869	20.7	993178	42.1	006822	70153	71264	27
34	846175	21.4	852745	20.7	993430	42.1	006570	70174	71243	26
35	846304	21.4	852620	20.7	993683	42.1	006317	70195	71223	25
36	846432	21.3	852496	20.8	993936	42.1	006064	70215	71203	24
37	846560	21.3	852371	20.8	994189	42.1	005811	70236	71182	23
38	846688	21.3	852247	20.8	994441	42.1	005559	70257	71162	22
39	846816	21.3	852122	20.8	994694	42.1	005306	70277	71141	21
40	846944	21.3	851997	20.8	994947	42.1	005053	70298	71121	20
41	9.847071	21.3	9.851872	20.8	9.995199	42.1	10.004801	70319	71100	19
42	847199	21.3	851747	20.8	995452	42.1	004548	70339	71080	18
43	847327	21.3	851622	20.8	995705	42.1	004295	70360	71059	17
44	847454	21.2	851497	20.9	995957	42.1	004043	70381	71039	16
45	847582	21.2	851372	20.9	996210	42.1	003790	70401	71019	15
46	847709	21.2	851246	20.9	996463	42.1	003537	70422	70998	14
47	847836	21.2	851121	20.9	996715	42.1	003285	70443	70978	13
48	847964	21.2	850996	20.9	996968	42.1	003032	70463	70957	12
49	848091	21.2	850870	20.9	997221	42.1	002779	70484	70937	11
50	848218	21.2	850745	20.9	997473	42.1	002527	70505	70916	10
51	9.848345	21.2	9.850619	20.9	9.997726	42.1	10.002274	70525	70896	9
52	848472	21.1	850493	21.0	997979	42.1	002021	70546	70875	8
53	848599	21.1	850368	21.0	998231	42.1	001769	70567	70855	7
54	848726	21.1	850242	21.0	998484	42.1	001516	70587	70834	6
55	848852	21.1	850116	21.0	998737	42.1	001263	70608	70813	5
56	848979	21.1	849990	21.0	998989	42.1	001011	70628	70793	4
57	849106	21.1	849864	21.0	999242	42.1	000758	70649	70772	3
58	849232	21.1	849738	21.0	999495	42.1	000505	70670	70752	2
59	849359	21.1	849611	21.0	999748	42.1	000253	70690	70731	1
60	849485		849485		10.000000		000000	70711	70711	0
	Cosine.		Sine.		Cotang.		Tang.	N. cos.	N. sine.	′

45 Degrees.

TABLE III.

LOGARITHMS OF NUMBERS.

FROM 1 TO 200,

INCLUDING TWELVE DECIMAL PLACES.

N.	Log.	N.	Log.	N.	Log.
1	000000 000000	41	612783 856720	81	908485 018879
2	301029 995664	42	623249 290398	82	913813 852384
3	477121 254720	43	633468 455580	83	919078 092376
4	602059 991328	44	643452 676486	84	924279 286062
5	698970 004336	45	653212 513775	85	929418 925714
6	778151 250384	46	662757 831682	86	934498 451244
7	845098 040014	47	672097 857926	87	939519 252619
8	903089 986992	48	681241 237376	88	944482 672150
9	954242 509439	49	690196 080028	89	949390 006645
10	Same as to 1.	50	Same as to 5.	90	Same as to 9.
11	041392 685158	51	707570 176098	91	959041 392321
12	079181 246048	52	716003 343635	92	963787 827346
13	113943 352307	53	724275 869601	93	968482 948554
14	146128 035678	54	732393 759823	94	973127 853600
15	176091 259056	55	740362 689494	95	977723 605889
16	204119 982656	56	748188 027006	96	982271 233040
17	230448 921378	57	755874 855672	97	986771 734266
18	255272 505103	58	763427 993563	98	991226 075692
19	278753 600953	59	770852 011642	99	995635 194598
20	Same as to 2.	60	Same as to 6.	100	Same as to 10.
21	322219 2947	61	785329 835011	101	004321 373783
22	342422 680822	62	792391 699498	102	008600 171762
23	361727 836018	63	799340 549453	103	012837 224705
24	380211 241712	64	806179 973984	104	017033 339299
25	397940 008672	65	812913 356643	105	021189 299070
26	414973 347971	66	819543 935542	106	025305 865265
27	431363 764159	67	826074 802701	107	029383 777685
28	447158 031342	68	832508 912706	108	033423 755487
29	462397 997899	69	838849 090737	109	037426 497941
30	Same as to 3.	70	Same as to 7.	110	Same as to 11.
31	491361 693834	71	851258 348719	111	045322 978787
32	505149 978320	72	857332 496431	112	049218 022670
33	518513 939878	73	863322 860120	113	053078 443483
34	531478 917042	74	869231 719731	114	056904 851336
35	544068 044350	75	875061 263392	115	060697 840354
36	556302 500767	76	880813 592281	116	064457 989227
37	568201 724067	77	886490 725172	117	068185 861746
38	579783 596617	78	892094 602690	118	071882 007306
39	591064 607026	79	897627 091290	119	075546 961393
40	Same as to 4.	80	Same as to 8.	120	Same as to 12.

N.	Log.	N.	Log.	N.	Log
121	082785 370316	148	170261 715395	175	243038 048686
122	086359 830675	149	173186 268412	176	245512 667814
123	089905 111439	150	176091 259056	177	247973 266362
124	093421 685162	151	178976 947293	178	250420 002309
125	096910 013008	152	181843 587945	179	252853 030980
126	100370 545118	153	184691 430818	180	255272 505103
127	103803 720956	154	187520 720836	181	257678 574869
128	107209 969648	155	190331 698170	182	260071 387985
129	110589 710299	156	193124 588354	183	262451 089730
130	Same as to 13.	157	195899 652409	184	264817 823010
131	117271 295656	158	198657 086954	185	267171 728403
132	120573 931206	159	201397 124320	186	269512 944218
133	123851 640967	160	204119 982656	187	271841 606536
134	127104 798365	161	206825 876032	188	274157 849264
135	130333 768495	162	209515 014543	189	276461 804173
136	133538 908370	163	212187 604404	190	278753 600953
137	136720 567156	164	214843 848048	191	281033 367248
138	139879 086401	165	217483 944214	192	283301 228704
139	143014 800254	166	220108 088040	193	285557 309008
140	146128 035678	167	222716 471148	194	287801 729930
141	149219 112655	168	225309 281726	195	290034 611362
142	152288 344383	169	227886 704614	196	292256 071356
143	155336 037465	170	230448 921378	197	294466 226162
144	158362 492095	171	232996 110392	198	296665 190262
145	161368 002235	172	235528 446908	199	298853 076410
146	164352 855784	173	238046 103129		
147	167317 334748	174	240549 248283		

LOGARITHMS OF THE PRIME NUMBERS

From 200 to 1543,

INCLUDING TWELVE DECIMAL PLACES.

N.	Log.	N.	Log.	N.	Log.
201	303196 057420	277	442479 769064	379	578639 209968
203	307496 037913	281	448706 319905	383	583198 773968
207	315970 345457	283	451786 435524	389	589949 601326
209	320146 286111	293	466867 620354	397	598790 506763
211	324282 455298	307	487138 375477	401	603144 372620
223	348304 863048	311	492760 389027	409	611723 308007
227	356025 857193	313	495544 337546	419	622214 022966
229	359835 482340	317	501059 262218	421	624282 095836
233	367355 921026	331	519827 993776	431	634477 270161
239	378397 900948	337	527629 900871	433	636487 896353
241	382017 042575	347	540329 474791	439	642424 520242
251	399673 721481	349	542825 426959	443	646403 726223
257	409933 123331	353	547774 705388	449	652246 341003
263	419955 748490	359	555094 448578	457	659916 200070
269	429752 280002	367	564666 064252	461	663700 925390
271	432969 290874	373	571708 831809	463	665580 991018

[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]
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[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]
[illegible]	[illegible]	[illegible]	[illegible]	1439	158060 730919
[illegible]	[illegible]	[illegible]	[illegible] 353401	1447	[illegible] 531109
[illegible]	[illegible]	[illegible]	[illegible]	1451	161667 412427
[illegible]	[illegible]	[illegible]	[illegible]	1453	162265 614286
733	[illegible]	1097	[illegible]	1459	164055 291583
739	[illegible]	1091	037824 750588	1471	167612 672629
743	[illegible] 813761	1093	[illegible] 161950	1481	170555 058512
751	[illegible]	1097	[illegible] 627575	1483	171141 151014
757	[illegible]	1103	042595 512440	1487	172310 965489
761	[illegible] 656771	1109	044931 546119	1489	172894 731332
769	885926 339801	1117	048053 173116	1493	174059 807708
773	888179 493918	1123	050379 756261	1499	175801 632866
787	895974 732359	1129	052693 941925	1511	179264 464329
797	901458 321396	1151	061075 323630	1523	182699 903324
809	907948 521612	1153	061829 307295	1531	184975 190807
811	909020 854211	1163	065579 714728	1543	188365 926053

AUXILIARY LOGARITHMS.

N.	Log.		N.	Log.	
1.009	003891166237	A	1.0009	000390689248	B
1.008	003460532110		1.0008	000347296684	
1.007	003029470554		1.0007	000303899784	
1.006	002598080685		1.0006	000260498547	
1.005	002166061756		1.0005	000217092970	
1.004	001733712775		1.0004	000173683057	
1.003	001300933020		1.0003	000130268804	
1.002	000867721529		1.0002	000086850211	
1.001	000434077479		1.0001	000043427277	

C

N.	Log.	N.	Log.
1.00009	000039083266	1.000009	000003908628
1.00008	000034740691	1.000008	000003474338
1.00007	000030398072	1.000007	000003040047
1.00006	000026055410	1.000006	000002605756
1.00005	000021712704	1.000005	000002171464
1.00004	000017371430	1.000004	000001737173
1.00003	000013028638	1.000003	000001302880
1.00002	000008685802	1.000002	000000868587
1.00001	000004342923	1.000001	000000434294

N.	Log.	
1.0000001	000000043429	(n)
1.00000001	000000004343	(o)
1.000000001	000000000434	(p)
1.0000000001	000000000043	(q)

$m=0.4342944819$ log. —1.637784298.

By the preceding tables—and the auxiliaries *A*, *B*, and *C*, we can find the logarithm of any number, true to at least ten decimal places.

But some may prefer to use the following direct formula, which may be found in any of the standard works on algebra:

$$\text{Log. }(z+1)=\text{log.}z+0.8685889638\left(\frac{1}{2z+1}\right)$$

The result will be true to twelve decimal places, if z be over 2000.

The log. of composite numbers can be determined by the combination of logarithms, already in the table, and the prime numbers from the formula.

Thus, the number 3083 is a prime number, find its logarithm.

We first find the log. of the number 3082. By factoring, we discover that this is the product of 46 into 67.

Log. 46,	1.6627578316
Log. 67,	1.8260748027
Log. 3082	3.4888326343

$$\text{Log. } 3083 = 3.4888326343 + \frac{0.8685889638}{6165}$$

NUMBERS AND THEIR LOGARITHMS,

OFTEN USED IN COMPUTATIONS.

		Log.
Circumference of a circle to dia. 1 Surface of a sphere to diameter 1 Area of a circle to *radius* 1	=3.14159265	0.4971499
Area of a circle to diameter 1	= .7853982	—1.8950899
Capacity of a sphere to diameter 1	= .5235988	—1.7189986
Capacity of a sphere to radius 1	=4.1887902	0.6220886
Arc of any circle equal to the radius	=57°29578	1.7581226
Arc equal to radius expressed in sec.	=206264″8	5.3144251
Length of a degree, (radius unity)	=.01745329	—2.2418773
12 hours expressed in seconds,	= 43200	4.6354837
Complement of the same,	=0.00002315	—5.3645163
360 degrees expressed in seconds,	= 1296000	6.1126050

A gallon of distilled water, when the temperature is 62° Fahrenheit, and Barometer 30 inches, is 277.$\frac{274}{1000}$ cubic inches.

$\sqrt{277.274}=16.651542$ nearly.

$\sqrt{\frac{277.274}{.775398}}=18.78925284$ $\sqrt{231}=15.198684.$

$\sqrt{282}=16.792855.$

$\sqrt{\frac{282.}{.785398}}=18.948708.$

The French Metre=3.2808992, English *feet* linear measure, =39.3707904 inches, the length of a pendulum vibrating seconds.

Distance.	¼ Deg.		½ Deg.		¾ Deg.	
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.
1	1. 00	0. 00	1. 00	0. 01	1. 00	0. 01
2	2. 00	0. 01	2. 00	0. 02	2. 00	0. 03
3	3. 00	0. 01	3. 00	0. 03	3. 00	0. 04
4	4. 00	0. 02	4. 00	0. 03	4. 00	0. 05
5	5. 00	0. 02	5. 00	0. 04	5. 00	0. 07
6	6. 00	0. 03	6. 00	0. 05	6. 00	0. 08
7	7. 00	0. 03	7. 00	0. 06	7. 00	0. 09
8	8. 00	0. 03	8. 00	0. 07	8. 00	0. 10
9	9. 00	0. 04	9. 00	0. 08	9. 00	0. 12
10	10. 00	0. 04	10. 00	0. 09	10. 00	0. 13
11	11. 00	0. 05	11. 00	0. 10	11. 00	0. 14
12	12. 00	0. 05	12. 00	0. 10	12. 00	0. 16
13	13. 00	0. 06	13. 00	0. 11	13. 00	0. 17
14	14. 00	0. 06	14. 00	0. 12	14. 00	0. 18
15	15. 00	0. 07	15. 00	0. 13	15. 00	0. 20
16	16. 00	0. 07	16. 00	0. 14	16. 00	0. 21
17	17. 00	0. 07	17. 00	0. 15	17. 00	0. 22
18	18. 00	0. 08	18. 00	0. 16	18. 00	0. 24
19	19. 00	0. 08	19. 00	0. 17	19. 00	0. 25
20	20. 00	0. 09	20. 00	0. 17	20. 00	0. 26
21	21. 00	0. 09	21. 00	0. 18	21. 00	0. 27
22	22. 00	0. 10	22. 00	0. 19	22. 00	0. 29
23	23. 00	0. 10	23. 00	0. 20	23. 00	0. 30
24	24. 00	0. 10	24. 00	0. 21	24. 00	0. 31
25	25. 00	0. 11	25. 00	0. 22	25. 00	0. 33
26	26. 00	0. 11	26. 00	0. 23	26. 00	0. 34
27	27. 00	0. 12	27. 00	0. 24	27. 00	0. 35
28	28. 00	0. 12	28. 00	0. 24	28. 00	0. 37
29	29. 00	0. 13	29. 00	0. 25	29. 00	0. 38
30	30. 00	0. 13	30. 00	0. 26	30. 00	0. 39
35	35. 00	0. 15	35. 00	0. 31	35. 00	0. 46
40	40. 00	0. 17	40. 00	0. 35	40. 00	0. 52
45	45. 00	0. 20	45. 00	0. 39	45. 00	0. 59
50	50. 00	0. 22	50. 00	0. 44	50. 00	0. 65
55	55. 00	0. 24	55. 00	0. 48	55. 00	0. 72
60	60. 00	0. 26	60. 00	0. 52	59. 99	0. 79
65	65. 00	0. 28	65. 00	0. 57	64. 99	0. 85
70	70. 00	0. 31	70. 00	0. 61	69. 99	0. 92
75	75. 00	0. 33	75. 00	0. 65	74. 99	0. 98
80	80. 00	0. 35	80. 00	0. 70	79. 99	1. 05
85	85. 00	0. 37	85. 00	0. 74	84. 99	1. 11
90	90. 00	0. 39	90. 00	0. 79	89. 99	1. 18
95	95. 00	0. 41	95. 00	0. 83	94. 99	1. 24
100	100. 00	0. 44	100. 00	0. 87	99. 99	1. 31
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.
	89¾ Deg.		89½ Deg.		89¼ Deg.	

TRAVERSE TABLE.

Distance.	1 Deg.		1¼ Deg.		1½ Deg.		1¾ Deg.	
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.
1	1. 00	0. 02	1. 00	0. 02	1. 00	0. 03	1. 00	0. 03
2	2. 00	0. 03	2. 00	0. 04	2. 00	0. 05	2. 00	0. 06
3	3. 00	0. 05	3. 00	0. 07	3. 00	0. 08	3. 00	0. 09
4	4. 00	0. 07	4. 00	0. 09	4. 00	0. 10	4. 00	0. 12
5	5. 00	0. 09	5. 00	0. 11	5. 00	0. 13	5. 00	0. 15
6	6. 00	0. 10	6. 00	0. 13	6. 00	0. 16	6. 00	0. 18
7	7. 00	0. 12	7. 00	0. 15	7. 00	0. 18	7. 00	0. 21
8	8. 00	0. 14	8. 00	0. 17	8. 00	0. 21	8. 00	0. 25
9	9. 00	0. 16	9. 00	0. 20	9. 00	0. 24	9. 00	0. 28
10	10. 00	0. 17	10. 00	0. 22	10. 00	0. 26	10. 00	0. 31
11	11. 00	0. 19	11. 00	0. 24	11. 00	0. 28	10. 99	0. 34
12	12. 00	0. 21	12. 00	0. 26	12. 00	0. 31	11. 99	0. 37
13	13. 00	0. 23	13. 00	0. 28	13. 00	0. 34	12. 99	0. 40
14	14. 00	0. 24	14. 00	0. 31	14. 00	0. 37	13. 99	0. 43
15	15. 00	0. 26	15. 00	0. 33	14. 99	0. 39	14. 99	0. 46
16	16. 00	0. 28	16. 00	0. 35	15. 99	0. 42	15. 99	0. 49
17	17. 00	0. 30	17. 00	0. 37	16. 99	0. 45	16. 99	0. 52
18	18. 00	0. 31	18. 00	0. 39	17. 99	0. 47	17. 99	0. 55
19	19. 00	0. 33	19. 00	0. 41	18. 99	0. 50	18. 99	0. 58
20	20. 00	0. 35	20. 00	0. 44	19. 99	0. 52	19. 99	0. 61
21	21. 00	0. 37	21. 00	0. 46	20. 99	0. 55	20. 99	0. 64
22	22. 00	0. 38	21. 99	0. 48	21. 99	0. 58	21. 99	0. 67
23	23. 00	0. 40	22. 99	0. 50	22. 99	0. 60	22. 99	0. 70
24	24. 00	0. 42	23. 99	0. 52	23. 99	0. 63	23. 99	0. 73
25	25. 00	0. 44	24. 99	0. 55	24. 99	0. 65	24. 99	0. 76
26	26. 00	0. 45	25. 99	0. 57	25. 99	0. 68	25. 99	0. 79
27	27. 00	0. 47	26. 99	0. 59	26. 99	0. 71	26. 99	0. 83
28	28. 00	0. 49	27. 99	0. 61	27. 99	0. 73	27. 99	0. 86
29	29. 00	0. 51	28. 99	0. 63	28. 99	0. 76	28. 99	0. 89
30	30. 00	0. 52	29. 99	0. 65	29. 99	0. 79	29. 99	0. 92
35	34. 99	0. 61	34. 99	0. 76	34. 99	0. 92	34. 98	1. 07
40	39. 99	0. 70	39. 99	0. 87	39. 99	1. 05	39. 98	1. 22
45	44. 99	0. 79	44. 99	0. 98	44. 99	1. 18	44. 98	1. 37
50	49. 99	0. 87	49. 99	1. 09	49. 98	1. 31	49. 98	1. 53
55	54. 99	0. 96	54. 99	1. 20	54. 98	1. 44	54. 97	1. 68
60	59. 99	1. 05	59. 99	1. 31	59. 98	1. 57	59. 97	1. 83
65	64. 99	1. 13	64. 98	1. 42	64. 98	1. 70	64. 97	1. 99
70	69. 99	1. 22	69. 98	1. 53	69. 98	1. 83	69. 97	2. 14
75	74. 99	1. 31	74. 98	1. 64	74. 97	1. 96	74. 97	2. 29
80	79. 99	1. 40	79. 98	1. 75	79. 97	2. 09	79. 96	2. 44
85	84. 99	1. 48	84. 98	1. 85	84. 97	2. 23	84. 96	2. 60
90	89. 99	1. 57	89. 98	1. 96	89. 97	2. 36	89. 96	2. 75
95	94. 99	1. 66	94. 98	2. 07	94. 97	2. 49	94. 96	2. 90
100	99. 98	1. 75	99. 98	2. 18	99. 97	2. 62	99. 95	3. 05
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.
	89 Deg.		88¾ Deg.		88½ Deg.		88¼ Deg.	

Distance.	2 Deg.		2¼ Deg.		2½ Deg.		2¾ Deg.	
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.
1	1. 00	0. 03	1. 00	0. 04	1. 00	0. 04	1. 00	0. 05
2	2. 00	0. 07	2. 00	0. 08	2. 00	0. 09	2. 00	0. 10
3	3. 00	0. 10	3. 00	0. 12	3. 00	0. 13	3. 00	0. 14
4	4. 00	0. 14	4. 00	0. 16	4. 00	0. 17	4. 00	0. 19
5	5. 00	0. 17	5. 00	0. 20	5. 00	0. 22	4. 99	0. 24
6	6. 00	0. 21	6. 00	0. 24	5. 99	0. 26	5. 99	0. 29
7	7. 00	0. 24	6. 99	0. 27	6. 99	0. 31	6. 99	0. 34
8	7. 99	0. 28	7. 99	0. 31	7. 99	0. 35	7. 99	0. 38
9	8. 99	0. 31	8. 99	0. 35	8. 99	0. 39	8. 99	0. 43
10	9. 99	0. 35	9. 99	0. 39	9. 99	0. 44	9. 99	0. 48
11	10. 99	0. 38	10. 99	0. 43	10. 99	0. 48	10. 99	0. 53
12	11. 99	0. 42	11. 99	0. 47	11. 99	0. 52	11. 99	0. 58
13	12. 99	0. 45	12. 99	0. 51	12. 99	0. 57	12. 99	0. 62
14	13. 99	0. 49	13. 99	0. 55	13. 99	0. 61	13. 98	0. 67
15	14. 99	0. 52	14. 99	0. 59	14. 99	0. 65	14. 98	0. 72
16	15. 99	0. 56	15. 99	0. 63	15. 99	0. 70	15. 98	0. 77
17	16. 99	0. 59	16. 99	0. 67	16. 98	0. 74	16. 98	0. 82
18	17. 99	0. 63	17. 99	0. 71	17. 98	0. 79	17. 98	0. 86
19	18. 99	0. 66	18. 99	0. 75	18. 98	0. 83	18. 98	0. 91
20	19. 99	0. 70	19. 98	0. 79	19. 98	0. 87	19. 98	0. 96
21	20. 99	0. 73	20. 98	0. 82	20. 98	0. 92	20. 98	1. 01
22	21. 99	0. 77	21. 98	0. 86	21. 98	0. 96	21. 97	1. 06
23	22. 99	0. 80	22. 98	0. 90	22. 98	1. 00	22. 97	1. 10
24	23. 99	0. 84	23. 98	0. 94	23. 98	1. 05	23. 97	1. 15
25	24. 98	0. 87	24. 98	0. 98	24. 98	1. 09	24. 97	1. 20
26	25. 98	0. 91	25. 98	1. 02	25. 98	1. 13	25. 97	1. 25
27	26. 98	0. 94	26. 98	1. 06	26. 97	1. 18	26. 97	1. 30
28	27. 98	0. 98	27. 98	1. 10	27. 97	1. 22	27. 97	1. 34
29	28. 98	1. 01	28. 98	1. 14	28. 97	1. 26	28. 97	1. 39
30	29. 98	1. 05	29. 98	1. 18	29. 97	1. 31	29. 97	1. 44
35	34. 98	1. 22	34. 97	1. 37	34. 97	1. 53	34. 96	1. 68
40	39. 98	1. 40	39. 97	1. 57	39. 96	1. 75	39. 95	1. 92
45	44. 97	1. 57	44. 97	1. 77	44. 96	1. 96	44. 95	2. 16
50	49. 97	1. 74	49. 96	1. 96	49. 95	2. 18	49. 94	2. 40
55	54. 97	1. 92	54. 96	2. 16	54. 95	2. 40	54. 94	2. 64
60	59. 96	2. 09	59. 95	2. 36	59. 94	2. 62	59. 93	2. 88
65	64. 96	2. 27	64. 95	2. 55	64. 94	2. 84	64. 93	3. 12
70	69. 96	2. 44	69. 95	2. 75	69. 93	3. 05	69. 92	3. 36
75	74. 95	2. 62	74. 94	2. 94	74. 93	3. 27	74. 91	3. 60
80	79. 95	2. 79	79. 94	3. 14	79. 92	3. 49	79. 91	3. 84
85	84. 95	2. 97	84. 93	3. 34	84. 92	3. 71	84. 90	4. 08
90	89. 95	3. 14	89. 93	3. 53	89. 91	3. 93	89. 90	4. 32
95	94. 94	3. 32	94. 93	3. 73	94. 91	4. 14	94. 89	4. 56
100	99. 94	3. 49	99. 92	3. 93	99. 91	4. 36	99. 88	4. 80
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.
	88 Deg.		87¾ Deg.		87½ Deg.		87¼ Deg.	

Distance.	3 Deg.		3¼ Deg.		3½ Deg.		3¾ Deg.	
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.
1	1. 00	0. 05	1. 00	0. 06	1. 00	0. 06	1. 00	0. 06
2	2. 00	0. 10	2. 00	0. 11	2. 00	0. 12	2. 00	0. 13
3	3. 00	0. 16	3. 00	0. 17	2. 99	0. 18	2. 99	0. 20
4	3. 99	0. 21	3. 99	0. 23	3. 99	0. 24	3. 99	0. 26
5	4. 99	0. 26	4. 99	0. 28	4. 99	0. 31	4. 99	0. 33
6	5. 99	0. 31	5. 99	0. 34	5. 99	0. 37	5. 99	0. 39
7	6. 99	0. 37	6. 99	0. 40	6. 99	0. 43	6. 99	0. 46
8	7. 99	0. 42	7. 99	0. 45	7. 99	0. 49	7. 98	0. 52
9	8. 99	0. 47	8. 99	0. 51	8. 98	0. 55	8. 98	0. 59
10	9. 99	0. 52	9. 98	0. 57	9. 98	0. 61	9. 98	0. 65
11	10. 98	0. 58	10. 98	0. 62	10. 98	0. 67	10. 98	0. 72
12	11. 98	0. 63	11. 98	0. 68	11. 98	0. 73	11. 97	0. 78
13	12. 98	0. 68	12. 98	0. 73	12. 98	0. 79	12. 97	0. 85
14	13. 98	0. 73	13. 98	0. 79	13. 97	0. 85	13. 97	0. 92
15	14. 98	0. 79	14. 98	0. 85	14. 97	0. 92	14. 97	0. 98
16	15. 98	0. 84	15. 97	0. 91	15. 97	0. 98	15. 97	1. 05
17	16. 98	0. 89	16. 97	0. 96	16. 97	1. 04	16. 96	1. 11
18	17. 98	0. 94	17. 97	1. 02	17. 97	1. 10	17. 96	1. 18
19	18. 98	0. 99	18. 97	1. 08	18. 96	1. 16	18. 96	1. 24
20	19. 97	1. 05	19. 97	1. 13	19. 96	1. 22	19. 96	1. 31
21	20. 97	1. 10	20. 97	1. 19	20. 96	1. 28	20. 96	1. 37
22	21. 97	1. 15	21. 96	1. 25	21. 96	1. 34	21. 95	1. 44
23	22. 97	1. 20	22. 96	1. 30	22. 96	1. 40	22. 95	1. 50
24	23. 97	1. 26	23. 96	1. 36	23. 96	1. 47	23. 95	1. 57
25	24. 97	1. 31	24. 96	1. 42	24. 95	1. 53	24. 95	1. 64
26	25. 96	1. 36	25. 96	1. 47	25. 95	1. 59	25. 94	1. 70
27	26. 96	1. 41	26. 96	1. 53	26. 95	1. 65	26. 94	1. 77
28	27. 96	1. 47	27. 95	1. 59	27. 95	1. 71	27. 94	1. 83
29	28. 96	1. 52	28. 95	1. 64	28. 95	1. 77	28. 94	1. 90
30	29. 96	1. 57	29. 95	1. 70	29. 94	1. 83	29. 94	1. 96
35	34. 95	1. 83	34. 94	1. 98	34. 93	2. 14	34. 92	2. 29
40	39. 95	2. 09	39. 94	2. 27	39. 93	2. 44	39. 91	2. 62
45	44. 94	2. 36	44. 93	2. 55	44. 92	2. 75	44. 90	2. 94
50	49. 93	2. 62	49. 92	2. 83	49. 91	3. 05	49. 89	3. 27
55	54. 92	2. 88	54. 91	3. 12	54. 90	3. 36	54. 88	3. 60
60	59. 92	3. 14	59. 90	3. 40	59. 89	3. 66	59. 87	3. 92
65	64. 91	3. 40	64. 90	3. 69	64. 88	3. 97	64. 86	4. 25
70	69. 90	3. 66	69. 89	3. 97	69. 87	4. 27	69. 85	4. 58
75	74. 90	3. 93	74. 88	4. 25	74. 86	4. 58	74. 84	4. 91
80	79. 89	4. 19	79. 87	4. 54	79. 85	4. 88	79. 83	5. 23
85	84. 88	4. 45	84. 86	4. 82	84. 84	5. 19	84. 82	5. 56
90	89. 88	4. 71	89. 86	5. 10	89. 83	5. 49	89. 81	5. 89
95	94. 87	4. 97	94. 85	5. 39	94. 82	5. 80	94. 80	6. 21
00	99. 86	5. 23	99. 84	5. 67	99. 81	6. 10	99. 79	6. 54
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.
	87 Deg.		86¾ Deg.		86½ Deg.		86¼ Deg.	

Distance.	4 Deg.		4¼ Deg.		4½ Deg.		4¾ Deg.	
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.
1	1. 00	0. 07	1. 00	0. 07	1. 00	0. 08	1. 00	0. 08
2	2. 00	0. 14	1. 99	0. 15	1. 99	0. 16	1. 99	0. 17
3	2. 99	0. 21	2. 99	0. 22	2. 99	0. 24	2. 99	0. 25
4	3. 99	0. 28	3. 99	0. 30	3. 99	0. 31	3. 98	0. 33
5	4. 99	0. 35	4. 99	0. 37	4. 98	0. 39	4. 98	0. 41
6	5. 99	0. 42	5. 98	0. 44	5. 98	0. 47	5. 98	0. 50
7	6. 98	0. 49	6. 98	0. 52	6. 98	0. 55	6. 97	0. 58
8	7. 98	0. 56	7. 98	0. 59	7. 98	0. 63	7. 97	0. 66
9	8. 98	0. 63	8. 98	0. 67	8. 97	0. 71	8. 97	0. 75
10	9. 98	0. 70	9. 97	0. 74	9. 97	0. 78	9. 97	0. 83
11	10. 97	0. 77	10. 97	0. 82	10. 97	0. 86	10. 96	0. 91
12	11. 97	0. 84	11. 97	0. 89	11. 96	0. 94	11. 96	0. 99
13	12. 97	0. 91	12. 96	0. 96	12. 96	1. 02	12. 96	1. 08
14	13. 97	0. 98	13. 96	1. 04	13. 96	1. 10	13. 95	1. 16
15	14. 96	1. 05	14. 96	1. 11	14. 95	1. 18	14. 95	1. 24
16	15. 96	1. 12	15. 96	1. 19	15. 95	1. 26	15. 95	1. 32
17	16. 96	1. 19	16. 95	1. 26	16. 95	1. 33	16. 94	1. 41
18	17. 96	1. 26	17. 95	1. 33	17. 94	1. 41	17. 94	1. 49
19	18. 95	1. 33	18. 95	1. 40	18. 94	1. 49	18. 93	1. 57
20	19. 95	1. 40	19. 95	1. 48	19. 94	1. 57	19. 93	1. 66
21	20. 95	1. 46	20. 94	1. 53	20. 94	1. 65	20. 93	1. 74
22	21. 95	1. 53	21. 94	1. 63	21. 93	1. 73	21. 92	1. 82
23	22. 94	1. 60	22. 94	1. 70	22. 93	1. 80	22. 92	1. 90
24	23. 94	1. 67	23. 93	1. 78	23. 93	1. 88	23. 92	1. 99
25	24. 94	1. 74	24. 93	1. 85	24. 92	1. 96	24. 91	2. 07
26	25. 94	1. 81	25. 93	1. 93	25. 92	2. 04	25. 91	2. 15
27	26. 93	1. 88	26. 93	2. 00	26. 92	2. 12	26. 91	2. 24
28	27. 93	1. 95	27. 92	2. 08	27. 91	2. 20	27. 90	2. 32
29	28. 93	2. 02	28. 92	2. 15	28. 91	2. 28	28. 90	2. 40
30	29. 93	2. 09	29. 92	2. 22	29. 91	2. 35	29. 90	2. 48
35	34. 91	2. 44	34. 90	2. 59	34. 89	2. 75	34. 88	2. 90
40	39. 90	2. 79	39. 89	2. 96	39. 88	3. 14	39. 86	3. 31
45	44. 89	3. 14	44. 83	3. 33	44. 86	3. 53	44. 85	3. 73
50	49. 88	3. 49	49. 86	3. 71	49. 85	3. 92	49. 83	4. 14
55	54. 87	3. 84	54. 85	4. 08	54. 83	4. 32	54. 81	4. 55
60	59. 85	4. 19	59. 84	4. 45	59. 82	4. 71	59. 79	4. 97
65	64. 84	4. 53	64. 82	4. 82	64. 80	5. 10	64. 78	5. 38
70	69. 83	4. 83	69. 81	5. 19	69. 78	5. 49	69. 76	5. 80
75	74. 82	5. 23	74. 79	5. 56	74. 77	5. 88	74. 74	6. 21
80	79. 81	5. 58	79. 78	5. 93	79. 75	6. 28	79. 73	6. 62
85	84. 79	5. 93	84. 77	6. 30	84. 74	6. 67	84. 71	7. 04
90	89. 78	6. 28	89. 75	6. 67	89. 72	7. 06	89. 69	7. 45
95	94. 77	6. 63	94. 74	7. 04	94. 71	7. 45	94. 67	7. 87
100	99. 76	6. 98	99. 73	7. 41	99. 69	7. 85	99. 66	8. 28
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.
	86 Deg.		85¾ Deg.		85½ Deg.		85¼ Deg.	

Distance.	5 Deg.		5¼ Deg.		5½ Deg.		5¾ Deg.	
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.
1	1. 00	0. 09	1. 00	0. 09	1. 00	0. 10	0. 99	0. 10
2	1. 99	0. 17	1. 99	0. 18	1. 99	0. 19	1. 99	0. 20
3	2. 99	0. 26	2. 99	0. 27	2. 99	0. 29	2. 98	0. 30
4	3. 98	0. 35	3. 98	0. 37	3. 98	0. 38	3. 98	0. 40
5	4. 98	0. 44	4. 98	0. 46	4. 98	0. 48	4. 97	0. 50
6	5. 98	0. 52	5. 97	0. 55	5. 97	0. 58	5. 97	0. 60
7	6. 97	0. 61	6. 97	0. 64	6. 97	0. 67	6. 96	0. 70
8	7. 97	0. 70	7. 97	0. 73	7. 96	0. 76	7. 96	0. 80
9	8. 97	0. 78	8. 96	0. 82	8. 96	0. 86	8. 95	0. 90
10	9. 96	0. 87	9. 96	0. 92	9. 95	0. 96	9. 95	1. 00
11	10. 96	0. 96	10. 95	1. 01	10. 95	1. 05	10. 94	1. 10
12	11. 95	1. 05	11. 95	1. 10	11. 94	1. 15	11. 94	1. 20
13	12. 95	1. 13	12. 95	1. 19	12. 94	1. 25	12. 93	1. 30
14	13. 95	1. 22	13. 94	1. 28	13. 94	1. 34	13. 93	1. 40
15	14. 94	1. 31	14. 94	1. 37	14. 93	1. 44	14. 92	1. 50
16	15. 94	1. 39	15. 93	1. 46	15. 93	1. 53	15. 92	1. 60
17	16. 94	1. 48	16. 93	1. 56	16. 92	1. 63	16. 91	1. 70
18	17. 93	1. 57	17. 92	1. 65	17. 92	1. 73	17. 91	1. 80
19	18. 93	1. 66	18. 92	1. 74	18. 91	1. 82	18. 90	1. 90
20	19. 92	1. 74	19. 92	1. 83	19. 91	1. 92	19. 90	2. 00
21	20. 92	1. 83	20. 91	1. 92	20. 90	2. 01	20. 89	2. 10
22	21. 92	1. 92	21. 91	2. 01	21. 90	2. 11	21. 89	2. 20
23	22. 91	2. 00	22. 90	2. 10	22. 89	2. 20	22. 88	2. 30
24	23. 91	2. 09	23. 90	2. 20	23. 89	2. 30	23. 88	2. 40
25	24. 90	2. 18	24. 90	2. 29	24. 88	2. 40	24. 87	2. 50
26	25. 90	2. 27	25. 89	2. 38	25. 88	2. 49	25. 87	2. 60
27	26. 90	2. 35	26. 89	2. 47	26. 88	2. 59	26. 86	2. 71
28	27. 89	2. 44	27. 88	2. 56	27. 87	2. 68	27. 86	2. 81
29	28. 89	2. 53	28. 88	2. 65	28. 87	2. 78	28. 85	2. 91
30	29. 89	2. 61	29. 87	2. 75	29. 86	2. 88	29. 85	3. 01
35	34. 87	3. 05	34. 85	3. 20	34. 84	3. 35	34. 82	3. 51
40	39. 85	3. 49	39. 83	3. 66	39. 82	3. 83	39. 80	4. 01
45	44. 83	3. 92	44. 81	4. 12	44. 79	4. 31	44. 77	4. 51
50	49. 81	4. 36	49. 79	4. 58	49. 77	4. 79	49. 75	5. 01
55	54. 79	4. 79	54. 77	5. 03	54. 75	5. 27	54. 72	5. 51
60	59. 77	5. 23	59. 75	5. 49	59. 72	5. 75	59. 70	6. 01
65	64. 75	5. 67	64. 73	5. 95	64. 70	6. 23	64. 67	6. 51
70	69. 73	6. 10	69. 71	6. 41	69. 68	6. 71	69. 65	7. 01
75	74. 71	6. 54	74. 69	6. 86	74. 65	7. 19	74. 62	7. 51
80	79. 70	6. 97	79. 66	7. 32	79. 63	7. 67	79. 60	8. 02
85	84. 68	7. 41	84. 64	7. 78	84. 61	8. 15	84. 57	8. 52
90	89. 66	7. 84	89. 62	8. 24	89. 59	8. 63	89. 55	9. 02
95	94. 64	8. 28	94. 60	8. 69	94. 56	9. 11	94. 52	9. 52
00	99. 62	8. 72	99. 58	9. 15	99. 54	9. 58	99. 50	10. 02
	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.
	85 Deg.		84¾ Deg.		84½ Deg.		84¼ Deg.	

Distance.	6 Deg.		6¼ Deg.		6½ Deg.		6¾ Deg.	
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.
1	0. 99	0. 10	0. 99	0. 11	0. 99	0. 11	0. 99	0. 12
2	1. 99	0. 21	1. 99	0. 22	1. 99	0. 23	1. 99	0. 24
3	2. 98	0. 31	2. 98	0. 33	2. 98	0. 34	2. 98	0. 35
4	3. 98	0. 41	3. 98	0. 44	3. 97	0. 45	3. 97	0. 47
5	4. 97	0. 52	4. 97	0. 54	4. 97	0. 57	4. 97	0. 59
6	5. 97	0. 63	5. 96	0. 65	5. 96	0. 68	5. 96	0. 71
7	6. 96	0. 73	6. 96	0. 76	6. 96	0. 79	6. 95	0. 82
8	7. 96	0. 84	7. 95	0. 87	7. 95	0. 91	7. 94	0. 94
9	8. 95	0. 94	8. 95	0. 98	8. 94	1. 02	8. 94	1. 06
10	9. 95	1. 05	9. 94	1. 09	9. 94	1. 13	9. 93	1. 18
11	10. 94	1. 15	10. 93	1. 20	10. 93	1. 25	10. 92	1. 29
12	11. 93	1. 25	11. 93	1. 31	11. 92	1. 36	11. 92	1. 41
13	12. 93	1. 36	12. 92	1. 42	12. 92	1. 47	12. 91	1. 53
14	13. 92	1. 46	13. 92	1. 52	13. 91	1. 59	13. 90	1. 65
15	14. 92	1. 57	14. 91	1. 63	14. 90	1. 70	14. 90	1. 76
16	15. 91	1. 67	15. 90	1. 74	15. 90	1. 81	15. 89	1. 83
17	16. 91	1. 78	16. 90	1. 85	16. 89	1. 92	16. 88	2. 00
18	17. 90	1. 88	17. 89	1. 96	17. 88	2. 04	17. 88	2. 12
19	18. 90	1. 99	18. 89	2. 07	18. 88	2. 15	18. 87	2. 23
20	19. 89	2. 09	19. 88	2. 18	19. 87	2. 26	19. 86	2. 35
21	20. 88	2. 20	20. 88	2. 29	20. 87	2. 38	20. 85	2. 47
22	21. 88	2. 30	21. 87	2. 40	21. 86	2. 49	21. 85	2. 59
23	22. 87	2. 40	22. 86	2. 50	22. 85	2. 60	22. 84	2. 70
24	23. 87	2. 51	23. 86	2. 61	23. 85	2. 72	23. 83	2. 82
25	24. 86	2. 61	24. 85	2. 72	24. 84	2. 83	24. 83	2. 94
26	25. 86	2. 72	25. 85	2. 83	25. 83	2. 94	25. 82	3. 03
27	26. 85	2. 82	26. 84	2. 94	26. 83	3. 06	26. 81	3. 17
28	27. 85	2. 93	27. 83	3. 05	27. 82	3. 17	27. 81	3. 29
29	28. 84	3. 03	28. 83	3. 16	28. 81	3. 28	28. 80	3. 41
30	29. 84	3. 14	29. 82	3. 27	29. 81	3. 40	29. 79	3. 53
35	34. 81	3. 66	34. 79	3. 81	34. 78	3. 96	34. 76	4. 11
40	39. 78	4. 18	39. 76	4. 35	39. 74	4. 53	39. 72	4. 70
45	44. 75	4. 70	44. 73	4. 90	44. 71	5. 09	44. 69	5. 29
50	49. 73	5. 23	49. 70	5. 44	49. 68	5. 66	49. 65	5. 83
55	54. 70	5. 75	54. 67	5. 99	54. 65	6. 23	54. 62	6. 46
60	59. 67	6. 27	59. 64	6. 53	59. 61	6. 79	59. 58	7. 05
65	64. 64	6. 79	64. 61	7. 08	64. 58	7. 36	64. 55	7. 64
70	69. 62	7. 32	69. 58	7. 62	69. 55	7. 92	69. 51	8. 23
75	74. 59	7. 84	74. 55	8. 17	74. 52	8. 49	74. 48	8. 82
80	79. 56	8. 36	79. 53	8. 71	79. 49	9. 06	79. 45	9. 40
85	84. 53	8. 83	84. 50	9. 25	84. 45	9. 62	84. 41	9. 99
90	89. 51	9. 41	89. 47	9. 80	89. 42	10. 19	89. 38	10. 58
95	94. 48	9. 93	94. 44	10. 34	94. 39	10. 75	94. 34	11. 17
100	99. 45	10. 45	99. 41	10. 89	99. 36	11. 32	99. 31	11. 75
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.
	84 Deg.		83¾ Deg.		83½ Deg.		83¼ Deg.	

Distance.	7 Deg.		7¼ Deg.		7½ Deg.		7¾ Deg.	
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.
1	0. 99	0. 12	0. 99	0. 13	0. 99	0. 13	0. 99	0. 13
2	1. 99	0. 24	1. 98	0. 25	1. 98	0. 26	1. 98	0. 27
3	2. 98	0. 37	2. 98	0. 38	2. 97	0. 39	2. 97	0. 40
4	3. 97	0. 49	3. 97	0. 50	3. 97	0. 52	3. 96	0. 54
5	4. 96	0. 61	4. 96	0. 63	4. 96	0. 65	4. 95	0. 67
6	5. 96	0. 73	5. 95	0. 76	5. 95	0. 78	5. 95	0. 81
7	6. 95	0. 85	6. 94	0. 88	6. 94	0. 91	6. 94	0. 94
8	7. 94	0. 97	7. 94	1. 01	7. 93	1. 04	7. 93	1. 08
9	8. 93	1. 10	8. 93	1. 14	8. 92	1. 17	8. 92	1. 21
10	9. 93	1. 22	9. 92	1. 26	9. 91	1. 31	9. 91	1. 35
11	10. 92	1. 34	10. 91	1. 39	10. 91	1. 44	10. 90	1. 48
12	11. 91	1. 46	11. 90	1. 51	11. 90	1. 57	11. 89	1. 62
13	12. 90	1. 58	12. 90	1. 64	12. 89	1. 70	12. 88	1. 75
14	13. 90	1. 71	13. 89	1. 77	13. 88	1. 83	13. 87	1. 89
15	14. 89	1. 83	14. 88	1. 89	14. 87	1. 96	14. 86	2. 02
16	15. 88	1. 95	15. 87	2. 02	15. 86	2. 09	15. 85	2. 16
17	16. 87	2. 07	16. 86	2. 15	16. 85	2. 22	16. 84	2. 29
18	17. 87	2. 19	17. 86	2. 27	17. 85	2. 35	17. 84	2. 43
19	18. 86	2. 32	18. 85	2. 40	18. 84	2. 48	18. 83	2. 56
20	19. 85	2. 44	19. 84	2. 52	19. 83	2. 61	19. 82	2. 70
21	20. 84	2. 56	20. 83	2. 65	20. 82	2. 74	20. 81	2. 83
22	21. 84	2. 68	21. 82	2. 78	21. 81	2. 87	21. 80	2. 97
23	22. 83	2. 80	22. 82	2. 90	22. 80	3. 00	22. 79	3. 10
24	23. 82	2. 92	23. 81	3. 03	23. 79	3. 13	23. 78	3. 24
25	24. 81	3. 05	24. 80	3. 15	24. 79	3. 26	24. 77	3. 37
26	25. 81	3. 17	25. 79	3. 28	25. 78	3. 39	25. 76	3. 51
27	26. 80	3. 29	26. 78	3. 41	26. 77	3. 52	26. 75	3. 64
28	27. 79	3. 41	27. 78	3. 53	27. 76	3. 65	27. 74	3. 78
29	28. 78	3. 53	28. 77	3. 66	28. 75	3. 79	28. 74	3. 91
30	29. 78	3. 66	29. 76	3. 79	29. 74	3. 92	29. 73	4. 05
35	34. 74	4. 27	34. 72	4. 42	34. 70	4. 57	34. 68	4. 72
40	39. 70	4. 87	39. 68	5. 05	39. 66	5. 22	39. 63	5. 39
45	44. 67	5. 48	44. 64	5. 68	44. 62	5. 87	44. 59	6. 07
50	49. 63	6. 09	49. 60	6. 31	49. 57	6. 53	49. 54	6. 74
55	54. 59	6. 70	54. 56	6. 94	54. 53	7. 18	54. 50	7. 42
60	59. 55	7. 31	59. 52	7. 57	59. 49	7. 83	59. 45	8. 09
65	64. 52	7. 92	64. 48	8. 20	64. 44	8. 48	64. 41	8. 77
70	69. 48	8. 53	69. 44	8. 83	69. 40	9. 14	69. 36	9. 44
75	74. 44	9. 14	74. 40	9. 46	74. 36	9. 79	74. 31	10. 11
80	79. 40	9. 75	79. 36	10. 10	79. 32	10. 44	79. 27	10. 79
85	84. 37	10. 36	84. 32	10. 73	84. 27	11. 09	84. 22	11. 46
90	89. 33	10. 97	89. 28	11. 36	89. 23	11. 75	89. 18	12. 14
95	94. 29	11. 58	94. 24	11. 99	94. 19	12. 40	94. 13	12. 81
00	99. 25	12. 19	99. 20	12. 62	99. 14	13. 05	99. 09	13. 49
	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.
	83 Deg.		82¾ Deg.		82½ Deg.		82¼ Deg.	

Distance.	8 Deg.		8¼ Deg.		8½ Deg.		8¾ Deg.	
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.
1	0. 99	0. 14	0. 99	0. 14	0. 99	0. 15	0. 99	0. 15
2	1. 98	0. 28	1. 98	0. 29	1. 98	0. 30	1. 98	0. 30
3	2. 97	0. 42	2. 97	0. 43	2. 97	0. 44	2. 97	0. 46
4	3. 96	0. 56	3. 96	0. 57	3. 96	0. 59	3. 95	0. 61
5	4. 95	0. 70	4. 95	0. 72	4. 95	0. 74	4. 94	0. 76
6	5. 94	0. 84	5. 94	0. 86	5. 93	0. 89	5. 93	0. 91
7	6. 93	0. 97	6. 93	1. 00	6. 92	1. 03	6. 92	1. 06
8	7. 92	1. 11	7. 92	1. 15	7. 91	1. 18	7. 91	1. 22
9	8. 91	1. 25	8. 91	1. 29	8. 90	1. 33	8. 90	1. 37
10	9. 90	1. 39	9. 90	1 43	9. 89	1. 43	9. 88	1. 52
11	10. 89	1. 53	10. 89	1. 58	10. 88	1. 63	10. 87	1. 67
12	11. 88	1. 67	11. 88	1. 72	11. 87	1. 77	11. 86	1. 83
13	12. 87	1. 81	12. 87	1. 87	12. 86	1. 92	12. 85	1. 98
14	13. 86	1. 95	13. 86	2. 01	13. 85	2. 07	13. 84	2. 13
15	14. 85	2. 09	14. 85	2. 15	14. 84	2. 22	14. 83	2. 28
16	15. 84	2. 23	15. 84	2. 30	15. 82	2. 36	15. 81	2. 43
17	16. 83	2. 37	16. 83	2. 44	16. 81	2. 51	16. 80	2. 59
18	17. 82	2. 51	17. 81	2. 58	17. 80	2. 66	17. 79	2. 74
19	18. 82	2. 64	18. 80	2. 73	18. 79	2. 81	18. 78	2. 89
20	19. 81	2. 78	19. 79	2. 87	19. 78	2. 96	19. 77	3. 04
21	20. 80	2. 92	20. 78	3. 01	20. 77	3. 10	20. 76	3. 19
22	21. 79	3. 06	21. 77	3. 16	21. 76	3. 25	21. 74	3. 35
23	22. 78	3. 20	22. 76	3. 30	22. 75	3. 40	22. 73	3. 50
24	23. 77	3. 34	23. 75	3. 44	23. 74	3. 55	23. 72	3. 65
25	24. 76	3. 48	24. 74	3. 59	24. 73	3. 70	24. 71	3. 80
26	25. 75	3. 62	25. 73	3. 73	25. 71	3. 84	25. 70	3. 96
27	26. 74	3. 76	26. 72	3. 87	26. 70	3. 99	26. 69	4. 11
28	27. 73	3. 90	27. 71	4. 02	27. 69	4. 14	27. 67	4. 26
29	28. 72	4. 04	28. 70	4. 16	28. 68	4. 29	28. 66	4. 41
30	29. 71	4. 18	29. 69	4. 30	29. 67	4. 43	29. 65	4. 56
35	34. 66	4. 87	34. 64	5. 02	34. 62	5. 17	34. 59	5. 32
40	39. 61	5. 57	39. 59	5. 74	39. 56	5. 91	39. 53	6. 08
45	44. 56	6. 26	44. 53	6. 46	44. 51	6. 65	44. 48	6. 85
50	49. 51	6. 96	49. 48	7. 17	49. 45	7. 39	49. 42	7. 61
55	54. 46	7. 65	54. 43	7. 89	54. 40	8. 13	54. 36	8. 37
60	59. 42	8. 35	59. 38	8. 61	59. 34	8. 87	59. 30	9. 13
65	64. 37	9. 05	64. 33	9. 33	64. 29	9. 61	64. 24	9. 89
70	69. 32	9. 74	69. 28	10. 04	69. 23	10. 35	69. 19	10. 65
75	74. 27	10. 44	74. 22	10. 76	74. 18	11. 09	74. 13	11. 41
80	79. 22	11. 13	79. 17	11. 48	79. 12	11. 82	79. 07	12. 17
85	84. 17	11. 83	84. 12	12. 20	84. 07	12. 56	84. 01	12. 93
90	89. 12	12. 53	89. 07	12. 91	89. 01	13. 30	88. 95	13. 69
95	94. 08	13. 22	94. 02	13. 63	93. 96	14. 04	93. 89	14. 45
100	99. 03	13. 92	98. 97	14. 35	98. 90	14. 78	98. 84	15. 21
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.
	82 Deg.		81¾ Deg.		81½ Deg.		81¼ Deg.	

Distance.	9 Deg.		9¼ Deg.		9½ Deg.		9¾ Deg.	
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.
1	0.99	0.16	0.99	0.16	0.99	0.17	0.99	0.17
2	1.98	0.31	1.97	0.32	1.97	0.33	1.97	0.34
3	2.96	0.47	2.96	0.48	2.96	0.50	2.96	0.51
4	3.95	0.63	3.95	0.64	3.95	0.66	3.94	0.68
5	4.94	0.78	4.93	0.80	4.93	0.83	4.93	0.85
6	5.93	0.94	5.92	0.96	5.92	0.99	5.91	1.02
7	6.91	1.10	6.91	1.13	6.90	1.16	6.90	1.19
8	7.90	1.25	7.90	1.29	7.89	1.32	7.88	1.35
9	8.89	1.41	8.88	1.45	8.88	1.49	8.87	1.52
10	9.88	1.56	9.87	1.61	9.86	1.65	9.86	1.69
11	10.86	1.72	10.86	1.77	10.85	1.82	10.84	1.86
12	11.85	1.88	11.84	1.93	11.84	1.98	11.83	2.03
13	12.84	2.03	12.83	2.09	12.82	2.15	12.81	2.20
14	13.83	2.19	13.82	2.25	13.81	2.31	13.80	2.37
15	14.82	2.35	14.80	2.41	14.79	2.48	14.78	2.54
16	15.80	2.50	15.79	2.57	15.78	2.64	15.77	2.71
17	16.79	2.66	16.78	2.73	16.77	2.81	16.75	2.88
18	17.78	2.82	17.77	2.89	17.75	2.97	17.74	3.05
19	18.77	2.97	18.75	3.05	18.74	3.14	18.73	3.22
20	19.75	3.13	19.74	3.21	19.73	3.30	19.71	3.39
21	20.74	3.29	20.73	3.38	20.71	3.47	20.70	3.56
22	21.73	3.44	21.71	3.54	21.70	3.63	21.68	3.73
23	22.72	3.60	22.70	3.70	22.68	3.80	22.67	3.90
24	23.70	3.75	23.69	3.86	23.67	3.96	23.65	4.06
25	24.69	3.91	24.67	4.02	24.66	4.13	24.64	4.23
26	25.68	4.07	25.66	4.18	25.64	4.29	25.62	4.40
27	26.67	4.22	26.65	4.34	26.63	4.46	26.61	4.57
28	27.66	4.38	27.64	4.50	27.62	4.62	27.60	4.74
29	28.64	4.54	28.62	4.66	28.60	4.79	28.58	4.91
30	29.63	4.69	29.61	4.82	29.59	4.95	29.57	5.08
35	34.57	5.48	34.54	5.63	34.52	5.78	34.49	5.93
40	39.51	6.26	39.48	6.43	39.45	6.60	39.42	6.77
45	44.45	7.04	44.41	7.23	44.38	7.43	44.35	7.62
50	49.33	7.82	49.35	8.04	49.32	8.25	49.28	8.47
55	54.32	8.60	54.28	8.84	54.25	9.08	54.21	9.31
60	59.26	9.39	59.22	9.64	59.18	9.90	59.13	10.16
65	64.20	10.17	64.15	10.45	64.11	10.73	64.06	11.01
70	69.14	10.95	69.09	11.25	69.04	11.55	68.99	11.85
75	74.08	11.73	74.02	12.06	73.97	12.38	73.92	12.70
80	79.02	12.51	78.96	12.86	78.90	13.20	78.84	13.55
85	83.95	13.30	83.89	13.66	83.83	14.03	83.77	14.39
90	88.89	14.08	88.83	14.47	88.77	14.85	88.70	15.24
95	93.83	14.86	93.76	15.27	93.70	15.68	93.63	16.09
00	98.77	15.64	98.70	16.07	98.63	16.50	98.56	16.93
ance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.
	81 Deg.		80¾ Deg.		80½ Deg.		80¼ Deg.	

TRAVERSE TABLE.

Distance.	10 Deg.		10¼ Deg.		10½ Deg.		10¾ Deg.	
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.
1	0. 98	0. 17	0. 98	0. 13	0. 93	0. 18	0. 98	0. 19
2	1. 97	0. 35	1. 97	0. 36	1. 97	0. 36	1. 96	0. 37
3	2. 95	0. 52	2. 95	0. 53	2. 95	0. 55	2. 95	0. 56
4	3. 94	0. 69	3. 94	0. 71	3. 93	0. 73	3. 93	0. 75
5	4. 92	0. 87	4. 92	0. 89	4. 92	0. 91	4. 91	0. 93
6	5. 91	1. 04	5. 90	1. 07	5. 90	1. 09	5. 89	1. 12
7	~~6. 89~~	~~1. 22~~	6. 89	1. 25	6. 88	1. 28	6. 88	1. 31
8	7. 88	1. 39	7. 87	1. 42	7. 87	1. 46	7. 86	1. 49
9	8. 86	1. 56	8. 86	1. 60	8. 85	1. 64	8. 84	1. 68
10	9. 85	1. 74	9. 84	1. 78	9. 83	1. 82	9. 82	1. 87
11	10. 83	1. 91	10. 82	1. 96	10. 82	2. 00	10. 81	2. 05
12	11. 82	2. 08	11. 81	2. 14	11. 80	2. 19	11. 79	2. 24
13	12. 80	2. 26	12. 79	2. 31	12. 78	2. 37	12. 77	2. 42
14	13. 79	2. 43	13. 78	2. 49	13. 77	2. 55	13. 75	2. 61
15	14. 77	2. 60	14. 76	2. 67	14. 75	2. 73	14. 74	2. 80
16	15. 76	2. 78	15. 74	2. 85	15. 73	2. 92	15. 72	2. 98
17	16. 74	2. 95	16. 73	3. 03	16. 72	3. 10	16. 70	3. 17
18	17. 73	3. 13	17. 71	3. 20	17. 70	3. 28	17. 68	3. 36
19	18. 71	3. 30	18. 70	3. 38	18. 68	3. 46	18. 67	3. 54
20	19. 70	3. 47	19. 68	3. 56	19. 67	3. 64	19. 65	3. 73
21	20. 68	3. 65	~~20. 66~~	~~3. 74~~	20. 65	3. 83	20. 63	3. 92
22	21. 67	3. 82	21. 65	3. 91	21. 63	4. 01	21. 61	4. 10
23	22. 65	3. 99	22. 63	4. 09	22. 61	4. 19	22. 60	4. 29
24	23. 64	4. 17	23. 62	4. 27	23. 60	4. 37	23. 58	4. 48
25	24. 62	4. 34	24. 60	4. 45	24. 58	4. 56	24. 56	4. 66
26	25. 61	4. 51	25. 59	4. 63	25. 56	4. 74	25. 54	4. 85
27	26. 59	4. 69	26. 57	4. 80	26. 55	4. 92	26. 53	5. 04
28	27. 57	4. 86	27. 55	4. 98	27. 53	5. 10	27. 51	5. 22
29	28. 56	5. 04	28. 54	5. 16	28. 51	5. 28	28. 49	5. 41
30	29. 54	5. 21	29. 52	5. 34	29. 50	5. 47	29. 47	5. 60
35	34. 47	6. 08	34. 44	6. 23	34. 41	6. 38	34. 39	6. 53
40	39. 39	6. 95	39. 36	7. 12	39. 33	7. 29	39. 30	7. 46
45	44. 32	7. 81	44. 28	8. 01	44. 25	8. 20	44. 21	8. 39
50	49. 24	8. 68	49. 20	8. 90	49. 16	9. 11	49. 12	9. 33
55	54. 16	9. 55	54. 12	9. 79	54. 08	10. 02	54. 03	10. 26
60	59. 09	10. 42	59. 04	10. 68	59. 00	10. 93	58. 95	11. 19
65	64. 01	11. 29	63. 96	11. 57	63. 91	11. 85	63. 86	12. 12
70	68. 94	12. 16	68. 88	12. 46	68. 83	12. 76	68. 77	13. 06
75	73. 86	13. 02	73. 80	13. 35	73. 74	13. 67	73. 68	13. 99
80	78. 78	13. 89	78. 72	14. 24	78. 66	14. 58	78. 60	14. 92
85	83. 71	14. 76	83. 64	15. 13	83. 58	15. 49	83. 51	15. 85
90	88. 63	15. 63	88. 56	16. 01	88. 49	16. 40	88. 42	16. 79
95	93. 56	16. 50	93. 48	16. 90	93. 41	17. 31	93. 33	17. 72
100	98. 48	17. 36	98. 40	17. 79	98. 33	18. 22	98. 25	18. 65
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.
	80 Deg.		79¾ Deg.		79½ Deg.		79¼ Deg.	

Distance.	11 Deg.		11¼ Deg.		11½ Deg.		11¾ Deg.	
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.
1	0. 98	0. 19	0. 98	0. 20	0. 98	0. 20	0. 98	0. 20
2	1. 96	0. 38	1. 96	0. 39	1. 96	0. 40	1. 96	0. 41
3	2. 94	0. 57	2. 94	0. 59	2. 94	0. 60	2. 94	0. 61
4	3. 93	0. 76	3. 92	0. 78	3. 92	0. 80	3. 92	0. 82
5	4. 91	0. 95	4. 90	0. 98	4. 90	1. 00	4. 90	1. 02
6	5. 89	1. 14	5. 88	1. 17	5. 88	1. 20	5. 87	1. 22
7	6. 87	1. 34	6. 87	1. 37	6. 86	1. 40	6. 85	1. 43
8	7. 85	1. 53	7. 85	1. 56	7. 84	1. 59	7. 83	1. 63
9	8. 83	1. 72	8. 83	1. 76	8. 82	1. 79	8. 81	1. 83
10	9. 82	1. 91	9. 81	1. 95	9. 80	1. 99	9. 79	2. 04
11	10. 80	2. 10	10. 79	2. 15	10. 78	2. 19	10 77	2. 24
12	11. 78	2. 29	11. 77	2. 34	11. 76	2. 39	11 75	2. 44
13	12. 76	2. 48	12. 75	2. 54	12. 74	2. 59	12. 73	2. 65
14	13. 74	2. 67	13. 73	2. 73	13. 72	2. 79	13. 71	2. 85
15	14. 72	2. 86	14. 71	2. 93	14. 70	2. 99	14. 69	3. 06
16	15. 71	3. 05	15. 69	3. 12	15. 68	3. 19	15. 66	3. 26
17	16. 69	3. 24	16. 67	3. 32	16. 66	3. 39	16. 64	3. 46
18	17. 67	3. 43	17. 65	3. 51	17. 64	3. 59	17. 62	3. 66
19	18. 65	3. 63	18. 63	3. 71	18. 62	3. 79	18. 60	3. 87
20	19 63	3. 82	19. 62	3. 90	19. 60	3. 99	19. 58	4. 07
21	20. 61	4. 01	20. 60	4. 10	20. 58	4. 19	20. 56	4. 28
22	21. 60	4. 20	21. 58	4. 29	21. 56	4. 39	21. 54	4. 48
23	22. 58	4. 39	22. 56	4. 49	22. 54	4. 59	22. 52	4. 68
24	23. 56	4. 58	23. 54	4. 68	23. 52	4. 78	23. 50	4. 89
25	24. 54	4. 77	24. 52	4. 83	24. 50	4. 98	24. 48	5. 09
26	25. 52	4. 96	25. 50	5. 07	25. 48	5. 18	25. 46	5. 30
27	26. 50	5. 15	26. 48	5. 27	26. 46	5. 38	26. 43	5. 50
28	27. 49	5. 34	27. 46	5. 46	27. 44	5. 58	27. 41	5. 70
29	28. 47	5. 53	28. 44	5. 66	28. 42	5. 78	28. 39	5. 91
30	29. 45	5. 72	29. 42	5. 85	29. 40	5. 98	29. 37	6. 11
35	34. 36	6. 68	34. 33	6. 83	34. 30	6. 98	34. 27	7. 13
40	39. 27	7. 63	39. 23	7. 80	39. 20	7. 97	39. 16	8. 15
45	44. 17	8. 59	44. 14	8. 78	44. 10	8. 97	44. 06	9. 16
50	49. 03	9. 54	49. 04	9. 75	49. 00	9. 97	48. 95	10. 18
55	53. 99	10. 49	53. 94	10. 73	52. 90	10. 97	53. 85	11. 20
60	58. 90	11. 45	58. 85	11. 71	58. 80	11. 96	58. 74	12. 22
65	63. 81	12. 40	63. 75	12. 63	63. 70	12. 96	63. 64	13. 24
70	68. 71	13. 36	68. 66	13. 66	68. 59	13. 96	68. 53	14. 25
75	73. 62	14. 31	73. 56	14. 63	73. 49	14. 95	73. 43	15. 27
80	78. 53	15. 26	78. 46	15. 61	78. 39	15. 95	78. 32	16. 29
85	83. 44	16. 22	83. 37	16. 53	83. 29	16. 95	83. 22	17. 31
90	88. 35	17. 17	88. 27	17. 56	88. 19	17. 94	88. 11	18. 33
95	93. 25	18. 13	93. 17	18. 53	93. 09	18. 94	93. 01	19. 35
100	98. 16	19. 08	98. 08	19. 51	97. 99	19. 94	97. 90	20. 36
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.
	79 Deg.		78¾ Deg.		78½ Deg.		78¼ Deg.	

Distance.	12 Deg.		12¼ Deg.		12½ Deg.		12¾ Deg.	
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.
1	0. 98	0. 21	0. 98	0. 21	0. 98	0. 22	0. 98	0. 22
2	1. 96	0. 42	1. 95	0. 42	1. 95	0. 43	1. 95	0. 44
3	2. 93	0. 62	2. 93	0. 64	2. 93	0. 65	2. 93	0. 66
4	3. 91	0. 83	3. 91	0. 85	3. 91	0. 87	3. 90	0. 88
5	4. 89	1. 04	4. 89	1. 06	4. 88	1. 08	4. 88	1. 10
6	5. 87	1. 25	5. 86	1. 27	5. 86	1. 30	5. 85	1. 32
7	6. 85	1. 46	6. 84	1. 49	6. 83	1. 52	6. 83	1. 54
8	7. 83	1. 66	7. 82	1. 70	7. 81	1. 73	7. 80	1. 77
9	8. 80	1. 87	8. 80	1. 91	8. 79	1. 95	8. 78	1. 99
10	9. 78	2. 08	9. 77	2. 12	9. 76	2. 16	9. 75	2. 21
11	10. 76	2. 29	10. 75	2. 33	10. 74	2. 38	10. 73	2. 43
12	11. 74	2. 49	11. 73	2. 55	11. 72	2. 60	11. 70	2. 65
13	12. 72	2. 70	12. 70	2. 76	12. 69	2. 81	12. 68	2. 87
14	13. 69	2. 91	13. 68	2. 97	13. 67	3. 03	13. 65	3. 09
15	14. 67	3. 12	14. 66	3. 18	14. 64	3. 25	14. 63	3. 31
16	15. 65	3. 33	15. 64	3. 39	15. 62	3. 46	15. 61	3. 53
17	16. 63	3. 53	16. 61	3. 61	16. 60	3. 68	16. 58	3. 75
18	17. 61	3. 74	17. 59	3. 82	17. 57	3. 90	17. 56	3. 97
19	18. 58	3. 95	18. 57	4. 03	18. 55	4. 11	18. 53	4. 19
20	19. 56	4. 16	19. 54	4. 24	19. 53	4. 33	19. 51	4. 41
21	20. 54	4. 37	20. 52	4. 46	20. 50	4. 55	20. 48	4. 63
22	21. 52	4. 57	21. 50	4. 67	21. 48	4. 76	21. 46	4. 86
23	22. 50	4. 78	22. 48	4. 88	22. 45	4. 98	22. 43	5. 08
24	23. 48	4. 99	23. 45	5. 09	23. 43	5. 19	23. 41	5. 30
25	24. 45	5. 20	24. 43	5. 30	24. 41	5. 41	24. 38	5. 52
26	25. 43	5. 41	25. 41	5. 52	25. 38	5. 63	25. 36	5. 74
27	26. 41	5. 61	26. 39	5. 73	26. 36	5. 84	26. 33	5. 96
28	27. 39	5. 82	27. 36	5. 94	27. 34	6. 06	27. 31	6. 18
29	28. 37	6. 03	28. 34	6. 15	28. 31	6. 28	28. 28	6. 40
30	29. 34	6. 24	29. 32	6. 37	29. 29	6. 49	29. 26	6. 62
35	34. 24	7. 28	34. 20	7. 43	34. 17	7. 58	34. 14	7. 72
40	39. 13	8. 32	39. 09	8. 49	39. 05	8. 66	39. 01	8. 83
45	44. 02	9. 36	43. 98	9. 55	43. 93	9. 74	43. 89	9. 93
50	48. 91	10. 40	48. 86	10. 61	48. 81	10. 82	48. 77	11. 03
55	53. 80	11. 44	53. 75	11. 67	53. 70	11. 90	53. 64	12. 14
60	58. 69	12. 47	58. 63	12. 73	58. 58	12. 99	58. 52	13. 24
65	63. 58	13. 51	63. 52	13. 79	63. 46	14. 07	63. 40	14. 35
70	68. 47	14. 55	68. 41	14. 85	68. 34	15. 15	68. 27	15. 45
75	73. 36	15. 59	73. 29	15. 91	73. 22	16. 23	73. 15	16. 55
80	78. 25	16. 63	78. 18	16. 97	78. 10	17. 32	78. 03	17. 66
85	83. 14	17. 67	83. 06	18. 04	82. 99	18. 40	82. 90	18. 76
90	88. 03	18. 71	87. 95	19. 10	87. 87	19. 48	87. 78	19. 86
95	92. 92	19. 75	92. 84	20. 16	92. 75	20. 56	92. 66	20. 97
100	97. 81	20. 79	97. 72	21. 22	97. 63	21. 64	97. 53	22. 07
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.
	78 Deg.		77¾ Deg.		77½ Deg.		77¼ Deg.	

Distance.	13 Deg.		13¼ Deg.		13½ Deg.		13¾ Deg.	
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.
1	0.97	0.23	0.97	0.23	0.97	0.23	0.97	0.24
2	1.95	0.45	1.95	0.46	1.95	0.47	1.94	0.48
3	2.92	0.67	2.92	0.69	2.92	0.70	2.91	0.71
4	3.90	0.90	3.89	0.92	3.89	0.93	3.89	0.95
5	4.87	1.12	4.87	1.15	4.86	1.17	4.86	1.19
6	5.85	1.35	5.84	1.38	5.83	1.40	5.83	1.43
7	6.82	1.57	6.81	1.60	6.81	1.63	6.80	1.66
8	7.80	1.80	7.79	1.83	7.78	1.87	7.77	1.90
9	8.77	2.02	8.76	2.06	8.75	2.10	8.74	2.14
10	9.74	2.25	9.73	2.29	9.72	2.33	9.71	2.38
11	10.72	2.47	10.71	2.52	10.70	2.57	10.68	2.61
12	11.69	2.70	11.68	2.75	11.67	2.80	11.66	2.85
13	12.67	2.92	12.65	2.98	12.64	3.03	12.63	3.09
14	13.64	3.15	13.63	3.21	13.61	3.27	13.60	3.33
15	14.62	3.37	14.60	3.44	14.59	3.50	14.57	3.57
16	15.59	3.60	15.57	3.67	15.56	3.74	15.54	3.80
17	16.57	3.82	16.55	3.90	16.53	3.97	16.51	4.04
18	17.54	4.05	17.52	4.13	17.50	4.20	17.48	4.28
19	18.51	4.27	18.49	4.35	18.48	4.44	18.46	4.52
20	19.49	4.50	19.47	4.58	19.45	4.67	19.43	4.75
21	20.46	4.72	20.44	4.81	20.42	4.90	20.40	4.99
22	21.44	4.95	21.41	5.04	21.39	5.14	21.37	5.23
23	22.41	5.17	22.39	5.27	22.36	5.37	22.34	5.47
24	23.38	5.40	23.36	5.50	23.34	5.60	23.31	5.70
25	24.36	5.62	24.33	5.73	24.31	5.84	24.28	5.94
26	25.33	5.85	25.31	5.96	25.28	6.07	25.25	6.18
27	26.31	6.07	26.28	6.19	26.25	6.30	26.23	6.42
28	27.28	6.30	27.25	6.42	27.23	6.54	27.20	6.66
29	28.26	6.52	28.23	6.65	28.20	6.77	28.17	6.89
30	29.23	6.75	29.20	6.88	29.17	7.00	29.14	7.13
35	34.10	7.87	34.07	8.02	34.03	8.17	34.00	8.32
40	38.97	9.00	38.94	9.17	38.89	9.34	38.85	9.51
45	43.85	10.12	43.80	10.31	43.76	10.51	43.71	10.70
50	48.72	11.25	48.67	11.46	48.62	11.67	48.57	11.88
55	53.59	12.37	53.54	12.61	53.48	12.84	53.42	13.07
60	58.46	13.50	58.40	13.75	58.34	14.01	58.28	14.26
65	63.33	14.62	63.27	14.90	63.20	15.17	63.14	15.45
70	68.21	15.75	68.14	16.04	68.07	16.34	67.99	16.64
75	73.08	16.87	73.00	17.19	72.93	17.50	72.85	17.83
80	77.95	18.00	77.87	18.34	77.79	18.68	77.71	19.01
85	82.82	19.12	82.74	19.48	82.65	19.84	82.56	20.20
90	87.69	20.25	87.60	20.63	87.51	21.01	87.42	21.39
95	92.57	21.37	92.47	21.77	92.38	22.18	92.28	22.58
100	97.44	22.50	97.34	22.92	97.24	23.34	97.13	23.77
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.
	77 Deg.		76¾ Deg.		76½ Deg.		76¼ Deg.	

Distance.	14 Deg.		14¼ Deg.		14½ Deg.		14¾ Deg.	
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.
1	0. 97	0. 24	0. 97	0. 25	0. 97	0. 25	0. 97	0. 25
2	1. 94	0. 48	1. 94	0. 49	1. 94	0. 50	1. 93	0. 51
3	2. 91	0. 73	2. 91	0. 74	2. 90	0. 75	2. 90	0. 76
4	3. 88	0. 97	3. 88	0. 98	3. 87	1. 00	3. 87	1. 02
5	4. 85	1. 21	4. 85	1. 23	4. 84	1. 25	4. 84	1. 27
6	5. 82	1. 45	5. 82	1. 48	5. 81	1. 50	5. 80	1. 53
7	6. 79	1. 69	6. 78	1. 72	6. 78	1. 75	6. 77	1. 78
8	7. 76	1. 94	7. 75	1. 97	7. 75	2. 00	7. 74	2. 04
9	8. 73	2. 18	8. 72	2. 22	8. 71	2. 25	8. 70	2. 29
10	9. 70	2. 42	9. 69	2. 46	9. 68	2. 50	9. 67	2. 55
11	10. 67	2. 66	10. 66	2. 71	10. 65	2. 75	10. 64	2. 80
12	11. 64	2. 90	11. 63	2. 95	11. 62	3. 00	11. 60	3. 06
13	12. 61	3. 15	12. 60	3. 20	12. 59	3. 25	12. 57	3. 31
14	13. 58	3. 39	13. 57	3. 45	13. 55	3. 51	13. 54	3. 56
15	14. 55	3. 63	14. 54	3. 69	14. 52	3. 76	14. 51	3. 82
16	15. 52	3. 87	15. 51	3. 94	15. 49	4. 01	15. 47	4. 07
17	16. 50	4. 11	16. 48	4. 18	16. 46	4. 26	16. 44	4. 33
18	17. 47	4. 35	17. 45	4. 43	17. 43	4. 51	17. 41	4. 58
19	18. 44	4. 60	18. 42	4. 68	18. 39	4. 76	18. 37	4. 84
20	19. 41	4. 84	19. 38	4. 92	19. 36	5. 01	19. 34	5. 09
21	20. 38	5. 08	20. 35	5. 17	20. 33	5. 26	20. 31	5. 35
22	21. 35	5. 32	21. 32	5. 42	21. 30	5. 51	21. 28	5. 60
23	22. 32	5. 56	22. 29	5. 66	22. 27	5. 76	22. 24	5. 86
24	23. 29	5. 81	23. 26	5. 91	23. 24	6. 01	23. 21	6. 11
25	24. 26	6. 05	24. 23	6. 15	24. 20	6. 26	24. 18	6. 37
26	25. 23	6. 29	25. 20	6. 40	25. 17	6. 51	25. 14	6. 62
27	26. 20	6. 53	26. 17	6. 65	26. 14	6. 76	26. 11	6. 87
28	27. 17	6. 77	27. 14	6. 89	27. 11	7. 01	27. 08	7. 13
29	28. 14	7. 02	28. 11	7. 14	28. 08	7. 26	28. 04	7. 38
30	29. 11	7. 26	29. 08	7. 38	29. 04	7. 51	29. 01	7. 64
35	33. 96	8. 47	33. 92	8. 62	33. 89	8. 76	33. 85	8. 91
40	38. 81	9. 68	38. 77	9. 85	38. 73	10. 02	38. 68	10. 18
45	43. 66	10. 89	43. 62	11. 08	43. 57	11. 27	43. 52	11. 46
50	48. 51	12. 10	48. 46	12. 31	48. 41	12. 52	48. 35	12. 73
55	53. 37	13. 31	53. 31	13. 54	53. 25	13. 77	53. 19	14. 00
60	58. 22	14. 52	58. 15	14. 77	58. 09	15. 02	58. 02	15. 28
65	63. 07	15. 72	63. 00	16. 00	62. 93	16. 27	62. 86	16. 55
70	67. 92	16. 93	67. 85	17. 23	67. 77	17. 53	67. 69	17. 82
75	72. 77	18. 14	72. 69	18. 46	72. 61	18. 78	72. 53	19. 10
80	77. 62	19. 35	77. 54	19. 69	77. 45	20. 03	77. 36	20. 37
85	82. 48	20. 56	82. 38	20. 92	82. 29	21. 28	82. 20	21. 64
90	87. 33	21. 77	87. 23	22. 15	87. 13	22. 53	87. 03	22. 91
95	92. 18	22. 98	92. 08	23. 38	91. 97	23. 79	91. 87	24. 19
100	97. 03	24. 19	96. 92	24. 62	96. 81	25. 04	96. 70	25. 46
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.
	76 Deg.		75¾ Deg.		75½ Deg.		75¼ Deg.	

Distance.	15 Deg.		15¼ Deg.		15½ Deg.		15¾ Deg.	
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.
1	0. 97	0. 26	0. 96	0. 26	0. 96	0. 27	0. 96	0. 27
2	1. 93	0. 52	1. 93	0. 53	1. 93	0. 53	1. 92	0. 54
3	2. 90	0. 78	2. 89	0. 79	2. 89	0. 80	2. 89	0. 81
4	3. 86	1. 04	3. 86	1. 05	3. 85	1. 07	3. 85	1. 09
5	4. 83	1. 29	4. 82	1. 32	4. 82	1. 34	4. 81	1. 36
6	5. 80	1. 55	5. 79	1. 58	5. 78	1. 60	5. 77	1. 63
7	6. 76	1. 81	6. 75	1. 84	6. 75	1. 87	6. 74	1. 90
8	7. 73	2. 07	7. 72	2. 10	7. 71	2. 14	7. 70	2. 17
9	8. 69	2. 33	8. 68	2. 37	8. 67	2. 41	8. 66	2. 44
10	9. 66	2. 59	9. 65	2. 63	9. 64	2. 67	9. 62	2. 71
11	10. 63	2. 85	10. 61	2. 89	10. 60	2. 94	10. 59	2. 99
12	11. 59	3. 11	11. 58	3. 16	11. 56	3. 21	11. 55	3. 26
13	12. 56	3. 36	12. 54	3. 42	12. 53	3. 47	12. 51	3. 53
14	13. 52	3. 62	13. 51	3. 68	13. 49	3. 74	13. 47	3. 80
15	14. 49	3. 88	14. 47	3. 95	14. 45	4. 01	14. 44	4. 07
16	15. 45	4. 14	15. 44	4. 21	15. 42	4. 28	15. 40	4. 34
17	16. 42	4. 40	16. 40	4. 47	16. 38	4. 54	16. 36	4. 61
18	17. 39	4. 66	17. 37	4. 73	17. 35	4. 81	17. 32	4. 89
19	18. 35	4. 92	18. 33	5. 00	18. 31	5. 08	18. 29	5. 16
20	19. 32	5. 18	19. 30	5. 26	19. 27	5. 34	19. 25	5. 43
21	20. 28	5. 44	20. 26	5. 52	20. 24	5. 61	20. 21	5. 70
22	21. 25	5. 69	21. 23	5. 79	21. 20	5. 88	21. 17	5. 97
23	22. 22	5. 95	22. 19	6. 05	22. 16	6. 15	22. 14	6. 24
24	23. 18	6. 21	23. 15	6. 31	23. 13	6. 41	23. 10	6. 51
25	24. 15	6. 47	24. 12	6. 58	24. 09	6. 68	24. 06	6. 79
26	25. 11	6. 73	25. 08	6. 84	25. 05	6. 95	25. 02	7. 06
27	26. 08	6. 99	26. 05	7. 10	26. 02	7. 22	25. 99	7. 33
28	27. 05	7. 25	27. 01	7. 36	26. 98	7. 48	26. 95	7. 60
29	28. 01	7. 51	27. 98	7. 63	27. 95	7. 75	27. 91	7. 87
30	28. 98	7. 76	28. 94	7. 89	28. 91	8. 02	28. 87	8. 14
35	33. 81	9. 06	33. 77	9. 21	33. 73	9. 35	33. 69	9. 50
40	38. 64	10. 35	38. 59	10. 52	38. 55	10. 69	38. 50	10. 86
45	43. 47	11. 65	43. 42	11. 84	43. 36	12. 03	43. 31	12. 21
50	48. 30	12. 94	48. 24	13. 15	48. 18	13. 36	48. 12	13. 57
55	53. 13	14. 24	53. 06	14. 47	53. 00	14. 70	52. 94	14. 93
60	57. 96	15. 53	57. 89	15. 78	57. 82	16. 03	57. 75	16. 29
65	62. 79	16. 82	62. 71	17. 10	62. 64	17. 37	62. 56	17. 64
70	67. 61	18. 12	67. 54	18. 41	67. 45	18. 71	67. 37	19. 00
75	72. 44	19. 41	72. 36	19. 73	72. 27	20. 04	72. 18	20. 36
80	77. 27	20. 71	77. 18	21. 04	77. 09	21. 38	77. 00	21. 72
85	82. 10	22. 00	82. 01	22. 36	81. 91	22. 72	81. 81	23. 07
90	86. 93	23. 29	86. 83	23. 67	86. 73	24. 05	86. 62	24. 43
95	91. 76	24. 59	91. 65	24. 99	91. 54	25. 39	91. 43	25. 79
100	96. 59	25. 88	96. 48	26. 30	96. 36	26. 72	96. 25	27. 14
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.
	75 Deg.		74¾ Deg.		74½ Deg.		74¼ Deg.	

Distance.	16 Deg.		16¼ Deg.		16½ Deg.		16¾ Deg.	
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.
1	0. 96	0. 28	0. 96	0. 28	0. 96	0. 28	0. 96	0. 29
2	1. 92	0. 55	1. 92	0. 56	1. 92	0. 57	1. 92	0. 58
3	2. 88	0. 83	2. 88	0. 84	2. 88	0. 85	2. 87	0. 86
4	3. 85	1. 10	3. 84	1. 12	3. 84	1. 14	3. 83	1. 15
5	4. 81	1. 38	4. 80	1. 40	4. 79	1. 42	4. 79	1. 44
6	5. 77	1. 65	5. 76	1. 68	5. 75	1. 70	5. 75	1. 73
7	6. 73	1. 93	6. 72	1. 96	6. 71	1. 99	6. 70	2. 02
8	7. 69	2. 21	7. 68	2. 24	7. 67	2. 27	7. 66	2. 31
9	8. 65	2. 48	8. 64	2. 52	8. 63	2. 56	8. 62	2. 59
10	9. 61	2. 76	9. 60	2. 80	9. 59	2. 84	9. 58	2. 88
11	10. 57	3. 03	10. 56	3. 08	10. 55	3. 12	10. 53	3. 17
12	11. 54	3. 31	11. 52	3. 36	11. 51	3. 41	11. 49	3. 46
13	12. 50	3. 58	12. 48	3. 64	12. 46	3. 69	12. 45	3. 75
14	13. 46	3. 86	13. 44	3. 92	13. 42	3. 98	13. 41	4. 03
15	14. 42	4. 13	14. 40	4. 20	14. 38	4. 26	14. 36	4. 32
16	15. 38	4. 41	15. 36	4. 48	15. 34	4. 54	15. 32	4. 61
17	16. 34	4. 69	16. 32	4. 76	16. 30	4. 83	16. 28	4. 90
18	17. 30	4. 96	17. 28	5. 04	17. 26	5. 11	17. 24	5. 19
19	18. 26	5. 24	18. 24	5. 32	18. 22	5. 40	18. 19	5. 48
20	19. 23	5. 51	19. 20	5. 60	19. 18	5. 68	19. 15	5. 76
21	20. 19	5. 79	20. 16	5. 88	20. 14	5. 96	20. 11	6. 05
22	21. 15	6. 06	21. 12	6. 16	21. 09	6. 25	21. 07	6. 34
23	22. 11	6. 34	22. 08	6. 44	22. 05	6. 53	22. 02	6. 63
24	23. 07	6. 62	23. 04	6. 72	23. 01	6. 82	22. 98	6. 92
25	24. 03	6. 89	24. 00	7. 00	23. 97	7. 10	23. 94	7. 20
26	24. 99	7. 17	24. 96	7. 28	24. 93	7. 38	24. 90	7. 49
27	25. 95	7. 44	25. 92	7. 56	25. 89	7. 67	25. 85	7. 78
28	26. 92	7. 72	26. 88	7. 84	26. 85	7. 95	26. 81	8. 07
29	27. 88	7. 99	27. 84	8. 11	27. 81	8. 24	27. 77	8. 36
30	28. 84	8. 27	28. 80	8. 39	28. 76	8. 52	28. 73	8. 65
35	33. 64	9. 65	33. 60	9. 79	33. 56	9. 94	33. 51	10. 09
40	38. 45	11. 03	38. 40	11. 19	38. 35	11. 36	38. 30	11. 53
45	43. 26	12. 40	43. 20	12. 59	43. 15	12. 78	43. 09	12. 97
50	48. 06	13. 78	48. 00	13. 99	47. 94	14. 20	47. 88	14. 41
55	52. 87	15. 16	52. 80	15. 39	52. 74	15. 62	52. 67	15. 85
60	57. 68	16. 54	57. 60	16. 79	57. 53	17. 04	57. 45	17. 29
65	62. 48	17. 92	62. 40	18. 19	62. 32	18. 46	62. 24	18. 73
70	67. 29	19. 29	67. 20	19. 59	67. 12	19. 88	67. 03	20. 17
75	72. 09	20. 67	72. 00	20. 99	71. 91	21. 30	71. 82	21. 61
80	76. 90	22. 05	76. 80	22. 39	76. 71	22. 72	76. 61	23. 06
85	81. 71	23. 43	81. 60	23. 79	81. 50	24. 14	81. 39	24. 50
90	86. 51	24. 81	86. 40	25. 18	86. 29	25. 56	86. 18	25. 94
95	91. 32	26. 19	91. 20	26. 58	91. 09	26. 98	90. 97	27. 38
100	96. 13	27. 56	96. 00	27. 98	95. 88	28. 40	95. 76	28. 82
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.
	74 Deg.		73¾ Deg.		73½ Deg.		73¼ Deg.	

TRAVERSE TABLE.

Distance.	17 Deg.		17¼ Deg.		17½ Deg.		17¾ Deg.	
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.
1	0. 96	0. 29	0. 95	0. 30	0. 95	0. 30	0. 95	0. 30
2	1. 91	0. 58	1. 91	0. 59	1. 91	0. 60	1. 90	0. 61
3	2. 87	0. 88	2. 87	0. 89	2. 86	0. 90	2. 86	0. 91
4	3. 83	1. 17	3. 82	1. 19	3. 81	1. 20	3. 81	1. 22
5	4. 78	1. 46	4. 78	1. 48	4. 77	1. 50	4. 76	1. 52
6	5. 74	1. 75	5. 73	1. 78	5. 72	1. 80	5. 71	1. 83
7	6. 69	2. 05	6. 69	2. 08	6. 68	2. 10	6. 67	2. 13
8	7. 65	2. 34	7. 64	2. 37	7. 63	2. 41	7. 62	2. 44
9	8. 61	2. 63	8. 60	2. 67	8. 58	2. 71	8. 57	2. 74
10	9. 56	2. 92	9. 55	2. 97	9. 54	3. 01	9. 52	3. 05
11	10. 52	3. 22	10. 51	3. 26	10. 49	3. 31	10. 48	3. 35
12	11. 48	3. 51	11. 46	3. 56	11. 44	3. 61	11. 43	3. 66
13	12. 43	3. 80	12. 42	3. 85	12. 40	3. 91	12. 38	3. 96
14	13. 39	4. 09	13. 37	4. 15	13. 35	4. 21	13. 33	4. 27
15	14. 34	4. 39	14. 33	4. 45	14. 31	4. 51	14. 29	4. 57
16	15. 30	4. 68	15. 28	4. 74	15. 26	4. 81	15. 24	4. 88
17	16. 26	4. 97	16. 24	5. 04	16. 21	5. 11	16. 19	5. 18
18	17. 21	5. 26	17. 19	5. 34	17. 17	5. 41	17. 14	5. 49
19	18. 17	5. 56	18. 15	5. 63	18. 12	5. 71	18. 10	5. 79
20	19. 13	5. 85	19. 10	5. 93	19. 07	6. 01	19. 05	6. 10
21	20. 08	6. 14	20. 06	6. 23	20. 03	6. 31	20. 00	6. 40
22	21. 04	6. 43	21. 01	6. 52	20. 98	6. 62	20. 95	6. 71
23	21. 99	6. 72	21. 97	6. 82	21. 94	6. 92	21. 91	7. 01
24	22. 95	7. 02	22. 92	7. 12	22. 89	7. 22	22. 86	7. 32
25	23. 91	7. 31	23. 88	7. 41	23. 84	7. 52	23. 81	7. 62
26	24. 86	7. 60	24. 83	7. 71	24. 80	7. 82	24. 76	7. 93
27	25. 82	7. 89	25. 79	8. 01	25. 75	8. 12	25. 71	8. 23
28	26. 78	8. 19	26. 74	8. 30	26. 70	8. 42	26. 67	8. 54
29	27. 73	8. 48	27. 70	8. 60	27. 66	8. 72	27. 62	8. 84
30	28. 69	8. 77	28. 65	8. 90	28. 61	9. 02	28. 57	9. 15
35	33. 47	10. 23	33. 43	10. 38	33. 38	10. 52	33. 33	10. 67
40	38. 25	11. 69	38. 20	11. 86	38. 15	12. 03	38. 10	12. 19
45	43. 03	13. 16	42. 98	13. 34	42. 92	13. 53	42. 86	13. 72
50	47. 82	14. 62	47. 75	14. 83	47. 69	15. 04	47. 62	15. 24
55	52. 60	16. 08	52. 53	16. 31	52. 45	16. 54	52. 38	16. 77
60	57. 38	17. 54	57. 30	17. 79	57. 22	18. 04	57. 14	18. 29
65	62. 16	19. 00	62. 08	19. 28	61. 99	19. 55	61. 91	19. 82
70	66. 94	20. 47	66. 85	20. 76	66. 76	21. 05	66. 67	21. 34
75	71. 72	21. 93	71. 63	22. 24	71. 53	22. 55	71. 43	22. 86
80	76. 50	23. 39	76. 40	23. 72	76. 30	24. 06	76. 19	24. 39
85	81. 29	24. 85	81. 18	25. 21	81. 07	25. 56	80. 95	25. 91
90	86. 07	26. 31	85. 95	26. 69	85. 83	27. 06	85. 72	27. 44
95	90. 85	27. 78	90. 73	28. 17	90. 60	28. 57	90. 48	28. 96
100	95. 63	29. 24	95. 50	29. 65	95. 37	30. 07	95. 24	30. 49
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.
	73 Deg.		72¾ Deg.		72½ Deg.		72¼ Deg.	

Distance.	18 Deg.		18¼ Deg.		18½ Deg.		18¾ Deg.	
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.
1	0. 95	0. 31	0. 95	0. 31	0. 95	0. 32	0. 95	0. 32
2	1. 90	0. 62	1. 90	0. 63	1. 90	0. 63	1. 89	0. 64
3	2. 85	0. 93	2. 85	0. 94	2. 84	0. 95	2. 84	0. 96
4	3. 80	1. 24	3. 80	1. 25	3. 79	1. 27	3. 79	1. 29
5	4. 76	1. 55	4. 75	1. 57	4. 74	1. 59	4. 73	1. 61
6	5. 71	1. 85	5. 70	1. 88	5. 69	1. 90	5. 68	1. 93
7	6. 66	2. 16	6. 65	2. 19	6. 64	2. 22	6. 63	2. 25
8	7. 61	2. 47	7. 60	2. 51	7. 59	2. 54	7. 58	2. 57
9	8. 56	2. 78	8. 55	2. 82	8. 53	2. 86	8. 52	2. 89
10	9. 51	3. 09	9. 50	3. 13	9. 48	3. 17	9. 47	3. 21
11	10. 46	3. 40	10. 45	3. 44	10. 43	3. 49	10. 42	3. 54
12	11. 41	3. 71	11. 40	3. 76	11. 38	3. 81	11. 36	3. 86
13	12. 36	4. 02	12. 35	4. 07	12. 33	4. 12	12. 31	4. 18
14	13. 31	4. 33	13. 30	4. 38	13. 28	4. 44	13. 26	4. 50
15	14. 27	4. 64	14. 25	4. 70	14. 22	4. 76	14. 20	4. 82
16	15. 22	4. 94	15. 20	5. 01	15. 17	5. 08	15. 15	5. 14
17	16. 17	5. 25	16. 14	5. 32	16. 12	5. 39	16. 10	5. 46
18	17. 12	5. 56	17. 09	5. 64	17. 07	5. 71	17. 04	5. 79
19	18. 07	5. 87	18. 04	5. 95	18. 02	6. 03	17. 99	6. 11
20	19. 02	6. 18	18. 99	6. 26	18. 97	6. 35	18. 94	6. 43
21	19. 97	6. 49	19. 94	6. 58	19. 91	6. 66	19. 89	6. 75
22	20. 92	6. 80	20. 89	6. 89	20. 86	6. 98	20. 83	7. 07
23	21. 87	7. 11	21. 84	7. 20	21. 81	7. 30	21. 78	7. 39
24	22. 83	7. 42	22. 79	7. 52	22. 76	7. 62	22. 73	7. 71
25	23. 78	7. 73	23. 74	7. 83	23. 71	7. 93	23. 67	8. 04
26	24. 73	8. 03	24. 69	8. 14	24. 66	8. 25	24. 62	8. 36
27	25. 68	8. 34	25. 64	8. 46	25. 60	8. 57	25. 57	8. 68
28	26. 63	8. 65	26. 59	8. 77	26. 55	8. 88	26. 51	9. 00
29	27. 58	8. 96	27. 54	9. 08	27. 50	9. 20	27. 46	9. 32
30	28. 53	9. 27	28. 49	9. 39	28. 45	9. 52	28. 41	9. 64
35	33. 29	10. 82	33. 24	10. 96	33. 19	11. 11	33. 14	11. 25
40	38. 04	12. 36	37. 99	12. 53	37. 93	12. 69	37. 88	12. 86
45	42. 80	13. 91	42. 74	14. 09	42. 67	14. 28	42. 61	14. 46
50	47. 55	15. 45	47. 48	15. 66	47. 42	15. 87	47. 35	16. 07
55	52. 31	17. 00	52. 23	17. 22	52. 16	17. 45	52. 08	17. 68
60	57. 06	18. 54	56. 98	18. 79	56. 90	19. 04	56. 82	19. 29
65	61. 82	20. 09	61. 73	20. 36	61. 64	20. 62	61. 55	20. 89
70	66. 57	21. 63	66. 48	21. 92	66. 38	22. 21	66. 29	22. 50
75	71. 33	23. 18	71. 23	23. 49	71. 12	23. 80	71. 02	24. 11
80	76. 08	24. 72	75. 98	25. 05	75. 87	25. 38	75. 75	25. 72
85	80. 84	26. 27	80. 72	26. 62	80. 61	26. 97	80. 49	27. 32
90	85. 60	27. 81	85. 47	28. 18	85. 35	28. 56	85. 22	28. 93
95	90. 35	29. 36	90. 22	29. 75	90. 09	30. 14	89. 96	30. 54
100	95. 11	30. 90	94. 97	31. 32	94. 83	31. 73	94. 69	32. 14
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.
	72 Deg.		71¾ Deg.		71½ Deg.		71¼ Deg.	

Distance.	19 Deg.		19¼ Deg.		19½ Deg.		19¾ Deg.	
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.
1	0.95	0.33	0.94	0.33	0.94	0.33	0.94	0.34
2	1.89	0.65	1.89	0.66	1.89	0.67	1.88	0.68
3	2.84	0.98	2.83	0.99	2.83	1.00	2.82	1.01
4	3.78	1.30	3.78	1.32	3.77	1.34	3.76	1.35
5	4.73	1.63	4.72	1.65	4.71	1.67	4.71	1.69
6	5.67	1.95	5.66	1.98	5.66	2.00	5.65	2.03
7	6.62	2.28	6.61	2.31	6.60	2.24	6.59	2.37
8	7.56	2.60	7.55	2.64	7.54	2.67	7.53	2.70
9	8.51	2.93	8.50	2.97	8.48	3.00	8.47	3.04
10	9.46	3.26	9.44	3.30	9.43	3.34	9.41	3.38
11	10.40	3.58	10.38	3.63	10.37	3.67	10.35	3.72
12	11.35	3.91	11.33	3.96	11.31	4.01	11.29	4.06
13	12.29	4.23	12.27	4.29	12.25	4.34	12.24	4.39
14	13.24	4.56	13.22	4.62	13.20	4.67	13.18	4.73
15	14.18	4.88	14.16	4.95	14.14	5.01	14.12	5.07
16	15.13	5.21	15.11	5.28	15.08	5.34	15.06	5.41
17	16.07	5.53	16.05	5.60	16.02	5.67	16.00	5.74
18	17.02	5.86	16.99	5.93	16.97	6.01	16.94	6.08
19	17.96	6.19	17.94	6.26	17.91	6.34	17.88	6.42
20	18.91	6.51	18.88	6.59	18.85	6.68	18.82	6.76
21	19.86	6.84	19.83	6.92	19.80	7.01	19.76	7.10
22	20.80	7.16	20.77	7.25	20.74	7.34	20.71	7.43
23	21.75	7.49	21.71	7.58	21.68	7.68	21.65	7.77
24	22.69	7.81	22.66	7.91	22.62	8.01	22.59	8.11
25	23.64	8.14	23.60	8.24	23.57	8.35	23.53	8.45
26	24.58	8.46	24.55	8.57	24.51	8.68	24.47	8.79
27	25.53	8.79	25.49	8.90	25.45	9.01	25.41	9.12
28	26.47	9.12	26.43	9.23	26.39	9.35	26.35	9.46
29	27.42	9.44	27.38	9.56	27.34	9.68	27.29	9.80
30	28.37	9.77	28.32	9.89	28.28	10.01	28.24	10.14
35	33.09	11.39	33.04	11.54	32.99	11.68	32.94	11.83
40	37.82	13.02	37.76	13.19	37.71	13.35	37.65	13.52
45	42.55	14.65	42.48	14.84	42.42	15.02	42.35	15.21
50	47.28	16.28	47.20	16.48	47.13	16.69	47.06	16.90
55	52.00	17.91	51.92	18.13	51.85	18.36	51.76	18.59
60	56.73	19.53	56.65	19.78	56.56	20.03	56.47	20.27
65	61.46	21.16	61.37	21.43	61.27	21.70	61.18	21.96
70	66.19	22.79	66.09	23.08	65.98	23.37	65.88	23.65
75	70.91	24.42	70.81	24.73	70.70	25.04	70.59	25.34
80	75.64	26.05	75.53	26.38	75.41	26.70	75.29	27.03
85	80.37	27.67	80.25	28.02	80.12	28.37	80.00	28.72
90	85.10	29.30	84.97	29.67	84.84	30.04	84.71	30.41
95	89.82	30.93	89.69	31.32	89.55	31.71	89.41	32.10
100	94.55	32.56	94.41	32.97	94.26	33.38	94.12	33.79
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.
	71 Deg.		70¾ Deg.		70½ Deg.		70¼ Deg.	

Distance.	20 Deg.		20¼ Deg.		20½ Deg.		20¾ Deg.	
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.
1	0. 94	0. 34	0. 94	0. 35	0. 94	0. 35	0. 94	0. 35
2	1. 88	0. 68	1. 88	0. 69	1. 87	0. 70	1. 87	0. 71
3	2. 82	1. 03	2. 81	1. 04	2. 81	1. 05	2. 81	1. 06
4	3. 76	1. 37	3. 75	1. 38	3. 75	1. 40	3. 74	1. 42
5	4. 70	1. 71	4. 69	1. 73	4. 68	1. 75	4. 68	1. 77
6	5. 64	2. 05	5. 63	2. 08	5. 62	2. 10	5. 61	2. 13
7	6. 58	2. 39	6. 57	2. 42	6. 56	2. 45	6. 55	2. 48
8	7. 52	2. 74	7. 51	2. 77	7. 49	2. 80	7. 48	2. 83
9	8. 46	3. 08	8. 44	3. 12	8. 43	3. 15	8. 42	3. 19
10	9. 40	3. 42	9. 38	3. 46	9. 37	3. 50	9. 35	3. 54
11	10. 34	3. 76	10. 32	3. 81	10. 30	3. 85	10. 29	3. 90
12	11. 28	4. 10	11. 26	4. 15	11. 24	4. 20	11. 22	4. 25
13	12. 22	4. 45	12. 20	4. 50	12. 18	4. 55	12. 16	4. 61
14	13. 16	4. 79	13. 13	4. 85	13. 11	4. 90	13. 09	4. 96
15	14. 10	5. 13	14. 07	5. 19	14. 05	5. 25	14. 03	5. 31
16	15. 04	5. 47	15. 01	5. 54	14. 99	5. 60	14. 96	5. 67
17	15. 97	5. 81	15. 95	5. 88	15. 92	5. 95	15. 90	6. 02
18	16. 91	6. 16	16. 89	6. 23	16. 86	6. 30	16. 83	6. 38
19	17. 85	6. 50	17. 83	6. 58	17. 80	6. 65	17. 77	6. 73
20	18. 79	6. 84	18. 76	6. 92	18. 73	7. 00	18. 70	7. 09
21	19. 73	7. 18	19. 70	7. 27	19. 67	7. 35	19. 64	7. 44
22	20. 67	7. 52	20. 64	7. 61	20. 61	7. 70	20. 57	7. 79
23	21. 01	7. 87	21. 58	7. 96	21. 54	8. 05	21. 51	8. 15
24	22. 55	8. 21	22. 52	8. 31	22. 48	8. 40	22. 44	8. 50
25	23. 49	8. 55	23. 45	8. 65	23. 42	8. 76	23. 38	8. 86
26	24. 43	8. 89	24. 39	9. 00	24. 35	9. 11	24. 31	9. 21
27	25. 37	9. 23	25. 33	9. 35	25. 29	9. 46	25. 25	9. 57
28	26. 31	9. 58	26. 27	9. 69	26. 23	9. 81	26. 18	9. 92
29	27. 25	9. 92	27. 21	10. 04	27. 16	10. 16	27. 12	10. 27
30	28. 19	10. 26	28. 15	10. 38	28. 10	10. 51	28. 05	10. 63
35	32. 89	11. 97	32. 84	12. 11	32. 78	12. 26	32. 73	12. 40
40	37. 59	13. 68	37. 53	13. 84	37. 47	14. 01	37. 41	14. 17
45	42. 29	15. 39	42. 22	15. 58	42. 15	15. 76	42. 08	15. 94
50	46. 98	17. 10	46. 91	17. 31	46. 83	17. 51	46. 76	17. 71
55	51. 68	18. 81	51. 60	19. 04	51. 52	19. 26	51. 43	19. 49
60	56. 38	20. 52	56. 29	20. 77	56. 20	21. 01	56. 11	21. 26
65	61. 08	22. 23	60. 98	22. 50	60. 88	22. 76	60. 78	23. 03
70	65. 78	23. 94	65. 67	24. 23	65. 57	24. 51	65. 46	24. 80
75	70. 48	25. 65	70. 36	25. 96	70. 25	26. 27	70. 14	26. 57
80	75. 18	27. 36	75. 06	27. 69	74. 93	28. 02	74. 81	28. 34
85	79. 87	29. 07	79. 75	29. 42	79. 62	29. 77	79. 49	30. 11
90	84. 57	30. 78	84. 44	31. 15	84. 30	31. 52	84. 16	31. 89
95	89. 27	32. 49	89. 13	32. 88	88. 98	33. 27	88. 84	33. 66
100	93. 97	34. 20	93. 82	34. 61	93. 67	35. 02	93. 51	35. 43
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.
	70 Deg.		69¾ Deg.		69½ Deg.		69¼ Deg.	

TRAVERSE TABLE.

Distance.	21 Deg.		21¼ Deg.		21½ Deg.		21¾ Deg.	
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.
1	0. 93	0. 36	0. 93	0. 36	0. 93	0. 37	0. 93	0. 37
2	1. 87	0. 72	1. 86	0. 72	1. 86	0. 73	1. 86	0. 74
3	2. 80	1. 08	2. 80	1. 09	2. 79	1. 10	2. 79	1. 11
4	3. 73	1. 43	3. 73	1. 45	3. 72	1. 47	3. 72	1. 48
5	4. 67	1. 79	4. 66	1. 81	4. 65	1. 83	4. 64	1. 85
6	5. 60	2. 15	5. 59	2. 17	5. 58	2. 20	5. 57	2. 22
7	6. 54	2. 51	6. 52	2. 54	6. 51	2. 57	6. 50	2. 59
8	7. 47	2. 87	7. 46	2. 90	7. 44	2. 93	7. 43	2. 96
9	8. 40	3. 23	8. 39	3. 26	8. 37	3. 30	8. 36	3. 34
10	9. 34	3. 58	9. 32	3. 62	9. 30	3. 67	9. 29	3. 71
11	10. 27	3. 94	10. 25	3. 99	10. 23	4. 03	10. 22	4. 08
12	11. 20	4. 30	11. 18	4. 35	11. 17	4. 40	11. 15	4. 45
13	12. 14	4. 66	12. 12	4. 71	12. 10	4. 76	12. 07	4. 82
14	13. 07	5. 02	13. 05	5. 07	13. 03	5. 13	13. 00	5. 19
15	14. 00	5. 38	13. 98	5. 44	13. 96	5. 50	13. 93	5. 56
16	14. 94	5. 73	14. 91	5. 80	14. 89	5. 86	14. 86	5. 93
17	15. 87	6. 09	15. 84	6. 16	15. 82	6. 23	15. 79	6. 30
18	16. 80	6. 45	16. 78	6. 52	16. 75	6. 60	16. 72	6. 67
19	17. 74	6. 81	17. 71	6. 89	17. 68	6. 96	17. 65	7. 04
20	18. 67	7. 17	18. 64	7. 25	18. 61	7. 33	18. 58	7. 41
21	19. 61	7. 53	19. 57	7. 61	19. 54	7. 70	19. 50	7. 78
22	20. 54	7. 88	20. 50	7. 97	20. 47	8. 06	20. 43	8. 15
23	21. 47	8. 24	21. 44	8. 34	21. 40	8. 43	21. 36	8. 52
24	22. 41	8. 60	22. 37	8. 70	22. 33	8. 80	22. 29	8. 89
25	23. 34	8. 96	23. 30	9. 06	23. 26	9. 16	23. 22	9. 26
26	24. 27	9. 32	24. 23	9. 42	24. 19	9. 53	24. 15	9. 63
27	25. 21	9. 68	25. 16	9. 79	25. 12	9. 90	25. 08	10. 01
28	26. 14	10. 03	26. 10	10. 15	26. 05	10. 26	26. 01	10. 38
29	27. 07	10. 39	27. 03	10. 51	26. 98	10. 63	26. 94	10. 75
30	28. 01	10. 75	27. 96	10. 87	27. 91	11. 00	27. 86	11. 12
35	32. 68	12. 54	32. 62	12. 69	32. 56	12. 85	32. 51	12. 97
40	37. 34	14. 33	37. 28	14. 50	37. 22	14. 66	37. 15	14. 82
45	42. 01	16. 13	41. 94	16. 31	41. 87	16. 49	41. 80	16. 68
50	46. 68	17. 92	46. 60	18. 12	46. 52	18. 33	46. 44	18. 53
55	51. 35	19. 71	51. 26	19. 93	51. 17	20. 16	51. 08	20. 38
60	56. 01	21. 50	55. 92	21. 75	55. 83	21. 99	55. 73	22. 23
65	60. 68	23. 29	60. 58	23. 56	60. 48	23. 82	60. 37	24. 09
70	65. 35	25. 09	65. 24	25. 37	65. 13	25. 66	65. 02	25. 94
75	70. 02	26. 88	69. 90	27. 18	69. 78	27. 49	69. 66	27. 79
80	74. 69	28. 67	74. 56	29. 00	74. 43	29. 32	74. 30	29. 64
85	79. 35	30. 46	79. 22	30. 81	79. 09	31. 15	78. 95	31. 50
90	84. 02	32. 25	83. 88	32. 62	83. 74	32. 99	83. 59	33. 35
95	88. 69	34. 04	88. 54	34. 43	88. 39	34. 82	88. 24	35. 20
00	93. 36	35. 84	93. 20	36. 24	93. 04	36. 65	92. 88	37. 06
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.
	69 Deg.		68¾ Deg.		68½ Deg.		68¼ Deg.	

Distance.	22 DEG.		22¼ DEG.		22½ DEG.		22¾ DEG.	
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.
1	0. 93	0. 37	0. 93	0. 38	0. 92	0. 38	0. 92	0. 39
2	1. 85	0. 75	1. 85	0. 76	1. 85	0. 77	1. 84	0. 77
3	2. 78	1. 12	2. 78	1. 14	2. 77	1. 15	2. 77	1. 16
4	3. 71	1. 50	3. 70	1. 51	3. 70	1. 53	3. 69	1. 55
5	4. 64	1. 87	4. 63	1. 89	4. 62	1. 91	4. 61	1. 93
6	5. 56	2. 25	5. 55	2. 27	5. 54	2. 30	5. 53	2. 32
7	6. 49	2. 62	6. 48	2. 65	6. 47	2. 68	6. 46	2. 71
8	7. 42	3. 00	7. 40	3. 03	7. 39	3. 06	7. 38	3. 09
9	8. 34	3. 37	8. 33	3. 41	8. 31	3. 44	8. 30	3. 48
10	9. 27	3. 75	9. 26	3. 79	9. 24	3. 83	9. 22	3. 87
11	10. 20	4. 12	10. 18	4. 17	10. 16	4. 21	10. 14	4. 25
12	11. 13	4. 50	11. 11	4. 54	11. 09	4. 59	11. 07	4. 64
13	12. 05	4. 87	12. 03	4. 92	12. 01	4. 97	11. 99	5. 03
14	12. 98	5. 24	12. 96	5. 30	12. 93	5. 36	12. 91	5. 41
15	13. 91	5. 62	13. 88	5. 68	13. 86	5. 74	13. 83	5. 80
16	14. 83	5. 99	14. 81	6. 06	14. 78	6. 12	14. 76	6. 19
17	15. 76	6. 37	15. 73	6. 44	15. 71	6. 51	15. 68	6. 57
18	16. 69	6. 74	16. 66	6. 82	16. 63	6. 89	16. 60	6. 96
19	17. 62	7. 12	17. 59	7. 19	17. 55	7. 27	17. 52	7. 35
20	18. 54	7. 49	18. 51	7. 57	18. 48	7. 65	18. 44	7. 73
21	19. 47	7. 87	19. 44	7. 95	19. 40	8. 04	19. 37	8. 12
22	20. 40	8. 24	20. 36	8. 33	20. 33	8. 42	20. 29	8. 51
23	21. 33	8. 62	21. 29	8. 71	21. 25	8. 80	21. 21	8. 89
24	22. 25	8. 99	22. 21	9. 09	22. 17	9. 18	22. 13	9. 28
25	23. 18	9. 37	23. 14	9. 47	23. 10	9. 57	23. 05	9. 67
26	24. 11	9. 74	24. 06	9. 84	24. 02	9. 95	23. 98	10. 05
27	25. 03	10. 11	24. 99	10. 22	24. 94	10. 33	24. 90	10. 44
28	25. 96	10. 49	25. 92	10. 60	25. 87	10. 72	25. 82	10. 83
29	26. 89	10. 86	26. 84	10. 98	26. 79	11. 10	26. 74	11. 21
30	27. 82	11. 24	27. 77	11. 36	27. 72	11. 48	27. 67	11. 60
35	32. 45	13. 11	32. 39	13. 25	32. 34	13. 39	32. 28	13. 53
40	37. 09	14. 98	37. 02	15. 15	36. 96	15. 31	36. 89	15. 47
45	41. 72	16. 86	41. 65	17. 04	41. 57	17. 22	41. 50	17. 40
50	46. 36	18. 73	46. 28	18. 93	46. 19	19. 13	46. 11	19. 34
55	51. 00	20. 60	50. 90	20. 83	50. 81	21. 05	50. 72	21. 27
60	55. 63	22. 48	55. 53	22. 72	55. 43	22. 96	55. 33	23. 20
65	60. 27	24. 35	60. 16	24. 61	60. 05	24. 87	59. 94	25. 14
70	64. 90	26. 22	64. 79	26. 51	64. 67	26. 79	64. 55	27. 07
75	69. 54	28. 10	69. 42	28. 40	69. 29	28. 70	69. 17	29. 00
80	74. 17	29. 97	74. 04	30. 29	73. 91	30. 61	73. 78	30. 94
85	78. 81	31. 84	78. 67	32. 19	78. 53	32. 53	78. 39	32. 87
90	83. 45	33. 71	83. 30	34. 08	83. 15	34. 44	83. 00	34. 80
95	88. 08	35. 59	87. 93	35. 97	87. 77	36. 35	87. 61	36. 74
100	92. 72	37. 46	92. 55	37. 86	92. 39	38. 27	92. 22	38. 67
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.
	68 DEG.		67¾ DEG.		67½ DEG.		67¼ DEG.	

Distance.	23 Deg.		23¼ Deg.		23½ Deg.		23¾ Deg.		Distance.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
1	0. 92	0. 39	0. 92	0. 39	0. 92	0. 40	0. 92	0. 40	
2	1. 84	0. 78	1. 84	0. 79	1. 83	0. 80	1. 83	0. 81	
3	2. 76	1. 17	2. 76	1. 18	2. 75	1. 20	2. 75	1. 21	
4	3. 68	1. 56	3. 68	1. 58	3. 67	1. 59	3. 66	1. 61	
5	4. 60	1. 95	4. 59	1. 97	4. 59	1. 99	4. 58	2. 01	
6	5. 52	2. 34	5. 51	2. 37	5. 50	2. 39	5. 49	2. 42	
7	6. 44	2. 74	6. 43	2. 76	6. 42	2. 79	6. 41	2. 82	
8	7. 36	3. 13	7. 35	3. 16	7. 34	3. 19	7. 32	3. 22	
9	8. 28	3. 52	8. 27	3. 55	8. 25	3. 59	8. 24	3. 62	
10	9. 20	3. 91	9. 19	3. 95	9. 17	3. 99	9. 15	4. 03	
11	10. 13	4. 30	10. 11	4. 34	10. 09	4. 39	10. 07	4. 43	
12	11. 05	4. 69	11. 03	4. 74	11. 00	4. 78	10. 98	4. 83	
13	11. 97	5. 08	11. 94	5. 13	11. 92	5. 18	11. 90	5. 24	
14	12. 89	5. 47	12. 86	5. 53	12. 84	5. 58	12. 81	5. 64	
15	13. 81	5. 86	13. 78	5. 92	13. 76	5. 98	13. 73	6. 04	
16	14. 73	6. 25	14. 70	6. 32	14. 67	6. 38	14. 64	6. 44	
17	15. 65	6. 64	15. 62	6. 71	15. 59	6. 78	15. 56	6. 85	
18	16. 57	7. 03	16. 54	7. 11	16. 51	7. 18	16. 48	7. 25	
19	17. 49	7. 42	17. 46	7. 50	17. 42	7. 58	17. 39	7. 65	
20	18. 41	7. 81	18. 38	7. 89	18. 34	7. 97	18. 31	8. 05	
21	19. 33	8. 21	19. 29	8. 29	19. 26	8. 37	19. 22	8. 46	
22	20. 25	8. 60	20. 21	8. 68	20. 18	8. 77	20. 14	8. 86	
23	21. 17	8. 99	21. 13	9. 08	21. 09	9. 17	21. 05	9. 26	
24	22. 09	9. 38	22. 05	9. 47	22. 01	9. 57	21. 97	9. 67	
25	23. 01	9. 77	22. 97	9. 87	22. 93	9. 97	22. 88	10. 07	
26	23. 93	10. 16	23. 89	10. 26	23. 84	10. 37	23. 80	10. 47	
27	24. 85	10. 55	24. 81	10. 66	24. 76	10. 77	24. 71	10. 87	
28	25. 77	10. 94	25. 73	11. 05	25. 68	11. 16	25. 63	11. 28	
29	26. 69	11. 33	26. 64	11. 45	26. 59	11. 56	26. 54	11. 68	
30	27. 62	11. 72	27. 56	11. 84	27. 51	11. 96	27. 46	12. 08	
35	32. 22	13. 68	32. 16	13. 82	32. 10	13. 96	32. 04	14. 10	
40	36. 82	15. 63	36. 75	15. 79	36. 68	15. 95	36. 61	16. 11	
45	41. 42	17. 58	41. 35	17. 76	41. 27	17. 94	41. 19	18. 12	
50	46. 03	19. 54	45. 94	19. 74	45. 85	19. 94	45. 77	20. 14	
55	50. 63	21. 49	50. 53	21. 71	50. 44	21. 93	50. 34	22. 15	
60	55. 23	23. 44	55. 13	23. 68	55. 02	23. 92	54. 92	24. 16	
65	59. 83	25. 40	59. 72	25. 66	59. 61	25. 92	59. 50	26. 18	
70	64. 44	27. 35	64. 32	27. 63	64. 19	27. 91	64. 07	28. 19	
75	69. 04	29. 30	68. 91	29. 61	68. 78	29. 91	68. 65	30. 21	
80	73. 64	31. 26	73. 50	31. 58	73. 36	31. 90	73. 22	32. 22	
85	78. 24	33. 21	78. 10	33. 55	77. 95	33. 89	77. 80	34. 23	
90	82. 85	35. 17	82. 69	35. 53	82. 54	35. 89	82. 38	36. 25	
95	87. 45	37. 12	87. 29	37. 50	87. 12	37. 88	86. 95	38. 26	
100	92. 05	39. 07	91. 83	39. 47	91. 71	39. 87	91. 53	40. 27	
	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	
	67 Deg.		66¾ Deg.		66½ Deg.		66¼ Deg.		Distance.

Distance.	24 Deg.		24¼ Deg.		24½ Deg.		24¾ Deg.	
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.
1	0. 91	0. 41	0. 91	0. 41	0. 91	0. 41	0. 91	0. 42
2	1. 83	0. 81	1. 82	0. 82	1. 82	0. 83	1. 82	0. 84
3	2. 74	1. 22	2. 74	1. 23	2. 73	1. 24	2. 72	1. 26
4	3. 65	1. 63	3. 65	1. 64	3. 64	1. 66	3. 63	1. 67
5	4. 57	2. 03	4. 56	2. 05	4. 55	2. 07	4. 54	2. 09
6	5. 48	2. 44	5. 47	2. 46	5. 46	2. 49	5. 45	2. 51
7	6. 39	2. 85	6. 38	2. 87	6. 37	2. 90	6. 36	2. 93
8	7. 31	3. 25	7. 29	3. 29	7. 28	3. 32	7. 27	3. 35
9	8. 22	3. 66	8. 21	3. 70	8. 19	3. 73	8. 17	3. 77
10	9. 14	4. 07	9. 12	4. 11	9. 10	4. 15	9. 08	4. 19
11	10. 05	4. 47	10. 03	4. 52	10. 01	4. 56	9. 99	4. 61
12	10. 96	4. 88	10. 94	4. 93	10. 92	4. 98	10. 90	5. 02
13	11. 88	5. 29	11. 85	5. 34	11. 83	5. 39	11. 81	5. 44
14	12. 79	5. 69	12. 76	5. 75	12. 74	5. 81	12. 71	5. 86
15	13. 70	6. 10	13. 68	6. 16	13. 65	6. 22	13. 62	6. 28
16	14. 62	6. 51	14. 59	6. 57	14. 56	6. 64	14. 53	6. 70
17	15. 53	6. 92	15. 50	6. 98	15. 47	7. 05	15. 44	7. 12
18	16. 44	7. 32	16. 41	7. 39	16. 38	7. 46	16. 35	7. 54
19	17. 36	7. 73	17. 32	7. 80	17. 29	7. 88	17. 25	7. 96
20	18. 27	8. 13	18. 24	8. 21	18. 20	8. 29	18. 16	8. 37
21	19. 18	8. 54	19. 15	8. 63	19. 11	8. 71	19. 07	8. 79
22	20. 10	8. 95	20. 06	9. 04	20. 02	9. 12	19. 98	9. 21
23	21. 01	9. 35	20. 97	9. 45	20. 93	9. 54	20. 89	9. 63
24	21. 93	9. 76	21. 88	9. 86	21. 84	9. 95	21. 80	10. 05
25	22. 84	10. 17	22. 79	10. 27	22. 75	10. 37	22. 70	10. 47
26	23. 75	10. 58	23. 71	10. 68	23. 66	10. 78	23. 61	10. 89
27	24. 67	10. 98	24. 62	11. 09	24. 57	11. 20	24. 52	11. 30
28	25. 58	11. 39	25. 53	11. 50	25. 48	11. 61	25. 43	11. 72
29	26. 49	11. 80	26. 44	11. 91	26. 39	12. 03	26. 34	12. 14
30	27. 41	12. 20	27. 35	12. 32	27. 30	12. 44	27. 24	12. 56
35	31. 97	14. 24	31. 91	14. 38	31. 85	14. 51	31. 78	14. 65
40	36. 54	16. 27	36. 47	16. 43	36. 40	16. 59	36. 33	16. 75
45	41. 11	18. 30	41. 03	18. 48	40. 95	18. 66	40. 87	18. 84
50	45. 68	20. 34	45. 59	20. 54	45. 50	20. 73	45. 41	20. 93
55	50. 24	22. 37	50. 15	22. 59	50. 05	22. 81	49. 95	23. 03
60	54. 81	24. 40	54. 71	24. 64	54. 60	24. 88	54. 49	25. 12
65	59. 38	26. 44	59. 26	26. 70	59. 15	26. 96	59. 03	27. 21
70	63. 95	28. 47	63. 82	28. 75	63. 70	29. 03	63. 57	29. 31
75	68. 52	30. 51	68. 38	30. 80	68. 25	31. 10	68. 11	31. 40
80	73. 08	32. 54	72. 94	32. 86	72. 80	33. 18	72. 65	33. 49
85	77. 65	34. 57	77. 50	34. 91	77. 35	35. 25	77. 19	35. 59
90	82. 22	36. 61	82. 06	36. 96	81. 90	37. 32	81. 73	37. 68
95	86. 79	38. 64	86. 62	39. 02	86. 45	39. 40	86. 27	39. 77
100	91. 35	40. 67	91. 18	41. 07	91. 00	41. 47	90. 81	41. 87
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.
	66 Deg.		65¾ Deg.		65½ Deg.		65¼ Deg.	

Distance.	25 Deg.		25¼ Deg.		25½ Deg.		25¾ Deg.	
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.
1	0. 91	0. 42	0. 90	0. 43	0. 90	0. 43	0. 90	0. 43
2	1. 81	0. 85	1. 81	0. 85	1. 81	0. 86	1. 80	0. 87
3	2. 72	1. 27	2. 71	1. 28	2. 71	1. 29	2. 70	1. 30
4	3. 63	1. 69	3. 62	1. 71	3. 61	1. 72	3. 60	1. 74
5	4. 53	2. 11	4. 52	2. 13	4. 51	2. 15	4. 50	2. 17
6	5. 44	2. 54	5. 43	2. 56	5. 42	2. 58	5. 40	2. 61
7	6. 34	2. 96	6. 33	2. 99	6. 32	3. 01	6. 30	3. 04
8	7. 25	3. 38	7. 24	3. 41	7. 22	3. 44	7. 21	3. 48
9	8. 16	3. 80	8. 14	3. 84	8. 12	3. 87	8. 11	3. 91
10	9. 06	4. 23	9. 04	4. 27	9. 03	4. 31	9. 01	4. 34
11	9. 97	4. 65	9. 95	4. 69	9. 93	4. 74	9. 91	4. 78
12	10. 88	5. 07	10. 85	5. 12	10. 83	5. 17	10. 81	5. 21
13	11. 78	5. 49	11. 76	5. 55	11. 73	5. 60	11. 71	5. 65
14	12. 69	5. 92	12. 66	5. 97	12. 64	6. 03	12. 61	6. 08
15	13. 59	6. 34	13. 57	6. 40	13. 54	6. 46	13. 51	6. 52
16	14. 50	6. 76	14. 47	6. 83	14. 44	6. 89	14. 41	6. 95
17	15. 41	7. 18	15. 38	7. 25	15. 34	7. 32	15. 31	7. 39
18	16. 31	7. 61	16. 28	7. 68	16. 25	7. 75	16. 21	7. 82
19	17. 22	8. 03	17. 18	8. 10	17. 15	8. 18	17. 11	8. 25
20	18. 13	8. 45	18. 09	8. 53	18. 05	8. 61	18. 01	8. 69
21	19. 03	8. 87	18. 99	8. 96	18. 95	9. 04	18. 91	9. 12
22	19. 94	9. 30	19. 90	9. 38	19. 86	9. 47	19. 82	9. 56
23	20. 85	9. 72	20. 80	9. 81	20. 76	9. 90	20. 72	9. 99
24	21. 75	10. 14	21. 71	10. 24	21. 66	10. 33	21. 62	10. 43
25	22. 66	10. 57	22. 61	10. 66	22. 56	10. 76	22. 52	10. 86
26	23. 56	10. 99	23. 52	11. 09	23. 47	11. 19	23. 42	11. 30
27	24. 47	11. 41	24. 42	11. 52	24. 37	11. 62	24. 32	11. 73
28	25. 38	11. 83	25. 32	11. 94	25. 27	12. 05	25. 22	12. 16
29	26. 28	12. 26	26. 23	12. 37	26. 17	12. 48	26. 12	12. 60
30	27. 19	12. 68	27. 13	12. 80	27. 08	12. 92	27. 02	13. 03
35	31. 72	14. 79	31. 66	14. 93	31. 59	15. 07	31. 52	15. 21
40	36. 25	16. 90	36. 18	17. 06	36. 10	17. 22	36. 03	17. 38
45	40. 78	19. 02	40. 70	19. 20	40. 62	19. 37	40. 53	19. 55
50	45. 32	21. 13	45. 22	21. 33	45. 13	21. 53	45. 03	21. 72
55	49. 85	23. 24	49. 74	23. 46	49. 64	23. 68	49. 54	23. 89
60	54. 38	25. 36	54. 27	25. 59	54. 16	25. 83	54. 04	26. 07
65	58. 91	27. 47	58. 79	27. 73	58. 67	27. 98	58. 55	28. 24
70	63. 44	29. 58	63. 31	29. 86	63. 18	30. 14	63. 05	30. 41
75	67. 97	31. 70	67. 83	31. 99	67. 69	32. 29	67. 55	32. 58
80	72. 50	33. 81	72. 36	34. 13	72. 21	34. 44	72. 06	34. 76
85	77. 04	35. 92	76. 88	36. 26	76. 72	36. 59	76. 56	36. 93
90	81. 57	38. 04	81. 40	38. 39	81. 23	38. 75	81. 06	39. 10
95	86. 10	40. 15	85. 92	40. 52	85. 75	40. 90	85. 57	41. 27
100	90. 63	42. 26	90. 45	42. 66	90. 26	43. 05	90. 07	43. 44
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.
	65 Deg.		64¾ Deg.		64½ Deg.		64¼ Deg.	

Distance.	26 Deg.		26¼ Deg.		26½ Deg.		26¾ Deg.	
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.
1	0. 90	0. 44	0. 90	0. 44	0. 89	0. 45	0. 89	0. 45
2	1. 80	0. 88	1. 79	0. 88	1. 79	0. 89	1. 79	0. 90
3	2. 70	1. 32	2. 69	1. 33	2. 68	1. 34	2. 68	1. 35
4	3. 60	1. 75	3. 59	1. 77	3. 58	1. 78	3. 57	1. 80
5	4. 49	2. 19	4. 48	2. 21	4. 47	2. 23	4. 46	2. 25
6	5. 39	2. 63	5. 38	2. 65	5. 37	2. 68	5. 36	2. 70
7	6. 29	3. 07	6. 28	3. 10	6. 26	3. 12	6. 25	3. 15
8	7. 19	3. 51	7. 17	3. 54	7. 16	3. 57	7. 14	3. 60
9	8. 09	3. 95	8. 07	3. 98	8. 05	4. 02	8. 04	4. 05
10	8. 99	4. 38	8. 97	4. 42	8. 95	4. 46	8. 93	4. 50
11	9. 89	4. 82	9. 87	4. 87	9. 84	4. 91	9. 82	4. 95
12	10. 79	5. 26	10. 76	5. 31	10. 74	5. 35	10. 72	5. 40
13	11. 68	5. 70	11. 66	5. 75	11. 63	5. 80	11. 61	5. 85
14	12. 58	6. 14	12. 56	6. 19	12. 53	6. 25	12. 50	6. 30
15	13. 48	6. 58	13. 45	6. 63	13. 42	6. 69	13. 39	6. 75
16	14. 38	7. 01	14. 35	7. 08	14. 32	7. 14	14. 29	7. 20
17	15. 28	7. 45	15. 25	7. 52	15. 21	7. 59	15. 18	7. 65
18	16. 18	7. 89	16. 14	7. 96	16. 11	8. 03	16. 07	8. 10
19	17. 08	8. 33	17. 04	8. 40	17. 00	8. 48	16. 97	8. 55
20	17. 98	8. 77	17. 94	8. 85	17. 90	8. 92	17. 86	9. 00
21	18. 87	9. 21	18. 83	9. 29	18. 79	9. 37	18. 75	9. 45
22	19. 77	9. 64	19. 73	9. 73	19. 69	9. 82	19. 65	9. 90
23	20. 67	10. 08	20. 63	10. 17	20. 58	10. 26	20. 54	10. 35
24	21. 57	10. 52	21. 52	10. 61	21. 48	10. 71	21. 43	10. 80
25	22. 47	10. 96	22. 42	11. 06	22. 37	11. 15	22. 32	11. 25
26	23. 37	11. 40	23. 32	11. 50	23. 27	11. 60	23. 22	11. 70
27	24. 27	11. 84	24. 22	11. 94	24. 16	12. 05	24. 11	12. 15
28	25. 17	12. 27	25. 11	12. 38	25. 06	12. 49	25. 00	12. 60
29	26. 06	12. 71	26. 01	12. 83	25. 95	12. 94	25. 90	13. 05
30	26. 96	13. 15	26. 91	13. 27	26. 85	13. 39	26. 79	13. 50
35	31. 46	15. 34	31. 39	15. 48	31. 32	15. 62	31. 25	15. 75
40	35. 95	17. 53	35. 87	17. 69	35. 80	17. 85	35. 72	18. 00
45	40. 45	19. 73	40. 36	19. 90	40. 27	20. 08	40. 18	20. 25
50	44. 94	21. 92	44. 84	22. 11	44. 75	22. 31	44. 65	22. 50
55	49. 43	24. 11	49. 33	24. 33	49. 22	24. 54	49. 11	24. 76
60	53. 93	26. 30	53. 81	26. 54	53. 70	26. 77	53. 58	27. 01
65	58. 42	28. 49	58. 30	28. 75	58. 17	29. 00	58. 04	29. 26
70	62. 92	30. 69	62. 78	30. 96	62. 65	31. 23	62. 51	31. 51
75	67. 41	32. 88	67. 27	33. 17	67. 12	33. 46	66. 97	33. 76
80	71. 90	35. 07	71. 75	35. 38	71. 59	35. 70	71. 44	36. 01
85	76. 40	37. 26	76. 23	37. 59	76. 07	37. 93	75. 90	38. 26
90	80. 89	39. 45	80. 72	39. 81	80. 54	40. 16	80. 37	40. 51
95	85. 39	41. 65	85. 20	42. 02	85. 02	42. 29	84. 83	42. 76
100	89. 88	43. 84	89. 69	44. 23	89. 49	44. 62	89. 30	45. 01
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.
	64 Deg.		63¾ Deg.		63½ Deg.		63¼ Deg.	

Distance.	27 Deg.		27¼ Deg.		27½ Deg.		27¾ Deg.	
	Lat	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.
1	0.89	0.45	0.89	0.46	0.89	0.46	0.88	0.47
2	1.78	0.91	1.78	0.92	1.77	0.92	1.77	0.93
3	2.67	1.36	2.67	1.37	2.66	1.39	2.65	1.40
4	3.56	1.82	3.56	1.83	3.55	1.85	3.54	1.86
5	4.45	2.27	4.45	2.29	4.44	2.31	4.42	2.33
6	5.35	2.72	5.33	2.75	5.32	2.77	5.31	2.79
7	6.24	3.18	6.22	3.21	6.21	3.23	6.19	3.26
8	7.13	3.63	7.11	3.66	7.10	3.69	7.08	3.72
9	8.02	4.09	8.00	4.12	7.98	4.16	7.96	4.19
10	8.91	4.54	8.89	4.58	8.87	4.62	8.85	4.66
11	9.80	4.99	9.78	5.04	9.76	5.08	9.73	5.12
12	10.69	5.45	10.67	5.49	10.64	5.54	10.62	5.59
13	11.58	5.90	11.56	5.95	11.53	6.00	11.50	6.05
14	12.47	6.36	12.45	6.41	12.42	6.46	12.39	6.52
15	13.37	6.81	13.34	6.87	13.31	6.93	13.27	6.98
16	14.26	7.26	14.22	7.33	14.19	7.39	14.16	7.45
17	15.15	7.72	15.11	7.78	15.08	7.85	15.04	7.92
18	16.04	8.17	16.00	8.24	15.97	8.31	15.93	8.38
19	16.93	8.63	16.89	8.70	16.85	8.77	16.81	8.85
20	17.82	9.08	17.78	9.16	17.74	9.23	17.70	9.31
21	18.71	9.53	18.67	9.62	18.63	9.70	18.58	9.78
22	19.60	9.99	19.56	10.07	19.51	10.16	19.47	10.24
23	20.49	10.44	20.45	10.53	20.40	10.62	20.35	10.71
24	21.38	10.90	21.34	10.99	21.29	11.08	21.24	11.17
25	22.28	11.35	22.23	11.45	22.18	11.54	22.12	11.64
26	23.17	11.80	23.11	11.90	23.06	12.01	23.01	12.11
27	24.06	12.26	24.00	12.36	23.95	12.47	23.89	12.57
28	24.95	12.71	24.89	12.82	24.84	12.93	24.78	13.04
29	25.84	13.17	25.78	13.28	25.72	13.39	25.66	13.50
30	26.73	13.62	26.67	13.74	26.61	13.85	26.55	13.97
35	31.19	15.89	31.12	16.03	31.05	16.16	30.97	16.30
40	35.64	18.16	35.56	18.31	35.48	18.47	35.40	18.62
45	40.10	20.43	40.01	20.60	39.92	20.78	39.82	20.95
50	44.55	22.70	44.45	22.89	44.35	23.00	44.25	23.28
55	49.01	24.97	48.90	25.18	48.79	25.40	48.67	25.61
60	53.46	27.24	53.34	27.47	53.22	27.70	53.10	27.94
65	57.92	29.51	57.79	29.76	57.66	30.01	57.52	30.26
70	62.37	31.78	62.23	32.05	62.09	32.32	61.95	32.59
75	66.83	34.05	66.68	34.34	66.53	34.63	66.37	34.92
80	71.23	36.32	71.12	36.63	70.96	36.94	70.80	37.25
85	75.74	38.59	75.57	38.92	75.40	39.25	75.22	39.58
90	80.19	40.86	80.01	41.21	79.83	41.56	79.65	41.91
95	84.65	43.13	84.46	43.50	84.27	43.87	84.07	44.23
00	89.10	45.40	88.90	45.79	88.70	46.17	88.50	46.56
	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.
	63 Deg.		62¾ Deg.		62½ Deg.		62¼ Deg.	

Distance.	28 Deg.		28¼ Deg.		28½ Deg.		28¾ Deg.	
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.
1	0.88	0.47	0.88	0.47	0.88	0.48	0.88	0.48
2	1.77	0.94	1.76	0.95	1.76	0.95	1.75	0.96
3	2.65	1.41	2.64	1.42	2.64	1.43	2.63	1.44
4	3.53	1.88	3.52	1.89	3.52	1.91	3.51	1.92
5	4.41	2.35	4.40	2.37	4.39	2.39	4.38	2.40
6	5.30	2.82	5.29	2.84	5.27	2.86	5.26	2.89
7	6.18	3.29	6.17	3.31	6.15	3.34	6.14	3.37
8	7.06	3.76	7.05	3.79	7.03	3.82	7.01	3.85
9	7.95	4.23	7.93	4.26	7.91	4.29	7.89	4.33
10	8.83	4.69	8.81	4.73	8.79	4.77	8.77	4.81
11	9.71	5.16	9.69	5.21	9.67	5.25	9.64	5.29
12	10.60	5.63	10.57	5.68	10.55	5.73	10.52	5.77
13	11.48	6.10	11.45	6.15	11.42	6.20	11.40	6.25
14	12.36	6.57	12.33	6.63	12.30	6.68	12.27	6.73
15	13.24	7.04	13.21	7.10	13.18	7.16	13.15	7.21
16	14.13	7.51	14.09	7.57	14.06	7.63	14.03	7.70
17	15.01	7.98	14.98	8.05	14.94	8.11	14.90	8.18
18	15.89	8.45	15.86	8.52	15.82	8.59	15.78	8.66
19	16.78	8.92	16.74	8.99	16.70	9.07	16.66	9.14
20	17.66	9.39	17.62	9.47	17.58	9.54	17.53	9.62
21	18.54	9.86	18.50	9.94	18.46	10.02	18.41	10.10
22	19.42	10.33	19.38	10.41	19.33	10.50	19.29	10.58
23	20.31	10.80	20.26	10.89	20.21	10.97	20.16	11.06
24	21.19	11.27	21.14	11.36	21.09	11.45	21.04	11.54
25	22.07	11.74	22.02	11.83	21.97	11.93	21.92	12.02
26	22.96	12.21	22.90	12.31	22.85	12.41	22.79	12.51
27	23.84	12.68	23.78	12.78	23.73	12.88	23.67	12.99
28	24.72	13.15	24.66	13.25	24.61	13.36	24.55	13.47
29	25.61	13.61	25.55	13.73	25.49	13.84	25.43	13.95
30	26.49	14.08	26.43	14.20	26.36	14.31	26.30	14.43
35	30.90	16.43	30.83	16.57	30.76	16.70	30.69	16.83
40	35.32	18.78	35.24	18.93	35.15	19.09	35.07	19.24
45	39.73	21.13	39.64	21.30	39.55	21.47	39.45	21.64
50	44.15	23.47	44.04	23.67	43.94	23.86	43.84	24.05
55	48.56	25.82	48.45	26.03	48.33	26.24	48.22	26.45
60	52.98	28.17	52.85	28.40	52.73	28.63	52.60	28.86
65	57.39	30.52	57.26	30.77	57.12	31.02	56.99	31.26
70	61.81	32.86	61.66	33.13	61.52	33.40	61.37	33.67
75	66.22	35.21	66.07	35.50	65.91	35.79	65.75	36.07
80	70.64	37.56	70.47	37.87	70.31	38.17	70.14	38.48
85	75.05	39.91	74.88	40.23	74.70	40.56	74.52	40.88
90	79.47	42.25	79.28	42.60	79.09	42.94	78.91	43.29
95	83.88	44.60	83.68	44.97	83.49	45.33	83.29	45.69
100	88.29	46.95	88.09	47.33	87.88	47.72	87.67	48.10
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.
	62 Deg.		61¾ Deg.		61½ Deg.		61¼ Deg.	

Distance.	29 Deg.		29¼ Deg.		29½ Deg.		29¾ Deg.	
	Lat.	Dep.	Lat	Dep.	Lat.	Dep.	Lat.	Dep.
1	0. 87	0. 48	0. 87	0. 49	0. 87	0. 49	0. 87	0. 50
2	1. 75	0. 97	1. 74	0. 98	1. 74	0. 98	1. 74	0. 99
3	2. 62	1. 45	2. 62	1. 47	2. 61	1. 48	2. 60	1. 49
4	3. 50	1. 94	3. 49	1. 95	3. 48	1. 97	3. 47	1. 98
5	4. 37	2. 42	4. 36	2. 44	4. 35	2. 46	4. 34	2. 48
6	5. 25	2. 91	5. 23	2. 93	5. 22	2. 95	5. 21	2. 98
7	6. 12	3. 39	6. 11	3. 42	6. 09	3. 45	6. 08	3. 47
8	7. 00	3. 88	6. 98	3. 91	6. 96	3. 94	6. 95	3. 97
9	7. 87	4. 36	7. 85	4. 40	7. 83	4. 43	7. 81	4. 47
10	8. 75	4. 85	8. 72	4. 89	8. 70	4. 92	8. 68	4. 96
11	9. 62	5. 33	9. 60	5. 37	9. 57	5. 42	9. 55	5. 46
12	10. 50	5. 82	10. 47	5. 86	10. 44	5. 91	10. 42	5. 95
13	11. 37	6. 30	11. 34	6. 35	11. 31	6. 40	11. 29	6. 45
14	12. 24	6. 79	12. 21	6. 84	12. 18	6. 89	12. 15	6. 95
15	13. 12	7. 27	13. 09	7. 33	13. 06	7. 39	13. 02	7. 44
16	13. 99	7. 76	13. 96	7. 82	13. 93	7. 88	13. 89	7. 94
17	14. 87	8. 24	14. 83	8. 31	14. 80	8. 37	14. 76	8. 44
18	15. 74	8. 73	15. 70	8. 80	15. 67	8. 86	15. 63	8. 93
19	16. 62	9. 21	16. 58	9. 28	16. 54	9. 36	16. 50	9. 43
20	17. 49	9. 70	17. 45	9. 77	17. 41	9. 85	17. 36	9. 92
21	18. 37	10. 18	18. 32	10. 26	18. 28	10. 34	18. 23	10. 42
22	19. 24	10. 67	19. 19	10. 75	19. 15	10. 83	19. 10	10. 92
23	20. 12	11. 15	20. 07	11. 24	20. 02	11. 33	19. 97	11. 41
24	20. 99	11. 64	20. 94	11. 73	20. 89	11. 82	20. 84	11. 91
25	21. 87	12. 12	21. 81	12. 22	21. 76	12. 31	21. 70	12. 41
26	22. 74	12. 60	22. 68	12. 70	22. 63	12. 80	22. 57	12. 90
27	23. 61	13. 09	23. 56	13. 19	23. 50	13. 30	23. 44	13. 40
28	24. 49	13. 57	24. 43	13. 68	24. 37	13. 79	24. 31	13. 89
29	25. 36	14. 06	25. 30	14. 17	25. 24	14. 28	25. 18	14. 39
30	26. 24	14. 54	26. 17	14. 66	26. 11	14. 77	26. 05	14. 89
35	30. 61	16. 97	30. 54	17. 10	30. 46	17. 23	30. 39	17. 37
40	34. 98	19. 39	34. 90	19. 54	34. 81	19. 70	34. 73	19. 85
45	39. 36	21. 82	39. 26	21. 99	39. 17	22. 16	39. 07	22. 33
50	43. 73	24. 24	43. 62	24. 43	43. 52	24. 62	43. 41	24. 81
55	48. 10	26. 66	47. 99	26. 87	47. 87	27. 08	47. 75	27. 29
60	52. 48	29. 09	52. 35	29. 32	52. 22	29. 55	52. 09	29. 77
65	56. 85	31. 51	56. 71	31. 76	56. 57	32. 01	56. 43	32. 25
70	61. 22	33. 94	61. 07	34. 20	60. 92	34. 47	60. 77	34. 74
75	65. 60	36. 36	65. 44	36. 65	65. 28	36. 93	65. 11	37. 22
80	69. 97	38. 78	69. 80	39. 09	69. 63	39. 39	69. 46	39. 70
85	74. 34	41. 21	74. 16	41. 53	73. 98	41. 86	73. 80	42. 18
90	78. 72	43. 63	78. 52	43. 98	78. 33	44. 32	78. 14	44. 66
95	83. 09	46. 06	82. 89	46. 42	82. 68	46. 78	82. 48	47. 14
100	87. 46	48. 48	87. 25	48. 86	87. 04	49. 24	86. 82	49. 62
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.
	61 Deg.		60¾ Deg.		60½ Deg.		60¼ Deg.	

Distance.	30 Deg.		30¼ Deg.		30½ Deg.		30¾ Deg.	
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.
1	0. 87	0. 50	0. 86	0. 50	0. 86	0. 51	0. 86	0. 51
2	1. 73	1. 00	1. 73	1. 01	1. 72	1. 02	1. 72	1. 02
3	2. 60	1. 50	2. 59	1. 51	2. 58	1. 52	2. 58	1. 53
4	3. 46	2. 00	3. 46	2. 02	3. 45	2. 03	3. 44	2. 05
5	4. 33	2. 50	4. 32	2. 52	4. 31	2. 54	4. 30	2. 56
6	5. 20	3. 00	5. 18	3. 02	5. 17	3. 05	5. 16	3. 07
7	6. 06	3. 50	6. 05	3. 53	6. 03	3. 55	6. 02	3. 58
8	6. 93	4. 00	6. 91	4. 03	6. 89	4. 06	6. 88	4. 09
9	7. 79	4. 50	7. 77	4. 53	7. 75	4. 57	7. 73	4. 60
10	8. 66	5. 00	8. 64	5. 04	8. 62	5. 08	8. 59	5. 11
11	9. 53	5. 50	9. 50	5. 54	9. 48	5. 58	9. 45	5. 62
12	10. 39	6. 00	10. 37	6. 05	10. 34	6. 09	10. 31	6. 14
13	11. 26	6. 50	11. 23	6. 55	11. 20	6. 60	11. 17	6. 65
14	12. 12	7. 00	12. 09	7. 05	12. 06	7. 11	12. 03	7. 16
15	12. 99	7. 50	12. 96	7. 56	12. 92	7. 61	12. 89	7. 67
16	13. 86	8. 00	13. 82	8. 06	13. 79	8. 12	13. 75	8. 18
17	14. 72	8. 50	14. 69	8. 56	14. 65	8. 63	14. 61	8. 69
18	15. 59	9. 00	15. 55	9. 07	15. 51	9. 14	15. 47	9. 20
19	16. 45	9. 50	16. 41	9. 57	16. 37	9. 64	16. 33	9. 71
20	17. 32	10. 00	17. 28	10. 08	17. 23	10. 15	17. 19	10. 23
21	18. 19	10. 50	18. 14	10. 58	18. 09	10. 66	18. 05	10. 74
22	19. 05	11. 00	19. 00	11. 08	18. 96	11. 17	18. 91	11. 25
23	19. 92	11. 50	19. 87	11. 59	19. 82	11. 67	19. 77	11. 76
24	20. 78	12. 00	20. 73	12. 09	20. 68	12. 18	20. 63	12. 27
25	21. 65	12. 50	21. 60	12. 59	21. 54	12. 69	21. 49	12. 78
26	22. 52	13. 00	22. 46	13. 10	22. 40	13. 20	22. 34	13. 29
27	23. 38	13. 50	23. 32	13. 60	23. 26	13. 70	23. 20	13. 80
28	24. 25	14. 00	24. 19	14. 11	24. 13	14. 21	24. 06	14. 32
29	25. 11	14. 50	25. 05	14. 61	24. 99	14. 72	24. 92	14. 83
30	25. 98	15. 00	25. 92	15. 11	25. 85	15. 23	25. 78	15. 34
35	30. 31	17. 50	30. 23	17. 63	30. 16	17. 76	30. 08	17. 90
40	34. 64	20. 00	34. 55	20. 15	34. 47	20. 30	34. 38	20. 45
45	38. 97	22. 50	38. 87	22. 67	38. 77	22. 84	38. 67	23. 01
50	43. 30	25. 00	43. 19	25. 19	43. 08	25. 38	42. 97	25. 56
55	47. 63	27. 50	47. 51	27. 71	47. 39	27. 91	47. 27	28. 12
60	51. 96	30. 00	51. 83	30. 23	51. 70	30. 45	51. 56	30. 68
65	56. 29	32. 50	56. 15	32. 75	56. 01	32. 99	55. 86	33. 23
70	60. 62	35. 00	60. 47	35. 26	60. 31	35. 53	60. 16	35. 79
75	64. 95	37. 50	64. 79	37. 78	64. 62	38. 07	64. 46	38. 35
80	69. 28	40. 00	69. 11	40. 30	68. 93	40. 60	68. 75	40. 90
85	73. 61	42. 50	73. 43	42. 82	73. 24	43. 14	73. 05	43. 46
90	77. 94	45. 00	77. 75	45. 34	77. 55	45. 68	77. 35	46. 02
95	82. 27	47. 50	82. 06	47. 86	81. 85	48. 22	81. 64	48. 57
100	86. 60	50. 00	86. 38	50. 38	86. 16	50. 75	85. 94	51. 13
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.
	60 Deg.		59¾ Deg.		59½ Deg.		59¼ Deg.	

Distance.	31 Deg.		31¼ Deg.		31½ Deg.		31¾ Deg.	
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.
1	0.86	0.51	0.85	0.52	0.85	0.52	0.85	0.53
2	1.71	1.03	1.71	1.04	1.71	1.04	1.70	1.05
3	2.57	1.55	2.56	1.56	2.56	1.57	2.55	1.58
4	3.43	2.06	3.42	2.08	3.41	2.09	3.40	2.10
5	4.29	2.58	4.27	2.59	4.26	2.61	4.25	2.63
6	5.14	3.09	5.13	3.11	5.12	3.13	5.10	3.16
7	6.00	3.61	5.98	3.63	5.97	3.66	5.95	3.68
8	6.86	4.12	6.84	4.15	6.82	4.18	6.80	4.21
9	7.71	4.64	7.69	4.67	7.67	4.70	7.65	4.74
10	8.57	5.15	8.55	5.19	8.53	5.22	8.50	5.26
11	9.43	5.67	9.40	5.71	9.38	5.75	9.35	5.79
12	10.29	6.18	10.26	6.23	10.23	6.27	10.20	6.31
13	11.14	6.70	11.11	6.74	11.08	6.79	11.05	6.84
14	12.00	7.21	11.97	7.26	11.94	7.31	11.90	7.37
15	12.86	7.73	12.82	7.78	12.79	7.84	12.76	7.89
16	13.71	8.24	13.68	8.30	13.64	8.36	13.61	8.42
17	14.57	8.76	14.53	8.82	14.49	8.88	14.46	8.95
18	15.43	9.27	15.39	9.34	15.35	9.40	15.31	9.47
19	16.29	9.79	16.24	9.86	16.20	9.93	16.16	10.00
20	17.14	10.30	17.10	10.38	17.05	10.45	17.01	10.52
21	18.00	10.82	17.95	10.89	17.91	10.97	17.86	11.05
22	18.86	11.33	18.81	11.41	18.76	11.49	18.71	11.58
23	19.71	11.85	19.66	11.93	19.61	12.02	19.56	12.10
24	20.57	12.36	20.52	12.45	20.46	12.54	20.41	12.63
25	21.43	12.88	21.37	12.97	21.32	13.06	21.26	13.16
26	22.29	13.39	22.23	13.49	22.17	13.58	22.11	13.68
27	23.14	13.91	23.08	14.01	23.02	14.11	22.96	14.21
28	24.00	14.42	23.94	14.53	23.87	14.63	23.81	14.73
29	24.86	14.94	24.79	15.04	24.73	15.15	24.66	15.26
30	25.71	15.45	25.65	15.56	25.58	15.67	25.51	15.79
35	30.00	18.03	29.92	18.16	29.84	18.29	29.76	18.42
40	34.29	20.60	34.20	20.75	34.11	20.90	34.01	21.05
45	38.57	23.18	38.47	23.34	38.37	23.51	38.27	23.68
50	42.86	25.75	42.75	25.94	42.63	26.12	42.52	26.31
55	47.14	28.33	47.02	28.53	46.90	28.74	46.77	28.94
60	51.43	30.90	51.29	31.13	51.16	31.35	51.02	31.57
65	55.72	33.48	55.57	33.72	55.42	33.96	55.27	34.20
70	60.00	36.05	59.84	36.31	59.68	36.57	59.52	36.83
75	64.29	38.63	64.12	38.91	63.95	39.19	63.78	39.47
80	68.57	41.20	68.39	41.50	68.21	41.80	68.03	42.10
85	72.86	43.78	72.67	44.10	72.47	44.41	72.28	44.73
90	77.15	46.35	76.94	46.69	76.74	47.02	76.53	47.36
95	81.43	48.93	81.22	49.28	81.00	49.64	80.78	49.99
100	85.72	51.50	85.49	51.88	85.26	52.25	85.04	52.62
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.
	59 Deg.		58¾ Deg.		58½ Deg.		58¼ Deg.	

Distance.	32 Deg.		32¼ Deg.		32½ Deg.		32¾ Deg.	
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.
1	0. 85	0. 53	0. 85	0. 53	0. 84	0. 54	0. 84	0. 54
2	1. 70	1. 06	1. 69	1. 07	1. 69	1. 07	1. 68	1. 08
3	2. 54	1. 59	2. 54	1. 60	2. 53	1. 61	2. 52	1. 62
4	3. 39	2. 12	3. 38	2. 13	3. 37	2. 15	3. 36	2. 16
5	4. 24	2. 65	4. 23	2. 67	4. 22	2. 69	4. 21	2. 70
6	5. 09	3. 18	5. 07	3. 20	5. 06	3. 22	5. 05	3. 25
7	5. 94	3. 71	5. 92	3. 74	5. 90	3. 76	5. 89	3. 79
8	6. 78	4. 24	6. 77	4. 27	6. 75	4. 30	6. 73	4. 33
9	7. 63	4. 77	7. 61	4. 80	7. 59	4. 84	7. 57	4. 87
10	8. 48	5. 30	8. 46	5. 34	8. 43	5. 37	8. 41	5. 41
11	9. 33	5. 83	9. 30	5. 87	9. 28	5. 91	9. 25	5. 95
12	10. 18	6. 36	10. 15	6. 40	10. 12	6. 45	10. 09	6. 49
13	11. 02	6. 89	10. 99	6. 94	10. 96	6. 98	10. 93	7. 03
14	11. 87	7, 42	11. 84	7. 47	11. 81	7. 52	11. 77	7. 57
15	12. 72	7. 95	12. 69	8. 00	12. 65	8. 06	12. 62	8. 11
16	13. 57	8. 48	13. 53	8. 54	13. 49	8. 60	13. 46	8. 66
17	14. 42	9. 01	14. 38	9. 07	14. 84	9. 13	14. 30	9. 20
18	15. 26	9. 54	15. 22	9. 61	15. 18	9. 67	15. 14	9. 74
19	16. 11	10. 07	16. 07	10. 14	16. 02	10. 21	15. 98	10. 28
20	16. 96	10. 60	16. 91	10. 67	16. 87	10. 75	16. 82	10. 82
21	17. 81	11. 13	17. 76	11. 21	17. 71	11. 28	17. 66	11. 36
22	18. 66	11. 66	18. 61	11. 74	18. 55	11. 82	18. 50	11. 90
23	19. 51	12. 19	19. 45	12. 27	19. 40	12. 36	19. 34	12. 44
24	20. 35	12. 72	20. 30	12. 81	20. 24	12. 90	20. 18	12. 98
25	21. 20	13. 25	21. 14	13. 34	21. 08	13. 43	21. 03	13. 52
26	22. 05	13. 78	21. 99	13. 87	21. 93	13. 97	21. 87	14. 07
27	22. 90	14. 31	22. 83	14. 41	22. 77	14. 51	22. 71	14. 61
28	23. 75	14. 84	23. 68	14. 94	23. 61	15. 04	23. 55	15. 15
29	24. 59	15. 37	24. 53	15. 47	24. 46	15. 58	24. 39	15. 69
30	25. 44	15. 90	25. 37	16. 01	25. 30	16. 12	25. 23	16. 23
35	29. 68	18. 55	29. 60	18. 68	29. 52	18. 81	29. 44	18. 93
40	33. 92	21. 20	33. 83	21. 34	33. 74	21. 49	33. 64	21. 64
45	38. 16	23. 85	38. 06	24. 01	37. 95	24. 18	37. 85	24. 34
50	42. 40	26. 50	42. 29	26. 68	42. 17	26. 86	42. 05	27. 05
55	46. 64	29. 15	46. 51	29. 35	46. 39	29. 55	46. 26	29. 75
60	50. 88	31. 80	50. 74	32. 02	50. 60	32. 24	50. 46	32. 46
65	55. 12	34. 44	54. 97	34. 68	54. 82	34. 92	54. 67	35. 16
70	59. 36	37. 09	59. 20	37. 35	59. 04	37. 61	58. 87	37. 87
75	63. 60	39. 74	63. 43	40. 02	63. 25	40. 30	63. 08	40. 57
80	67. 84	42. 39	67. 66	42. 69	67. 47	42. 98	67. 28	43. 28
85	72. 08	45. 04	71. 89	45. 36	71. 69	45. 67	71. 49	45. 98
90	76. 32	47. 69	76. 12	48. 03	75. 91	48. 36	75. 69	48. 69
95	80. 56	50. 34	80. 34	50. 69	80. 12	51. 04	79. 90	51. 39
100	84. 80	52. 99	84. 57	53. 36	84. 34	53. 73	84. 10	54. 10
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.
	58 Deg.		57¾ Deg.		57½ Deg.		57¼ Deg.	

Distance.	33 Deg.		33¼ Deg.		33½ Deg.		33¾ Deg.	
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.
1	0. 84	0. 54	0. 84	0. 55	0. 83	0. 55	0. 83	0. 56
2	1. 68	1. 09	1. 67	1. 10	1. 67	1. 10	1. 66	1. 11
3	2. 52	1. 63	2. 51	1. 64	2. 50	1. 66	2. 49	1. 67
4	3. 35	2. 18	3. 35	2. 19	3. 34	2. 21	3. 33	2. 22
5	4. 19	2. 72	4. 18	2. 74	4. 17	2. 76	4. 16	2. 78
6	5. 03	3. 27	5. 02	3. 29	5. 00	3. 31	4. 99	3. 33
7	5. 87	3. 81	5. 85	3. 84	5. 84	3. 86	5. 82	3. 89
8	6. 71	4. 36	6. 69	4. 39	6. 67	4. 42	6. 65	4. 44
9	7. 55	4. 90	7. 53	4. 93	7. 50	4. 97	7. 48	5. 00
10	8. 39	5. 45	8. 36	5. 48	8. 34	5. 52	8. 31	5. 56
11	9. 23	5. 99	9. 20	6. 03	9. 17	6. 07	9. 15	6. 11
12	10. 06	6. 54	10. 04	6. 58	10. 01	6. 62	9. 98	6. 67
13	10. 90	7. 08	10. 87	7. 13	10. 84	7. 18	10. 81	7. 22
14	11. 74	7. 62	11. 71	7. 68	11. 67	7. 73	11. 64	7. 78
15	12. 58	8. 17	12. 54	8. 22	12. 51	8. 28	12. 47	8. 33
16	13. 42	8. 71	13. 38	8. 77	13. 34	8. 83	13. 30	8. 89
17	14. 26	9. 26	14. 22	9. 32	14. 18	9. 38	14. 13	9. 44
18	15. 10	9. 80	15. 05	9. 87	15. 01	9. 93	14. 97	10. 00
19	15. 93	10. 35	15. 89	10. 42	15. 84	10. 49	15. 80	10. 56
20	16. 77	10. 89	16. 73	10. 97	16. 68	11. 04	16. 63	11. 11
21	17. 61	11. 44	17. 56	11. 51	17. 51	11. 59	17. 46	11. 67
22	18. 45	11. 98	18. 40	12. 06	18. 35	12. 14	18. 29	12. 22
23	19. 29	12. 53	19. 23	12. 61	19. 18	12. 69	19. 12	12. 78
24	20. 13	13. 07	20. 07	13. 16	20. 01	13. 25	19. 96	13. 33
25	20. 97	13. 62	20. 91	13. 71	20. 85	13. 80	20. 79	13. 89
26	21. 81	14. 16	21. 74	14. 26	21. 68	14. 35	21. 62	14. 44
27	22. 64	14. 71	22. 58	14. 80	22. 51	14. 90	22. 45	15. 00
28	23. 48	15. 25	23. 42	15. 35	23. 35	15. 45	23. 28	15. 56
29	24. 32	15. 79	24. 25	15. 90	24. 18	16. 01	24. 11	16. 11
30	25. 16	16. 34	25. 09	16. 45	25. 02	16. 56	24. 94	16. 67
35	29. 35	19. 06	29. 27	19. 19	29. 19	19. 32	29. 10	19. 44
40	33. 55	21. 79	33. 45	21. 93	33. 36	22. 08	33. 26	22. 22
45	37. 74	24. 51	37. 63	24. 67	37. 52	24. 84	37. 42	25. 00
50	41. 93	27. 23	41. 81	27. 41	41. 69	27. 60	41. 57	27. 78
55	46. 13	29. 96	46. 00	30. 16	45. 86	30. 36	45. 73	30. 56
60	50. 32	32. 68	50. 18	32. 90	50. 03	33. 12	49. 89	33. 33
65	54. 51	35. 40	54. 36	35. 64	54. 20	35. 88	54. 05	36. 11
70	58. 71	38. 12	58. 54	38. 38	58. 37	38. 64	58. 20	38. 89
75	62. 90	40. 85	62. 72	41. 12	62. 54	41. 40	62. 36	41. 67
80	67. 09	43. 57	66. 90	43. 86	66. 71	44. 15	66. 52	44. 45
85	71. 29	46. 29	71. 08	46. 60	70. 88	46. 91	70. 67	47. 22
90	75. 48	49. 02	75. 27	49. 35	75. 05	49. 67	74. 83	50. 00
95	79. 67	51. 74	79. 45	52. 09	79. 22	52. 43	78. 99	52. 78
100	83. 87	54. 46	83. 63	54. 83	83. 39	55. 19	83. 15	55. 56
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.
	57 Deg.		56¾ Deg.		56½ Deg.		56¼ Deg.	

Distance.	34 Deg.		34¼ Deg.		34½ Deg.		34¾ Deg.	
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep
1	0.83	0.56	0.83	0.56	0.82	0.57	0.82	0.57
2	1.66	1.12	1.65	1.13	1.65	1.13	1.64	1.14
3	2.49	1.68	2.48	1.69	2.47	1.70	2.46	1.71
4	3.32	2.24	3.31	2.25	3.30	2.27	3.29	2.28
5	4.15	2.80	4.13	2.81	4.12	2.83	4.11	2.85
6	4.97	3.36	4.96	3.38	4.94	3.40	4.93	3.42
7	5.80	3.91	5.79	3.94	5.77	3.96	5.75	3.99
8	6.63	4.47	6.61	4.50	6.59	4.53	6.57	4.56
9	7.46	5.03	7.44	5.07	7.42	5.10	7.39	5.13
10	8.29	5.59	8.27	5.63	8.24	5.66	8.22	5.70
11	9.12	6.15	9.09	6.19	9.07	6.23	9.04	6.27
12	9.95	6.71	9.92	6.75	9.89	6.80	9.86	6.84
13	10.78	7.27	10.75	7.32	10.71	7.36	10.68	7.41
14	11.61	7.83	11.57	7.88	11.54	7.93	11.50	7.98
15	12.44	8.39	12.40	8.44	12.36	8.50	12.32	8.55
16	13.26	8.95	13.23	9.00	13.19	9.06	13.15	9.12
17	14.09	9.51	14.05	9.57	14.01	9.63	13.97	9.69
18	14.92	10.07	14.88	10.13	14.83	10.20	14.79	10.26
19	15.75	10.62	15.71	10.69	15.66	10.76	15.61	10.83
20	16.58	11.18	16.53	11.26	16.48	11.33	16.43	11.40
21	17.41	11.74	17.36	11.82	17.31	11.89	17.25	11.97
22	18.24	12.30	18.18	12.38	18.13	12.46	18.08	12.54
23	19.07	12.86	19.01	12.94	18.95	13.03	18.90	13.11
24	19.90	13.42	19.84	13.51	19.78	13.59	19.72	13.68
25	20.73	13.98	20.66	14.07	20.60	14.16	20.54	14.25
26	21.55	14.54	21.49	14.63	21.43	14.73	21.36	14.82
27	22.38	15.10	22.32	15.20	22.25	15.29	22.18	15.39
28	23.21	15.66	23.14	15.76	23.08	15.86	23.01	15.96
29	24.04	16.22	23.97	16.32	23.90	16.48	23.83	16.53
30	24.87	16.78	24.80	16.88	24.72	16.99	24.65	17.10
35	29.02	19.57	28.93	19.70	28.84	19.82	28.76	19.95
40	33.16	22.37	33.06	22.51	32.97	22.66	32.87	22.80
45	37.31	25.16	37.20	25.33	37.09	25.49	36.97	25.65
50	41.45	27.96	41.33	28.14	41.21	28.32	41.08	28.50
55	45.60	30.76	45.46	30.95	45.33	31.15	45.19	31.35
60	49.74	33.55	49.60	33.77	49.45	33.98	49.30	34.20
65	53.89	36.35	53.73	36.58	53.57	36.82	53.41	37.05
70	58.03	39.14	57.86	39.40	57.69	39.65	57.52	39.90
75	62.18	41.94	61.99	42.21	61.81	42.48	61.62	42.75
80	66.32	44.74	66.13	45.02	65.98	45.31	65.78	45.60
85	70.47	47.53	70.26	47.84	70.05	48.14	69.84	48.45
90	74.61	50.33	74.39	50.65	74.17	50.98	73.95	51.30
95	78.76	53.12	78.53	53.47	78.29	53.81	78.06	54.15
100	82.90	55.92	82.66	56.28	82.41	56.64	82.16	57.00
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.
	56 Deg.		55¾ Deg.		55½ Deg.		55¼ Deg.	

Distance.	35 Deg.		35¼ Deg.		35½ Deg.		35¾ Deg.	
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.
1	0. 82	0. 57	0. 82	0. 58	0. 81	0. 58	0. 81	0. 58
2	1. 64	1. 15	1. 63	1. 15	1. 63	1. 16	1. 62	1. 17
3	2. 46	1. 72	2. 45	1. 73	2. 44	1. 74	2. 43	1. 75
4	3. 28	2. 29	3. 27	2. 31	3. 26	2. 32	3. 25	2. 34
5	4. 10	2. 87	4. 08	2. 89	4. 07	2. 90	4. 06	2. 92
6	4. 91	3. 44	4. 90	3. 46	4. 88	3. 48	4. 87	3. 51
7	5. 73	4. 01	5. 72	4. 04	5. 70	4. 06	5. 68	4. 09
8	6. 55	4. 59	6. 53	4. 62	6. 51	4. 65	6. 49	4. 67
9	7. 37	5. 16	7. 35	5. 19	7. 33	5. 23	7. 30	5. 26
10	8. 19	5. 74	8. 17	5. 77	8. 14	5. 81	8. 12	5. 84
11	9. 01	6. 31	8. 98	6. 35	8. 96	6. 39	8. 93	6. 43
12	9. 83	6. 88	9. 80	6. 93	9. 77	6. 97	9. 74	7. 01
13	10. 65	7. 46	10. 62	7. 50	10. 58	7. 55	10. 55	7. 60
14	11. 47	8. 03	11. 43	8. 08	11. 40	8. 13	11. 36	8. 18
15	12. 29	8. 60	12. 25	8. 66	12. 21	8. 71	12. 17	8. 76
16	13. 11	9. 18	13. 07	9. 23	13. 03	9. 29	12. 99	9. 35
17	13. 93	9. 75	13. 88	9. 81	13. 84	9. 87	13. 80	9. 93
18	14. 74	10. 32	14. 70	10. 39	14. 65	10. 45	14. 61	10. 52
19	15. 56	10. 90	15. 52	10. 97	15. 47	11. 03	15. 42	11. 10
20	16. 38	11. 47	16. 33	11. 54	16. 28	11. 61	16. 23	11. 68
21	17. 20	12. 05	17. 15	12. 12	17. 10	12. 19	17. 04	12. 27
22	18. 02	12. 62	17. 97	12. 70	17. 91	12. 78	17. 85	12. 85
23	18. 84	13. 19	18. 78	13. 27	18. 72	13. 36	18. 67	13. 44
24	19. 66	13. 77	19. 60	13. 85	19. 54	13. 94	19. 48	14. 02
25	20. 48	14. 34	20. 42	14. 43	20. 35	14. 52	20. 29	14. 61
26	21. 30	14. 91	21. 23	15. 01	21. 17	15. 10	21. 10	15. 19
27	22. 12	15. 49	22. 05	15. 58	21. 98	15. 68	21. 91	15. 77
28	22. 94	16. 06	22. 87	16. 16	22. 80	16. 26	22. 72	16. 36
29	23. 76	16. 63	23. 68	16. 74	23. 61	16. 84	23. 54	16. 94
30	24. 57	17. 21	24. 50	17. 31	24. 42	17. 42	24. 35	17. 58
35	28. 67	20. 08	28. 58	20. 20	28. 49	20. 32	28. 41	20. 45
40	32. 77	22. 94	32. 67	23. 09	32. 56	23. 23	32. 46	23. 37
45	36. 86	25. 81	36. 75	25. 97	36. 64	26. 13	36 52	26. 29
50	40. 96	28. 68	40. 83	28. 86	40. 71	29. 04	40. 58	29. 21
55	45. 05	31. 55	44. 92	31. 74	44. 78	31. 94	44. 64	32. 13
60	49. 15	34. 41	49. 00	34. 63	48. 85	34. 84	48. 69	35. 05
65	53. 24	37. 28	53. 08	37. 51	52. 92	37. 75	52. 75	37. 98
70	57. 34	40. 15	57. 16	40. 40	56. 99	40. 65	56. 81	40. 90
75	61. 44	43. 02	61. 25	43. 29	61. 06	43. 55	60. 87	43. 82
80	65. 53	45. 89	65. 33	46. 17	65. 13	46. 46	64. 93	46. 74
85	69. 63	48. 75	69. 41	49. 06	69. 20	49. 36	68. 98	49. 66
90	73. 72	51. 62	73. 50	51. 94	73. 27	52. 26	73. 04	52. 58
95	77. 82	54. 49	77. 58	54. 83	77. 34	55. 17	77. 10	55. 50
100	81. 92	57. 36	81. 66	57. 71	81. 41	58. 07	81. 16	58. 42
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.
	55 Deg.		54¾ Deg.		54½ Deg.		54¼ Deg.	

Distance.	36 Deg.		36¼ Deg.		36½ Deg.		36¾ Deg.	
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.
1	0.81	0.59	0.81	0.59	0.80	0.59	0.80	0.60
2	1.62	1.18	1.61	1.18	1.61	1.19	1.60	1.20
3	2.43	1.76	2.42	1.77	2.41	1.78	2.40	1.79
4	3.24	2.35	3.23	2.37	3.22	2.38	3.20	2.39
5	4.05	2.94	4.03	2.96	4.02	2.97	4.01	2.99
6	4.85	3.53	4.84	3.55	4.82	3.57	4.81	3.59
7	5.66	4.11	5.65	4.14	5.63	4.16	5.61	4.19
8	6.47	4.70	6.45	4.73	6.43	4.76	6.41	4.79
9	7.28	5.29	7.26	5.32	7.23	5.35	7.21	5.38
10	8.09	5.88	8.06	5.91	8.04	5.95	8.01	5.98
11	8.90	6.47	8.87	6.50	8.84	6.54	8.81	6.58
12	9.71	7.05	9.68	7.10	9.65	7.14	9.61	7.18
13	10.52	7.64	10.48	7.69	10.45	7.73	10.42	7.78
14	11.33	8.23	11.29	8.28	11.25	8.33	11.22	8.38
15	12.14	8.82	12.10	8.87	12.06	8.92	12.02	8.97
16	12.94	9.40	12.90	9.46	12.86	9.52	12.82	9.57
17	13.75	9.99	13.71	10.05	13.67	10.11	13.62	10.17
18	14.56	10.58	14.52	10.64	14.47	10.71	14.42	10.77
19	15.37	11.17	15.32	11.23	15.27	11.30	15.22	11.37
20	16.18	11.76	16.13	11.83	16.08	11.90	16.03	11.97
21	16.99	12.34	16.94	12.42	16.88	12.49	16.83	12.56
22	17.80	12.93	17.74	13.01	17.68	13.09	17.63	13.16
23	18.61	13.52	18.55	13.60	18.49	13.68	18.43	13.76
24	19.42	14.11	19.35	14.19	19.29	14.28	19.23	14.36
25	20.23	14.69	20.16	14.78	20.10	14.87	20.03	14.96
26	21.03	15.28	20.97	15.37	20.90	15.47	20.83	15.56
27	21.84	15.87	21.77	15.97	21.70	16.06	21.63	16.15
28	22.65	16.46	22.58	16.56	22.51	16.65	22.44	16.75
29	23.46	17.05	23.39	17.15	23.31	17.25	23.24	17.35
30	24.27	17.63	24.19	17.74	24.12	17.84	24.04	17.95
35	28.32	20.57	28.23	20.70	28.13	20.82	28.04	20.94
40	32.36	23.51	32.26	23.65	32.15	23.79	32.05	23.93
45	36.41	26.45	36.29	26.61	36.17	26.77	36.06	26.92
50	40.45	29.39	40.32	29.57	40.19	29.74	40.06	29.92
55	44.50	32.33	44.35	32.52	44.21	32.72	44.07	32.91
60	48.54	35.27	48.39	35.48	48.23	35.69	48.08	35.90
65	52.59	38.21	52.42	38.44	52.25	38.66	52.08	38.89
70	56.63	41.14	56.45	41.39	56.27	41.64	56.09	41.88
75	60.68	44.08	60.48	44.35	60.29	44.61	60.09	44.87
80	64.72	47.02	64.52	47.30	64.31	47.59	64.10	47.87
85	68.77	49.96	68.55	50.26	68.33	50.56	68.11	50.86
90	72.81	52.90	72.58	53.22	72.35	53.53	72.11	53.85
95	76.86	55.84	76.61	56.17	76.37	56.51	76.12	56.84
100	80.90	58.78	80.64	59.13	80.39	59.48	80.13	59.83
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.
	54 Deg.		53¾ Deg.		53½ Deg.		53¼ Deg.	

Distance.	37 Deg.		37¼ Deg.		37½ Deg.		37¾ Deg.	
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.
1	0.80	0.60	0.80	0.61	0.79	0.61	0.79	0.61
2	1.60	1.20	1.59	1.21	1.59	1.22	1.58	1.22
3	2.40	1.81	2.39	1.82	2.38	1.83	2.37	1.84
4	3.19	2.41	3.18	2.42	3.17	2.43	3.16	2.45
5	3.99	3.01	3.98	3.03	3.97	3.04	3.95	3.06
6	4.79	3.61	4.78	3.63	4.76	3.65	4.74	3.67
7	5.59	4.21	5.57	4.24	5.55	4.26	5.53	4.29
8	6.39	4.81	6.37	4.84	6.35	4.87	6.33	4.90
9	7.19	5.42	7.16	5.45	7.14	5.48	7.12	5.51
10	7.99	6.02	7.96	6.05	7.93	6.09	7.91	6.12
11	8.78	6.62	8.76	6.66	8.73	6.70	8.70	6.73
12	9.58	7.22	9.55	7.26	9.52	7.31	9.49	7.35
13	10.38	7.82	10.35	7.87	10.31	7.91	10.28	7.96
14	11.18	8.43	11.14	8.47	11.11	8.52	11.07	8.57
15	11.98	9.03	11.94	9.08	11.90	9.13	11.86	9.18
16	12.78	9.63	12.74	9.68	12.69	9.74	12.65	9.80
17	13.58	10.23	13.53	10.29	13.49	10.35	13.44	10.41
18	14.38	10.83	14.33	10.90	14.28	10.96	14.23	11.02
19	15.17	11.43	15.12	11.50	15.07	11.57	15.02	11.63
20	15.97	12.04	15.92	12.11	15.87	12.18	15.81	12.24
21	16.77	12.64	16.72	12.71	16.66	12.78	16.60	12.86
22	17.57	13.24	17.51	13.32	17.45	13.39	17.40	13.47
23	18.37	13.84	18.31	13.92	18.25	14.00	18.19	14.08
24	19.17	14.44	19.10	14.53	19.04	14.61	18.98	14.69
25	19.97	15.05	19.90	15.13	19.83	15.22	19.77	15.31
26	20.76	15.65	20.70	15.74	20.63	15.83	20.56	15.92
27	21.56	16.25	21.49	16.34	21.42	16.44	21.35	16.53
28	22.36	16.85	22.29	16.95	22.21	17.05	22.14	17.14
29	23.16	17.45	23.08	17.55	23.01	17.65	22.93	17.75
30	23.96	18.05	23.88	18.16	23.80	18.26	23.72	18.37
35	27.95	21.06	27.86	21.19	27.77	21.31	27.67	21.43
40	31.95	24.07	31.84	24.21	31.73	24.35	31.63	24.49
45	35.94	27.08	35.82	27.24	35.70	27.39	35.58	27.55
50	39.93	30.09	39.80	30.26	39.67	30.44	39.53	30.61
55	43.92	33.10	43.78	33.29	43.63	33.48	43.49	33.67
60	47.92	36.11	47.76	36.32	47.60	36.53	47.44	36.73
65	51.91	39.12	51.74	39.34	51.57	39.57	51.39	39.79
70	55.90	42.13	55.72	42.37	55.53	42.61	55.35	42.86
75	59.90	45.14	59.70	45.40	59.50	45.66	59.30	45.92
80	63.89	48.15	63.68	48.42	63.47	48.70	63.26	48.98
85	67.88	51.15	67.66	51.45	67.43	51.74	67.21	52.04
90	71.88	54.16	71.64	54.48	71.40	54.79	71.16	55.10
95	75.87	57.17	75.62	57.50	75.37	57.83	75.12	58.16
100	79.86	60.18	79.60	60.53	79.34	60.88	79.07	61.22
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.
	53 Deg.		52¾ Deg.		52½ Deg.		52¼ Deg.	

Distance.	38 Deg.		38¼ Deg.		38½ Deg.		38¾ Deg.	
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.
1	0. 79	0. 62	0. 79	0. 62	0. 78	0. 62	0. 78	0. 63
2	1. 58	1. 23	1. 57	1. 24	1. 57	1. 24	1. 56	1. 25
3	2. 36	1. 85	2. 36	1. 86	2. 35	1. 87	2. 34	1. 88
4	3. 15	2. 46	3. 14	2. 48	3. 13	2. 49	3. 12	2. 50
5	3. 94	3. 08	3. 93	3. 10	3. 91	3. 11	3. 90	3. 13
6	4. 73	3. 69	4. 71	3. 71	4. 70	3. 74	4. 68	3. 76
7	5. 52	4. 31	5. 50	4. 33	5. 48	4. 36	5. 46	4. 38
8	6. 30	4. 93	6. 28	4. 95	6. 26	4. 98	6. 24	5. 01
9	7. 09	5. 54	7. 07	5. 57	7. 04	5. 60	7. 02	5. 63
10	7. 88	6. 16	7. 85	6. 19	7. 83	6. 23	7. 80	6. 26
11	8. 67	6. 77	8. 64	6. 81	8. 61	6. 85	8. 58	6. 89
12	9. 46	7. 39	9. 42	7. 43	9. 39	7. 47	9. 36	7. 51
13	10. 24	8. 00	10. 21	8. 05	10. 17	8. 09	10. 14	8. 14
14	11. 03	8. 62	10. 99	8. 67	10. 96	8. 72	10. 92	8. 76
15	11. 82	9. 23	11. 78	9. 29	11. 74	9. 34	11. 70	9. 39
16	12. 61	9. 85	12. 57	9. 91	12. 52	9. 96	12. 48	10. 01
17	13. 40	10. 47	~~13. 35~~	~~10. 52~~	13. 30	10. 58	13. 26	10. 64
18	14. 18	11. 08	14. 14	11. 14	14. 09	11. 21	14. 04	11. 27
19	14. 97	11. 70	14. 92	11. 76	14. 87	11. 83	14. 82	11. 89
20	15. 76	12. 31	15. 71	12. 38	15. 65	12. 45	15. 60	12. 52
21	16. 55	12. 93	16. 49	13. 00	16. 43	13. 07	16. 38	13. 14
22	17. 34	13. 54	17. 28	13. 62	17. 22	13. 70	17. 16	13. 77
23	18. 12	14. 16	18. 06	14. 24	18. 00	14. 32	17. 94	14. 40
24	18. 91	14. 78	18. 85	14. 86	18. 78	14. 94	18. 72	15. 02
25	19. 70	15. 39	19. 63	15. 48	19. 57	15. 56	19. 50	15. 65
26	20. 49	16. 01	20. 42	16. 10	20. 35	16. 19	20. 28	16. 27
27	21. 28	16. 62	21. 20	16. 72	21. 13	16. 81	21. 06	16. 90
28	22. 06	17. 24	21. 99	17. 33	21. 91	17. 43	21. 84	17. 53
29	22. 85	17. 85	22. 77	17. 95	22. 70	18. 05	22. 62	18. 15
30	23. 64	18. 47	23. 56	18. 57	23. 48	18. 68	23. 40	18. 78
35	27. 58	21. 55	27. 49	21. 67	27. 39	21. 79	27. 30	21. 91
40	31. 52	24. 63	31. 41	24. 76	31. 30	24. 90	31. 20	25. 04
45	35. 46	27. 70	35. 34	27. 86	35. 22	28. 01	35. 09	28. 17
50	39. 40	30. 78	39. 27	30. 95	39. 13	31. 13	38. 99	31. 30
55	43. 34	33. 86	43. 19	34. 05	43. 04	34. 24	42. 89	34. 43
60	47. 28	36. 94	47. 12	37. 15	46. 96	37. 35	46. 79	37. 56
65	51. 22	40. 02	51. 05	40. 24	50. 87	40. 46	50. 69	40. 68
70	55. 16	43. 10	54. 97	43. 34	54. 78	43. 58	54. 59	43. 81
75	59. 10	46. 17	58. 90	46. 43	58. 70	46. 69	58. 49	46. 94
80	63. 04	49. 25	62. 83	49. 53	62. 61	49. 80	62. 39	50. 07
85	66. 98	52. 33	66. 75	52. 62	66. 52	52. 91	66. 29	53. 20
90	70. 92	55. 41	70. 68	55. 72	70. 43	56. 03	70. 19	56. 33
95	74. 86	58. 49	74. 61	58. 81	74. 35	59. 14	74. 09	59. 46
100	78. 80	61. 57	78. 53	61. 91	78. 26	62. 25	77. 99	62. 59
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.
	52 Deg.		51¾ Deg.		51½ Deg.		51¼ Deg.	

Distance.	39 Deg.		39¼ Deg.		39½ Deg.		39¾ Deg.	
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.
1	0.78	0.63	0.77	0.63	0.77	0.64	0.77	0.64
2	1.55	1.26	1.55	1.27	1.54	1.27	1.54	1.28
3	2.33	1.89	2.32	1.90	2.31	1.91	2.31	1.92
4	3.11	2.52	3.10	2.53	3.09	2.54	3.08	2.56
5	3.89	3.15	3.87	3.16	3.86	3.18	3.84	3.20
6	4.66	3.78	4.65	3.80	4.63	3.82	4.61	3.84
7	5.44	4.41	5.42	4.43	5.40	4.45	5.38	4.48
8	6.22	5.03	6.20	5.06	6.17	5.09	6.15	5.12
9	6.99	5.66	6.97	5.69	6.94	5.72	6.92	5.75
10	7.77	6.29	7.74	6.33	7.72	6.36	7.69	6.39
11	8.55	6.92	8.52	6.96	8.49	7.00	8.46	7.03
12	9.33	7.55	9.29	7.59	9.26	7.63	9.23	7.67
13	10.10	8.18	10.07	8.23	10.03	8.27	9.99	8.31
14	10.88	8.81	10.84	8.86	10.80	8.91	10.76	8.95
15	11.66	9.44	11.62	9.49	11.57	9.54	11.53	9.59
16	12.43	10.07	12.39	10.12	12.35	10.18	12.30	10.23
17	13.21	10.70	13.16	10.76	13.12	10.81	13.07	10.87
18	13.99	11.33	13.94	11.39	13.89	11.45	13.84	11.51
19	14.77	11.96	14.71	12.02	14.66	12.09	14.61	12.15
20	15.54	12.59	15.49	12.65	15.43	12.72	15.38	12.79
21	16.32	13.22	16.26	13.29	16.20	13.36	16.15	13.43
22	17.10	13.84	17.04	13.92	16.98	13.99	16.91	14.07
23	17.87	14.47	17.81	14.55	17.75	14.63	17.68	14.71
24	18.65	15.10	18.59	15.18	18.52	15.27	18.45	15.35
25	19.43	15.73	19.36	15.82	19.29	15.90	19.22	15.99
26	20.21	16.36	20.13	16.45	20.06	16.54	19.99	16.63
27	20.98	16.99	20.91	17.08	20.83	17.17	20.76	17.26
28	21.76	17.62	21.68	17.72	21.61	17.81	21.53	17.90
29	22.54	18.25	22.46	18.35	22.38	18.45	22.30	18.54
30	23.31	18.88	23.23	18.98	23.15	19.08	23.07	19.18
35	27.20	22.03	27.10	22.14	27.01	22.26	26.91	22.38
40	31.09	25.17	30.98	25.31	30.86	25.44	30.75	25.58
45	34.97	28.32	34.85	28.47	34.72	28.62	34.60	28.77
50	38.86	31.47	38.72	31.64	38.58	31.80	38.44	31.97
55	42.74	34.61	42.59	34.80	42.44	34.98	42.29	35.17
60	46.63	37.76	46.46	37.96	46.30	38.16	46.13	38.37
65	50.51	40.91	50.34	41.13	50.16	41.35	49.97	41.56
70	54.40	44.05	54.21	44.29	54.01	44.53	53.82	44.76
75	58.29	47.20	58.08	47.45	57.87	47.71	57.66	47.96
80	62.17	50.35	61.95	50.62	61.73	50.89	61.51	51.16
85	66.06	53.49	65.82	53.78	65.59	54.07	65.35	54.35
90	69.94	56.64	69.70	56.94	69.45	57.25	69.20	57.55
95	73.83	59.79	73.57	60.11	73.30	60.43	73.04	60.75
100	77.71	62.93	77.44	63.27	77.16	63.61	76.88	63.94
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.
	51 Deg.		50¾ Deg.		50½ Deg.		50¼ Deg.	

Distance	40 Deg.		40¼ Deg.		40½ Deg.		40¾ Deg.	
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.
1	0. 77	0. 64	0. 76	0. 65	0. 76	0. 65	0. 76	0. 65
2	1. 53	1. 29	1. 53	1. 29	1. 52	1. 30	1. 52	1. 31
3	2. 30	1. 93	2. 29	1. 94	2. 28	1. 95	2. 27	1. 96
4	3. 06	2. 57	3. 05	2. 58	3. 04	2. 60	3. 03	2. 61
5	3. 83	3. 21	3. 82	3. 23	3. 80	3. 25	3. 79	3. 26
6	4. 60	3. 86	4. 58	3. 88	4. 56	3. 90	4. 55	3. 92
7	5. 36	4. 50	5. 34	4. 52	5. 32	4. 55	5. 30	4. 57
8	6. 13	5. 14	6. 11	5. 17	6. 08	5. 20	6. 06	5. 22
9	6. 89	5. 79	6. 87	5. 82	6. 84	5. 85	6. 82	5. 87
10	7. 66	6. 43	7. 63	6. 46	7. 60	6. 49	7. 58	6. 53
11	8. 43	7. 07	8. 40	7. 11	8. 36	7. 14	8. 33	7. 18
12	9. 19	7. 71	9. 16	7. 75	9. 12	7. 79	9. 09	7. 83
13	9. 96	8. 36	9. 92	8. 40	9. 89	8. 44	9. 85	8. 49
14	10. 72	9. 00	10. 69	9. 05	10. 65	9. 09	10. 61	9. 14
15	11. 49	9. 64	11. 45	9. 69	11. 41	9. 74	11. 36	9. 79
16	12. 26	10. 28	12. 21	10. 34	12. 17	10. 39	12. 12	10. 44
17	13. 02	10. 93	12. 97	10. 98	12. 93	11. 04	12. 88	11. 10
18	13. 79	11. 57	13. 74	11. 63	13. 69	11. 69	13. 64	11. 75
19	14. 55	12. 21	14. 50	12. 28	14. 45	12. 34	14. 39	12. 40
20	15. 32	12. 86	15. 26	12. 92	15. 21	12. 99	15. 15	13. 06
21	16. 09	13. 50	16. 03	13. 57	15. 97	13. 64	15. 91	13. 71
22	16. 85	14. 14	16. 79	14. 21	16. 73	14. 29	16. 67	14. 36
23	17. 62	14. 78	17. 55	14. 86	17. 49	14. 94	17. 42	15. 01
24	18. 39	15. 43	18. 32	15. 51	18. 25	15. 59	18. 18	15. 67
25	19. 15	16. 07	19. 08	16. 15	19. 01	16. 24	18. 94	16. 32
26	19. 92	16. 71	19. 84	16. 80	19. 77	16. 89	19. 70	16. 97
27	20. 68	17. 36	20. 61	17. 45	20. 53	17. 54	20. 45	17. 62
28	21. 45	18. 00	21. 37	18. 09	21. 29	18. 18	21. 21	18. 28
29	22. 22	18. 64	22. 13	18. 74	22. 05	18. 83	21. 97	18. 93
30	22. 98	19. 28	22. 90	19. 38	22. 81	19. 48	22. 73	19. 58
35	26. 81	22. 50	26. 71	22. 61	26. 61	22. 73	26. 51	22. 85
40	30. 64	25. 71	30. 53	25. 84	30. 42	25. 98	30. 30	26. 11
45	34. 47	28. 93	34. 35	29. 08	34. 22	29. 23	34. 09	29. 37
50	38. 30	32. 14	38. 16	32. 31	38. 02	32. 47	37. 88	32. 64
55	42. 13	35. 35	41. 98	35. 54	41. 82	35. 72	41. 67	35. 90
60	45. 96	38. 57	45. 79	38. 77	45. 62	38. 97	45. 45	39. 17
65	49. 79	41. 78	49. 61	42. 00	49. 43	42. 21	49. 24	42. 43
70	53. 62	45. 00	53. 43	45. 23	53. 23	45. 46	53. 03	45. 69
75	57. 45	48. 21	57. 24	48. 46	57. 03	48. 71	56. 82	48. 96
80	61. 28	51. 42	61. 06	51. 69	60. 83	51. 96	60. 61	52. 22
85	65. 11	54. 64	64. 87	54. 92	64. 63	55. 20	64. 39	55. 48
90	68. 94	57. 85	68. 69	58. 15	68. 44	58. 45	68. 18	58. 75
95	72. 77	61. 06	72. 51	61. 38	72. 24	61. 70	71. 97	62. 01
100	76. 60	64. 28	76. 32	64. 61	76. 04	64. 94	75. 76	65. 28
Distance	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.
	50 Deg.		49¾ Deg.		49½ Deg.		49¼ Deg.	

Distance.	41 Deg.		41¼ Deg.		41½ Deg.		41¾ Deg.	
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.
1	0. 75	0. 66	0. 75	0. 66	0. 75	0. 66	0. 75	0. 67
2	1. 51	1. 31	1. 50	1. 32	1. 50	1. 33	1. 49	1. 33
3	2. 26	1. 97	2. 26	1. 98	2. 25	1. 99	2. 24	2. 00
4	3. 02	2. 62	3. 01	2. 64	3. 00	2. 65	2. 98	2. 66
5	3. 77	3. 28	3. 76	3. 30	3. 74	3. 31	3. 73	3. 33
6	4. 53	3. 94	4. 51	3. 96	4. 49	3. 98	4. 48	4. 00
7	5. 28	4. 59	5. 26	4. 62	5. 24	4. 64	5. 22	4. 66
8	6. 04	5. 25	6. 01	5. 27	5. 99	5. 30	5. 97	5. 33
9	6. 79	5. 90	6. 77	5. 93	6. 74	5. 96	6. 71	5. 99
10	7. 55	6. 56	7. 52	6. 59	7. 49	6. 63	7. 46	6. 66
11	8. 30	7. 22	8. 27	7. 25	8. 24	7. 29	8. 21	7. 32
12	9. 06	7. 87	9. 02	7. 91	8. 99	7. 95	8. 95	7. 99
13	9. 81	8. 53	9. 77	8. 57	9. 74	8. 61	9. 70	8. 66
14	10. 57	9. 18	10. 53	9. 23	10. 49	9. 28	10. 44	9. 32
15	11. 32	9. 84	11. 28	9. 89	11. 23	9. 94	11. 19	9. 99
16	12. 08	10. 50	12. 03	10. 55	11. 98	10. 60	11. 94	10. 65
17	12. 83	11. 15	12. 78	11. 21	12. 73	11. 26	12. 68	11. 32
18	13. 58	11. 81	13. 53	11. 87	13. 48	11. 93	13. 43	11. 99
19	14. 34	12. 47	14. 28	12. 53	14. 23	12. 59	14. 18	12. 65
20	15. 09	13. 12	15. 04	13. 19	14. 98	13. 25	14. 92	13. 32
21	15. 85	13. 78	15. 79	13. 85	15. 73	13. 91	15. 67	13. 98
22	16. 60	14. 43	16. 54	14. 51	16. 48	14. 58	16. 41	14. 65
23	17. 36	15. 09	17. 29	15. 16	17. 23	15. 24	17. 16	15. 32
24	18. 11	15. 75	18. 04	15. 82	17. 97	15. 00	17. 91	15. 98
25	18. 87	16. 40	18. 80	16. 48	18. 72	16. 57	18. 65	16. 65
26	19. 62	17. 06	19. 55	17. 14	19. 47	17. 23	19. 40	17. 31
27	20. 38	17. 71	20. 30	17. 80	20. 22	17. 89	20. 14	17. 98
28	21. 13	18. 37	21. 05	18. 46	20. 97	18. 55	20. 89	18. 64
29	21. 89	19. 03	21. 80	19. 12	21. 72	19. 22	21. 64	19. 31
30	22. 64	19. 68	22. 56	19. 78	22. 47	19. 88	22. 38	19. 98
35	26. 41	22. 96	26. 31	23. 08	26. 21	23. 19	26. 11	23. 31
40	30. 19	26. 24	30. 07	26. 37	29. 96	26. 50	29. 84	26. 64
45	33. 96	29. 52	33. 83	29. 67	33. 70	29. 82	33. 57	29. 97
50	37. 74	32. 80	37. 59	32. 97	37. 45	33. 13	37. 30	33. 29
55	41. 51	36. 08	41. 35	36. 26	41. 19	36. 44	41. 03	36. 62
60	45. 28	39. 36	45. 11	39. 56	44. 94	39. 76	44. 76	39. 95
65	49. 06	42. 64	48. 87	42. 86	48. 68	43. 07	48. 49	43. 28
70	52. 83	45. 92	52. 63	46. 15	52. 43	46. 38	52. 22	46. 61
75	56. 60	49. 20	56. 39	49. 45	56. 17	49. 70	55. 95	49. 94
80	60. 38	52. 48	60. 15	52. 75	59. 92	53. 01	59. 68	53. 27
85	64. 15	55. 76	63. 91	56. 01	63. 66	56. 32	63. 41	56. 60
90	67. 92	59. 05	67. 67	59. 34	67. 41	59. 64	67. 15	59. 93
95	71. 70	62. 33	71. 43	62. 64	71. 15	62. 95	70. 88	63. 26
100	75. 47	65. 61	75. 18	65. 93	74. 90	66. 26	74. 61	66. 59
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.
	49 Deg.		48¾ Deg.		48½ Deg.		48¼ Deg.	

Distance.	42 Deg.		42¼ Deg.		42½ Deg.		42¾ Deg.	
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.
1	0. 74	0. 67	0. 74	0. 67	0. 74	0. 68	0. 73	0. 68
2	1. 49	1. 34	1. 48	1. 34	1. 47	1. 35	1. 47	1. 36
3	2. 23	2. 01	2. 22	2. 02	2. 21	2. 03	2. 20	2. 04
4	2. 97	2. 68	2. 96	2. 69	2. 95	2. 70	2. 94	2. 72
5	3. 72	3. 35	3. 70	3. 36	3. 69	3. 38	3. 67	3. 39
6	4. 46	4. 01	4. 44	4. 03	4. 42	4. 05	4. 41	4. 07
7	5. 20	4. 68	5. 18	4. 71	5. 16	4. 73	5. 14	4. 75
8	5. 95	5. 35	5. 92	5. 38	5. 90	5. 40	5. 87	5. 43
9	6. 69	6. 02	6. 66	6. 05	6. 64	6. 08	6. 61	6. 11
10	7. 43	6. 69	7. 40	6. 72	7. 37	6. 76	7. 34	6. 79
11	8. 17	7. 36	8. 14	7. 40	8. 11	7. 43	8. 08	7. 47
12	8. 92	8. 03	8. 88	8. 07	8. 85	8. 11	8. 81	8. 15
13	9. 66	8. 70	9. 62	8. 74	9. 58	8. 78	9. 55	8. 82
14	10. 40	9. 37	10. 36	9. 41	10. 32	9. 46	10. 28	9. 50
15	11. 15	10. 04	11. 10	10. 09	11. 06	10. 13	11. 01	10. 18
16	11. 89	10. 71	11. 84	10. 76	11. 80	10. 81	11. 75	10. 86
17	12. 63	11. 38	12. 58	11. 43	12. 53	11. 48	12. 48	11. 54
18	13. 38	12. 04	13. 32	12. 10	13. 27	12. 16	13. 22	12. 22
19	14. 12	12. 71	14. 06	12. 77	14. 01	12. 84	13. 95	12. 90
20	14. 86	13. 38	14. 80	13. 45	14. 75	13. 51	14. 69	13. 58
21	15. 61	14. 05	15. 54	14. 12	15. 48	14. 19	15. 42	14. 25
22	16. 35	14. 72	16. 28	14. 79	16. 22	14. 86	16. 16	14. 93
23	17. 09	15. 39	17. 02	15. 46	16. 96	15. 54	16. 89	15. 61
24	17. 84	16. 06	17. 77	16. 14	17. 69	16. 21	17. 62	16. 29
25	18. 58	16. 73	18. 51	16. 81	18. 43	16. 89	18. 36	16. 97
26	19. 32	17. 40	19. 25	17. 48	19. 17	17. 57	19. 09	17. 65
27	20. 06	18. 07	19. 99	18. 15	19. 91	18. 24	19. 83	18. 33
28	20. 81	18. 74	20. 73	18. 83	20. 64	18. 92	20. 56	19. 01
29	21. 55	19. 40	21. 47	19. 50	21. 38	19. 59	21. 30	19. 69
30	22. 29	20. 07	22. 21	20. 17	22. 12	20. 27	22. 03	20. 36
35	26. 01	23. 42	25. 91	23. 53	25. 80	23. 65	25. 70	23. 76
40	29. 73	26. 77	29. 61	26. 89	29. 49	27. 02	29. 37	27. 15
45	33. 44	30. 11	33. 31	30. 26	33. 18	30. 40	33. 04	30. 55
50	37. 16	33. 46	37. 01	33. 62	36. 86	33. 78	36. 72	33. 94
55	40. 87	36. 80	40. 71	36. 98	40. 55	37. 16	40. 39	37. 33
60	44. 59	40. 15	44. 41	40. 34	44. 24	40. 54	44. 06	40. 73
65	48. 30	43. 49	48. 11	43. 70	47. 92	43. 91	47. 73	44. 12
70	52. 02	46. 84	51. 82	47. 07	51. 61	47. 29	51. 40	47. 52
75	55. 74	50. 18	55. 52	50. 43	55. 30	50. 67	55. 07	50. 91
80	59. 45	53. 53	59. 22	53. 79	58. 98	54. 05	58. 75	54. 30
85	63. 17	56. 88	62. 92	57. 15	62. 67	57. 43	62. 42	57. 70
90	66. 88	60. 22	66. 62	60. 51	66. 35	60. 80	66. 09	61. 09
95	70. 60	63. 57	70. 32	63. 87	70. 04	64. 18	69. 76	64. 49
100	74. 31	66. 61	74. 02	67. 24	73. 73	67. 56	73. 43	67. 88
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.
	48 Deg.		47¾ Deg.		47½ Deg.		47¼ Deg.	

Distance.	43 Deg.		43¼ Deg.		43½ Deg.		4 ¾ Deg.	
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.
1	0.73	0.68	0.73	0.69	0.73	0.69	0.72	0.69
2	1.46	1.36	1.46	1.37	1.45	1.38	1.44	1.38
3	2.19	2.05	2.19	2.06	2.18	2.07	2.17	2.07
4	2.93	2.73	2.91	2.74	2.90	2.75	2.89	2.77
5	3.66	3.41	3.64	3.43	3.63	3.44	3.61	3.46
6	4.39	4.09	4.37	4.11	4.35	4.13	4.33	4.15
7	5.12	4.77	5.10	4.80	5.08	4.82	5.06	4.84
8	5.85	5.46	5.83	5.48	5.80	5.51	5.78	5.53
9	6.58	6.14	6.56	6.17	6.53	6.20	6.50	6.22
10	7.31	6.82	7.28	6.85	7.25	6.88	7.22	6.92
11	8.04	7.50	8.01	7.54	7.98	7.57	7.95	7.61
12	8.78	8.18	8.74	8.22	8.70	8.26	8.67	8.30
13	9.51	8.87	9.47	8.91	9.43	8.95	9.39	8.99
14	10.24	9.55	10.20	9.59	10.16	9.64	10.11	9.68
15	10.97	10.23	10.93	10.28	10.88	10.33	10.84	10.37
16	11.70	10.91	11.65	10.96	11.61	11.01	11.56	11.06
17	12.43	11.59	12.38	11.65	12.33	11.70	12.28	11.76
18	13.16	12.28	13.11	12.33	13.06	12.39	13.00	12.45
19	13.90	12.96	13.84	13.02	13.78	13.08	13.72	13.14
20	14.63	13.64	14.57	13.70	14.51	13.77	14.45	13.83
21	15.36	14.32	15.30	14.39	15.23	14.46	15.17	14.52
22	16.09	15.00	16.02	15.07	15.96	15.14	15.89	15.21
23	16.82	15.69	16.75	15.76	16.68	15.83	16.61	15.90
24	17.55	16.37	17.48	16.44	17.41	16.52	17.34	16.60
25	18.28	17.05	18.21	17.13	18.13	17.21	18.06	17.29
26	19.02	17.73	18.94	17.81	18.86	17.90	18.78	17.98
27	19.75	18.41	19.67	18.50	19.59	18.59	19.50	18.67
28	20.48	19.10	20.39	19.19	20.31	19.27	20.23	19.36
29	21.21	19.78	21.12	19.87	21.04	19.96	20.95	20.05
30	21.94	20.46	21.85	20.56	21.76	20.65	21.67	20.75
35	25.60	23.87	25.49	23.98	25.39	24.09	25.28	24.20
40	29.25	27.28	29.13	27.41	29.01	27.53	28.89	27.66
45	32.91	30.69	32.78	30.83	32.64	30.98	32.51	31.12
50	36.57	34.10	36.42	34.26	36.27	34.42	36.12	34.58
55	40.22	37.51	40.06	37.69	39.90	37.86	39.73	38.03
60	43.88	40.92	43.70	41.11	43.52	41.30	43.34	41.49
65	47.54	44.33	47.34	44.54	47.15	44.74	46.95	44.95
70	51.19	47.74	50.99	47.96	50.78	48.18	50.57	48.41
75	54.85	51.15	54.63	51.39	54.40	51.63	54.18	51.86
80	58.51	54.56	58.27	54.81	58.03	55.07	57.79	55.32
85	62.17	57.97	61.91	58.24	61.66	58.51	61.40	58.78
90	65.82	61.38	65.55	61.67	65.28	61.95	65.01	62.24
95	69.48	64.79	69.20	65.09	68.91	65.39	68.62	65.69
100	73.14	68.20	72.84	68.52	72.54	68.84	72.24	69.15
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.
	47 Deg.		46¾ Deg.		46½ Deg.		46¼ Deg.	

Distance.	44 Deg.		41¼ Deg.		44½ Deg.		44¾ Deg.		45 Deg.	
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.
1	0.72	0.69	0.72	0.70	0.71	0.70	0.71	0.71	0.71	0.71
2	1.44	1.39	1.43	1.40	1.43	1.40	1.42	1.41	1.41	1.41
3	2.16	2.08	2 15	2.09	2.14	2.10	2.13	2.11	2.12	2.12
4	2.88	2.78	2.87	2.79	2.85	2.80	2.84	2.82	2.83	2.83
5	3.60	3.47	3.58	3.49	3.57	3.50	3.55	3.52	3.54	3.54
6	4 32	4.17	4.30	4.19	4.28	4.21	4.26	4.22	4.24	4.24
7	5.04	4 86	5.01	4.88	4.99	4.91	4.97	4.93	4.95	4.95
8	5.75	5.56	5.73	5.58	5.71	5.61	5.68	5.63	5.66	5.66
9	6.47	6.25	6.45	6.28	6.42	6.31	6.39	6.34	6.36	6.36
10	7.19	6.95	7.16	6.98	7.13	7.01	7.10	7.04	7.07	7.07
11	7.91	7.64	7.88	7.68	7.85	7.71	7.81	7.74	7.78	7.78
12	8.63	8.34	8.60	8.37	8.56	8 41	8.52	8.45	8.49	8.49
13	9.35	9 03	9.31	9.07	9.27	9.11	9.23	9.15	9.19	9.19
14	10.07	9.73	10 03	9.77	9.99	9.81	9.94	9.86	9.90	9 90
15	10.79	10.42	10.74	10.74	10.70	10.51	10.65	10.56	10.61	10.61
16	11 51	11.11	11.46	11.16	11.41	11.21	11.36	11.26	11.31	11.31
17	12.23	11.81	12.18	11 86	12 13	11.92	12.07	11.97	12.02	12.02
18	12.95	12.50	12.89	12.56	12.84	12.62	12.78	12.67	12.73	12.73
19	13.67	13.20	13.61	13.26	13.55	13.32	13.49	13.38	13.43	13.43
20	14.39	13.89	14.33	13.96	14.26	14.02	14.20	14.08	14.14	14.14
21	15.11	14.59	15.04	14.65	14.98	14.72	14.91	14.78	14.85	14.85
22	15.83	15.28	15 76	15.35	15.69	15.42	15.62	15.49	15.56	15.56
23	16.54	15.98	16.47	16.05	16.40	16.12	16.33	16.19	16.26	16.26
24	17.26	16.67	17.19	16.75	17.12	16.82	17.04	16.90	16.97	16.97
25	17.98	17.37	17.91	17.44	17.83	17.52	17.75	17.60	17.68	17.68
26	18.70	18.06	18.62	18.14	18.54	18.22	18.46	18.30	18.38	18.38
27	19.42	18.76	19.34	18.84	19.26	18.92	19.17	19.01	19.09	19.09
28	20.14	19.45	20.06	19.54	19.97	19.63	19.89	19.71	19 80	19.80
29	20.86	20.15	20.77	20.24	20.68	20.33	20.60	20.42	20.51	20.51
30	21.58	20.84	21.49	20.93	21.40	21.03	21.31	21.12	21.21	21.21
35	25.18	24.31	25 07	24.42	24.96	24.53	24.86	24.64	24.75	24.75
40	28.77	27.79	28.65	27.91	28.53	28.04	28.41	28.16	28.28	28.28
45	32.37	31.26	32.23	31.40	32.10	31.54	31.96	31.68	31.82	31.82
50	35.97	34.73	35.82	34.89	35.66	35.05	35.51	35.20	35.36	35.36
55	39 56	38.21	39.40	38.38	39.23	38.55	39.06	38.72	38.89	38.89
60	43.16	41.68	42.98	41.87	42.79	42.05	42 61	42.24	42.43	42.43
65	46.76	45.15	46.56	45.36	46.36	45.56	46.16	45.76	45.96	45.96
70	50.35	48.63	50.14	48.85	49.93	49.06	49.71	49.28	49.50	49 50
75	53.95	52.10	53.72	52.33	53.49	52.57	53.26	52.80	53.03	53.03
80	57.55	55.57	57.30	55.82	57.06	56.07	56.81	56.32	56.57	56.57
85	61.14	59.05	60.89	59.31	60.63	59.58	60.37	59.84	60.10	60.10
90	64.74	62.52	64.47	62.80	64.19	63.08	63.92	63.36	63.64	63.64
95	68.34	65.99	68.05	66.29	67.76	66.59	67.47	66.88	67.18	67.18
100	71 93	69.47	71.63	69.78	71.33	70.09	71.02	70.40	70.71	70.71
Distance.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.
	46 Deg.		45¾ Deg.		45½ Deg.		45¼ Deg.		45 Deg.	

'	0°	1°	2°	3°	4°	5°	6°	7°	8°	9°	10°	11°	12°	13°	14°	15°
0	0	60	120	180	240	300	361	421	482	542	603	664	725	787	848	910
1	1	61	121	181	241	301	362	422	483	543	604	665	726	788	850	911
2	2	62	122	182	242	302	363	423	484	544	605	666	727	789	851	913
3	3	63	123	183	243	303	364	424	485	545	606	667	728	790	852	914
4	4	64	124	184	244	304	365	425	486	546	607	668	729	791	853	915
5	5	65	125	185	245	305	366	426	487	547	608	669	730	792	854	916
6	6	66	126	186	246	306	367	427	488	548	609	670	731	793	855	917
7	7	67	127	187	247	307	368	428	489	549	610	671	732	794	856	918
8	8	68	128	188	248	308	369	429	490	550	611	672	734	795	857	919
9	9	69	129	189	249	309	370	430	491	551	612	673	735	796	858	920
10	10	70	130	190	250	310	371	431	492	552	613	674	736	797	859	921
11	11	71	131	191	251	311	372	432	493	553	614	675	737	798	860	922
12	12	72	132	192	252	312	373	433	494	554	615	676	738	799	861	923
13	13	73	133	193	253	313	374	434	495	555	616	677	739	800	862	924
14	14	74	134	194	254	314	375	435	496	556	617	678	740	801	863	925
15	15	75	135	195	255	315	376	436	497	557	618	679	741	802	864	926
16	16	76	136	196	256	316	377	437	498	558	619	680	742	803	865	927
17	17	77	137	197	257	317	378	438	499	559	620	681	743	804	866	928
18	18	78	138	198	258	318	379	439	500	560	621	682	744	805	867	929
19	19	79	139	199	259	319	380	440	501	561	622	683	745	806	868	930
20	20	80	140	200	260	320	381	441	502	562	623	684	746	807	869	931
21	21	81	141	201	261	321	382	442	503	564	624	685	747	808	870	932
22	22	82	142	202	262	322	383	443	504	565	625	687	748	809	871	933
23	23	83	143	203	263	323	384	444	505	566	626	688	749	810	872	934
24	24	84	144	204	264	324	385	445	506	567	627	689	750	811	873	935
25	25	85	145	205	265	325	386	446	507	568	628	690	751	812	874	936
26	26	86	146	206	266	326	387	447	508	569	629	691	752	813	875	937
27	27	87	147	207	267	327	388	448	509	570	631	692	753	815	876	938
28	28	88	148	208	268	328	389	449	510	571	632	693	754	816	877	939
29	29	89	149	209	269	330	390	450	511	572	633	694	755	817	878	941
30	30	90	150	210	270	331	391	451	512	573	634	695	756	818	879	942
31	31	91	151	211	271	332	392	452	513	574	635	696	757	819	880	943
32	32	92	152	212	272	333	393	453	514	575	636	697	758	820	882	944
33	33	93	153	213	273	334	394	454	515	576	637	698	759	821	883	945
34	34	94	154	214	274	335	395	455	516	577	638	699	760	822	884	946
35	35	95	155	215	275	336	396	456	517	578	639	700	761	823	885	947
36	36	96	156	216	276	337	397	457	518	579	640	701	762	824	886	948
37	37	97	157	217	277	338	398	458	519	580	641	702	763	825	887	949
38	38	98	158	218	278	339	399	459	520	581	642	703	764	826	888	950
39	39	99	159	219	279	340	400	460	521	582	643	704	765	827	889	951
40	40	100	160	220	280	341	401	461	522	583	644	705	766	828	890	952
41	41	101	161	221	281	342	402	462	523	584	645	706	767	829	891	953
42	42	102	162	222	282	343	403	463	524	585	646	707	768	830	892	954
43	43	103	163	223	283	344	404	464	525	586	647	708	769	831	893	955
44	44	104	164	224	284	345	405	465	526	587	648	709	770	832	894	956
45	45	105	165	225	285	346	406	466	527	588	649	710	771	833	895	957
46	46	106	166	226	286	347	407	467	528	589	650	711	772	834	896	958
47	47	107	167	227	287	348	408	468	529	590	651	712	773	835	897	959
48	48	108	168	228	288	349	409	469	530	591	652	713	774	836	898	960
49	49	109	169	229	289	350	410	470	531	592	653	714	775	837	899	961
50	50	110	170	230	200	351	411	471	532	593	654	715	777	838	900	962
51	51	111	171	231	291	352	412	472	533	594	655	716	778	839	901	963
52	52	112	172	232	292	353	413	473	534	595	656	717	779	840	902	964
53	53	113	173	233	293	354	414	474	535	596	657	718	780	841	903	965
54	54	114	174	234	294	355	415	476	536	597	658	719	781	842	904	966
55	55	115	175	235	295	356	416	477	537	598	659	720	782	843	905	968
56	56	116	176	236	296	357	417	478	538	599	660	721	783	844	906	969
57	57	117	177	237	297	358	418	479	539	600	661	722	784	845	907	970
58	58	118	178	238	298	359	419	480	540	601	662	723	785	846	908	971
59	59	119	179	239	299	360	420	481	541	602	663	724	786	847	909	972

′	16°	17°	18°	19°	20°	21°	22°	23°	24°	25°	26°	27°	28°
0	973	1035	1098	1161	1225	1289	1354	1419	1484	1550	1616	1684	1751
1	974	1036	1099	1163	1226	1290	1355	1420	1485	1551	1618	1685	1752
2	975	1037	1100	1164	1227	1291	1356	1421	1486	1552	1619	1686	1753
3	976	1038	1101	1165	1228	1292	1357	1422	1487	1553	1620	1687	1755
4	977	1039	1102	1166	1229	1293	1358	1423	1488	1554	1621	1688	1756
5	978	1041	1103	1167	1230	1295	1359	1424	1490	1556	1622	1689	1757
6	979	1042	1105	1168	1232	1296	1360	1425	1491	1557	1623	1690	1758
7	980	1043	1106	1169	1233	1297	1361	1426	1492	1558	1624	1692	1759
8	981	1044	1107	1170	1234	1298	1362	1427	1493	1559	1625	1693	1760
9	982	1045	1108	1171	1235	1299	1363	1428	1494	1560	1626	1694	1761
10	983	1046	1109	1172	1236	1300	1364	1430	1495	1561	1628	1695	1762
11	984	1047	1110	1173	1237	1301	1366	1431	1496	1562	1629	1696	1764
12	985	1048	1111	1174	1238	1302	1367	1432	1497	1563	1630	1697	1765
13	986	1049	1112	1175	1239	1303	1368	1433	1498	1564	1631	1698	1766
14	987	1050	1113	1176	1240	1304	1369	1434	1499	1565	1632	1699	1767
15	988	1051	1114	1177	1241	1305	1370	1435	1500	1567	1633	1700	1768
16	989	1052	1115	1178	1242	1306	1371	1436	1502	1568	1634	1701	1769
17	990	1053	1116	1179	1243	1307	1372	1437	1503	1569	1635	1703	1770
18	991	1054	1117	1181	1244	1308	1373	1438	1504	1570	1637	1704	1772
19	893	1055	1118	1182	1245	1310	1374	1439	1505	1571	1638	1705	1773
20	994	1056	1119	1183	1246	1311	1375	1440	1506	1572	1639	1706	1774
21	995	1057	1120	1184	1248	1312	1376	1441	1507	1573	1640	1707	1775
22	996	1058	1121	1185	1249	1313	1377	1443	1508	1574	1641	1708	1776
23	997	1059	1122	1186	1250	1314	1379	1444	1509	1575	1642	1709	1777
24	998	1060	1123	1187	1251	1315	1380	1445	1510	1577	1643	1711	1778
25	999	1061	1125	1188	1252	1316	1381	1446	1511	1578	1644	1712	1780
26	1000	1063	1126	1189	1253	1317	1382	1447	1513	1579	1645	1713	1781
27	1001	1064	1127	1190	1254	1318	1383	1448	1514	1580	1647	1714	1782
28	1002	1065	1128	1191	1255	1319	1384	1449	1515	1581	1648	1715	1783
29	1003	1066	1129	1192	1256	1320	1385	1450	1516	1582	1649	1716	1784
30	1004	1067	1130	1193	1257	1321	1386	1451	1517	1583	1650	1717	1785
31	1005	1068	1131	1194	1258	1322	1387	1452	1518	1584	1651	1718	1786
32	1006	1069	1132	1195	1259	1324	1388	1453	1519	1585	1652	1720	1787
33	1007	1070	1133	1196	1260	1325	1389	1455	1520	1586	1653	1721	1789
34	1008	1071	1134	1198	1261	1326	1390	1456	1521	1588	1654	1722	1790
35	1009	1072	1135	1199	1262	1327	1392	1457	1522	1589	1656	1723	1791
36	1010	1073	1136	1200	1264	1328	1393	1458	1524	1590	1657	1724	1792
37	1011	1074	1137	1201	1265	1329	1394	1459	1525	1591	1658	1725	1793
38	1012	1075	1138	1202	1266	1330	1395	1460	1526	1592	1659	1726	1794
39	1013	1076	1139	1203	1267	1331	1396	1461	1527	1593	1660	1727	1795
40	1014	1077	1140	1204	1268	1332	1397	1462	1528	1594	1661	1729	1797
41	1015	1078	1141	1205	1269	1333	1398	1463	1529	1595	1662	1730	1798
42	1016	1079	1142	1206	1270	1334	1399	1464	1530	1596	1663	1731	1799
43	1018	1080	1144	1207	1271	1335	1400	1465	1531	1598	1664	1732	1800
44	1019	1081	1145	1208	1272	1336	1401	1467	1532	1599	1666	1733	1801
45	1020	1082	1146	1209	1273	1338	1402	1468	1533	1600	1667	1734	1802
46	1021	1084	1147	1210	1274	1339	1403	1469	1535	1601	1668	1735	1803
47	1022	1085	1148	1211	1275	1340	1405	1470	1536	1602	1669	1736	1805
48	1023	1086	1149	1212	1276	1341	1406	1471	1537	1603	1670	1737	1806
49	1024	1087	1150	1213	1277	1342	1407	1472	1538	1604	1671	1739	1807
50	1025	1088	1151	1215	1278	1343	1408	1473	1539	1605	1672	1740	1808
51	1026	1089	1152	1216	1280	1344	1409	1474	1540	1606	1673	1741	1809
52	1027	1090	1153	1217	1281	1345	1410	1475	1541	1608	1675	1742	1810
53	1028	1091	1154	1218	1282	1346	1411	1476	1542	1609	1676	1743	1811
54	1029	1092	1155	1219	1283	1347	1412	1477	1543	1610	1677	1744	1813
55	1030	1093	1156	1220	1284	1348	1413	1479	1544	1611	1678	1746	1814
56	1031	1094	1157	1221	1285	1349	1414	1480	1546	1612	1679	1747	1815
57	1032	1095	1158	1222	1286	1350	1415	1481	1547	1613	1680	1748	1816
58	1033	1096	1159	1223	1287	1352	1416	1482	1548	1614	1681	1749	1817
59	1034	1097	1160	1224	1288	1353	1418	1483	1549	1615	1682	1750	1818

′	29°	30°	31°	32°	33°	34°	35°	36°	37°	38°	39°	40°	41°
0	1819	1888	1958	2028	210	2171	2244	2318	2393	2468	2545	2623	2702
1	1821	1890	1959	2030	2101	2173	2246	2319	2394	2470	2546	2624	2703
2	1822	1891	1960	2031	2102	2174	2247	2320	2395	2471	2548	2625	2704
3	1823	1892	1962	2032	2103	2175	2248	2322	2396	2472	2549	2627	2706
4	1824	1893	1963	2033	2104	2176	2249	2323	2398	2473	2550	2628	2707
5	1825	1894	1964	2034	2105	2178	2250	2324	2399	2475	2551	2629	2708
6	1826	1895	1965	2035	2107	2179	2252	2325	2400	2476	2553	2631	2710
7	1827	1896	1966	2037	2108	2180	2253	2327	2401	2477	2554	2632	2711
8	1829	1898	1967	2038	2109	2181	2254	2328	2403	2478	2555	2633	2712
9	1830	1899	1969	2039	2110	2182	2255	2329	2404	2480	2557	2634	2714
10	1831	1900	1970	2040	2111	2184	2257	2330	2405	2481	2558	2636	2715
11	1832	1901	1971	2041	2113	2185	2258	2332	2406	2482	2559	2637	2716
12	1833	1902	1972	2043	2114	2186	2259	2333	2408	2484	2560	2638	2718
13	1834	1903	1973	2044	2115	2187	2260	2334	2409	2485	2562	2640	2719
14	1835	1905	1974	2045	2116	2188	2261	2335	2410	2486	2563	2641	2720
15	1837	1906	1976	2046	2117	2190	2263	2337	2411	2487	2564	2642	2722
16	1838	1907	1977	2047	2119	2191	2264	2338	2413	2489	2566	2644	2723
17	1839	1908	1978	2048	2120	2192	2265	2339	2414	2490	2567	2645	2724
18	1840	1909	1979	2050	2121	2193	2266	2340	2415	2491	2568	2646	2726
19	1841	1910	1980	2051	2122	2194	2268	2342	2416	2492	2569	2648	2727
20	1842	1912	1981	2052	2123	2196	2269	2343	2418	2494	2571	2649	2728
21	1843	1913	1983	2053	2125	2197	2270	2344	2419	2495	2572	2650	2729
22	1845	1914	1984	2054	2126	2198	2271	2345	2420	2496	2573	2651	2731
23	1846	1915	1985	2056	2127	2199	2272	2346	2422	2498	2575	2653	2732
24	1847	1916	1986	2057	2128	2200	2274	2348	2423	2499	2576	2654	2733
25	1848	1917	1987	2058	2129	2202	2275	2349	2424	2500	2577	2655	2735
26	1849	1918	1988	2059	2131	2203	2276	2350	2425	2501	2578	2657	2736
27	1850	1920	1990	2060	2132	2204	2277	2351	2427	2503	2580	2658	2737
28	1852	1921	1991	2061	2133	2205	2279	2353	2428	2504	2581	2659	2739
29	1853	1922	1992	2063	2134	2207	2280	2354	2429	2505	2582	2661	2740
30	1854	1923	1993	2064	2135	2208	2281	2355	2430	2506	2584	2662	2742
31	1855	1924	1994	2065	2137	2209	2282	2356	2432	2508	2585	2663	2743
32	1856	1925	1995	2066	2138	2210	2283	2358	2433	2509	2586	2665	2744
33	1857	1927	1997	2067	2139	2211	2285	2359	2434	2510	2588	2666	2746
34	1858	1928	1998	2069	2140	2213	2286	2360	2435	2512	2589	2667	2747
35	1860	1929	1999	2070	2141	2214	2287	2361	2437	2513	2590	2669	2748
36	1861	1930	2000	2071	2143	2215	2288	2363	2438	2514	2591	2670	2750
37	1862	1931	2001	2072	2144	2216	2290	2364	2439	2515	2593	2671	2751
38	1863	1932	2002	2073	2145	2217	2291	2365	2440	2517	2594	2673	2752
39	1864	1934	2004	2075	2146	2219	2292	2366	2442	2518	2595	2674	2754
40	1865	1935	2005	2076	2147	2220	2293	2368	2443	2519	2597	2675	2755
41	1866	1936	2006	2077	2149	2221	2295	2369	2444	2521	2598	2676	2756
42	1868	1937	2007	2078	2150	2222	2296	2370	2445	2522	2599	2678	2758
43	1869	1938	2008	2079	2151	2224	2297	2371	2447	2523	2601	2679	2759
44	1870	1939	2010	2080	2152	2225	2298	2373	2448	2524	2602	2680	2760
45	1871	1941	2011	2082	2153	2226	2299	2374	2449	2526	2603	2682	2762
46	1872	1942	2012	2083	2154	2227	2301	2375	2451	2527	2604	2683	2763
47	1873	1943	2013	2084	2156	2228	2302	2376	2452	2528	2606	2684	2764
48	1875	1944	2014	2085	2157	2230	2303	2378	2453	2530	2607	2686	2766
49	1876	1945	2015	2086	2158	2231	2304	2379	2454	2531	2608	2687	2767
50	1877	1946	2017	2088	2159	2232	2306	2380	2456	2532	2610	2688	2768
51	1878	1948	2018	2089	2161	2233	2307	2381	2457	2533	2611	2690	2770
52	1879	1949	2019	2090	2162	2235	2308	2383	2458	2535	2612	2691	2771
53	1880	1950	2020	2091	2163	2236	2309	2384	2459	2536	2614	2692	2772
54	1881	1951	2021	2092	2164	2237	2311	2385	2461	2537	2615	2694	2774
55	1883	1952	2022	2094	2165	2238	2312	2386	2462	2538	2616	2695	2775
56	1884	1953	2024	2095	2167	2239	2313	2388	2463	2540	2617	2696	2776
57	1885	1955	2025	2096	2168	224	2314	2389	2464	2541	2619	2698	2778
58	1886	1956	2026	2097	2169	2242	2316	2390	2466	2542	2620	2699	2779
59	1887	1957	2027	2098	2170	2243	2317	2391	2467	2544	2621	2700	2780

′	42°	43°	44°	45°	46°	47°	48°	49°	50°	51°	52°	53°	54°
0	2782	2863	2946	3030	3116	3203	3292	3382	3474	3569	3665	3764	3865
1	2783	2864	2947	3031	3117	3204	3293	3384	3476	3570	3667	3765	3866
2	2784	2866	2949	3033	3118	3206	3295	3385	3478	3572	3668	3767	3868
3	2786	2867	2950	3034	3120	3207	3296	3387	3479	3573	3670	3769	3870
4	2787	2869	2951	3036	3121	3209	3298	3388	3481	3575	3672	3770	3871
5	2788	2870	2953	3037	3123	3210	3299	3390	3482	3577	3673	3772	3873
6	2790	2871	2954	3038	3125	3212	3301	3391	3484	3578	3675	3774	3875
7	2791	2873	2956	3040	3126	3213	3302	3393	3485	3580	3677	3775	3877
8	2792	2874	2957	3041	3127	3214	3303	3394	3487	3582	3678	3777	3878
9	2794	2875	2958	3043	3129	3216	3305	3396	3488	3583	3680	3779	3880
10	2795	2877	2960	3044	3130	3217	3306	3397	3490	3585	3681	3780	3882
11	2797	2878	2961	3046	3131	3219	3308	3399	3492	3586	3683	3782	3883
12	2798	2880	2963	3047	3133	3220	3309	3400	3493	3588	3685	3784	3885
13	2799	2881	2964	3048	3134	3222	3311	3402	3495	3590	3686	3785	3887
14	2801	2882	2965	3050	3136	3224	3312	3403	3496	3591	3688	3787	3889
15	2802	2884	2967	3051	3137	3225	3314	3405	3498	3593	3690	3789	3890
16	2803	2885	2968	3053	3139	3226	3316	3407	3499	3594	3691	3790	3892
17	2805	2886	2970	3054	3140	3228	3317	3408	3501	3596	3693	3792	3894
18	2806	2888	2971	3055	3142	3229	3319	3410	3503	3598	3695	3794	3895
19	2807	2889	2972	3057	3143	3231	3320	3411	3504	3599	3696	3795	3897
20	2809	2891	2974	3058	3144	3232	3322	3413	3506	3601	3698	3797	3899
21	2810	2892	2975	3060	3146	3234	3323	3414	3507	3602	3699	3799	3901
22	2811	2893	2976	3061	3147	3235	3325	3416	3509	3604	3701	3800	3902
23	2813	2895	2978	3063	3149	3237	3326	3417	3510	3606	3703	3802	3904
24	2814	2896	2979	3064	3150	3238	3328	3419	3512	3607	3704	3804	3906
25	2815	2897	2981	3065	3152	3240	3329	3420	3514	3609	3706	3806	3907
26	2817	2899	2982	3067	3153	3241	3331	3422	3515	3610	3708	3807	3909
27	2818	2900	2983	3068	3155	3242	3332	3423	3517	3612	3709	3809	3911
28	2820	2902	2985	3070	3156	3244	3334	3425	3518	3614	3711	3811	3913
29	2821	2903	2986	3071	3157	3245	3335	3427	3520	3615	3713	3812	3914
30	9822	2904	2988	3073	3159	3247	3337	3428	3521	3617	3714	3814	3916
31	2824	2906	2989	3074	3160	3248	3338	3430	3523	3618	3716	3816	3918
32	2825	2907	2991	3075	3162	3250	3340	3431	3525	3620	3717	3817	3919
33	2826	2908	2992	3077	3163	3251	3341	3433	3526	3622	3719	3819	3921
34	2828	2910	2993	3078	3165	3253	3343	3434	3528	3623	3721	3821	3923
35	2829	2911	2995	3080	3166	3254	3344	3436	3529	3625	3722	3822	3925
36	2830	2913	2996	3081	3168	3256	3346	3437	3531	3626	3724	3824	3926
37	2832	2914	2998	3083	3169	3257	3347	3439	3532	3628	3726	3826	3928
38	2833	2915	2999	3084	3171	3259	3349	3440	3534	3630	3727	3827	3930
39	2834	2917	3000	3085	3172	3260	3350	3442	3536	3631	3729	3829	3932
40	2836	2918	3002	3087	3173	3262	3352	3443	3537	3633	3731	3831	3933
41	2837	2919	3003	3088	3175	3263	3353	3445	3539	3634	3732	3832	3935
42	2839	2921	3005	3090	3176	3265	3355	3447	3540	3636	3734	3834	3937
43	2840	2922	3006	3091	3178	3266	3356	3448	3542	3638	3736	3836	3938
44	2841	2924	3007	3093	3179	3268	3358	3450	3543	3639	3737	3838	3940
45	2843	2925	3009	3094	3181	3269	3359	3451	3545	3641	3739	3839	3942
46	2844	2926	3010	3095	3182	3271	3361	3453	3547	3643	3741	3841	3944
47	2845	2928	3012	3097	3184	3272	3362	3454	3548	3644	3742	3843	3945
48	2847	2929	3013	3098	3185	3274	3364	3456	3550	3646	3744	3844	3947
49	2848	2931	3014	3100	3187	3275	3365	3457	3551	3647	3746	3846	3949
50	2849	2932	3016	3101	3188	3277	3367	3459	3553	3649	3747	3848	3951
51	2851	2933	3017	3103	3190	3278	3368	3460	3555	3651	3749	3849	3952
52	2852	2935	3019	3104	3191	3280	3370	3462	3556	3652	3750	3851	3954
53	2854	2936	3020	3105	3192	3281	3371	3464	3558	3654	3752	3853	3956
54	2855	2937	3021	3107	3194	3283	3373	3465	3559	3655	3754	3854	3958
5	2856	2939	3023	3108	3195	3284	3374	3467	3561	3657	3755	3856	3959
56	2858	2940	3024	3110	3197	3286	3376	3468	3562	3659	3757	3858	3961
57	2859	2942	3026	3111	3198	3287	3378	3470	3564	3660	3759	3860	3963
58	2860	2943	3027	3113	3200	3289	3379	3471	3566	3662	3760	3861	3964
59	2862	2944	3029	3114	3201	3290	3381	3473	3567	3664	3762	3863	3966

′	55°	56°	57°	58°	59°	60°	61°	62°	63°	64°	65°	66°	67°
0	3968	4074	4183	4294	4409	4527	4649	4775	4905	5039	5179	5324	5474
1	3970	4076	4184	4296	4411	4529	4651	4777	4907	5042	5181	5326	5477
2	3971	4077	4186	4298	4413	4531	4653	4779	4909	5044	5184	5328	5479
3	3973	4079	4188	4300	4415	4533	4655	4781	4912	5046	5186	5331	5482
4	3975	4081	4190	4302	4417	4535	4657	4784	4914	5049	5188	5333	5484
5	3977	4083	4192	4304	4419	4537	4660	4786	4916	5051	5191	5336	5487
6	3978	4085	4194	4306	4421	4539	4662	4788	4918	5053	5193	5338	5489
7	3980	4086	4195	4308	4423	4541	4664	4790	4920	5055	5195	5341	5492
8	3982	4088	4197	4309	4425	4543	4666	4792	4923	5058	5198	5343	5495
9	3984	4090	4199	4311	4427	4545	4668	4794	4925	5060	5200	5346	5497
10	3985	4092	4202	4313	4429	4547	4670	4796	4927	5062	5203	5348	5500
11	3987	4094	4203	4315	4431	4549	4672	4798	4929	5065	5205	5351	5502
12	3989	4095	4205	4317	4433	4551	4674	4801	4931	5067	5207	5353	5505
13	3991	4097	4207	4319	4434	4553	4676	4803	4934	5069	5210	5356	5507
14	3992	4099	4208	4321	4436	4555	4678	4805	4936	5071	5212	5358	5510
15	3994	4101	4210	4323	4438	4557	4680	4807	4938	5074	5214	5361	5513
16	3996	4103	4212	4325	4440	4559	4682	4809	4940	5076	5217	5363	5515
17	3998	4104	4214	4327	4442	4562	4684	4811	4943	5078	5219	5366	5518
18	3999	4106	4216	4328	4444	4564	4687	4814	4945	5081	5222	5368	5520
19	4001	4108	4218	4330	4446	4566	4689	4816	4947	5083	5224	5371	5523
20	4003	4110	4220	4332	4448	4568	4691	4818	4949	5085	5226	5373	5526
21	4005	4112	4221	4334	4450	4570	4693	4820	4951	5088	5229	5376	5528
22	4006	4113	4223	4336	4452	4572	4695	4822	4954	5090	5231	5378	5531
23	4008	4115	4225	4338	4454	4574	4697	4824	4956	5092	5234	5380	5533
24	4010	4117	4227	4340	4456	4576	4699	4826	4958	5095	5236	5383	5536
25	4012	4119	4229	4342	4458	4578	4701	4829	4960	5097	5238	5385	5539
26	4014	4121	4231	4344	4460	4580	4703	4831	4963	5099	5241	5388	5541
27	4015	4122	4232	4346	4462	4582	4705	4833	4965	5102	5243	5390	5544
28	4017	4124	4234	4347	4464	4584	4707	4835	4967	5104	5246	5393	5546
29	4019	4126	4236	4349	4466	4586	4710	4837	4969	5106	5248	5395	5549
30	4021	4128	4238	4351	4468	4588	4712	4839	4972	5108	5250	5398	5552
31	4022	4130	4240	4353	4470	4590	4714	4842	4974	5111	5253	5401	5554
32	4024	4132	4242	4355	4472	4592	4716	4844	4976	5113	5255	5403	5557
33	4026	4133	4244	4357	4474	4594	4718	4846	4978	5115	5258	5406	5559
34	4028	4135	4246	4359	4476	4596	4720	4848	4981	5118	5260	5408	5562
35	4029	4137	4247	4361	4478	4598	4722	4850	4983	5120	5263	5411	5565
36	4031	4139	4249	4363	4480	4600	4724	4852	4985	5122	5265	5413	5567
37	4033	4141	4251	4365	4482	4602	4726	4855	4987	5125	5267	5416	5570
38	4035	4142	4253	4367	4484	4604	4728	4857	4990	5127	5270	5418	5573
39	4037	4144	4255	4369	4486	4606	4731	4859	4992	5129	5272	5421	5575
40	4038	4146	4257	4370	4488	4608	4733	4861	4994	6132	5275	5423	5578
41	4040	4148	4259	4372	4490	4610	4735	4863	4996	5134	5277	5426	5580
42	4042	4150	4260	4374	4492	4612	4736	4865	4999	5136	5280	5428	5583
43	4044	4152	4262	4376	4494	4614	4739	4868	5001	5139	5282	5431	5586
44	4045	4153	4264	4378	4495	4616	4741	4870	5003	5141	5284	5433	5588
45	4047	4155	4266	4380	4497	4618	4743	4872	5005	5143	5287	5436	5591
46	4049	4157	4268	4382	4499	4620	4745	4874	5008	5146	5289	5438	5594
47	4051	4159	4270	4384	4501	4623	4747	4876	5010	5148	5292	5441	5596
48	4052	4161	4272	4386	4503	4625	4750	4879	5012	5151	5294	5443	5599
49	4054	4162	4274	4388	4505	4627	4752	4881	5014	5153	5297	5446	5602
50	4056	4164	4275	4390	4507	4629	4754	4883	5017	5155	5299	5448	5604
51	4058	4166	4277	4392	4509	4631	4756	4885	5019	5158	5301	5451	5607
52	4060	4168	4279	4394	4511	4633	4758	4887	5021	5160	5304	5454	5610
53	4061	4170	4281	4396	4513	4635	4760	4890	5023	5162	5306	5456	5612
54	4063	4172	4288	4398	4515	4637	4762	4892	5026	5165	5309	5458	5615
55	4065	4173	4285	4399	4517	4639	4764	4894	5028	5167	5311	5461	5617
56	4067	4175	4287	4401	4519	4641	4766	4896	5030	5169	5314	5464	5620
57	4069	4177	4289	4403	4521	4643	4769	4898	5033	5172	5316	5466	5623
58	4070	4179	4291	4405	4523	4645	4771	4901	5035	5174	5319	5469	5625
59	4072	4181	4292	4407	4525	4647	4773	4903	5037	5176	5321	5471	5628

′	68°	69°	70°	71°	72°	73°	74°	75°	76°	77°	78°	79°	80°
0	5631	5795	5966	6146	6335	6534	6746	6970	7210	7467	7745	8046	8375
1	5633	5797	5969	6149	6338	6538	6749	6974	7214	7472	7749	8051	8381
2	5636	5800	5972	6152	6341	6541	6753	6978	7218	7476	7754	8056	8387
3	5639	5803	5975	6155	6345	6545	6757	6982	7222	7481	7759	8061	8393
4	5642	5806	5978	6158	6348	6548	6760	6986	7227	7485	7764	8067	8398
5	5644	5809	5981	6161	6351	6552	6764	6990	7231	7490	7769	8072	8404
6	5646	5811	5984	6164	6354	6555	6768	6994	7235	7494	7774	8077	8410
7	5650	5814	5986	6167	6358	6558	6771	6997	7239	7498	7778	8083	8416
8	5652	5817	5989	6170	6361	6562	6775	7001	7243	7503	7783	8088	8422
9	5655	5820	5992	6173	6364	6565	6779	7005	7247	7507	7788	8093	8427
10	5658	5823	5995	6177	6367	6569	6782	7009	7252	7512	7793	8099	8433
11	5660	5825	5998	6180	6371	6572	6786	7013	7256	7516	7798	8104	8439
12	5663	5828	6001	6183	6374	6576	6790	7017	7260	7521	7803	8109	8445
13	5666	5831	6004	6186	6377	6579	6793	7021	7264	7525	7808	8115	8451
14	5668	5834	6007	6189	6380	6583	6797	7025	7268	7530	7813	8120	8457
15	5671	5837	6010	6192	6384	6586	6801	7029	7273	7535	7817	8125	8463
16	5674	5839	6013	6195	6387	6590	6804	7033	7277	7539	7821	8131	8469
17	5676	5842	6016	6198	6390	6593	6808	7037	7281	7544	7827	8136	8474
18	5679	5845	6019	6201	6394	6597	6812	7041	7285	7548	7832	8141	8480
19	5682	5848	6022	6205	6397	6600	6815	7045	7289	7553	7837	8147	8486
20	5685	5851	6025	6208	6400	6603	6819	7048	7294	7557	7842	8152	8492
21	5687	5854	6028	6211	6403	6607	6823	7052	7298	7562	7847	8158	8498
22	5690	5856	6031	6214	6407	6610	6826	7056	7302	7566	7852	8163	8504
23	5693	5859	6034	6217	6410	6614	6830	7060	7306	7571	7857	8168	8510
24	5695	5862	6037	6220	6413	6617	6834	7064	7311	7576	7862	8174	8516
25	5698	5865	6040	6223	6417	6621	6838	7068	7315	7580	7867	8179	8522
26	5701	5868	6043	6226	6420	6624	6841	7072	7319	7585	7872	8185	8528
27	5704	5871	6046	6230	6423	6628	6845	7076	7323	7589	7877	8190	8534
28	5706	5874	6049	6233	6427	6631	6849	7080	7328	7594	7882	8196	8540
29	5709	5876	6052	6236	6430	6635	6853	7084	7332	7599	7887	8201	8546
30	5712	5879	6055	6239	6433	6639	6856	7088	7336	7603	7892	8207	8552
31	5715	5882	6058	6242	6437	6642	6860	7092	7341	7608	7897	8212	8558
32	5717	5885	6061	6245	6440	6646	6864	7096	7345	7612	7902	8218	8565
33	5720	5888	6064	6249	6443	6649	6868	7100	7349	7617	7907	8223	8571
34	5723	5891	6067	6252	6447	6653	6871	7104	7353	7622	7912	8229	8577
35	5725	5894	6070	6255	6450	6656	6875	7108	7358	7626	7917	8234	8583
36	5728	5896	6073	6258	6453	6660	6879	7112	7362	7631	7922	8240	8589
37	5731	5899	6076	6261	6457	6663	6883	7116	7366	7636	7927	8245	8595
38	5734	5902	6079	6264	6460	6667	6886	7120	7371	7640	7932	8251	8601
39	5736	5905	6082	6268	6463	6670	6890	7124	7375	7645	7937	8256	8607
40	5739	5908	6085	6271	6467	6674	6894	7128	7379	7650	7942	8262	8614
41	5742	5911	6088	6274	6470	6677	6898	7132	7384	7654	7948	8267	8620
42	5745	5914	6091	6277	6473	6681	6901	7136	7388	7659	7953	8273	8626
43	5747	5917	6094	6280	6477	6685	6905	7140	7392	7664	7958	8279	8632
44	5750	5919	6097	6283	6480	6688	6909	7145	7397	7668	7963	8284	8638
45	5753	5922	6100	6287	6483	6692	6913	7149	7401	7673	7968	8290	8644
46	5756	5925	6103	6290	6487	6695	6917	7153	7406	7678	7973	8295	8651
47	5758	5928	6106	6293	6490	6699	6920	7157	7410	7683	7978	8301	8657
48	5761	5931	6109	6296	6494	6702	6924	7161	7414	7687	7983	8307	8663
49	5764	5934	6112	6299	6497	6706	6928	7165	7419	7692	7989	8312	8669
50	5767	5937	6115	6303	6500	6710	6932	7169	7423	7697	7994	8318	8676
51	5770	5940	6118	6306	6504	6713	6936	7173	7427	7702	7999	8324	8682
52	5772	5943	6121	6309	6507	6717	6940	7177	7432	7706	8004	8329	8688
53	5775	5946	6124	6312	6511	6720	6943	7181	7436	7711	8009	8335	8695
54	5778	5948	6127	6315	6514	6724	6947	7185	7441	7716	8014	8341	8701
55	5781	5951	6130	6319	6517	6728	6951	7189	7445	7721	8020	8347	8707
56	5783	5954	6133	6322	6521	6731	6955	7194	7449	7725	8025	8352	8714
57	5786	5957	6136	6325	6524	6735	6959	7198	7454	7730	8030	8358	8720
58	5789	5960	6140	6328	6528	6738	6963	7202	7458	7735	8035	8364	8726
59	5792	5963	6143	6332	6531	6742	6966	7206	7463	7740	8040	8369	8733

′	81°	82°	83°	84°	85°
0	8739	9145	9606	10137	10765
1	8745	9153	9614	10146	10776
2	8752	9160	9622	10156	10788
3	8758	9167	9631	10166	10799
4	8765	9174	9639	10175	10811
5	8771	9182	9647	10185	10822
6	8778	9189	9655	10195	10834
7	8784	9197	9664	10205	10846
8	8791	9203	9672	10214	10858
9	8797	9211	9683	10224	10869
10	8804	9218	9689	10234	10881
11	8810	9225	9697	10244	10893
12	8817	9233	9706	10254	10905
13	8823	9240	9714	10264	10917
14	8830	9248	9723	10273	10929
15	8836	9255	9731	10283	10941
16	8843	9262	9740	10293	10953
17	8849	9270	9748	10303	10965
18	8856	9277	9757	10314	10978
19	8863	9285	9765	10324	10990
20	8869	9292	9774	10334	11002
21	8876	9300	9783	10344	11014
22	8883	9307	9791	10354	11027
23	8889	9315	9800	10364	11039
24	8896	9322	9809	10374	11052
25	8903	9330	9817	10385	11064
26	8909	9337	9826	10395	11077
27	8916	9345	9835	10405	11089
28	8923	9353	9844	10416	11102
29	8930	9360	9852	10426	11115
30	8936	9368	9861	10437	11127
31	8943	9376	9870	10447	11140
32	8950	9383	9879	10457	11153
33	8957	9391	9888	10468	11166
34	8963	9399	9897	10479	11179
35	8970	9407	9906	10489	11192
36	8977	9414	9915	10500	11205
37	8984	9422	9924	10510	11218
38	8991	9430	9933	10521	11231
39	8998	9438	9942	10532	11244
40	9005	9445	9951	10542	11257
41	9012	9453	9960	10553	11270
42	9018	9461	9969	10564	11284
43	9025	9469	9978	10575	11297
44	9032	9477	9987	10586	11310
45	9039	9485	9996	10597	11324
46	9046	9493	10005	10608	11337
47	9053	9501	10015	10619	11351
48	9060	9509	10024	10630	11365
49	9067	9517	10033	10641	11378
50	9074	9525	10043	10652	11392
51	9081	9533	10052	10663	11406
52	9088	9541	10061	10674	11420
53	9096	9549	10071	10685	11434
54	9103	9557	10080	10696	11448
55	9110	9565	10089	10708	11462
56	9117	9573	10099	10719	11476
57	9124	9581	10108	10730	11490
58	9131	9589	10118	10742	11504
59	9138	9598	10127	10753	11518

TABLE V.
Dip of the Sea Horizon.

Hight of Eye in Ft.	Dip of the Horizon.	Hight of Eye in Ft.	Dip of the Horizon.
	° ′		° ′
1	0 59	38	6 4
2	1 24	41	6 18
3	1 42	44	6 32
4	1 58	47	6 45
5	2 12	50	6 58
6	2 25	53	7 10
7	2 36	56	7 12
8	2 47	59	7 24
9	2 57	62	7 45
10	3 07	65	7 56
11	3 16	68	8 07
12	3 25	71	8 18
13	3 33	74	8 28
14	3 41	77	8 38
15	3 49	80	8 48
16	3 56	83	8 58
17	4 04	86	9 08
18	4 11	89	9 17
19	4 17	92	9 26
20	4 24	95	9 36
21	4 31	98	9 45
22	4 37	101	9 54
23	4 43	104	10 02
24	4 49	107	10 11
25	4 55	110	10 19
26	5 01	113	10 28
27	5 07	116	10 36
28	5 13	119	10 44
29	5 18	122	10 52
30	5 24	125	11 00
31	5 29	128	11 08
32	5 34	131	11 16
33	5 39	134	11 24
34	5 44	137	11 31
35	5 49	140	11 39

TABLE VI.

Dip of the Sea Horizon at different Distances from it.

Dist. in Miles.	Hight of Eye in Ft.					
	5	10	15	20	25	30
	′	′	′	′	′	′
¼	11	22	34	45	56	68
½	6	11	17	22	28	34
¾	4	8	12	15	19	23
1	4	6	9	12	15	17
1¼	3	5	7	9	12	14
1½	3	4	6	8	9	12
2	2	3	5	6	8	10
2½	2	3	5	6	7	8
3	2	3	4	5	6	7
3½	2	3	4	5	6	6
4	2	3	4	4	5	6
5	2	3	4	4	5	5
6	2	3	4	4	5	5

TABLE VII.
Mean Refraction of Celestial Objects.

Alt.	Refr.	Alt.	Refr.	Alt.	Refr.	Alt.	Refr.	Alt.	Refr.
° ′	′ ″	° ′	′ ″	° ′	′ ″	° ′	′ ″	°	″
0 0	33 0	10 0	5 15	20 0	2 35	32 0	1 31	67	24
10	31 22	10	5 10	10	2 34	40	1 29	68	23
20	29 50	20	5 05	20	2 32	33 0	1 28	69	22
30	28 28	30	5 00	30	2 31	20	1 26	70	21
40	27 00	40	4 56	40	2 29	40	1 25	71	19
50	25 42	50	4 51	50	2 28	34 0	1 24	72	18
1 0	24 29	11 0	4 47	21 0	2 27	20	1 23	73	17
10	23 20	10	4 43	10	2 26	40	1 22	74	16
20	22 15	20	4 39	20	2 25	35 0	1 21	75	15
30	21 15	30	4 34	30	2 24	20	1 20	76	14
40	20 18	40	4 31	40	2 23	40	1 19	77	13
50	19 25	50	4 27	50	2 21	36 0	1 18	78	12
2 0	18 35	12 0	4 23	22 0	2 20	30	1 17	79	11
10	17 48	10	4 20	10	2 19	37 0	1 16	80	10
20	17 04	20	4 16	20	2 18	30	1 14	81	9
30	16 24	30	4 13	30	2 17	38 0	1 13	82	8
40	15 45	40	4 09	40	2 16	30	1 11	83	7
50	15 09	50	4 06	50	2 15	39 0	1 10	84	6
3 0	14 34	13 0	4 03	23 0	2 14	30	1 09	85	5
10	14 04	10	4 00	10	2 13	40 0	1 08	86	4
20	13 34	20	3 57	20	2 12	30	1 07	87	3
30	13 06	30	3 54	30	2 11	41 0	1 05	88	2
40	12 40	40	3 51	40	2 10	30	1 04	89	1
50	12 15	50	3 48	50	2 09	42 0	1 03	90	0
4 0	11 51	14 0	3 45	24 0	2 08	30	1 02		
10	11 29	10	3 43	10	2 07	43 0	1 01		
20	11 08	20	3 40	20	2 06	30	1 00		
30	10 48	30	3 38	30	2 05	44 0	0 59		
40	10 29	40	3 35	40	2 04	30	0 58		
50	10 11	50	3 33	50	2 03	45 0	0 57		
5 0	9 54	15 0	3 30	25 0	2 02	30	0 56		
10	9 38	10	3 28	10	2 01	46 0	0 55		
20	9 23	20	3 26	20	2 00	30	0 54		
30	9 08	30	3 24	30	1 59	47 0	0 53		
40	8 54	40	3 21	40	1 58	30	0 52		
50	8 41	50	3 19	50	1 57	48 0	0 51		
6 0	8 28	16 0	3 17	26 0	1 56	30	0 50		
10	8 15	10	3 15	10	1 55	49 0	0 49		
20	8 03	20	3 12	20	1 55	30	0 49		
30	7 51	30	3 10	30	1 54	50 0	0 48		
40	7 40	40	3 08	40	1 53	30	0 47		
50	7 30	50	3 06	50	1 52	51 0	0 46		
7 0	7 20	17 0	3 04	27 0	1 51	30	0 45		
10	7 11	10	3 03	15	1 50	52 0	0 44		
20	7 02	20	3 01	30	1 49	30	0 44		
30	6 53	30	2 59	45	1 48	53 0	0 43		
40	6 45	40	2 57	28 0	1 47	30	0 42		
50	6 37	50	2 55	15	1 46	54 0	0 41		
8 0	6 29	18 0	2 54	30	1 45	55 0	0 40		
10	6 22	10	2 52	45	1 44	56 0	0 38		
20	6 15	20	2 51	29 0	1 42	57 0	0 37		
30	6 08	30	2 49	20	1 41	58 0	0 35		
40	6 01	40	2 47	40	1 40	59 0	0 34		
50	5 55	50	2 46	30 0	1 38	60 0	0 33		
9 0	5 48	19 0	2 44	20	1 37	61 0	0 32		
10	5 32	10	2 43	40	1 36	62 0	0 30		
20	5 36	20	2 41	31 0	1 35	63 0	0 29		
20	5 41	30	2 40	20	1 33	64 0	0 28		
40	5 25	40	2 38	40	1 32	65 0	0 26		
50	5 20	50	2 37	32 0	1 31	66 0	0 25		

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